NASA

MODEL AERODYNAMIC TEST RESULTS
FOR TWO VARIABLE CYCLE ENGINE
COANNULAR EXHAUST SYSTEMS
AT SIMULATED TAKEOFF
AND CRUISE CONDITIONS

COMPREHENSIVE DATE REPORT VOLUME II TABULATED AERODYNAMIC DATA BOOK 1

By D.P. Nelson

Commercial Products Division
Pratt & Whitney Aircraft Group
United Technologies Corporation

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AERODYNAMIC TEST RESULTS FOR TWO VARIABLE
CYCLE ENGINE COANNULAR EXHAUST SYSTEMS AT
SIMULATED TAKEOFF AND CRUISE CONDITIONS.
COMPREHENSIVE (Pratt and Whitney Aircraft

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16 Abstract			
translating primary plug Tests were conducted at tacquired at Mach numbers operating conditions. At demonstrated good perform advanced supersonic propuconfigurations exhibited study assumptions. At tak	nical flow splitter. Both de and an auxiliary inlet ejector akeoff and simulated cruise of 0, 0.36, 0.9, and 2.0 for simulated supersonic cruise, ance, comparable to levels as lsion studies. However, at superformance that was 6 to 7.9 e-off conditions, the iris covels, while the short flap defined and the short flap	conditions. Dat a wide range of both configura ssumed in earli ubsonic cruise, percent less onfiguration pe	ca were of nozzle ations ier , both than the
17. Key Words (Suggested by Author(s)) Short Flap Ejector Iris Flap Ejector Coannular Exhaust Nozzle Inverted Velocity Profile	18. Distribution Statem	ent	
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FOREWORD

This report documents the work performed during the Nozzle Performance Tests (Task III) of Contract NAS3-20061. Because of the large amount of information, this report is presented in three Volumes to facilitate its use.

Volume I contains the design layouts and detailed design drawings of the nozzle models.

Volume II contains the tabular aerodynamic data generated in this program.

Volume III contains a graphical presentation of the data.

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A complete description of the test hardware and test facilities is contained in the companion Task III Final Report, CR-159818. Significant test results and conclusions are also included in the Final Report.

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5.	Tabulated Data	•

1. Introduction

Tabulated aerodynamic data presented in this volume were acquired during $\sin \varepsilon$ scale model nozzle performance wind tunnel test.

Section 2 contains an index that can be used to locate the tabulated data obtained during this program.

Section 3 provides a description of the tabulated data parameters.

The aerodynamic data presented in Section 5 include:

- o Nozzle thrust coefficient parameters
- o Nozzle discharge coefficients

o Static pressure tap measurements

2. Tabulated Data Index

The tabulated data are organized by run number sequence with each run number representing a specific test configuration. Each run is comprised of a sequence of reading numbers that represent specific data points for discrete nozzle operating conditions and tunnel Mach number.

A data matrix is provided in Table 2-I which relates each test configuration and nominal Mach number to the corresponding run number and reading numbers comprising that run. For example, to locate the data for the short flap nozzle subsonic cruise configuration C_2 tested at an ejector inlet position of 0.46 and clamshell angle of 17° at 0.9 Mach number, we find the desired run number is 30 and the reading numbers are (1718-1751).

TABLE 2-I

DATA MATRIX GUIDE

- o Supersonic Cruise Data
 - Short flap nossle-supersonic cruise configuration C1

M_O ™ 2.0

We corr <u>O</u> <u>0.02</u> <u>0.04</u>

Run No. (RD'G No.) 14 (1039–1070) 15 (1071–1102) 16 (1103–1144)

- Iris flap nozzle-supersonic cruise configuration A1

No - 2.0

We corr <u>0</u> <u>0.02</u> <u>0.04</u> Run No. (RD'G No.) 18 (1155-1184) 20 (1248-1277) 19 (1205-1235)

- o Subsonic Cruise Data
 - Short flap nossle-subsonic cruise configuration C2

Ejector Inlet Position Ainlet/Ag	No	130	Clamehell angle	210	Removed
(Mid) 0.46	0.9	29(1685-1717)	30(1718-1751)	31(1752-1785)	46(2265-2278)
(Mid) 0.46	0 4 0.9	-	-	-	47(2279-2292)
(Mid) 0.46	Vary 0 to 0.95	-	45(2224-2264)	-	•
(Min) 0.36	0 6 0.9	-	-	32(1786-1828)	~

TABLE 2-1 (Cont'd)

- Iris flap nossle-subsonic cruise configuration A2

Ejector Inlet Position Ainlet /Ag	H _o	130	Clamehell engle	210	Resoved
(Mid) 0.63	0.9	-	-	33(1829-1863)	•
(Mid) 0.63	0 6 0.9				38(2001-2058)
(Mid) 0.63	vary 0 to 0.95	-	44(2171-2223)		
(Modified) 0.42	0.9	•	•	•	39(2059-2090)
Ejector Removed	vary 0 to 0.95				63(2771-2820)

o Takeoff Data

- Short flap nozzle-takeoff configuration C3 plug extended C33 plug retracted

Ejector Inlet Primary Position Plug

Clambhell angle

Ainlet/Ag	Position	Mo	130	170	210	Removed
(Max) 0.60	extended	0 4 0.36	26(1528-1592)	-	•	-
(Mid) 0.46	extended	0 & 0.36	24(1438-1498)	22(1348-1407)	23(1408-1437) 25(1499-1527)	57 (2592-2627)
(Mid) 0.46 modified*	extended	0 & 0.36	59(2658-2693)	-	-	60(2694-2710)
(Min) 0.36	extended	0 & 0.36	27(1593-1653)	•	-	-
(Min) 0.36	retracted	0.36	28(1654-1684)	-	-	-
Removed	extended	0				58(2628-2657)
Removed Modified*	extended	0				61(2711-2727)

^{* 20°} segment inlet flap removed

- Iris flap nozzle-takeoff configuration A3 plug extended A33 plug retracted

Ejector Inlet Position	Primary Plug		Clamshell ang	le	
Ainlet/Ag	Position Mo	130	170	210	Removed
(Mid) 0.80	extended 0 & 0	.36 37(1940-2000)	-	-	65(2873-2893)
(Mid) 0.80	retracted 0 & 0	.36 35(1864-1927)	_	_	•

3. Data Identification Guide

THE RESIDENCE OF THE PARTY OF T

A set of tabulated data for each run consists of tunnel Mach number, nozzle operating conditions, discharge coefficients, thrust coefficients and surface static pressures. The nozzle operating conditions and performance coefficients for each reading of the run are summarized at the beginning of the data set followed by static pressure measurements for each reading. We will use the data set for run 30 listed on pages 585-619 book 2 and previous identified in the data matrix, as an example, to describe the information presented. The configuration description is listed at the top of the summary page. Directly below the description, the nozzle operating conditions and coefficients are tabulated by reading number (RDG) which appears on the extreme left of the page. Proceeding from left to right the parameters are; tunnel Mach number (MO), fan-to-primary stream pressure split (PTF/PTP), fan nozzle pressure ratio (PTF/PO), primary nozzle pressure ratio (PTP/PO), secondary flow (OMEGA), secondary-to-fan total pressure pumping characteristic (PTS/PTF), (note that the secondary flow and pumping characteristic parameters only apply to the supersonic cruise configuration), fan nozzle discharge coefficient (CDF), primary nozzle discharge coefficient (CDP), nozzle gross thrust coefficient as defined in Ref. 1, but including the external skin friction drag of the model (CF1), nozzle efficiency coefficient as defined in Ref. 1. but including external skin friction drag (ETA1), nozzle efficiency coefficient as defined in Ref. 1 (ETA1, INT), nozzle gross thrust coefficient as defined in Ref. 1 (CFP1), nozzle gross thrust coefficient as defined in Ref. 1, adjusted for the estimated internal duct friction losses from the charging station to nozzle exit plane (CFP2), stream thrust coefficient (F9). The definition of the additional thrust parameters not included in Ref. 1 are provided on page viii.

Following the run summary the model surface static pressure measurements are presented for each reading. These data are identified by the run and reading (RDG) number on the upper right hand corner of the page. The pressure measurements are grouped together for each model surface as identified by the heading such as; primary plug, flow splitter outer diameter, flow splitter inner diameter. Reading from left to right for each grouping the pressures are expressed in terms of absolute pressure, psia, (PL), normalized by ambient pressure (PL/PO), normalized by fan total pressure (PL/PTF), and normalized by primary total pressure (PL/PTP). (X/DMAX) describes the normalized axial location of each tap relative to the common model connection flange*. It should be noted that not all of the static tap instrumentation listed was applicable to all of test configurations. For cases that do not apply, the information is lined out.

*For the short flap nozzle configurations C_2 , C_3 and C_{33} , the correct axial location (X/Dmax) of the last inlet flap tap, #48, identified as AVD word 142 is 0.558 and not 0.588 as shown.

Additional Thrust Parameters

Gross thrust coef. CF1 =
$$\frac{(F-Dex)-Dsm}{m_f V_{if} + m_p V_{ip}}$$

Efficiency coef. ETA1 =
$$\frac{(F-Dex) - Dsm}{m_f V_{if} + m_p V_{ip} + m_s V_{is}}$$

Gross Thrust Coef. CFP2 =

$$\frac{F - Dex}{m_f V_{if} + m_p V_{ip}} + \frac{\Delta C_{fp_f} m_f V_{if} + \Delta C_{fp_p m_p V_{ip}}}{m_f V_{if} + m_p V_{ip}}$$

where
$$\Delta Cfp = \begin{bmatrix} \frac{\gamma-1}{2\gamma} \\ \frac{P_t}{P_0} & \frac{\gamma-1}{2} - 1 \end{bmatrix} = \begin{pmatrix} \Delta P_t \\ P_t \end{pmatrix}$$

and $\frac{\Delta P_t}{P_t}$ is the estimated duct friction loss from the instrumentation charging station to nozzle exit plane

Stream thrust Coef. F9 =
$$\frac{(F-Dex) + P_0 A_9}{P_{tf} A_f + P_{tp} A_p}$$

4. References

 Nelson, D.P., "Model Aerodynamic Test Results for Two Variable Cycle Engine Coannualar Exhaust Systems at Takeoff and Cruise Conditions," NASA CR-159818, 1980.

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	NCZZLE TYPE	POW RASE EJECTOR MOZZLE (MODEL C)
	FILGHT CONDITIONS	SUPER STAIL CRUISE (MS=0)
	NOZZLE COMFIGURATIOM	
	PRIMARY-NOTILE PHING	SPLIT PLUG (PETPACTER)
	FLOW SPLITTEP FAN NOZZLE	ISENTPOPIC SPLITTEP SHIPT FLAP
	CLAUSHELL POSTTION	SHOW A CHA
	FIFCTOR THEFT OPENING	
	a a series and a series and a series and a	
	POG MO PTE/PTP PTE/PD PTP/PG DNEGA	DYS /DYS - COR - CE1 - EVAL EVAL DAY - CE1 - CE12 - E4
		PTS/PTF CDF CDP CFL ETAL ETALLINT CFPL CFP2 F0
	1030 1.464 2.30 20.16 10.10 0.009	0.443 0.974 0.981 0.9699 0.9699 0.4729 0.4729 0.4734 1.4546
	1343 1.962 2.31 20.95 8.70 0.000	0.042 0.974 0.581 0.9701 0.9701 0.9734 0.9734 0.9739 1.4452
	1741 1.961 2.67 20.37 7.72 0.9 <u>0</u> 0	0. 16? J. 972 0.975 0.9711 0.9711 0.9745 0.9745 0.9750 1.4792

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142 2.6759 0.83308 0.761504 0.1078 1.3540  ***ANDRITHMAN PRESCRIPT PATENTS OF THE PROPERTY OF									
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March   Pt   Pt/Pf   Pt/Pf   Pt/Pf   Pt/Pf   X/DMAX     137   5.4413   1.6940   0.064393   0.21931   -1.0650     117   3.9461   1.2799   0.000765   0.15664   -/.0000     122   3.7711   1.1741   9.55552   0.15200   -1.0000     127   3.4660   1.0729   0.033450   0.13990   -1.0000     127   3.4660   1.0729   0.033450   0.13990   -1.0000     127   3.4660   0.43390   0.061534   0.40785   -1.0000     129   3.4610   1.0635   9.052585   0.13769   -1.0000     159   3.4610   1.0635   9.052585   0.13769   -1.0000     159   3.4610   1.0635   0.552085   0.13789   -1.0000     159   3.4600   1.0635   0.552085   0.13789   -1.0000     159   3.4600   1.0635   0.552085   0.13789   -1.0000     159   3.4600   1.0635   0.552085   0.13789   -1.0000     159   3.4610   1.0635   0.052085   0.13789   -1.0000     159   3.4610   1.0635   0.052085   0.13789   -1.0000     159   3.4610   1.0635   0.052085   0.13789   -1.0000     159   3.4610   1.0635   0.052085   0.13789   -1.0000     159   3.4610   1.0635   0.052085   0.13789   -1.0000     159   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.0000     150   3.4610   1.0635   0.052085   0.13789   -1.00			and the state of t						
137 5.4413 1.6940 0.08493 0.21931 -1.0000 117 3.9161 1.7799 0.066776 0.15664 -2.0000 122 3.7711 1.1741 0.055692 0.15200 -1.0000 127 3.4600 1.0729 0.053450 0.13890 -1.0000 147 3.9759 0.9766 0.047710 0.12300 -1.0000 149 2.4781 0.483330 0.041534 0.20785 -1.0000 150 3.4601 1.0635 0.072585 0.13789 -1.0000 151 3.4610 1.0635 0.072585 0.13789 -1.0000 152 3.4601 1.0635 0.072585 0.13789 -1.0000 153 3.4101 1.0635 0.072682 0.13789 -1.0000 154 3.4210 1.0635 0.057082 0.13789 -1.0000 157 3.4210 1.0635 0.057082 0.13789 -1.0000 157 3.4210 1.0635 0.057082 0.13789 -1.0000 157 3.4210 1.0635 0.057082 0.13789 -1.0000 167 3.4210 1.0635 0.057082 0.13789 -1.0000 167 3.4210 1.0635 0.057082 0.13789 -1.0000 167 3.4160 1.0635 0.057095 0.13789 -1.0000 167 3.4160 1.0635 0.057095 0.13789 -1.0000							and company of the Administration of		
112 1.996 1.2799 0.CC276 0.1506 -1.0000 122 3.7711 1.1761 9.55552 0.15200 -1.0000 127 3.6600 1.0779 0.053650 0.13900 -1.0000 127 3.0752 0.95766 0.0C7710 0.12347 -1.0000 147 3.0752 0.95766 0.0C7710 0.12347 -1.0000 150 3.4601 1.0635 9.0C52955 0.13769 -1.0000 151 3.4601 1.0631 9.0C5295 0.13769 -1.0000 152 3.4601 1.0651 0.057062 0.13769 -1.0000 153 3.4601 1.0651 0.057062 0.13769 -1.0000 157 3.4100 1.0635 0.057062 0.13769 -1.0000 157 3.4100 1.0635 0.057062 0.13769 -1.0000 167 3.4100 1.0635 0.057062 0.13769 -1.0000 167 3.4100 1.0635 0.057062 0.13769 -1.0000 167 3.4100 1.0635 0.057062 0.13769 -1.0000 167 3.4100 1.0635 0.057062 0.13769 -1.0000 167 3.4100 1.0635 0.057062 0.13769 -1.0000							•		
122   3.7711   1.1741   9.052452   0.15200   -1.0000     127   3.4660   1.0729   0.053650   0.13890   -1.0090     147   3.0759   0.4716   0.47110   0.12249   -1.0000     142   2.473   0.43390   0.041534   0.40785   -1.0000     157   3.4610   1.0635   9.052635   0.13749   -1.0000     157   3.46210   1.0635   0.057062   0.13789   -1.0000     157   3.46210   1.0635   0.057062   0.13789   -1.0000     159   3.4160   1.0635   0.052044   0.13769   -1.0000     157   3.4160   1.0635   0.052044   0.13769   -1.0000     157   3.4210   1.0635   0.052046   0.13789   -1.0000     2400171044   98855096 PATUS   20 066 SHPTOD 17CATION     VO HOPD   PL   MIMPO   M	107						AND A MARKET TO LANGE OF THE MARKET OF	e	
127   3.466)   1.0779   0.653.450   0.13890   -1.0009     137   3.4759   0.95766   0.647719   0.1238   -1.0000     142   2.451   0.43398   0.061534   0.40785   -1.0000     152   3.463   1.0635   9.072585   0.13769   -1.0000     157   3.4210   1.0651   9.057062   0.13780   -1.0000     157   3.4210   1.0635   0.057082   0.13780   -1.0000     157   3.460   1.0635   0.057084   0.13769   -1.0000     157   3.4210   1.0635   0.057082   0.13789   -1.0000     167   3.4210   1.0635   0.057082   0.13789   -1.0000     240011   1044   28855188   PATIS   2.20   2067095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1.0635   0.057095   0.13765   -1.0000     240011   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044   1044			1, 2399						
137   3.0159   0.95766   0.647710   0.1230   -1.0000     142   2.413   0.83308   0.041574   0.10785   -1.0000     157   3.4210   1.0635   9.25263   0.13789   -1.0000     157   3.4210   1.0651   0.757067   0.13789   -1.0000     26001110041   PRESSUPE PAYION   FAM NOTTIE FLAP					A 1630A	Z-1.0000			
142 2.471 0.4339A 0.041514 0.40785 -1.0000 157 3.4161 1.0635 9.055365 0.13769 -1.0000 157 3.4210 1.0651 9.057067 U.13784 -1.0000  >ANDITIONAL PRESSURE PATION, EAN NOTTIFICATION  VO HORD PL MI/PO 1.0635 0.155364 0.13769 -1.0000  >ANDITIONAL PRESSURE PATION, 20 DEC SHROW INCATION  VO HORD PL MI/PO 9/PTF MI/PTP X/DWAX 167 3.4164 1.0635 0.057995 J.13765 -1.0000  >ANDITIONAL PRESSURE PATION 0 /PTF MI/PTP X/DWAX 167 3.4164 1.0635 0.057995 J.13765 -1.0000  >ANDITIONAL PRESSURE PATION 0 /PTF MI/PTP X/DWAX 167 3.4164 1.0635 0.057995 J.13765 -1.0000  >ANDITIONAL PRESSURE PATION 0 /PTF MI/PTP X/DWAX 167 3.4164 1.0635 0.057995 J.13765 -1.0000  >ANDITIONAL PRESSURE PATION 0 /PTF MI/PTP X/DWAX 167 3.4164 1.0635 0.057995 J.13765 -1.0000	122	3.7711	1.1741						
15? 3.4(A) 1.0635 9.052635 0.13769 -1.0600 157 3.4210 1.0651 9.052062 0.13780 -1.0000  >>***PROTITIONAL PRESSURE PATION, FLM MO7715 1145  VO HOPD PL MI/PD 1.0635 0.352084 0.13769 -1.0000  157 3.4600 1.0635 0.352084 0.13789 -1.0000  >***PROTITIONAL PRESSURE PATION, PO DES SHORD INCATION  VO HOPD PL MI/PD MI/PD MI/PT MI/PTP X/DMAX  167 3.4160 1.0635 0.052995 0.13765 -1.0000  >***PROTITIONAL PRESSURE PATION, PO DES SHORD INCATION  VO HOPD PL MI/PD MI/PT MI/PTP X/DMAX  167 3.4160 1.0635 0.052995 0.13765 -1.0000  >****PROTITIONAL PRESSURE PATION, PO DES SHORD INCATION  VO 1/PTO PL MI/PD MI/PTP MI/PTP X/DMAX  >****PROTITIONAL PRESSURE PATION, PO DES SHORD INCATION  VO 1/PTO PL MI/PD MI/PTP MI/PTP X/DMAX	122	3.4460	1.0729	0.053450	C-13999	-1.0000			
157 3.4210 1.0651 0.057067 0.13780 -1.0000  >>***PROTITIONAL PRESSURE PATION, FAM NOTTIE FLAP  VO MOND PL MI/PO 1.0635 0.052085 0.13769 -1.0000  157 3.4210 1.0635 0.57062 0.13789 -1.0000  >***ANDITIONAL PRESSURE PATION, FO DEC SHOWING INCATION  VO MOND PL MI/PO MI/PTE MI/PTP X/DMAX  167 3.4164 1.0635 0.052095 0.13769 -1.0000  >***ANDITIONAL OPESSURE PATION, FO DEC SHOULD INCATION  VO MOND PL MI/PD MI/PTE MI/PTP X/DMAX  167 3.4164 1.0635 0.052095 0.13769 -1.0000  >***ANDITIONAL OPESSURE PATION, FO DEC SHOULD INCATION  VO MOND PL MI/PD MI/PTE PL/PTP X/DMAX	122 127 137	3.4460	1.1741 1.0729 0.95766	0.653450 9.647719	0.1234	-1.0099 -1.0090	r differ i to∰erwet de w	and the second s	
PAROTITIONAL PRESSURE PAYERS , FAM NOTITE TEAD  VO HOPO PL ML/PO	-122 -127 -137 -142	3.4660	1.1741 1.0729 9.95766 9.83398	0.653450 0.647710 0.041534	0.13890 0.12346 0.20785	-1.0099 -1.0090 -1.0000	e de de la compansión de las		
VO WPPO PL MI/PO PLOTE PLOTE PLOTE X/DMAX  157 3.4160 1.0635 0.052085 0.13769 -1.0000  >4001T 10 ML PRESSURE PATES . 20 DEC SHPPO INCATION  VO WPPO PL MI/PO MI/PO PLOTE VALUE PATES 0.052095 0.13769 -1.0000  >4001T 10 ML PRESSURE PATES . 20 DEC SHPPO INCATION  VO WPPO PL MI/PO N.052095 0.13765 -1.0000  >4001T 10 MI/PO N.052095 0.13765 -1.0000  >4001T 10 MI/PO N.052095 0.13765 -1.0000	122 127 137 142 152	3.4460 3.4460 3.4159 2.613 3.4160	1.1741 1.0729 0.95766 0.83398 1.0635	0.053450 0.047710 0.041534 0.052585	0.13490 0.12349 0.10745 0.13749	-1.0099 -1.0090 -1.0000 -1.0000	n de de la companya		
157 3.4169 1.0635 0.052085 0.13769 -1.0000 157 3.4210 1.0651 0.052082 0.13789 -1.0000  >ADDITIONAL PRESSURE PATES . 20 DEG SHAPRO INCATION  VO HORD PL MIJAN 91/APTA MIJANA 1.0635 0.052095 0.13765 -1.0000 177 3.4164 1.0635 0.052095 0.13765 -1.0000 177 3.6710 1.0651 0.052082 0.13769 -1.0000  >ADDITIONAL PRESSURE PATES . 80 DEG SHAPRO INCATION  VO 4250 PL MIJAN PLANT PLANT PLANT	122 127 137 142 152	3.4460 3.4460 3.4159 2.613 3.4160	1.1741 1.0729 0.95766 0.83398 1.0635	0.053450 0.047710 0.041534 0.052585	0.13490 0.12349 0.10745 0.13749	-1.0099 -1.0090 -1.0000 -1.0000			
187 3.4819 1.9651 0.657662 0.13789 -1.0000  >ADDITIONAL PRESSURE PATES . 29 DEC SHAPED INCATION  VO HORD PL MI/PD MI/PTP X/DMAX  167 3.4164 1.0635 0.052995 J.13765 -1.0030  177 3.6119 1.0651 0.052995 J.13765 -1.0000  >ADDITIONAL PRESSURE PATES . 80 DEC SHAPED INCATION  VO 4250 Pt MI/PD MI/PTP MI/PTP X/DMAX	122 127 137 142 152	3.4460 3.4460 3.4759 2.414 3.4460 3.4210	1.1741 1.0729 0.95766 0.#3398 1.0635 1.0651	0.653450 0.647710 0.041534 9.052585 9.057067	0.13450 0.12346 0.10785 0.13769 0.13789	-1.0099 -1.0090 -1.0000 -1.0000			and the second of the second o
187 3.4819 1.9651 0.657662 0.13789 -1.0000  >ADDITIONAL PRESSURE PATES . 29 DEC SHAPED INCATION  VO HORD PL MI/PD MI/PTP X/DMAX  167 3.4164 1.0635 0.052995 J.13765 -1.0030  177 3.6119 1.0651 0.052995 J.13765 -1.0000  >ADDITIONAL PRESSURE PATES . 80 DEC SHAPED INCATION  VO 4250 Pt MI/PD MI/PTP MI/PTP X/DMAX	122 127 137 142 152 157 260011 [0%	3.7711 3.466) 3.0759 2.453 3.4163 3.4210	1.1741 1.0729 0.95766 0.43398 1.0635 1.0651	0.653450 9.647719 0.041534 9.052585 9.052062	0.13850 0.12375 0.10785 0.13749 0.13789	-1.0099 -1.0090 -1.0000 -1.0000			androne engage of the second of
VD WORD PL MIPO MIPO MIPO MIPO MIPO MIPO MIPO MIPO	-11? -12? -137 -142 -15? -157 -260011104	3,7711 3,466) 3,9759 2,473 3,416) 3,4210 at pressure Pt	1.1741 1.0729 0.95766 0.83398 1.0635 1.0651	0.053450 0.047710 0.041534 0.052545 0.052647 HM7771E TYAP	0.13890 0.1234 0.20765 0.13749 0.13749	-1.0099 -1.0090 -1.0000 -1.0090 -1.0090			Adapata odd 🐷 🕡
167 3.4164 1.0635 0.052995 0.3765 -1.0000 177 3.6210 1.0651 0.052962 0.1369 -1.0000 SECOLD FOR SCHOOL FOR SHELLT FOREIGN WARREN VO 4900 BI MIJEO MIJET MIJET WARREN	122 127 137 142 157 157 2400 17 104	3.7711 3.666) 3.759 2.473 3.416) 3.4210 PRESSUPE PL 3.4169	1.1741 1.0729 9.95766 0.8339A 1.0635 1.0651 PAYIO . FER	0.053450 0.047710 0.041710 0.0415345 0.052545 0.057067	0.13490 0.12349 0.20785 0.13749 0.13749	-1.0099 -1.0000 -1.0000 -1.0090 -1.0090			androne and analysis of the second of the se
167 3.4164 1.0635 0.052995 0.3765 -1.0000 177 3.6210 1.0651 0.052962 0.1369 -1.0000 5670171019 0PFSSURE PATIOS . MO DEG SHPEUT [PESTION	122 127 137 142 152 157 >>nnition yn wren 152	3.7711 3.466) 3.759 2.473 3.416) 3.6210 at pressure Pt 3.4169 3.4219	1.1741 1.0729 0.95766 0.4339A 1.0635 1.0651 PAYIO FAY	0.053450 0.047710 0.041534 0.052545 0.057062 1.07715 Trap 1.057062	0.13490 0.12349 0.20745 3.13749 0.13749 0.13769 0.13769	-1.0099 -1.0000 -1.0000 -1.0090 -1.0090			ooksii Alpani (Ab V ) (
177 3.6/10 1.0551 0.552062 0.1369 -1.0000 SANDITION OPESSURE PATIOS . NO DEG SHREUT INCATION  VO 4700 RI N /PO M /PTF PI /PTP X/N48X	122 127 137 142 152 157 >4001T Intervention	3.7711 3.666) 3.6759 2.6751 3.6163 3.6210 at PRESSUPE Pt. 3.6162 3.6210 At PRESSUPE	1.1741 1.0729 9.95766 0.#339A 1.0635 1.0651 PAYIO . FAS #1/PO 1.0635 1.0655	0.053450 0.041719 0.041719 0.041714 0.052545 0.057067 0.057067 0.057062	C.13490 0.12349 0.20745 0.13749 0.13749 Pt /PTP 0.13769 0.13789	-1.0099 -1.0000 -1.0000 -1.0090 -1.0090 #/D#A# -1.0009			
SATISTICAL OPESSIVE OFFICE OF OPE SHOELD INCATION WAS A PART OF STATE OF STATES	122 127 137 142 152 157 >4001T INN VO WORD	3.7711 3.4660 3.4759 2.473 3.4160 3.4210 at PRESSUPE Pt. 3.4160 3.4210 At PRESSUPE	1.1741 1.0729 9.95766 0.#3398 1.0635 1.0651 PATITO . FAT	0.053A50 9.047719 0.041534 9.025485 9.057067 1 NOTTE TIAP 1.052045 0.052045 0.057062	0.1349 0.12349 0.10745 0.13749 0.13749 0.13769 0.13769	-1.0099 -1.0000 -1.0000 -1.0000 -1.0000 -1.0009			andream eleganica (elefe ser e e
NO 1990 BI MILPO MILPITE PILPETE NATIONALE	122 127 137 142 152 157 >AND TT INN 157 157 147 >AND WORD 167	3.7711 3.4660 3.457 3.4161 3.4210 at PRESSUPE PL 3.4160 3.4210 AL PRESSUPE PL 3.4160 PL 3.4160	1.1741 1.0729 9.95766 0.83398 1.0635 1.0651 PAYION, FEN M/PO 1.0635 1.9651 PATION . 20	0.053450 0.047719 0.041534 0.052545 0.052067 1.07715 T14P 0.052045 0.052045 0.052045	C.13890 0.12349 0.20785 0.13749 0.13749 0.13769 0.13769	-1.0099 -1.0090 -1.0000 -1.0090 -1.0099 -1.0099			
	122 127 137 142 152 157 260 2157 260 2157 260 260 260 260 260 260 260 260 260 260	3.7711 3.4660 3.4759 2.473 3.4167 3.4210 at pressure Pt 3.4162 3.4210 At pressure Pt 3.4162 3.4210	1.1741 1.0729 9.95766 0.#3398 1.0635 1.0651 PATITO . FAS #/PO 1.0635 1.0635 1.0635 1.0635 1.0635	0.053A50 0.047719 0.041534 0.0225A5 0.0526A7 I NOTTIE TIAP 0.0520A5 0.570A2 0.0520A5 0.7570A2 0.0520A5 0.0520A5	0.1349 0.12349 0.10745 0.13749 0.13749 0.13769 0.13789 0.13769 0.13769 0.13769	-1.0099 -1.0090 -1.0000 -1.0090 -1.0099 -1.0099			
	122 127 137 142 152 157 >hnotting 157 >4001ting 167 167 167 167	3.7711 3.4660 3.4759 2.473 3.4167 3.4210 at pressure Pt 3.4162 3.4210 At pressure Pt 3.4162 3.4210	1.1741 1.0729 9.95766 0.#3398 1.0635 1.0651 PATITO . FAS #/PO 1.0635 1.0635 1.0635 1.0635 1.0635	0.053A50 0.047719 0.041534 0.0225A5 0.0526A7 I NOTTIE TIAP 0.0520A5 0.570A2 0.0520A5 0.7570A2 0.0520A5 0.0520A5	0.1349 0.12349 0.10745 0.13749 0.13749 0.13769 0.13789 0.13769 0.13769 0.13769	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
197 3-7341 1-1632 0.657949 0.15059 -1.0000	122 127 137 142 152 157 >40017 (09) 167 >40017 (09) 167 167 177 >400 (17) >400 (17) >	3.7711 3.4663 3.4759 2.4751 3.4163 3.4163 3.4210 AL PRESSUPE PL 3.4163 3.4163 3.4163 3.4163 3.4163 3.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7.4163 7	1.1741 1.0729 9.95766 0.83398 1.0635 1.0651 PATION . EEN M/PO 1.0635 1.9651 PATION . 20 M/PO 1.0635 1.9651	0.053450 0.047719 0.041534 0.052545 0.052067 I MUTTIE TI AP 1.052045 0.052045 0.052045 0.052062 0.052062	C.13890 0.12349 0.20785 0.13749 0.13749 0.13769 0.13769 0.13769 0.13769 0.13769	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

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$\Box$	NASA-LEWIS	PRELIM	MARY DATA	07/07/79	CADDELL	REC 10/07/79	02:19:35.242	FAC BEEXL	P64 C034	RDG 1042
	>4UDITION	L PRESSURE	RATIOS . PRI	TAVBA BEAG		the constant of the constant o			***************************************	markatana ya ka wakatan e samana e rendandan
~	AAD HOKU	PL	PL / PG	PL/PTF	PL /PTP	X/CHAX				
	32	15.471	4.8289	0.21396	0.42708	0.43200				
	37	9.0177	7. 5025	0.11588	0.22133	0.53000				
_	47	14.596	4.5520	0.7:1173	0.40266	0.62900				
-	52	10.359	3.2330	0.14325	0.28593	J.72700				
~	>ADDIT TON	L PRESSURE	RATIOS . FLO	ON SPLITTER L	. D.				N · ·	
	AVD WORD	Pt.	PL / P11	PL/PTF	PL/PTP	X/DMAX				•
~	62	11.493	7.7120	0.16447	0.12820	J. 42200				
	67	8-3177	2.5962	9-11503	0.22961	u.67003				
							**************************************		-1.44W	The state of the s
•.	>ADDITIONA	IL PRESSURE	RATIOS . FLO	W SPLITTEP D	. D	· •				
	AVD MORT	PL	PL/PN	PL/PTF	PL/PTP	X/DMAX .		war and a second of the second	<u> </u>	or man
	77	29.744	9.2991	0.41163	0.82162	0.5 <b>080</b> 0				
	<u> </u>	15.796	4.5903	0.20239	0.40597	0.58300	·			
	c?	3.4504	1.0799	0.647#49	0.055500	0.47000				
	SANTITIONAL .	L PRESSURE	RATIOS . EJ	FETCH SHPMIN		g ya minan da sama		The contract of the contract o	u. u valentre <del>gistelle</del> er _{valen} går u	
	AVD WOPD	PL	PI / PO	PL/PTF	PL/PTP	X/DMAX		mit of the state o	war de a	
	107	6.1169	1.9093	0.054596	0.16886	0.62400				
	112	4.3607	1.3611	0. 560-08	0.12036	0.83000	,			
	127	4.2256	1.3189	0.058439	U-11665	2. 96000				
	127	3.4394	1.0737	9.047572	0.094956	1.0900				
	127	4.2779	1-2502	0.055353	0.11057	1-2200				
	137 142	4.0054 3.7371	1.2502 1.1549	0.055253	0.11057 0.10214	1.2200		y den schaden magnifiken den i is	remain on the second of the second	Manager was seen
=	142	3.7371		2.051171				e produce a supplier de la companya		
=	142 >40917 (004	3.7371 44F50MC	1.1549 ************************************	7.051171	0.10714	1.3590	7			
=	142 >ARSITIONS APQ MOPO	3.7371 H. MAFSKIME PL	1.1549 <b>8.1105 - FOI</b> PL/PO	7.051171 PL/PTF	0.10214 Pt /PTP	1.3590 X/DMAX	7			
<	ANO MORD	3.7371 1. 09F56MC Pt 5.1169	1.1549 ************************************	7.051171 PLATE IN ET PL/PTF 0.084596	0.10714 Pt /PTP 0.16886	1.3590 X/DMAX -1.0000	<b>7</b>	•		
5	142 	3.7311 H-94556MC PL - 6.1169 4.3607	1.1549 ************************************	7.051171 PL/PTF 0.084596 0.060308	0.10714 Pt /PTP 0.16886 0.12038	X/0MAX -1.0000 -1.0010	7			
<	142 >AND HOPD -10 -112 -122	3.7311 11 - 04-56-mc P1 - 6.1169 - 4.3607 - 4.2256	1.1549 ************************************	7.051171 PLATON IN EX- PLATON 0.04596 0.04596 0.058439	0.10714 P1 /P7P 0.16886 0.12038 0,11665	X/0MAX -1.0000 -1.0010	7			
-	142  >40017 1014  AND MIRPO -10 -112 -112 -127	3.7311 1	1.1549 PL/Pn 1.9093 1.3611 1.2189 1.0737	7.051171 PL/PTF 0.084596 0.06239 0.052439 0.067572	0.10214 Pt /PTP 0.16886 0.12038 0.11665 0.094**56	X/DMAX -1.0009 -1.0000 -1.0000	Z			
-	142	9.731 PL #45564mc PL 6.1169 4.3697 4.2256 3.4398 4.0154	1.1549 PI/Pn 1.9093 1.3611 1.2189 1.0737 1.2502	2.051171 PL/PTF D. 084596 G. 086298 C. 087572 U. 087572 U. 087533	0.10714 Pt /PTP 0.16886 0.12038 0.11665 0.094254	X/DMAX -1.0009 -1.0000 -1.0000 -1.0000		•		
-	142 340917 1000 AND MORD -107 -112 -122 -127 -177 -142	3.7311 PL 6.1169 4.3697 4.2256 3.4344 4.0354 3.7391	1.1549 PL/Pn 1.9093 1.3611 1.2189 1.0737 1.2592 1.1549	7.051171 PL/PTF 0.084596 0.04030R 0.058439 0.047572 0.075353 0.051171	0.10714 Pt /PTP 0.16886 0.12038 0.11665 0.094454 0.11957	X/DMAX -1.0009 -1.0000 -1.0000 -1.0000 -1.0000	7			
-	142 >40017 1014 ANO MIRTO -107 -112 -127 -127 -127 -127 -142 -162 -162	3.7311 PL 69.556MC PL 6.1169 4.3697 4.2256 3.4398 4.0154 3.7751 3.4398	1.1549 PL/PD 1.9093 1.3611 1.2189 1.0737 1.2502 1.1549 1.0643	2.051171 PL/PTF 0.064596 0.06239 0.052439 0.047572 0.075363 0.051171 0.047176	0.10714 Pt /PTP 0.16886 0.12038 0.11665 0.094456 0.11957 0.11927	1.3590 X/0MAH -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	142 340017 JONE 107 -117 -112 -127 -127 -147 -142 -167	3.7311 PL AGCSCHIE 6.1169 4.3697 4.2256 3.4398 4.0154 3.7791 3.4998 3.4998 3.4998	1.1549 PI/PR 1.9093 1.3611 1.2189 1.0737 1.2592 1.1540 1.0643 1.0658	7.051171 PL/PTF B. CR4596 G. DCC30R G. DCC30R G. DCF439 G. CF47572 U.OFF353 O.C51171 G.C471°6 D.O47226	0.10714 Pt /PTP 0.16886 0.12038 0.11665 0.094454 0.11957	X/DMAX -1.0009 -1.0000 -1.0000 -1.0000 -1.0000	7			
-	142 340017 JONE 107 -117 -112 -127 -127 -147 -142 -167	3.7311 PL AGCSCHIE 6.1169 4.3697 4.2256 3.4398 4.0154 3.7791 3.4998 3.4998 3.4998	1.1549 PI/PR 1.9093 1.3611 1.2189 1.0737 1.2592 1.1540 1.0643 1.0658	2.051171 PL/PTF 0.064596 0.06020A 0.052439 0.047572 0.051171 0.047176 0.047226	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094454 0.11957 0.11957 0.17274 0.094265	1.3590 X/0MAH -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
-	142  340017 10M  AND WIPT  -10  -112  -122  -127  -137  -142 -162 -167  240017 10M  AND WIPT	9.7311 PL ##FSSURF PL 6.1169 4.3607 4.2256 3.4399 4.0354 3.7351 3.4959 3.4148	1.1549  PL/PN 1.9093 1.3611 1.2189 1.0737 1.2502 1.1540 1.0643 1.0658	2.051171 PLATON INCT PL/PTF 0.084596 0.060300 0.058439 0.047572 0.075353 0.051171 0.047176 0.047226	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094056 0.11957 0.17927 0.344124 0.094265	1.3590 #/DMAX -1.0909 -1.0909 -1.0000 -1.0000 -1.0000 -1.0000				
_	142  340917 (0000  AND MORD  -107  -112  -127  -127  -142  -167  240217 (0400  AND MORD -152	9.7371 PL ##F554MC PL 6.1169 4.3607 4.2256 3.4398 4.0354 3.7391 3.4098 PL 3.4098	1.1549  PL/PN 1.9093 1.3611 1.2189 1.0737 1.2592 1.1540 1.0643 1.0658  PATIN FAR	7.051171  PL/PTF	0.10714  P1 /P7P 0.16886 0.12038 0.11665 0.094254 0.11957 0.17274 0.844124 0.94265	X/DMAX -1.0009 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
-	142  340017 10M  AND WIPT  -10  -112  -122  -127  -137  -142 -162 -167  240017 10M  AND WIPT	9.7311 PL ##FSSURF PL 6.1169 4.3607 4.2256 3.4399 4.0354 3.7351 3.4959 3.4148	1.1549  PL/PN 1.9093 1.3611 1.2189 1.0737 1.2502 1.1540 1.0643 1.0658	2.051171 PLATON INCT PL/PTF 0.084596 0.060300 0.058439 0.047572 0.075353 0.051171 0.047176 0.047226	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094056 0.11957 0.17927 0.344124 0.094265	1.3590 #/DMAX -1.0909 -1.0909 -1.0000 -1.0000 -1.0000 -1.0000				
	142  340017 1014  AND MIRED  -107  -112  -127  -127  -127  -127  -142  -162  -167  >400 117 1014  AVD MIRED  -152  -157	9.7371 PL PRESSURE PL 6.1169 4.3697 4.2256 3.4348 4.0354 3.4058 3.4058 7.6148	1.1549  PL/PN 1.9093 1.3611 1.2189 1.0737 1.2502 1.1540 1.0643 1.0658  PATION FAR	7.051171  PL/PTF	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094254 0.11957 0.11927 0.1927 0.1927 0.194128 0.094265	X/DMAX -1.0009 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	142  340017 1014  AND MIRED  -107  -112  -127  -127  -127  -127  -142  -162  -167  >400 117 1014  AVD MIRED  -152  -157	9.7371 PL PRESSURE PL 6.1169 4.3697 4.2256 3.4348 4.0354 3.4058 3.4058 7.6148	1.1549  PL/PN 1.9093 1.3611 1.2189 1.0737 1.2502 1.1540 1.0643 1.0658  PATION FAR	7.051171 PL/PTF 0.064596 0.06209 0.052439 0.057572 0.075363 0.051171 0.047176 0.047226  MO771F FMP 0.047276	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094254 0.11957 0.11927 0.1927 0.1927 0.194128 0.094265	X/DMAX -1.0009 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	142  340917 10M2  AND MORD  -107  -112  -122 -127  -142 -152 -157  240917 10M2  AND MORD -152 -157  >ADDIT 10M2	9.7371  PL	1.1549  PL/PN 1.9093 1.3611 1.2189 1.0737 1.2592 1.1549 1.0643 1.0658  PATIN FAR PL/PN 1.0649 1.0658	7.051171  PL / PTF	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094254 0.17274 0.17274 0.17274 0.17274 0.094265  Pt /PTP 0.094126 0.094265	1.3590  X/DMAX -1.0009 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	142  340917 1014  AND HOPD  107  -107  -112  -127  -127  -142 -167  -142 -167  AND HOPD  AND HOPD  AND HOPD	9.7371 PL	1.1549  PI/PN 1.9093 1.3611 1.2189 1.0737 1.2592 1.1549 1.0643 1.0658  PAYINE FAR PI/PN 1.0647 1.0658	7.051171  PL/PTF 0.084596 0.060308 0.052439 0.057572 0.057573 0.051171 0.047176 0.047226  MD771F EXTP PL/PTF DFG SHPPHRALL	0.10714  P1 /P7P 0.16886 0.12038 0.11665 0.094264 0.11957 0.11957 0.11957 0.19244 0.94265	1.3590  X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	142  340917 10144  AND MIRED -107 -112 -127 -127 -127 -142 -157 -157 -157 -157 -157 -157 -157 -157	9.7311 PL	1.1549  PL/PN 1.9093 1.3611 1.2189 1.0737 1.2592 1.1549 1.0643 1.0658  PAYIN FAR PL/PN 1.0647 1.0643 1.0643 1.0643 1.0643 1.3658	2.051171 PL/PTF 0.064596 0.062309 0.052439 0.057572 0.075353 0.C57171 0.C47176 0.047226  MO771F FMP PL/PTF 0.C47156	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094254 0.17274 0.17274 0.17274 0.094265  Pt /PTP 0.094126 0.094265	#/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	142  >ANOTE INM  AND MIRED -10 -112 -122 -127 -137 -142 -162 -167 -167 -167 -167 -167 -177  AND MIRED -167 -167 -167 -167 -167 -177	9.7311 PL 09F554ME PL 6.1169 4.3697 4.2256 3.434M 4.0154 3.405M 3.405M 3.405M 3.404M IL PRESSURE PL 3.409M 3.414M II PRESSURE OL 3.439M 3.434M	1.1549  PI/PR 1.9093 1.3611 1.2189 1.0737 1.2502 1.1540 1.0643 1.0658  PATION FAR PL/PR 1.0643 1.0658  PATION 80	7.051171 PL/PTF 0.064596 0.067572 0.052439 0.057572 0.0575171 0.047176 0.047276 PL/PTF 0.047276 DFG SHPFHM 11 PL/PTF 0.047126 DFG SHPFHM 11	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094054 0.11927 0.1927 0.1927 0.094265  PI /PTP 0.094265  CATION  PTP 0.854126 0.96265	#/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	142  340917 1000  AND HOPD  -107  -112 -122 -127 -142 -152 -157  240917 1000  AND HOPD -152 -157  >40017 1000  AND HOPD -167 -177  >40017 1000  AND HOPD -167 -177	9.7371  M. AGESCHIE  PL 6.1169 4.3697 4.2256 3.4398 4.054 3.7791 3.4058 PL 3.4098 3.4148  II DRESSURE  PL 3.4098 3.4148  II DRESSURE  PL 3.4098 3.4148	1.1549  PL/PN 1.9093 1.3611 1.2189 1.0737 1.2592 1.1540 1.0643 1.0658  PATION FAR PL/PN 1.0643 1.0658  PATION 80	7.051171  PL / PTF  0.084596  0.067572  0.058439  0.058439  0.051171  0.057176  0.047226  MP771F EMP  PL / PTF  0.047226  DEG SHPPHM 11  PL / PTF  0.047226  DEG SHPPHM 11  PL / PTF  0.047226	0.10714  P1 /PTP 0.16886 0.12038 0.11665 0.094256 0.11957 0.17274 0.84124 0.094265  P1 /PTP 0.094126 0.094265  PCATION P1 /PTP	1.3590  X/DMAX -1.0009 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000  X/DMAX -1.0000 -1.0000 -1.0000				
	142  >ANOTE INM  AND MIRED -10 -112 -122 -127 -137 -142 -162 -167 -167 -167 -167 -167 -177  AND MIRED -167 -167 -167 -167 -167 -177	9.7311 PL 09F554ME PL 6.1169 4.3697 4.2256 3.434M 4.0154 3.405M 3.405M 3.405M 3.404M IL PRESSURE PL 3.409M 3.414M II PRESSURE OL 3.439M 3.434M	1.1549  PI/PD 1.9093 1.3611 1.2189 1.0737 1.2502 1.1540 1.0643 1.0658  PATION FAR  PL/PD 1.0643 1.0658  PATION 80	7.051171 PL/PTF 0.064596 0.067572 0.052439 0.057572 0.0575171 0.047176 0.047276 PL/PTF 0.047276 DFG SHPFHM 11 PL/PTF 0.047126 DFG SHPFHM 11	0.10714  Pt /PTP 0.16886 0.12038 0.11665 0.094054 0.11927 0.1927 0.1927 0.094265  PI /PTP 0.094265  CATION  PTP 0.854126 0.96265	#/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

RUN 14

MASA-LF	IIS PRELIMI	MERY PETA	07/07/79	CADDELL	REC 13/07/79 02:20:33.079 FAC 8X6X1 PGM C834 RRG 1843
	NAL PRESSURE	PATIOS . CP.	THAPY PLUC		
AVD WORD	PL	PL/PR	PL/PTF	PL/PTP	X/DMAX
32	13.545	4.1941	0.18515	0.42708	
37	7.0724	2. 1899	0.006675	0.22300	
47	12.730	3.9417	9-17401	0.40138	
52	9.3756	2.8112	0.12410	0.28626	0.72700
>ADD1110	MAL PRESSURE.	RATIOS . FLO	OW SPLITTER L	• D•	and the second s
AVO HORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX
67	10.414	3.2747	0.14236	0.32837	0.42200
67	7-2876	2.25£5	0-099617	C-22578	0,67000
>APPIT IC	NAL PRESSURE	RATIOS . FLI	DN SPLITTER C	. D.,	
AVD WORD	PL	PL/PD	PL/PTF	PL/PTP	X/DMAX
77	30.024	9.2968	0-41041	0.94666	
82	14.935	4.5935	9. 20278	0.46775	<u>0.56300</u>
	3.4932	1.0795	0.047613	0.10083	0.67000
	MAL PRESSURE				
				*	entremental de le marie (per con composition de la composition della composition del
TAD AUSD	PL	PL / PO	PI /PTF	PI /PTP	x/nmax
107	6-1816	1.9151	0.004498	0.15491	0.62400
112	4,4045	1.3638	0.060207	0.13688	9.83000
122	4-2544				9-96000
		1.3266	0.058564	0.13509	
127	3.4682	1.0739	0.6474 )A	0.10935	1.0900
	3.6835	1.1496		0.11614	
142	3.3530	1.03#2	0.045833	0.10572	1.3500
>4001714	HAL PRESSURE	-41105 - FR	P <del>C NOW   104 CT</del>		
APO WORD	PL	PL/PO	PL /PTF	PL /PTP	X/DMAX .
-10	-	-			
-10/	6.1916		0.084498	0.19491	-1-1960
		1.363R	0. 060207	0.13888	-J. 6000
-112	4.4045		A 45 45//	0.13509	
	4.2944	L。3266	0-050564		
-112		1.0739	0.047408	0.10035/	<b>-1.0000</b>
-112 -122 -127	3.4682	1.0739	0.947408	0.10°35/	
-112 -122 -127 -137	4.2944 3.4682 3.4683	1.0739	0.947408 0.050351	0.10035	-1.0000
-112 -122 -127 -137 -142	4.2844 3.4682 3.6835 3.3190	1.0739 1.1406 1.0382	0.947408 0.050351 9.045833	0.10°35 0.11614 0.14572	-1.0000 -1.0000
-112 -122 -127 -137 -142 -152	4.2544 3.4682 3.6635 3.3190 3.4431	1.0739 1.1406 1.0382 1.0661	0.947408 0.050351 9.045833 0.047065	0.10°35 0.11614 0.16572 0.10856	-1.0000 -1.0000 -1.0000
-112 -127 -127 -137 -142 -152 -157	4.2844 3.4682 3.6835 3.3790 3.4431 3.4381	1.0739 1.1406 1.0382 1.0661 1.0646	0.047408 0.050351 0.045833 0.047065 0.046597	0.10°35 0.11614 0.10572 0.10856 0.10841	-1.0000 -1.0000
-112 -127 -127 -137 -142 -152 -157	4.2544 3.4682 3.6635 3.3190 3.4431	1.0739 1.1406 1.0382 1.0661 1.0646	0.047408 0.050351 0.045833 0.047065 0.046597	0.10°35 0.11614 0.10572 0.10856 0.10841	-1.0000 -1.0000 -1.0000
-112 -127 -127 -137 -142 -152 -157 >AND LT IO	4.2944 3.4692 3.46935 3.3950 3.4431 3.4381 PAIL PRESSURE	1.0739 1.1406 1.9382 1.0661 1.0646 RATION, FAI	0.047408 0.050351 0.045833 0.047065 0.046997 N NCZZIE PLAP	0.10°35 0.11614 0.16572 0.10856 0.10841	-1.0000 -1.0000 -1.0000 -1.0000
-112 -127 -127 -137 -142 -152 -157 >ADD [T [0	4.2944 3.4682 3.4685 3.3790 3.4431 3.4381 PAL PRESSIRE PL 3.4431	1.0739 1.1406 1.9382 1.0661 1.0646 RATIO FAI	0.947408 0.050351 9.045351 9.047065 0.046597 N NCZZIE PIAP	0.10°35 0.11614 0.10572 0.106572 0.10641 PL/PTP 0.10656	-1.0000 -1.0000 -1.0000 -1.0000
-112 -127 -127 -137 -142 -152 -157 >ADD [T [0	4.2944 3.4692 3.46935 3.3950 3.4431 3.4381 PAIL PRESSURE	1.0739 1.1406 1.9382 1.0661 1.0646 RATION, FAI	0.047408 0.050351 0.045833 0.047065 0.046997 N NCZZIE PLAP	0.10°35 0.11614 0.16572 0.10856 0.10841	-1.0000 -1.0000 -1.0000 -1.0000
-112 -122 -127 -137 -142 -152 -157 >ADDITION AVD MOPD -152 -157	4.2944 3.4682 3.4685 3.3790 3.4431 3.4381 PAL PRESSIRE PL 3.4431	1.0739 1.1406 1.9382 1.0661 1.0646 RATION, FAR PL/PD 1.0661 1.0646	0.947408 0.050351 9.045833 0.047065 0.046597 N NCZZIE PIAP 9/PTF 0.047065 D.046967	0.10°35 0.11614 0.16572 0.10856 0.10841 PL/PYP 0.10856 0.10841	-1.0000 -1.0000 -1.0000 -1.0000
-112 -122 -127 -137 -142 -152 -157 >AND LT IO AVD MOPD -152 -157	4.2944 3.4692 3.46935 3.3490 3.4431 3.4381 PARI PRESSIRE 1	1.0739 1.1406 1.9382 1.0661 1.0646 RATION, FAR PL/PD 1.0661 1.0646	0.947408 0.050351 9.045833 9.047065 0.046597 N NCZZIE PLAP 91 PTF 0.047065 D.046967	0.10°35 0.11614 0.10677 0.10841 PL/PYP 0.10856 0.10841 OCATION	-1.0000 -1.0000 -1.0000 -1.0000
-112 -127 -127 -137 -142 -152 -157 >ADDITION AVID WIPPI -152 -157 >ADDITION AVID WIPPI	4.2944 3.4692 3.46935 3.3990 3.4431 3.4381 PIAL PRESSIRE PL 3.4431 3.4381 PIAL PPESSIRE	1.0739 1.1406 1.9382 1.0661 1.0646 RATION, FAI PL/PD 1.0661 1.0646 RATION, 20	0.947408 0.050351 0.045833 0.047065 0.046997 N NCZZIE PIAP 91/PTF 0.047065 0.44997	0.10°35 0.11614 0.16572 0.10856 0.10841 PL/PTP 0.10856 0.10841	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-112 -122 -127 -137 -142 -152 -157 >ADDITIO AVD MOPD -152 -157	4.2944 3.4692 3.4693 3.3990 3.4431 3.4381 PL 3.4431 3.4391	1.0739 1.1406 1.9382 1.0661 1.0646 RATION , FAI	0.947408 0.050351 9.045833 9.047065 0.046597 N NCZZIE PLAP 91 PTF 0.047065 D.046967	0.10°35 0.11614 0.10677 0.10841 PL/PYP 0.10856 0.10841 OCATION	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-112 -127 -127 -137 -142 -152 -157 >ADDITIO AVD MORD -152 -157 >ADDITIO AVD MORD -167 -172	9.2949 3.4692 3.4693 3.4431 3.4391 PL 3.4431 3.4391 PL 3.4431 3.4391	1.0739 1.1406 1.0382 1.0661 1.0646  RATION FAI PLIPE 1.0661 1.0661 1.0661 1.0661	0.947408 0.050351 9.045833 0.047065 0.046597 N NCZZIE PIAP 91 PTF 0.047065 0.44997 DEG SHRIDO 10 PL/PTF 0.047065 0.647065	0.10°35 0.11614 0.16572 0.10856 0.10841 PL/PTP 0.10856 0.10841 OCATION 0.10856 0.10856	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-112 -127 -137 -142 -157 -157 -157 -157 -157 -157 -157 -157	4.2944 3.4692 3.46935 3.3490 3.4431 3.4381 PL 3.4431 3.4391 PL 3.4431 3.4431 3.4431 3.4431	1.0739 1.1406 1.9382 1.0661 1.0646 RATIOS, FAR PL/PD 1.0661 1.0661 1.9661	0.047408 0.050351 0.045833 0.047065 0.046597 N NCZZIE PLAP 9/PTF 0.047065 D.44997 DFG SHRCDQ 10 PL/PTF 0.047065 0.647065	0.10°35 0.11614 0.16572 0.10856 0.10841 PL/PYP 0.10856 0.10841 DEATION	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-112 -127 -137 -142 -157 -157 -157 -157 -157 -157 -157 -157	4.2944 3.4682 3.4682 3.4682 3.4790 3.4431 3.4381 PMAL PRESSIRE PL 3.4431 3.4381 PL 3.4431 3.4431 3.4431 7.4431	1.0739 1.1406 1.9382 1.0661 1.0646  RATION, FAR PL/PN 1.0661 1.9661 1.9661 RATION, 80 PL/PN	0.047408 0.050351 0.045833 0.047065 0.046997 N NCZZIE PLAP 0.047065 D.046997 DEG SHREDQ 10 PL/PTE 0.047065 0.047065	0.10°35 0.11614 0.16572 0.10856 0.10841 PL/PTP 0.10856 0.10841 OCATION 0.10856 0.10856	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-112 -122 -127 -137 -142 -157 -157 -157 -2001TIF AVD MOPD -157 -2001TIF AVD MOPD -167 -177	4.2944 3.4692 3.46935 3.3490 3.4431 3.4381 PL 3.4431 3.4391 PL 3.4431 3.4431 3.4431 3.4431	1.0739 1.1406 1.9382 1.0661 1.0646 RATIOS, FAR PL/PD 1.0661 1.0661 1.9661	0.947408 0.050351 9.045833 9.047065 0.046997 N NCZZIE PIAP 9/PTF 0.047065 0.44997 DEG SHRITO 11 PL/PTF 0.047065 0.C47065	0.10°35 0.11614 0.16572 0.10856 0.10841 PL/PYP 0.10856 0.10841 DEATION	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-112 -127 -137 -142 -152 -157 >ADDITION AVD MORD -152 -157 >ADDITION AVD MORD -167 -172 >ADDITION AVD MORD -167 -172	4.2944 3.4682 3.4682 3.4682 3.4790 3.4431 3.4381 PMAL PRESSIRE PL 3.4431 3.4381 PL 3.4431 3.4431 3.4431 7.4431	1.0739 1.1406 1.9382 1.0661 1.0646  RATION, FAR PL/PN 1.0661 1.9661 1.9661 RATION, 80 PL/PN	0.047408 0.050351 0.045833 0.047065 0.046997 N NCZZIE PLAP 0.047065 D.046997 DEG SHREDQ 10 PL/PTE 0.047065 0.047065	0.10°35 0.11614 0.16572 0.10856 0.10841 PL/PYP 0.10856 0.10841 OCATION 0.10856 0.10856 PL/PYP	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000

NASA-LFHIS	PREL 141	INAPY DATA	07/07/79	CADDETI	REC 10/07/79	02:21:27.250	SAC BRAKE	PG# C034	FON 14 RFG 1864
Swulliuw¥	LPRESSIRE	PATIOSPPI	MARY PLUG					ge mangatikan di salah sara samani salah salah sa	
LYD WORD	PL	PL/PG	PL/PTF	PL/PTP	X/DMAX				
32	12. 737	7.7176	0.16459	0.42734	0.43200			•	
37	6.2925	1.9482	0.396245	U. 72379	0.53000				
47	11.337	3.5101	0.15539	0.40320	0.62900		•		
52	9.3395	2.4491	0.11019	0.20592	0.72700				
SADD IT IONA	i PRESSIME	PATINS . FIR	W SPLITTER I	- 0-					
	- THE STORE	_		-					
IVD WORD	PL .	PL/PO	PL/PTF	PL/PTP	x/DMAX				
67	9.2456	2.8625	0.1267?	0.32482	0.42200				
67	6-5677	2.0025		0.23002	9.67000				
APRITITIONA	L PRESSURE	RATINS . FLO	EN SPLITTEP D	. D.				-	
AD MUSD	PL	PL / PO	PL/PTF	PL/PTP	X/DMAX				
77	79.948	9.2721	0.41047	1.0651	0.50000			we en al	
87	14.019	4,5880	0.22710	0.52702	2.50300				
92	3.4789	1.0768	0.047670	U.12365	0.67000				
>400111004	L PRESSIME	PATINS , FJF	CTOR SHPCUD	· Park of the second				40 - 1 - <b>40</b> - 1 <del>40</del> - 1 <del>40</del> - 1 <del>40</del> - 1 <del>40</del> - 1	
ND WORD	PL .	PI / PO	PL/PTF	PL /PTP	X/DMAX		· we want to be a section of		
107	6-1723	1.9110	Q. C84598	0.21952	0.62400				
112	4.3945	1.36CA	0.060233	0.1562¢	J. 83000		· · · · · · · · · · · · · · · · · · ·		
122	4.2744	1.3234	0.058596	0.15202	0.96000				
127	3.464)	1.0737	0.047533	0.12334	1-0900				** *
127	3-4930	1.0784	0.047730	0.12387	1.2290				
142	3.0221	0.43568	0.041422	0.10748	1.3500		The second restrict and the low		
SADDLY LONG		AA1105 . FOR	ERODY INVES						
		_						communication was a second or	
NUB J	PL	PI /PO	PL/PTF	PL /PTP	X/IMAY		•		
107	4-1723	1.9110	0. 684598	0.21952	-1-0900				
117	4.3346	1.3606	9.067233	0.15629	-8.0000				
122	4.2744	1.3234	O. CSASA6	0.15702	-1.0000				
127	4640	1.9737	0.547533	0.12335	-1.0020				
137	3. 4830	1.0784	0.047739	0.12347	-1-0000				super or an
142	3.322	0. 93569	0. 641472	0,20748	-1.0000				
152 157	3.4429	1.0669	0.547199 0.647259	0.12245 0.12763	-1.96 <b>90</b> -1.9930				
•	-			V-14/63	-1-2000				
SENDIT INME	PRESSIPE	RATIOS FAR	MOTTE TEAT						
AU HUBU	Pt	PI /PI	N 19TF	PI /PTP	X/DMAX	,			
-152	3.4479	1.9660	Q. 747189	0.12245	-1.0030				
157	3.4490	1.0575	0.367258	0.12763	-1.0000		F		
>2011	PRESSURE	PATION . 30	DEG SHEETING	CLATION					
VO WOPB	PL /	PI /PT	M /PTF	PKPIP	x/DMAX		a a last commentes		
167	3.4539	1.9691	9-947727	U. 172FO	-1.0000				
172	3.541)	1.0706	0.047355	0.127	-1.0000				
_		•	nec specim to	•					
Sendit time		•			<u>\</u> .				
ע שלפו חאו	PL	PL / PO	PI /PTF	PI /PŤP	X/DMAX				
-193	3.4988	1.2071	0.053437	0.13866	-1.0000				
4.4	3	1.3907	3.052279	0.11562	-1.0000	-		• •	
X67		THPHST PARAM		0.01 - 141	. 1.0000				

MASA-LEWI	S PRFL 141	HARY DATA	07/07/79	CADDELL	REC 10/07/79	02:22:03.473	FAC AVEXI	PG4 C034	PBG 1845
SADDITION	AL PRESSURE	RATIOS PRI	MAPY PLUG						
	Table of Marie Co.								
AVD HOPD	PL	PL/PT	PL/PTF	PL/PTP	X/DHAX				
32	17.425	5.3542	0.21226	0.42735	0.43200				
37	9.9913	2.7627	0.11004	0.22650	0.53000				
47	16.636	5.1724	0.27323	0.49725	J.62900				
52	11.612	3.5679	0-14211	0.28477	3.72700				
HO1 T1COA<	AL PRESSURE	RATIOS . FLO	W SPLITTER.I.	.D					
AVD WORD	PL	PL/P3	PL/PTF	PL/PTP	X/DMAX				
62	13.472	4.1178	0.16401	0.32867	J. 42200				
.67	7.3565	2.9719	0-11438	0.22021	J. 6 7000				
>ADDITION	AL PRESSURE	RATIOS . FLO	M SPLITTER D	Da			<del></del> .		
LVD WOR'S	.PL.	PL/PG	PL/PTF	PL/PTP	Y/DMAY				
77	33.450	10.278	0.40537	0.82033	3.50800	• • • • •		**************************************	
82	16.651	5.1162	0.20378	0.40035	0.58300				
92	3.5118	1.0790	0. 042578	0.086123	0.67000				<del></del>
>ADD IT ION	AL PRESSURE	RATIOS . FJF	CTCP SHREND	and the second contract of the second of			in the second of		
									- marker and a second a second and a second
AVD HUKD	PL	PL/PO	PL /PTF	PL /PTP	x/max				
107	6.9352	2.1309	0.064876	0.17008	9.62499				
115	4.9435	1.5189	0.040500	0.17123	0.03000				
122	4.7933	1.4728	0.058663	0.11755	0. 96000				a decreased a second
127	3.5769	1.0775	0.042917	0.084000	1.0900				
137	4.5130	_ 1.3067	0.055232	0.11068	1.2200				and the second second
142	4-1826	1.2952	0.351199	0.19258	1.3500				
SANDIT FOR	A PRESSURE	RATIOS - 500	E4004   141 EE		<del></del>				
מאחונים	Pt	Pt /Pn	PI / PTF	PL/PTP	X/IMAX				# 1 #11 · · · · · · · · · · · · · · · ·
-107	6.9352		2. 084876		1-9606		•		
-115	4.9435	7.1309 1.5199	0.060500	0-17006 0-12123	-1.0000				
			0.058663	0.12123	-1.9300				
:122 -127	4. 1933 5067	1.4728 1.9775	0.047517	0.086000	-1.0000				
-137	4.2130	1.3967	9-05-232	0-110	-1.0000				
-14?	4.1976	1.2952	0.051189	0-10259	-1.0000			research and the second of the second	no company transport
-152 -152	3.4667	1.0452	0.042427	0.085019	-1.0000				
-157	3.4717	1.0667	0.042498/	0.085141	-1.3030				•
	AL PRESSIBE								
AVD WOPD	P1	PI VAN	A / PTF	PL/PTP	X/DMAX			on the supplements of the supple	<b> </b>
AVN WOPN -152	P1 3.4667	7 /PO 1-0452	0.042427	0.075018	-1.0000				• • · · · · · · · · · · · · · · · · · ·
>A1017 (0%) AVD WOPD -152 -157	P1	PI VAN	A / PTF						
NYD WOPD -152 -157	P1 3.4667 3.4717	7 / Pri 1.0452 1.0667	0.042427	0.085018 0.085141	-1.0000				
AVD WOPD -152 -157 ->ADD[T]DN	P1 3.4667 3.4717 AL PRESSURE	1.0452 1.0667 PATINS , 20	0.042427 0.042427 0.042489	0.085018 0.085141	-1.0000 -1.0000				• • · · · · · · · · · · · · · · · · · ·
AVD WOPD -152 -157 ->ADD[1]DN	P1 3.4667 3.4717 AL DRESSIME PL	1.0452 1.0667 PATIOS . 20	0.042427 0.042489 DEG SHREIR	0.095018 0.095141 PLATITIN	-1.0000 -1.0000				
AVD WOPD -152 -157 ->ADD[T][DN AVD WOPD -167	P1 3.4667 3.4717 AL PRESSURE	1.0452 1.0667 PATINS , 20	0.042427 0.042427 0.042489	0.085018 0.085141	-1.0000 -1.0000				
AVD MOPD -152 -157 >ADDITION AVD MOPD -167 -172	PI 3.4667 3.4717 AL DRESSIME PL 3.4667	PATINS . 20 PL/P0 1.0452 1.0667	0.042427 0.042489 DEG SHECIND (1	0.095018 0.095141 TCATION PLATE OF THE O.DESO18 0.095018	-1.0000 -1.0000 x/bmay -1.0000				
AVD WOPD -157 -157 -ADDIT ION AVD WOPD -167 -172	PI 3.4667 3.4717 AL DRESSIME PL 3.4667 3.4117 M PRESSIME	PATINS . 20 PL/P0 1.0652 1.0667 PATINS . 70 PATINS . 70	0.042427 0.042489 DEG SHECIMO (1 PL/PTF 0.042427 0.042489 DEG SHECIMO (1	0.095018 0.095141 PCATION PLATE OF THE O.DESO18 0.095018	-1.0000 -1.0000 -1.0000				
AVD WOPD -157 >ADDIT ION AVD WOPD -167 -172 >ADDIT ION AVD WOPD	P1 3.4667 3.4717 AL DRESSIRE PL 3.4667 3.4717 M PRESSIRE	PATINE . 80	PL/PTF 0.042427 0.042489 DEG SHRCHD 19 0.042427 0.042489 DEG SHRCHD 19	0.095018 0.095141 PL/PTP 0.005018 0.095018 PL/PTP	-1.0000 -1.0000 -1.0000 -1.3000				
AVD MOPD -152 -157 >ADDITION AVD MOPD -167 -172	PI 3.4667 3.4717 AL DRESSIME PL 3.4667 3.4117 M PRESSIME	PATINS . 20 PL/P0 1.0652 1.0667 PATINS . 70 PATINS . 70	0.042427 0.042489 DEG SHECIMO (1 PL/PTF 0.042427 0.042489 DEG SHECIMO (1	0.095018 0.095141 PCATION PLATE OF THE O.DESO18 0.095018	-1.0000 -1.0000 -1.0000				

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NASA-LEHTS	S PECLIAI	MAPY DATA	07/77/79	Cibbeil	PEC 10/37/79	G2:24:25.399	FAC PRESS	PGM C034	ADM M RBG 1946
>+9DITION	L PRESSURE	PATEOS. a. PP.	IMARY PLUG						
IAU AUDU	PL	of \bil	PL/PTF	PL/PTP	X/DMAX				
32	14.785	4.5734	0.18341	0.42705	9.43700				
37	7.6302	2.3493	9.695494	J.27213	0.53000				
47 52	13.905 9.9137	4.3201 3.0791	0.17250 0.12295	0.40164	0.62900 0.72700				
							··· • · · · · · · · · · · · · · · · · ·	——————————————————————————————————————	and the second s
NOT TIECK	IL. PRESSURE	RATIOS . FLO	DW SPLITTEP 1	.0.			· •		
IVA WUKA	PL.	PI / PO	PL/PTF	PL/PTP	K/DMAX				
62	11.356	3.5?91	0. 14687	0.32800	0.42200				
67	7.9453	2.46.95	0.098568	0.22950	9-67000			····	
SAUDIT TONA	L PRESSURE	RATIOS . FLI	ON SPLITTER O	D					
ND HORD	PL	PL / P3	PI / PTF	PL /PTP	X/DMAX				
77	32.739	17.162	0.40578	0.94478	9.50800		and an analysis of the second	34 A	
92	16.344	5.9778	0.22775	0.47200	3.56399				
02	3.46??	1.0757	3.742651	9.10000	0.67000				
>ADDITIONA	L PRESSIRE	RATIŌS , FĴI	FCT(P SHP(HUD "		* * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * *	er com	- water a summary of the superior of the super	· · · · · · · · · · · · · · · · · · ·	
NU AUbu	PI	Pt /PO	Pt /PTF	PI /PTP	X/DMAX		r of a segundarian communication	*·· • · · · - ·	
197	6.3139	2.1149	0.014696	0.19699	9-62400				
113	4.9436	1.5.)48	0.060088	0.13990	U.83000				
122	4.7235	1.4675	0.058559	0.13644	0.56000				
127	3.46??	1.0757	0.642951	0.10000	1-0900	* - * - * - * - * - * - * - * - * - * -		****	* * * * * * * * * * * * * * * * * * * *
137	4.3428	1.2561	0.350154	0.11678	1.2200				
147	3.4624	1.1379	0.045435	0.17579	1.3500				
>4m+17 (0M	1 POF SSIME	*******	seven Iffet		<del></del>			······································	<del> </del>
מפחשונים	. _{PL}	PI /PO	PL/PTF	PL /PTP	X/DHAX				in the
107	6.8199	2.1189	0.094696	0.19699	-1.0000		-		
112	4.9436	1.5048	0. C40C88	0.13990	1.0000	E ***	magnification of the same states of the same of the same states of the		**
-122	4.7235	1.4575	0.058598	0.13644	-1.0000				
127	4527	1.0757	U. 347951	9.1000	-1.0000			<del></del>	
-137	4.0429	1.2561	0.050154	0.11676	-1.0000				
-142	3.557	1.1370	7.345475	9610579	-1.0000				
152	3.4221	1.0632	0. C42454	U.098847	-1.0000				
157	3.4?21	1.06 32	0. 142456	7.758847	-1.9090				
M'01 TICE 3<	I PRESSIME	PATING	H NO7717 FLSP	**************************************				···	-
VO SOPO	PL	PL / PO	PLIPTE	PI /PTP	X/THÁX		a waxan i sa asaa sa a		
-152	3.4221	1.9632	2.047454	9.098847	-1.0009				
-1 = -	3.4271	1.7532	35 663 4 54	0.098847	-1.0000				
>477111111	I PRESSIME	PAYMS . 25	DEC SHELLING	DCAT ION					
IAD MUBU	PL /	PL / P7	PL /PTF	PLIPTP	X/DMA X				
167	3.4126	1.0617	0.047397	0.600703	-1.0000				
-177	3 Mil	1.0417	0.042392	0.09703	-1.0000			· • • · · · · · · · · · · · · · · · · ·	
SAMOTT 1979	PAPERSIME	PATINS , ED	DEC SHEETING E	CATION	·				
מפושע מעו	₽ŧ	PL / P/I	PL /PTF	PL /PTP	KANAN		and the second second		
100	3.3*17	1.2358	0.049347	0.11490	-1.0000				
A A 7	3.1177	1.2172	0.049602	0.11316	-1.0000				
		THEUST PARA		~~~~~~~					

MEST-FLAL	s useflat	INARA DZAW	97/07/79	CADDEII	PFC 10/07/	79 02:25:11.7	'2) FA	C SECT	PG# F-934	Row 14 PRG 1047
POLITICONS.	AL PRESSUPE	PATIOS . PP	TMAPY PLUG.				a service service		marker de de	
AVO HOPD	o_L	PL/P9	P1 / P7 F	PL /PTP	X/OMAX					
32	13.212	4.1130	6-16441	0.42754	9.43200					
37	6.9327	2.14FP	3.085.894	3.22326	0.53000					
47	12.493	3, 8950	3.15545	0.43425	9.42500					
52	8-0931	2.7529	9.11534	0.2Mt15	u. 727uu					
MOD TEGCAC	AL PRESSURE	RATIOS . FLI	ON SPLITTEP 1	. D.						
AVP WIPD	PI	PL / PO	PL /PTF	PL /PTP	XAPPAX					
62	10.148	3.1591	0-12629	G.32838	0.42200			**		
_61	7-1127	2.2142	0. 088509	0.23616	U. £7000					e e <del>apagonia dese</del> rgen - e sepre adeleganço
>APDITION	AL PRESSURE	RATIOS FLO	DW SPLITTEP P	.D						
AVD WOPD	PL	FL/PO	PL /PTF	PL/PTP	XAMO\X					
77	12.669	13.170	0.42652	1.0571	J.50900	•				
92	16.311	5.0775	0.20296	0.52760	0.58300					
9?	3.46.12	1.0772	0.043057	0.11197	0.67000			····	***************************************	
NOT TECNA	AL PRESSURE	PATIOS . FJE	CTOP SHROUD			a a made comment of the comment	w A n		ability replicable and a	
AVD WOPD	PL	PI / P'7	PI / PT F	PL/PTP	X/IMAX	•				
_197	6.9076	2.1192	0.684711	0.22029	0.52400					
112	4.8415	1.5971	0.060245	0.15466	0. 73000					
122	4.7114	1.4566	0.058626	0-15245	0.96000					
127	3.4602	1.0772	0.042057	0.11197	1.0900				· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
137	3.8356	1.1940	0.047728	0.12411	1.2209					
147	3.3351	1.0382	0.941509	0.10792	1.3500		<del>-</del>		· · · · · · · · · · · · · · · · · · ·	•
>4001110#	M section	AATIOS , EOI	FACOL IM CE							
AVE WITE IT										4-
	PL	PL /PR	PI /PTF	PI /PTP	X/DMAX			•		
-107	6.8376	2.1192 1.5)71	0.094711	0-22029	-1,0000 -1,0000			· · · · ·		a way .
	4.9415		0.060245	0.15666						
-112			0.058626	0.15255	<u> </u>			~ <del>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</del>		
-122	- 4a1114	1.4555								
-122 -127	3.4502	1.0772	0.043057	0-11157	-1.0000					
-122 -127 -137	3.4502	1.0772	0.043057 0.64772#	0.12411	-1.0000		- wik v v		and the second s	re entire - i e
-122 -127 -137 -147	3.4502 3.4356 3.334	1.0772 1.1940 1.9392	0.043057 0.647728 0.641500	0.12411	-1.0000 -1.0000	- · · · ·	e sales — v — e		and the second s	uni manada — / m
-122 -127 -137	3.4502	1.0772	0.043057 0.64772#	0.12/11 0/07/92 0.11067	-1.0000 -1.0003 -1.3000	·· •	. w	, , , , , , , , , , , , , , , , , , ,		
-122 -127 -137 -147 -152 -157	3.4502 3.4356 3.33 3.4201 3.4201	1.0772 1.1940 1.9392 1.9647 1.9647	0.043057 0.647728 0.041503 0.342559	0.12411	-1.0000 -1.0000					
-122 -127 -137 -147 -147 -157 -157	3.4502 3.4356 3.334 3.4201 3.4201	1.0772 1.1940 1.9392 1.2647 1.3647	U.042057 O.647728 U.C41503 O.042559 O.C42559	0.12/11 0/07/92 0.11067 0.11067	-1.0000 -1.0503 -1.0900 -1.9000					
-122 -127 -137 -147 -142 -152 -157 >40017 109	3.4502 3.4356 3.3356 3.4201 3.4201 AL PRESSUPE	1.0772 1.1940 1.9192 1.9647 1.9647	0.042057 0.047728 0.04750 0.047559 0.042559 1 MT7715 FLAP	0.12/11 0.19792 0.11067 0.11067	0000 -1-0000 -1-0000 -1-0000					
-122 -127 -137 -147 -147 -157 -157	3.4502 3.4356 3.334 3.4201 3.4201	1.0772 1.1940 1.9392 1.2647 1.3647	U.042057 O.647728 U.C41503 O.042559 O.C42559	0.12/11 0/07/92 0.11067 0.11067	-1.0000 -1.0503 -1.0900 -1.9000					
-122 -127 -137 -142 -152 -157 >400111090 -152	1.4502 3.4356 3.4351 3.4201 3.4201 AL PRESSUPE PL 3.4201 3.4201	1.0772 1.1940 1.9192 1.9647 1.9647 PATIME, FAR PL/PH 1.0647 1.0647	U.042057 U.04772R U.041700 U.042559 U.042559 U.042559 U.042559	0.12/11 0.10792 0.11067 0.11067 PI/PTP 0.11067 2.11067	X/DMAY -1.0000 -1.0000 -1.0000	-				
-122 -127 -137 -142 -152 -157 >400111090 4VD 4CPO -152 -157 >400111000	1.4502 3.4356 3.3351 3.4201 3.4201 6L PRESSUPE PL 3.4201 3.4201 3.4201	1.0772 1.1940 1.9192 1.3447 1.3647 PATION FAR PLOGAT 1.0647 1.0443	U.042057 U.C41503 U.C41503 U.042559 U.C42559 U.C42559 U.C42559 U.C42559 U.C42559 U.C42559	0.12/11 0/19/22 0.11067 0.11067 0.11067 0.11067	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000	-				
-122 -127 -137 -147 -152 -157 >40017109/ 4VD 4CPQ -157 >40017109/ 4VD 4CPQ	1.4502 3.4356 3.4354 3.4201 3.4201 AL PRESSUPE PL 3.4201 3.4201 AI ORESSUPE	1.0772 1.1940 1.9392 1.9447 1.9647 PATIMY FAN PLOGAT 1.0647 1.0647 1.0647	0.042057 0.647728 0.641503 0.042559 0.642559 1. MC7715 F1AP 0.742559 0.642559 0.642559	0.12/11 0/07/92 0.11067 0.11067 0.11067 0.11067 0.11067	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000	-				
-122 -127 -137 -142 -152 -157 >400111090 4VD 4CPO -152 -157 >400111000	1.4502 3.4356 3.4356 3.4201 3.4201 3.4201 3.4201 41 messure	1.0772 1.1940 1.9192 1.3447 1.3647 PATION FAR PLOGAT 1.0647 1.0443	U.042057 U.C41503 U.C41503 U.042559 U.C42559 U.C42559 U.C42559 U.C42559 U.C42559 U.C42559	0.12/11 0/19/22 0.11067 0.11067 0.11067 0.11067	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000	-				
-122 -127 -137 -147 -152 -157 >400 4090 -152 -157 >400 4090 400 4090 400 4090	1.4502 3.4356 3.354 3.4201 3.4201 3.4201 3.4201 3.4201 3.4201 3.4201	1.0772 1.1940 1.9392 1.3447 1.3647 PATIMY FAN PLOGAT 1.0647 1.0647 1.0647 1.0647	0.042057 0.047728 0.041503 0.042559 0.042559 0.7715 FLAP 0.742559 0.042559 0.042550 0.042550	0.12/11 0/19/22 0.11067 0.11067 0.11067 0.11067 0.11067 0.11067	X/DMAY -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-00000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-000					
-122 -127 -137 -142 -152 -157 >400171000 4VD 4CPO -152 -157 >400171000 4VD 4CPO -157 -157 >400171000	1.4502 3.4356 3.4351 3.4201 3.4201 3.4201 3.4201 3.4201 7.401 7.401 7.401 7.401 7.401 7.401	1.0772 1.1940 1.9192 1.9447 1.9647 1.9647 1.0647 1.0647 1.0647 1.0647 1.0647	0.042057 0.047728 0.041500 0.042559 0.042559 0.7715 FLAP 0.742559 0.42559 0.42559 0.7715 FLAP 0.742559 0.042550 0.042550	0.12/11 0/19792 0.11067 0.11067 0.11067 0.11067 0.11067 0.11067 0.11067	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
-122 -127 -137 -142 -152 -157 >400111098 4VD 4CPD -152 -157 >400111088 4VD 4CPD -157 -157 -167 -167 -177	1.4502 3.4356 3.4351 3.4201 3.4201 3.4201 3.4201 41 00ESSUPE PL 3.4201 7.4011	1.0772 1.1940 1.9192 1.9447 1.9647 1.9647 1.0647 1.0647 1.0647 1.0647 1.0647	0.042057 0.047728 0.047529 0.042559 0.042559 0.042559 0.042559 0.042550 0.042550 0.042550	0.12/11 0/10/22 0.11067 0.11067 0.11067 0.11067 0.11067 0.11067 0.11067	X/MAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
-122 -127 -137 -142 -152 -157 >400171000 4VD 4CPO -152 -157 >400171000 4VD 4CPO -157 -157 >400171000	1.4502 3.4356 3.4351 3.4201 3.4201 3.4201 3.4201 3.4201 7.401 7.401 7.401 7.401 7.401 7.401	1.0772 1.1940 1.9192 1.9447 1.9647 1.9647 1.0647 1.0647 1.0647 1.0647 1.0647	0.042057 0.047728 0.041500 0.042559 0.042559 0.7715 FLAP 0.742559 0.42559 0.42559 0.7715 FLAP 0.742559 0.042550 0.042550	0.12/11 0/19792 0.11067 0.11067 0.11067 0.11067 0.11067 0.11067 0.11067	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					

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4-4-19-20-2

NASA-LEWE	S PRFL [4]	MAPY DATA	07/37/76	CADDELL	PEC 10/07/77	02:26:27.927	FAC BROXL	PGT C834 RRG 3868	
SADDLE SON	AL PRESSIME	PATINS PR	IMERY PLUG						
≟ಕರ್ಮ ಕ್ಷಾಗಿತ ಕ್ರಾಪ್	The should of the state of	Tarter ( Starter + Starter	C. Mini Liman, Andr. Mar. Son	-		to attended to the same of the same of		entre de la companya	•
WD WEED	PL	PL / PD	PI /PTF	PI /PTP	x/DMAX				
32	14.602	5. 755R	9.70°25	0.42772	0.43200				
37	9,5943	2.0454	0.19701	0.27916	<b>13.53100</b>				
47	17.658	5.4635	0.19862	0.40562	J-629UJ				
.52	12.409	3.0795	0.13559	0.28505	0,72799				
>403111094	AL PRESSURE	PATIOS . FLO	ON SPLITTER I	.D.				a e	
AD HUBB	PL	PL /PO	PL /PTF	PI /PTP	X/IMAX				
42	14.324	4.4320	0.16112	0.32904	9.42200			•	
67	2.9991	3.0927	0.11236	0.22546	0.67000				
>400 ET 50N	AL PRESSIME	RATIOS . FLO	W SPEITTEP N	.p.	· -		on garage and	- • • • • •	
AL RUBD	. Pl	PL /PI)	PL/PTF	PL /PTP	X/IMAY	-	· · · · · · · · · · · · · · · · · · ·		
77	35.9%	11-134	0.40477	0.82659	0.50800				
92	19.392 3.4796	5,59 <b>0</b> 0 1,0766	9.79351 9.639141	0.61561	3,50200 2,67000				
				30413131					
>ADD T TODAK	LI PRESSURE	HATIOS . FJI	FCTEP SHREED						
AU MUNU	Pl	PL/PO	PL / PTF	PI /PTP	X/DMAX		one o como construir o de est	one of the street of the stree	
107	7,539?	2, 3324	0,084795	3.17316	J. 62400				
112	5.3617	1.6590	0. ( 0311	0.12316	0.83300				
127	5.2215	1.6156	0.058735	0.11994	J.960 <b>9</b> 0				
127	3.4946	1.0782	0.03 < 1 57	0.020045	1.0900				
137	4-9262	1.4033	9.654288	0.1103c	1.2200			and the same of th	
147	4.4958	1.3880	0.950459	0.1930	1.3500				
>40017 IN	of mession	#47105 <b>,</b> for	EVINA 191 EL						
AU Aus D	PL	PL /PG	M /PTF	PL/PTP	¥ 1000			a naturnos esta se de la compania del compania de la compania del compania de la compania del compania de la compania del compania de la compania del	
107	7.5382	2.2324	0.084795	0.17316	x/nii)# -]_(1:000		-		
112	5.3617	1.6590	9.060311	0.12316	1.0000	•	and the second and a second and a second as	and a second	
127	5,2215	1,6156	0.058735	0.11594	-1-0999				
127	34946	1.07.42	0.035157	2.000045	-1.0909		<del></del>		
137	4. 862	1.4933	3.054289	0.110-4	··1.u908				
142	4.4959	1.3440	0.050459	961 03 04	-1.0000	•	- ng nga na nga nga nga nga nga nga nga n	p makey er follow - machige regular of management of the following error of the	
152	3.4395	1.0642	0.638650	0.079210	-1.0006				
157	3.4446	1.0658	U. 31P746	0.079125	-1.0000			A COMPANY OF THE CONTRACT OF T	
SADDLT ION	AL PRESSIBLE		HETTY FLAT						
					1 5222			and the second of the second o	
AU AUBU	Pt	PI /PO	XFI /PTF	PL/PTP	XAPRIX				
157 157	3,4395 3,6446	1.0642	0.038690	0.079010 0.079125	-1.0000		a grad	and an order of the second of	
					-1-0000				
>Anni Tinna<	AI PRESSIRE	*A 3/175 , 20	DEC SHRPING	CATION					
VO MOPO	PL /	91./90	Pt /PTF	MIPTE	X/DMAX		rain ng a déngran an amana manan i	a and a	
147	1.4195	1.0+42	0.02#690	1. 279010	-1.0000				
172	3,45.65	1.0627	0.078634	0.07	-1.0000		THE R. L. LEWIS CO., LANSING, MICH.	and the second s	
SANDIT IN	M ORESTIME	ne satta	THE SHAPE I	TEATING-					
ח אועצי מע	PI	81 /80	m /c75	D4 / D7 =			* **** · ***	and the second of the second o	
199	4.0453	PI /PP 1.2579	PI /FTF	PI /PTP	N/II-AX				
	4. 3553	1.2424	0.045729 3.045166	0.697385 0.092235	-1.0000	-			
Apr									

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			-						Aug 14
NASA-LEW IS	S PPELIMI	MAPY DATA	07/07/79	CYDOETI	REC 10/07/75	02:27:2).74	FAC SYCKI	PGM C034	PPC 3049
>400171004	L_PRESSURE	PATINS PE	IMAPY PLUG		ay and an a supplication of the supplementation of the supplementati	nigo ngg - nyan aniso kanan ngg May na Milinag	and the supplication on agency manager fields as after the consequence.		
IND MORD	PL	PL/PN	PL/PTF	PL/PTP	X/DMAX				
32	15.481	5.0085	0.1838F	0.47750	0.4320)				
37	0.5301	2.6336	0. 095171	0.22126	0.53000				
47	15.636	4.8184	0.17412	0.404P1	0.62900				
52	11.016	3.40:2	0-12291	0_20575					
WOLTICOAC	AL PRESSURE	RATIOS . FLO	DV SPLITTER I	• D•					
WORD CAUM	. PL	<b>ምL/</b> ምበ	PL/PTF	PL/PTP	X/CHAX				
62	12.661	3.91192	0.14126	3.32842	J. 4220J				
61	0.9553	2.7342	0.095799	0.22970					
MOSTECOAK	IL PRESSURE	RATIOS . FLI	ON SPLITTER C	.D.					
AD AUR D	94	ም /ያብ	PL/PTF	PL/PTP	X/DMAX		a mar was read as		
77	16.2AL	11.202	0.43470	0.94110	J. 50897				
<u> 12                                   </u>	19-261	5.6360	<u>v. 20274</u>	0.47366	2,59200				- 1
<b>6</b> 2	3.4749	1.9791	0, 638993	0.090655	0.67800				
>ADDITIONA	N PRESSIME	RATIOS , F.H	FCFCP SHPOND					ranning and the second of the second of	Fia Las Mere
VO HORD	PL	91 / PC	PL /PTF	PL/PTP	X/DMAX		an aqua a mihabir ny s-n		<b>*</b>
107	7.6295	2.3494	0.094099	0.19728	0.62400				
117	5-4174	1.6711	0.369247	0.14039	0.83000				
155	5.2723	1.6278	9.058923	0.13676	3. 96399				aio-
127	3.5500	1.0906	0.039049	0.090785	1,3900				
137 142	4.5164 4.3939	1.3944 1.2639	0.05C390 0.645641	9-11715 0-1 <b>0</b> 611	1.22 <b>00</b> 1.3500	*	The second second	of energy and decomposition	* 18
>4201 F 10W	u PAFSSIPF	******							
		-						Company of the compan	•
AUBU	PI .	PL/PO	PL / PTF	PL /PTP	X/IMAY		•		
137	7.6095	2.3494	0.044899	0-19739	-1,0000		and the second second		and the second second
117	5.4124 5.2723	1.6278	0.CE1367 0.058823	0.14939	-1.0030				
127	5010	1. 7406	n, C39049	0-090785	-1.0000			<del></del>	
127	4.11.54	1.3044	0.050350	0.11715	-1.0000				
14?	4.370	1.2630	0.045641	0.43411	-1.0000		and the contract of the second of the second	· · · · · · · · · · · · · · · · · · ·	
152	3,4499	1.0651	0.034491	10. 0P94R6	-1.0000				
157	3.4409	1.0551	0.738491	J.0894P6	-1.0000				
PHULL LUNG	L POFSSIME	RATION FA	POZZLE FLAP	<del></del>			· · · · · · · · · · · · · · · · · · ·		
VA MUNIO	Pt	PI /PI	PLIPTE	PL/PTP	X/DMAY	* *	4 Marie May 10		
165	3.4499	1.0651	0. (3949)	0.049486	-1.0000				
-1 = 7	3.4499	1.9651	35226461	9.989486	-1.0000		- 1996 1 80 1000		
>47711104	I PRESSIDE	MATION . 20	DEG SHEFTIME	DCATENY	**************************************		· · · · · · · · · · · · · · · · · · ·		
פים מע מע	Pl	91/80	M / PTF	M. PTP	X/IMAX		g w e		
163	3.4479	1-0651	0. (3849)	0.009484	-1.0000				
172	3.35	1.0651	9,739491	0.005686	-1.9460				•
DAN DIT HOW	TOFS SIDE	PATINS - MA	DEG SHPCIN I	CCATION -					de el constitution qualificação de la familia de la constitution qual constitution de la
	7								
			M / PTF	PL /PTP	x / fund x				
	PL	PI / PO							
197 - 1979 -197 -157	PL 4. )759 4. )2 )7	1.2584	7.945474 3.944859	0.10577	-1.0000 -1.0000				

NA 54-L F41	IS PRELIM	IHARY DETA	37/07/79	CADRETT	PEC 10/37/79 C	2:24:31.086	FAC 9X6X1	PG" (034	RDC 1950
POTATIOGES	AL PRESSURE	PATIOS . PRI	MAPY PLUG	an and an area of the same		according comments or again representation of applications	a dang ani nagan dagan ng nga nigan da nga ngangga nagan na nagan n	-	
		m 180		24 4222					
190 WDFD 32	PL 14.706	PL /PG 4,5624	PL/PTF 3.16462	PL/PTP 0.42766	#/09## 9.432 <b>0</b> 0		•		
37	7.5965	7.3705	0.085536	0.22229	0.53000				
47	14.774	4.3146	0.155#4	0.404#2	9.6290)				
52	9.3279	3.0619	0.11942	0.28709	9.72700				- Magazine / Japan - Japan
>ADDIT ION	ML PPESSUPE	PATEOS . FLO	SM SPILLTER I	. D.					
				** *-**					
IND AUED	PL 350	PL/PA 3.5029	PL/PTF 0.12640	PL/PTP 0.32#25	¥/8 <b>₽#</b> ¥ 0.427 <b>0</b> 0		• _		
67	11.350 7.9517	2.4523	U-637497	J-229.7	3.67000				
			W SPLITTEP O			delication of the secondary of the secondary	4-04		
Second of hind	ME PARSONE	PP1191 , FE1	- W. S. L. L.	• 17e			m : *	•	
IND MOKU	PL	Pt / PO	PI /PTF	PL /PTP	X/DMAX			1	
77	36.310	11.196	0.40406	1.0497	0. GAGG				
92	18,298	5.6432	v.27363	9.52697	0.5*349				
92	3.4967	1.0784	0.034917	0-1010#	J.670 <b>J</b> J				
MITTECIA<	ÀL PRESSIPE	RATIOS , EJE	CTOR SHPOUP		a posta man		<ul> <li>a prosper op companie as per objecte referen</li> </ul>	responding to the second of the second	
DAUR GA	PL	et /en	PL /PTF	P1 /PTP	X/DMAX	* *	the management of a contract		
107	7,6315	2,3536	3.254925	0.22061	2.424-10				
112	5. 5343	1.6760	0.060474	0.15710	U. 43000		· · · · · · · · · · · · · · · · · · ·		
122	5. 2892	1.6312	0. (58858	0.15290	0.96000				
127	3.4967	1.0794	9-130412	0.10100	1.3900				
127	4.2929	1.3239	0.347771	C-12410	1.2200				
142	3.7371	1.1525	0.C41 FA6	0.10403	1.3500				
240017104	44 PRESSIPE	AATING - FR	F POPY - 144 E S				·		
						-		****	*
AUBU	PL	PI /PO	of /ble	PI /PTP	X /DMAX		•		
107	7.4315	2.3536 1.6760	0_094924 0_069474	9.22961	-1.0200				
122	5.4343	1.6312	U. 35 PBER	0.15710	1.0000				
-127	3.4767	1.0784	6.038017	0.17290	-1.J000				
-137	4.2929	1.3239	0.647771	0.12540	-1.9300				
-143	3.774	1-1525	0.041596	0.1003	-1.0070		New York Company	Andrew Color Color Color Color	
152	3.4515	1.0645	0. 338410	# .090 TPU	-1.0500				
-157	3.4515	1. 1645	1. 336417	9.959760	-1.9072		and the second of the second		
POT TICOAK	AL PEFSSIPF	241175 FF	WATTE THE	angularizar in the agreement and the state					Manager 2000 per ar 2000 february of regularity of the February of the Februar
IAL AGEU	PL	21 / P(1	1011	PL /PTP	x/n=ax				
152	3.4516	1.0645	X0.338410	0.090780	-1.0006				
-1 = 7	3.4514	1.064	C3#410	0.059780	-1.3030		•		
			DEG SHEETE TE				~~~		
No Abbu	PL	PI.790	M NALE	M 1919	X \TOMA X				
	3.453	1.3645	0.038410	02099790	-1.0000				
-147	١٠٠٠	1.064 ^e	0.038410	0-0000100	-1.0000				
-172			nër timbin ki	NEAT INN		magne mg. amarite the training admitter with		-	and the state of t
	M. HARSHAR	PARIOS . PO	DED SECTION A		•				
-172		P41105 , P0			X CONTA Y				
-iz: >anitting wowo	PL	PI / PO	M /PTF	PI /PTP	PANNAY 100 Co.1-		* *		
-iz: >antiting					*/************************************	· • ·			

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HASA-LEHIS	ovef14	IMANY NATA	37/07/79	CARRELL	PFC 19/37/75	02:28:54,642	FAC PYORE	PGP C034	R96 1951
>ADDIT TOUA	L PRESSUPE	EATIOS PRI	MARY PING.			a marketing and	Sample of the second of the se	and the state of t	**
AVD 40PD	PL	oj /pn	PL/PTF	PĮ /PTP	X/IMAX				
37	17.437	5.5201	0. 19444	0.42911	0.43200				
37	9.2371	. 44 74	9.095142	0.27084	3.53770				
47	16.794	5.1770	0.17298	7.40151	J-62900				
	11.943	3.6916	2.12391	u. 29°53	J. 72790	kerdelikkingsiste daga kara kara sa sakara kera da			application and the second
>AODITIONA	L PRESSUPE	PATIOS . FLO	W SPLITTER I	. 0.					
AVD HOPD	PL	PL/PD	PL /PTF	*L /PTP	×/P=Ax				
62	13.785	4.244	0.14199	0.22956	J.4220J				
_67	9.5161	2.9644	0. C95051	0.22951	0.47040				-
>4791110H4	L PPESSUPE	PATIOS . FLO	W SPLITTER O	.D.					
AVD WORD	•t	PL/PD	PL/PTF	~L /P1P	X/DMAX				
77	38.896	11.990	0.40062	0.42089	J.50000		r w mod namen		
M2	19,734	6,0931	0.20326	0.47178	0.50300				
97	3.4868	1.0748	0.035913	0.083355	0.67000				
SANDIT INNA	PRESSURE	RATIOS . EJE	CTOR SHPONE	* * * * *		a service of	The second of the second particle operation		with war and a second
AVD WORD	PL	PL/PN	PL /PTF	PL /PTP	Y/DMAX		,		
107	5-2363	2.5395	Q. C84855	0-19696	9-62400				
112	5, 96.36	1.9066	0.060364	0.14011	0. R 3000				
122	5.710?	1.7604	0.058820	0.13653	0.96300				
127	3.5014	1.0794	0.076068	0.083717	1.0900				
137	4.9312	1.5108	0.050482	0.11717	1-2200				
142	4.4354	1.3676	0.045695	0.10606	1.3500				
>1001110m	f weither	441195 , FPR	FACTO - \$44 FT			7			
AVI WILL D	PL	PL/PD	PL /PTF	PI /PTP	#/DMAX		ale no respectively and an		
-107	0.2303	2.5395	0.094855	9.19696	-1.4000				
-112	5. 9696	1.4966	0.960364	0.14011	-140300			• /	
-12?	5.7107	1,7604	0. 658820	0.13653	1.9900				
-127	3.5019	1.0794	0.034048	2.003717	-1.0000				
-177	4.3017	1.5108	0.059447	0.1171	-1.0000				
-147	4.4306	1.3476	0.065495	2. M. C.	-1.0000				
-15?	3.4468	1.0625	J. 025502	2.382403	-1.0000				
-157	3.4469	1.0625	0. 035502	0.092403	-1.0000				
APOLITICAS	E PRESSURE	PATINS . FAM	*17771F PEAR		erietario de protecion semantesta el cultura de sem	an anni anni anni anni anni anni anni a	or a restricted in the spin of an easy spin season particle respectively.	COLIA (PROCESSIA), MINISTERIO (PERSONAL PROCESSIA)	designations of the second of
AVD 40PD	PL	M NAG	PETT	PL /PTP	W/RMAW				
-152	3.4468	1.06.5	<b>X</b> 0.0₹5502	0.002403	-1.0000				
-1=7	3.4468	1.00.25	235502	0.082403	-1.0000				
>4001TIONA	I PRESSUPE	PATION . 20	DEC SHOWING	PCATION			n - in a seeken. Am - kini dan ami nega gapitupanggapanindag - pangga	and the second s	natural variable de la company
AVD WOED	PŁ	PI 2911	PI /PTF	PL PTP	X/BMAZ				
-167	3.4519	1.9640	0.035553	0.002522	-1.0000				
-177	3.5519	1.0540	0.025553	0.002522	-1.0000				
Sannitin's	1 64:551145	PATINS , RO	DEG SIPPUN TI	CATTON					
AVD WITE	<b>*</b>	PL /PN	PI /PTF	P1 /P36	PEDMAX				
	4.2765	1.3143	G. 04404R	0.10724	-1.2000				
-102/									

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NACO S CLOSE	9951 5	MARY DATA	97407470	CADDELL	DEC LACATES	0 02-20-24 432	5AF A	Den case	Row M
HASS-L FUIS		MARY DATA	97/37/79	CARDELL	*:t 19/0///	9 02:29:34,437	FAC BX6X1	PG4 C034	RPG 3052
ווימן דור ראכ.	IL PRESSIPE	HATTUR , PE	TATEA MINE	or setting areas where the			radional contraction of a sign and service of		
THE HEFT	PL	PI / PG	of /PTF	PI /PTP	X/PMAX				
37	16. 353	4. £448	2.16425	9.47484	0.43200				
2 ¥	4.3)19	2.557*	7. JR4953	13. 22075	J.53UJ9				
47	15.190	4.6798	9.15545	0.49256	J*+5400				
.52	13.744	3.3115	0-11009	0.2555	Q. 72709	e encomprehension plant in the late Special Co.	distribution management of the contract of the	demonstrate in Africa, in such assertion in the special contraction and	
DADDET LONG	IL PRESSURE	PATIOS , FLO	PW SPLITTER I	. D.					
AVD WORD	PL	PI, / PO	M /PTF	PI /PTP	F/DHAX				
4.2	15.350	3.79R	0.12617	0.32785	J.42200				
. 67	9,5222	2.6564	0.049235	0.22930	9.67999				er er en melyamen san mang i also man
>APPLITIONA	I PRESSUPE	RATENS , FLO	NW SPEITTER O	.n.					
AVO HOPD	.PL , ,	PL/P0	M /PTF	PI /PTP	Y/DMAX		•		
77	39.115	12.051	0.43029	1.0402	J. 50800		<del>-</del>		
P2	19,910	6.1340	9.20375	0.52949	0.54300				
<b>92</b>	3 5010	1.0786	0.335924	0.053104	U. € 700U				
SADDIT INVA	E PRESSIPE	LT . COITAS	FCTCR SHROUP	Marian Carlos Carlos			· · · · · · · · · · · · · · · · · · ·		
AVD WOPD	<b>≠</b> i	PI / PO	PI /PYF	PI /PTP	X/DMAX		, and , danger up.		
107	9.3019	Z. 557A	0.094959	0.22079	0.67400				
115	5.9995	1.8707	0.060476	2.15716	J. #3900				
122	5.7593	1.7744	0.058939	0.15317	9.96000				
127	3.5113	1-0917	C. 335071	0.093775	1.0900				
137	4.6729	1,4397	0.947821	9.12477	1.2200			a section in	
142	4.9619	1.2515	0.041569	0.19903	1.3500				
->+001110M	f waterings		PERCON INCL				····	······································	
and muso	PL .	PL/PO	PL/PTF	PL /PTP	X/DMAX	* - **			
-107	8.3019	2.5578	0.044959	0.22079	-1,000				
-112	5.9395	1.8297	0.060476	0.15716	1.0000		. 100		
-122	5.7593	1.7744	0.05#939	0.15317	-1.0000				
-127	3.5117	1.0017	0.035631	0.953325	-1.9000				
-137	436729	1.4397	0.047821	0.12/7	-1.0000				
-147	4.3749	1.2515	0.041569	0.40003	-1.0000				
-123	3.6617	1.9663	9.035418	10.092G43	-1.9000				_
-1 = 7	7. 456)	1.0648	0.0?5367	U.091910	-1-0000	-	• • • • • • • • • • • • • • • • • • • •		
NA H TENCAC	E PRESSIPE	ORVINS . FAI	N 407715 FI AP	-			, — <del>——————————————————————————————————</del>		
AVD HOPD	PŁ	PI /PI	A IPTE	PL /PTP	X/BMAX		,	<b>.</b>	
-1">	3.4610	1.0663	× 0.03541#	9.092043	-1.0600				
-157	3.4567	1.76.49	035367	0.001010	-1.3000			#	
SASSIT FORK	PRESSIPE	RATURE . 25	UEU CHANGO	PRATION					anada salama ana ataun a inaday ing bi ata
AVD HOPD	PI /	PL /PO	M /PTF	21 /010	Y/DWAX		-,		
-147	3.4610	1.9663	0.035419	0.092043	-1.0000				
-17?	1.5760	1.0648	0.025367	0.031610	-1.0000	• •			
SANOTT TOW	N PPESSIPF	RATIOS , AN	neg simmin i	NEATICH -		AND THE PROPERTY OF THE PARTY O		manya minaga ii marakkamalakkita kalifotini an'iki	
חיצים חעם	PL	PL / PO	PI /PTF	PI /PTP	HANGER			10.0	
,	4.3123	1.3286	0.044131	0.11468	-1.00				
-173/	703473								
-1937 -187	4.3123	1.3286	0-044131	0.11468	-1.0003				

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HASA-LEUIS	DEFI TH	ATAC VGAN	07/07/79	CADDETT	REC 10/37/79 02:30:34.6	547 FIC REATE	FGM F034 RDG 10	•
">voo i + tu-nv	F bec23libe	P###75 . PP	14APY PLUG		and the second s			
ጀላህ 4 <u>ሀ</u> ክላ	PL	PI <b>/</b> PD	PI /PTF	PI /PTP	X/DMAX			
32	15.898	4.9337	(.16302	1.42745	2.43200			
37	9.2419	2.5591	0.095632	0.27174	3.53000			
47	15.)78	4.6600	G. 15484	0.40376	0.62500			
52	12.658	3.3052	0.10576	0.28674	0.72700			
						· · · · · · · · · · · · · · · · · · ·		
>AUTITIONA	L PRESSURE	RATIOS . FLI	C+ SPLITTER 1.	. D.				
AVD HIPD	PL.	PL/PN	PL/PTF	PL/PTP	X/DMAX			
42	12.209	3.7906	0.12555	0.32845	0.42700			
_67	8.5421	2.6523	9. C9P129	0.22992	0.67000			
>ADDIT TONA	L PRESSUPF	RATIOS . FLO	OW SPLITTER C.	0.				
AVD WORD	PL	PL / PO	PL / PT F	PE/PTP	X/DMAX			
77	34.771	12.039	0.40000	1.0431	0.50800			
92	9.732	6.1267	G.20357	0.53027	0.58300			
92	3.4772	1.0797	U. 035P74	0.093552	u.6700ú			
			ECTUP SHPUUD		* * * * * * * * * * * * * * * * * * * *	v v sampa gapangan v mandanadan	and the same of th	
	1 PRESSURE		-1.11.6 SHALIMI					
AVD WORD	PL	PL / PTI	PL /PTF	PL /PTP	X/DMAX			
127	8.2319	2,5560	0.284928	0.22147	0.62400			
112	5.8551	1.8180	0.060407	0.15752	0.83000			
122	5.7049	1.7714	0.058858	0.15349	0.56000			
127	3.4R22	1.0912	0.635576	0.093686	1.0900			
137	4.6?37	1.4357	0-647703	0.12440	1.2200			
142	4.0230	1.2491	0.041505	0.10924	1.3500			
2420   T 1044	- BRESSIME	****** FO	RESCRIPTION INTER					
AVITAINED	PL	PL/PO	PI /PTF	PL /PTP	K/DMAX			
-10?	A.2319	2.5560	0.08492#	0-22147	-1.0000	•		
-112	7.2317 5.8551	1.6160	G. CAC407	0.15753	<b>21.</b> 0000			
				0.15249	-1.0000			
-122	2.7349	1.7714	0.054858					<del></del>
-127	4922	1.0012	9.035526	0-003686	-1.3300			
-177	4.5037	1.4357	0.047703	0.12440	-1.0099		and the property and the second section of the second section of the second section of the second section sect	
-14?	4.1230	1.2491	0.041505	0 10R24	-1.0000			
-152	3.4321	1.0657	0.035479	0.092339	-1.0000			
-157	3.4721	1.3657	U-C35409	0.052339	-1.0000			
SECULT FORM	PRESSURE	PATTOS FAI	H MINTELE FLAP		7			
AVP HOPD	րլ	P1 / PO	MIPTE	PL /PTP	X/DMAX			
-152	3.4321	1.3657	025400	0.097339	-1.0000			
-1 = 7	3.4371	1.0552	0. 324409	0.092339	-1.0000			
SANDITIONS	E BESCIPE	PATENS . 20	DEG SHALID	CATION				
AVD HORD	PI /	Pt / PO	PI /PTF	PLYPIP	X/D#AX	The Edward College College		
-147	3.4321	1.0657	0.035430	0.0 2339	-1.0000			
-172	3,771	1.0641	0.035252	0.032746	-1.0000			
Sanhitting	PRESSIPE	PATING . AN	DEG SHPEUD TE	CAT LITT				
AVD WOPD		m 100	D 4875		x /pma		and a residue of the second of	
	PL 4 3333	<b>PI /</b> PO	P1 / PTF	PI /PTP				
-107 197	4.2332 4.1982	1.3144	9.042674 9.042213	0.11389 0.11295	-1.0000 -1.0000	-		

and the second of the second

	*854-15875	PRF1.14	MARY DITA	97/97/ <del>79</del>	CAPOFII	PEC 10/07/75 02:31:00.790	for great	PGM C034 PDG 105	4
J 	/89311 (00:2	I boEZZIBE	PATIOS , PP	MELA MING	manage or	and the second of the second o		and the second of the second o	· · · · e
	AUD HOPG	PĹ	PI /P7	PLIFTE	PI /PTP	7/D4A1			
	:2	17.755	5.5168	0.18483	0.42858	0-43200			
	37	2.1619	7.846.4	0.095367	0.22113	0.53000			
-	47	15. 935	5.2217	0.17494	9.40566	0.67500			
	52	11.995	2.6900	0.12322	9.20595				هيو. د
_	APOI TECCAC	L PPESSUPE	PATIOS . FLO	OW SPLITTER I	.0.				
	AVP WOFD	PL	PL/P7	PI /OTF	PL /PTP	X/D48X			
	62	13.651	4.2416	9.14211	0.32952	9.42799			
_		9.5312	2.9414	0. (95215	0.23034	24 6 7003			
	>A77] T [ (PM	L PPFSSIPE	RATIOS . FLE	W SPLITTEP C	.D.		·#	and the same of th	
	AVO WOPD	PL	PL / P1	PL /PTF	PL /PTP	至 57700 五 发			
	77	39.447	11.745	3.49622	0.92805	0.50000			
	e 2	19,579	6.0936	0.2027	0.47262	0.58309			
-	92	3.466?	1.0779	0.076087	0.08266R	0. ¢ 7000			
								and the contract of the contra	
	>400IT fore	1 PRESSIDE	PATERS . FUE	CTOP SHPOHO					
•	AVP MORT	Pl	PL /PO	PI / PTF	PL /PTP	T/DMAT	* * * * * * * * * * * * * * * * * * * *	e e e e	
	107	P.1554	2.5340	0.054896	0.15484	0,62490			
	117	5.4-)43	1.7)49	3.C694F4	0.14022	J.#3009			
	127	5.6456	1.7551	J. C5F801	0.13635	0.96000			
	127	2.481?	1.0317	0.076278	0.084031	1.0909		The state of the s	
	137	4.8528	1.5979	0.950517	0-11714	1.2200			
	147	4.3973	1.3663	0.045775	0.10615	1.3500			
-	Crootston	L PRESCURE	ALTION , FEE	-					
	'AVIT WIFE		<b>5</b> 40a						
	-197	PL 8.1556	PL /PI)	PI /PTF	PL /PTP	Y/DMAY	•		
			2.5346	7.574896	0.19486	-1.9609	in a company	a with the control of	
	-112	5.8)89	1.4343	9.365469	0.14022	7.0000			
-	127	5.4436	! • <u>7551</u>	2- 558901	0.13635	-1.090			
	-127	4112	1.0017	0.03/23#	0.084138	-1.0000			
	-137	4.3578	1.5379	0.056517	0.11114	-1.0000		was an an analysis of the same of	
	-142	4.3773	1.3663	7-14-775	13.615	-1.0000			
	-15?	3.4311	1,0661	0.035717	0.082877	-1.0000		and the second s	
	-157	3.4311	1.3641	0-03-717	0.08Z#22	-1.0000			
	>ton [ T Justa	( PRESSIPE	PATINE	KETTIS FLAD		All Marie and Sign colons, specifying and Marie Administration of the second specifying and the second specific and the second specifi			
	AVD MORD	PL	PL/P7	A 157F	PL /PTP	K/DMAX	, w .	and the second of the second o	
	-152	3-4311	1.0661	2.335717	0.007#22	-1.0000			
	-167	3.4311	1. 35:3	20-53-212	J.382°22	-1.0000			
	>:001110MA	6 00544118E	21116 . 20	THE SHEET TO	PATION .				
-	AVD WOPG	PL /	PL / PO	PI /PTF	M /PTP	X/DMAX	· · · · · · · · · · · · · · · · · · ·	•	
	-167	3.4334	1.9661	7.035717	03082877	-1.0000			
J	-177	3.7711	1. 3561	0.575717	0.3 4.77	-1.0000			
-	= >2791TING	ODE SSIME	RATING . "AG	HEG CHECKIN I	TEATION				
_	AVA USE 7	PI	Pt /P1	M /PTF	PL/PTP	X/Dux	•		
	-195	4.1971	1.3775	7.543630	9.10119	-1.0000			
					75 4 7				
	107	4.1773	1.2361	12.347777	9.14:22	-1.0000			

AVO HOPO	PE	FI / P7	PI/PTF	PL /PTP	x/DMAx		
77	14.836	4.4 155	9.16436	J.42636	0.43200		
37	7.7173	2.3765	70. 385457	0.271+5	3.53/03		
47	14.371	4.3563	9.15527	0.43292	0.62903		
52	11.111	3-1100	D-11CES	9.25745	0.72700		
>#00171004<	IAL PRESSURE	PATINS . FLO	DW SPLITTER I	. D.			e en
AVD WOPD	PL	PL/PO	PI /PTF	PL /PTP	X/DMAX		
42	11.400	2.54?1	0-12630	0.32761	0.42200		· · · · · · · · · · · · · · · · · · ·
57	7, 3795	2.4759	0.048350	0.22927	0.67000		
>40017104	IAL PRESSURE	RATIOS . FLE	N SPLITTER É	.n.		•	
AVD HORD	PL	PL / P1	PI /PTF	PI /PTP	X/DMAF		
77	36.144	11.230	0.47042	1-0-87	0.50000		to the control of the
92	19.351	5,7316	0.23337	0.52734	9,58300		
47	3.4692	1.0775	0.038421	0.059440	0.67000		
>ADDITION	IAL PPESSIPE	PATINS , FJ	FCTEP SHPPUN			<u>.</u>	The second secon
EN: HUND	PL	PI / PG	PI /PTF	PL /P TP	X/PHAX		en en en en remann plant de Monder e l'amb
10/	7.6733	2,3740	0.095009	0.22050	0.62400		
117	5.4559	1.6951	0.056444	0.15475	0.03603		
122	5.3158	1.6516	0.058891	0.15276	0.96900		
127	3.4731	1.0791	0.638477	0.099804	1.0900	*	and the transfer of the production was play and company of the production of the pro
		200.72					
	4-3144	1.3635	0.547767	n 1 2398	1.77:30		
137 142	4.3144 3.7535 WL PRESSURE	1.3475 1.1642	0.647757 0.041594	0.1239f 0.10776	1.2200		
142 142 140017100	3.7535 <del>IDE - PRESSUME</del> - PE	1 - 1642 ******** FRI PL /PD	0.041594 15000 Jules Pl /PTF	0.107P6	1.3500 X/0MAX	<del></del>	
137 142 +400-17-100 200 unen -137	3.7535 INL - PRESSURE PL 7.6733	1.1642 ******* FRI PE /PD 2.3140	0.041594 NEARCH   MILES PI / PTF 0.045009	0.107/6 PL/PTP 0.22/050	1.3500 X/044X -1.000(i.e.	· · · · · · · · · · · · · · · · · · ·	
127 142 340017 fm 120 unpn -127 -117	3.7535 <del>IDE - PRESSUME</del> - PE	1 - 1642 ******** FRI PL /PD	0.041594 PI/PTF 0.085009 0.060444	0.107P6	1.3500 X/0MAX		
127 142 340011100 200 unpn -137 -117 -122	3.7535 INL - PRESSURE PL 7.6733	1.1642 ******* FRI PE /PD 2.3140	0.041594 NEARCH   MILES PI / PTF 0.045009	0.10776 PL/PTP 0.22750 0.15678 0.15276	1.3500 X/044X -1.000(i.e.		
137 142 140 unpn -137 -112 -122 -127	3.7575 PL 7.6732 5.4559 5.3158 3.4731	1.1662 M /Pn 2.3940 1.69516 1.7751	0.041596 PERROW INTE- PL/PTF 0.085009 0.060444 0.05PR01 0.638477	0.10776 PL/PTP 0.22050 0.15678 0.15276 0.055894	1.3500 X/044X -1.9500 -2.0900	7	
127 142 340011100 200 unpn -137 -117 -122	3.7515 PL PRESSURE 7.6732 5.4550 5.3158 3.6731 632144	1.1642 ************************************	0.041594 PERFORM ENTER PLANTE 0.085009 0.060444 0.058801	0.10776 PL/PTP 0.22750 0.15678 0.15276	1.35-00 X/04AX -1.3000 -X.0000 -1.0000	7	
137 142 140 unpn -137 -112 -122 -127	3.7575 PL 7.6732 5.4559 5.3158 3.4731	1.1662 M /Pn 2.3940 1.69516 1.7751	0.041596 PERROW INTE- PL/PTF 0.085009 0.060444 0.05PR01 0.63P477	0.10776 PL/PTP 0.22050 0.15678 0.15276 0.055894	X/044X -1.3000 -2.0000 -1.0000		
127 142 142 140 unen 112 112 127 127 127	3.7515 PL PRESSURE 7.6732 5.4550 5.3158 3.6731 632144	1.1662 m/mn 2.3440 1.6951 1.0516 1.3495	0.041596 PI/PTF 0.085009 0.060446 0.058901 0.047797	0.10776 PL/PTP 0.22050 0.15678 0.15276 0.05580 0.12748 0.16784	1.35-00 X/04AN -1.9900 -2.0900 -1.9900 -1.9900 -1.9900		
137 142 140 140 1110 1110 1110 1127 127 127 127 127	3.7515  PL PACESUPE  PL 7.6733 5.4559 5.2158 3.4731 433,144 3.7345	1.1662 PATIONS FOR PATION FOR 2.3940 1.6951 1.69516 1.3751 1.3495 1.1662	0.041594 PI /PTF 0.085009 0.060444 0.058801 0.047797 0.04759	0.10776 0.22050 0.15678 0.15275 0.055897 0.12746	1.2500 x/044x -1.3500 -1.0000 -1.0000 -1.0000		
137 142 142 149 149 117 117 117 127 127 127 147 1167 1167 1167	3.7515  ML PACESUPE  PL 7.6733 5.4559 5.2158 3.4731 4.317945 3.4233 3.4280	1.1662 M /mn 2.3440 1.6951 1.05516 1.3495 1.1462 1.3635 1.9651	0.041594 PI /PTF 0.085009 0.080444 0.058801 0.047747 0.047747 0.047747 0.047747	0.10776 PL/PTP 0.22050 0.15678 0.15276 0.05890 0.12348 0.40786 0.058364 0.05850P	1.2500 X/044X -1.3500 -1.0900 -1.9300 -1.0000 -1.0000 -1.0900		
137 142 142 149 149 117 117 117 127 127 127 147 1167 1167 1167	3.7515  ML PACESUPE  PL 7.6733 5.4559 5.2158 3.4731 4.317945 3.4233 3.4280	1.1662 M /mn 2.3440 1.6951 1.05516 1.3495 1.1462 1.3635 1.9651	0.041594 PI /PTF 0.085009 0.060444 0.058801 0.047797 0.047597 0.047597 0.047597 0.047597	0.10776 PL/PTP 0.22050 0.15678 0.15276 0.05890 0.12348 0.40786 0.058364 0.05850P	1.2500 X/044X -1.3500 -1.0900 -1.9300 -1.0000 -1.0000 -1.0900		
137 142 149 149 117 117 127 127 137 147 169 169 169	3.7515  PL	1.1662 M /PO 2.3440 1.6951 1.6516 1.3495 1.1462 1.1435 1.9651	0.041594  PI /PTF 0.085009 0.060444 0.058801 0.04779 0.04779 0.041584 0.537522 0.037577	0.107P6  P1/PTP 0.22050 0.1567P 0.15276 0.055PP 0.1234P 0.167PA 0.058364 0.05850P	1.2500 X/04AX -1.9500 -1.9500 -1.9500 -1.9000 -1.9000 -1.0000 -1.0000		
137 142 142 142 103 113 113 113 113 113 113 114 115 115 115 115 115 115 115 115 115	3.7515  PL 7.6732 5.4559 5.2158 3.4731 63144 3.7795 3.4237 3.4280	1.1662 M /PH 2.3440 1.6951 1.0516 1.3495 1.1662 1.3435 1.3651 PATINS , FAR	0.041594 PI /PTF 0.085009 0.060444 92.058801 0.047707 0.041584 0.037672 0.037777	0.107P6  PL/PTP 0.22050 0.1567P 0.15276 0.055PP 0.1224P 0.107PA 0.058364 0.05850P	X/DMAX -1.3500 -X.0900 -1.9500 -1.9500 -1.0000 -1.0900 -1.0900		
137 142 142 142 142 1137 112 127 127 127 127 142 152 157 240 4000 440 4000 152 157	3.7515  PL 7.6733 5.4559 5.2158 3.4731 6.3144 3.7795 3.4237 3.4280  PI 3.4237 3.4270 3.4290	1.1662  M /PN 2.3440 1.6951 1.6951 1.3495 1.1662 1.3635 1.9651  PATTOS, FAR M /PN 1.9635 1.9651	0.041594  PI /PTF 0.085009 0.060444 0.058801 0.04779 0.04779 0.041584 0.537522 0.037577	P1/PTP 0.22050 0.15678 0.15276 0.05580 0.12248 0.10784 0.058364 0.05850P	1.3500 X/DMAX -1.3000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
137 142 142 142 142 1137 112 127 127 127 127 142 152 157 240 4000 440 4000 152 157	3.7515  PL 7.6733 5.4559 5.2158 3.4731 6.3144 3.7795 3.4237 3.4280  PI 3.4237 3.4270 3.4290	1.1662  M/PO 2.3940 1.6951 1.69516 1.3791 1.3495 1.1462 1.3435 1.9651  PATINS , FAR M/PO 1.9635 1.9651	0.041594 PI /PTF 0.085009 0.060444 0.058801 0.041584 0.037677 0.041584 0.037677 0.037677	0.10776  P1/PTP 0.22050 0.15678 0.15276 0.055804 0.1276 0.1276 0.1276 0.058364 0.05850P	1.3500 X/04AX -1.3500 -1.0900 -1.9300 -1.9000 -1.9000 -1.0000 -1.0000		
137 142 142 142 113 113 113 113 113 113 114 115 115 115 115 115 115 115 115 115	3.7515  PL PRESSURE  PL 7.6733 5.4559 5.2158 3.4731 43.17945 3.4233 3.4283 3.4283 3.4283 3.4283 91 3.4273 3.4280	1.1662  PI /PN 2.3440 1.6951 1.69516 1.3791 1.3495 1.3495 1.9651  PATINS FAN PI /PN 1.9635 1.9651  PATINS - FAN PI /PN 1.9635 1.9659	0.041594  PI /PTF 0.085009 0.060444 0.059801 0.638477 0.047797 0.047797 0.741584 0.037577  MOZZLE FLAP 1,37922 0.037577  OFG CHOMO TO	0.10776  PL/PTP 0.22050 0.15678 0.15276 0.05580 0.1278 0.10784 0.05650P  Pl/PTP 0.058364 0.09850P	1.3500 #/0948 -1.3500 -1.0900 -1.9300 -1.9300 -1.9000 -1.0900 -1.0900 #/DMAX -1.0300		
137 142 142 142 112 112 112 112 1137 1147 1147 1147 1167 1167 1167 1167 116	3.7515  PL PRESSIDE  PL 7.6733 5.4559 5.2158 3.4731 4.3.7795 3.4233 3.4283 141 PRESSIPE  PL PRESSIPE  PL	1.1662  M/PO 2.3940 1.6951 1.69516 1.3791 1.3495 1.1462 1.3435 1.9651  PATINS , FAR M/PO 1.9635 1.9651	0.041594 PI /PTF 0.085009 0.060444 0.058801 0.041584 0.04779 0.041584 0.037577 N MOTTLE FLAP 1/87F 0.137922 0.037577	0.10776  P1/PTP 0.22050 0.15678 0.15276 0.055804 0.1276 0.1276 0.1276 0.058364 0.05850P	1.3500 X/04AX -1.3500 -1.0900 -1.9300 -1.9000 -1.9000 -1.0000 -1.0000		
127 142 142 142 103 112 112 112 112 112 1137 1142 1157 1157 1157 1157 1157 1157 1157 115	3.7515  PL PRESSURE  PL 7.6733 5.4559 5.2158 3.4731 43.17945 3.4233 3.4283 144 9RESSUPE  PL 3.4299  PL 3.4299	1.1662  M /PO 2.3940 1.6951 1.69516 1.3495 1.3495 1.3495 1.3651  PATIOS , FAR M /PO 1.9635 1.9651  PATIOS , 20  PL/PO 1.9651 1.0651	0.041594  PI /PTF 0.085009 0.080444 0.059801 0.047797 0.041594 0.037522 0.037577  N NG77LE FLAP 1,037577  DFG SHORMO TI	0.10776  PL/PTP 0.22050 0.15678 0.15276 0.055804 0.15276 0.056364 0.05650P  PI/PTP 0.058364 0.09850P  PL/PTP 0.058364 0.09850P	1.2500 X/04AX -1.9500 -1.9500 -1.9500 -1.9500 -1.9500 -1.9500 X/DMAX -1.9500 -1.9500 -1.9500		
137 142  140  140  140  170  117  117  117  127  147  147  147  157  AND SEPT FOR A	3.7515  PL 7.6732 5.4559 5.2158 3.4731 63.144 3.7735 3.4231 3.4281 144 PRESSUPE PL 3.4231 3.4280 PL 3.4290 PL 3.4290 PL 3.4290	1.1662  M /PO 2.3440 1.6951 1.6951 1.3495 1.1462 1.3495 1.1462 1.3495 1.9651  PATIOS , FAR PI /PO 1.9635 1.9651 PATIOS , 80	0.041594  PI /PTF 0.085009 0.080444 0.059801 0.638477 0.041584 0.537522 0.037577  N NG77LE FLAP 1,077677  PI /PTF 0.037677  PI /PTF 0.037677  PI /PTF 0.037677  PI /PTF 0.037677  PI /PTF 0.037677	0.10776  PL/PTP 0.22050 0.15678 0.15276 0.05580 0.12748 0.058364 0.05850P  PL/PTP 0.058364 0.09850P  PL/PTP 0.05850A	X/04AX -1.9500 -1.9500 -1.9500 -1.9500 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000		
137 142 142 149 1117 1117 1127 1127 1127 1147 1147 1147	3.7515  PL PRESSURE  PL 7.6733 5.4559 5.2158 3.4731 43.17945 3.4233 3.4283 144 9RESSUPE  PL 3.4299  PL 3.4299	1.1662  M /PO 2.3940 1.6951 1.69516 1.3495 1.3495 1.3495 1.3651  PATIOS , FAR M /PO 1.9635 1.9651  PATIOS , 20  PL/PO 1.9651 1.0651	0.041594  PI /PTF 0.085009 0.060444 0.058801 0.047767 0.047767 0.047522 0.037677  MOZZIE FLAP 1.077677 0.127922 0.037677  OFG FLOTED II	0.10776  PL/PTP 0.22050 0.15678 0.15276 0.055804 0.15276 0.056364 0.05650P  PI/PTP 0.058364 0.09850P  PL/PTP 0.058364 0.09850P	1.2500 X/04AX -1.9500 -1.9500 -1.9500 -1.9500 -1.9500 -1.9500 X/DMAX -1.9500 -1.9500 -1.9500		

FAC REEKI

MACS-1 EMIS PRELIMINARY DATA 07/07/79 CADDESS PEC 10/07/79 02:32:13.435

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VASA-LEWIS	PRELIM	MARY DATA	07/07/79	CAMPELL	REC 10/01/19	02:33:30.986	FAC BYOKE	PGM C334 PMG 1856
SEGNET ENNA	PPESSURE	PATINGPP	IMARY PLUG					
						annesty aggress attenues to determine community and y are the - y		And the second to the second second second to the second s
AD AUBU	PL	PL / PO	PL /PTF	PL /PTP	X/DMAX			
32	16.376	5.0363	0.19304	0.42781	3.43700			
37	M.4517	2.6104	0.094873	0.22175	0.53000			•
47 52	15.496 10.947	4.7431 3.3912	0.17384 0.12288	3.436°0 3.29722	0.62900			
76,						-		
NOT TERRA	L PRESSURF	PATIOS . FLO	DW SPLITTEP I	. D.			•	
VO HORO	Pl	PLZPO	P1 /PTF	PI /PTP	Y /OMAX			
ęś	17.527	3.8441	3.14162	0.32667	0.42203			
67	<u> </u>	2.7378	0.098410	7.23091	3.67000	water special control of the second s		Additional and the group Additional and States and Stat
APOLTICOA	L PRESSURE	MATINS . FLI	W SPLITTER O	.0.				
VO WOFE	PL	PL /PD	PL/PTF	PI /PTP	X/DMAX		<u>.</u>	
77	35.714	11.931	0.40091	0.93704	3.50800		<del>-</del> -	•
<b>#2</b>	19.110	5,5935	0.20729	0,47514	J.58300			
92	3.448)	1.9773	0. (34154	0.091515	0.67000			
ANDST ECON	PRESSUPE	RATIOS , FJI	FOTOM SHRITING	# 86 + 1		www.w.w.x.x	was desired a stronger of the second	i en da gario de grando de la composición dela composición de la composición de la composición dela composición dela composición dela composición de la composición dela
vn พกสภ	PL	PL/PO	PL/PTF	PLIPTO	X/IMAX	v ·		- MARINE NAME AND ADDRESS OF THE PARTY NAME AND ADDRESS OF THE PAR
107	7.5664	2.3370	0.034735	0.19#52	0.62400			
112	5, 34 33	1.6517	0.066392	0.14115	0.#3000			
122	5.2349	1.6169	0.355763	0.13735	3.96003			
127	3.4933	1.0789	0.036213	0.091646	1-0900	,		
137	4.4741	1.3919	0.050223	0-11739	1.2200			
142	4.3497	1.2505	9.745449	0.19622	1.3590			
ANDITICEAC	PRESSURE	341105 <b>, 5</b> 01	ERCOY IN FT					
AU MUBU	Pŧ	PL/PO ""	P) / PTF	PI /PTP	X/IMAX		Lagrance of the contract of th	· · · · · · · · · · · · · · · · · ·
107	7.5664	2. 33 70	0. 384935	0-19852	-1 0000			
112	5.383)	1.6617	0.050392	0.14115	1.0000		and the second control of	
172	4.2158	1.6169	9.958743	0.13735	-1.0000			
1 77	4730	1.0789	0. 035210	0.091646	-1.0000			
137	4.3641	1.3410	0.050223	0.11/730	-1.0300			
142	4.367	1.2505	9.94544P	3/10622	-1-0000			
157	3,4489	1.0650	0.638765	0.09(464	-1.0000			
147	3.4483	1.7650	0.338705	0.090464	-1-4000			
APOST TOPIA	PRESSUPE	PATING FAI	1 472715 FLAD	,	and the following market extension			
VO ԿՈՒԴ	PL	21 / 100	PL/PTF	P[ /PTP	Y/IMAX		w , compression was	and a
1=>	3.4480	1.0450	0. 038705	0.090464	-1.0000			
57	3.94A}	1. 1559	DOSESSE	3.890464	-1.0000		. Age. a genta referèn	5-97
AITT TETA	PESSIPE	8 8 7 MS . 30	ors since	TCATION				
תחמע מע	PL /	PL / PS	M /PTF	AL PETP	X/DMAX		. He was a constitution of	mander of the second of the se
167	1.4493	1.0650	0.038755	02090464	-1-0000			
172	3.5630	1.0634	0.13#64#	1.000333	-1.0000		a war a same war and a same of	
					******			
SANSIT ION	L unterior	RATING . TAG	"ዕደດ" የነቀስትነኝ ች	nratine ~				
אישניאו מע	PI	PE / PO	of /off	PL/PTP	XAMILX	1 - 46	P1 18	· ·
102	4.1187	1.2721	3. 344 234	0.10806	-1.0760			
197	4. 1627	1.2521	5. 345534	3.11636	-1.0000	***		•
		THOUST PAPAR						

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MASS-LEKT	S PORT IN	IMARY DATE	97/97/79	CADDELL	REF 13/37/79 32:35:23.246 FAC 9X6X1 PGM C034 PNG 1057
SAUDITIONS.	AL PRESSION	PATTIS PR	IMARY PLUG		
AVD HOED	Pt.	Pt /PC	al lost	PL/PTP	X/DMAX
32	19.779	5.7897	1. 29540	2.42721	J. 43200
37	7.0730	2.0823	3-1 )792	0.22397	3.53000
47	17.654	5.4437	0.19659	0.40172	9-62503
52	12.536	3.8653	9.13985	0.28519	9.12100
NOT TECOA	AL PRESSURE	RATIOS . FLE	ON SPLITTEP I	i - D -	en e
AVD WORD	PL	PL/PN	PL/PTF	PL /PTP	x/max
67	14.497	4.4642	0.16156	0.32946	0.42200
<u> </u>	11,194	3.1055	9.11245	0.22041	U-67000
>APPLITIONA	AL PRESSUPE	RATIOS . FLE	ON SPLITTER (	*• D•	a a company of the co
AVD HORD	. Pt .	P[ / P7]	PL/PTF	PL/PTP	X/OMAX
77	35.959	11.785	0.49114	0.81804	0.50900
	19-229	5.6191	0.27335	0.41469	0.58300
97	3.4995	1.0757	0.02 M92A	0.079385	2.67400
PARTITIONAL	LL PRESSIRE	PATIOS . FJ			
AVD WOPD	PI	PL/PT	PI /PTF	PL/PTP	x/OMAX
107	7-6163	2.3478	0-084465	0.17327	0.62490
112	5-4131	1.6686	0.0603P7	0.12315	0.43300
122	5.2678	1.4239	0.058767	0.11554	0.96060
127	3.4995	1.9798	0.635949	0.979613	1.7500
137	4. 8822.	1.5050	0.054464	0.11107	1.2200
1-:	4.5315	1.3969	0.050553	0.10309	1.3500
~>+00 1 ± 104	ri-naeceme	<del>-243195</del>	research tofet		
THE HOPE	i Pi	Pt /PO	PL/PTF	PL /PTP	X/OHAV
-107	7.6163	2.3478	0.084965	0-17327	-1,0000
-112	5.4131	1.4686	n. 060397	0.12315	1.0000
-155	5.2679	1.6239	3.050767	0.11984	/ -1.Q020
-127	3.4995	1.3728	0.339049	0.079613	-1.0000
-177	e-6455	1.5050	0.C54464	0.13107	-1.9000
-142	4.575	1.3969	0.050553	9/10309	-1.0000
-152	3. 4494	1.0633	Q. C38491	0.078473	-1.0009
-157	1,4494	1.0633	0.738491	7.078473	-1.09%
Sent Trons	IL ORFSSIME	PATING FAI	HAZZIE FIAT		
AVD HOPD	Pf	PL/PII	JA INTE	PL /PTP	X/DMAY
-157	3. 4+94	1.3633	0.0386RI	0.078473	-1.0000
-157	3.4494	1.0433	USPERI	0.078473	-1.0030
>407111014	H PRESSIPE	*ATUK . 20	DEC SIMPLE	TCATION	
AVG UNPT	PL /	PL/PO	PI /PTF	CI IPTP	X/DNAX
-167	3.455	1. 2449	2.034537	0.0785R7	
-172	1.5004	1.0633	0.038481	0.074673	-1.0000
אייחן דדריר אכ	P. D. S. C. LOL	P+1175 . 90	NEG SIROUN I	DEATION -	
	O)	24 / 903	PI /PTF	PI /PTP	TANKE TO THE TANK OF THE PARTY
AVD HOPD					
-192	4.1333	1.2734	7.046382	0.093974	-1.0010

>4D91¥ Eu•	AL PRESSURF	BIALUZ FÜÜS	IANDA BERR			T - 1			
AVD WORD	PL	PL/PN	PL/PTF .	PL/PTP	X/OMAX				
32	13.255	4.1172	0.16420	0.47659	J. 43200				
37	6. 3753	2.1449	0.085540	0.22224	0.53000				
47	12.559	3.9012	0.15550	0.49422	J.62900				
52	9-0322	2.2356	0.11169	0.25070	J. 72700				
>ADDITION		RATIOS . FLO	CW SPLITTER I.	. D.					
AVC MUSD		PL/PN	PL/PTF	PL /PTP	x/DMAX				
	<b>PL</b> 13.103	3. 1562	0.12627	0.32906	9-42290				
62 67	7.1303	2.2148	0.000331	0-22945	0.67900				
>40011100			DW SPLITTER P.						
AVD WORD					X/DMAX				
	PL 32 531	PL / PG	PL/PTF	PL /PTP				g Art and the control of	
77	32.521	1-) - 1 92	9.40288	1.0467	0.50000				
_22	16.615	5.0990	0,20336	0.52032	9-58300				
<b>د</b> ۲	3.4749	i.0794	0.043049	0.11184	0.67900				
>49911106	ML PRESSIMF	RATIOS . FJ	FOTOR SHROUD		and the second s		man and the second of the seco		
AVD MOPO	PI.	PL/PO	M / PT F	PL/PTP	X/DMAX	* * ***	and the state of the second of the second		~ .
107	6.9500	2.1278	0.054859	0.22046	0.62400				
112	4,9773	1.5150	0.069423	0.15697	0.83000				
122	4,7371	1.4714	9.658683	0-15746	U-96000				
	3.4699	1.0778	0. 642994	0.11148	1.0900				
127									
127 137		1.1961	0.947793	0.12393	1.2200				
127 137 142	3.9506 3.3497	1.1961	0.947792	0.12393	1.3500			and the second s	
137	3.9506 3.3497		3.041476			<del>-</del>			
137 142 142	3.9506 3.3497	1.0495	3.041476 ************************************	0.10781	1.3500				
137 142 340017 (m)	3.9506 3.3497 ML PRESSURE	1.0495 #41195 , FEI	0.041476 FL/PYF	0.10781 PL/PTP	1.3500 x/0MAX				
137 142 >40017100 AVIT VIDEO -107	3.9506 3.3497 ML PRESSURE PI 6.4510	1.0495 PATES - FEE PL/PD 2.1278	9.041476 MERGRY 4MLET PL/PYF 9.044858	0.10781 PL/PTP 0.22046	1.3500 x/0MAX				·
137 142 140017400 AVID MIRES -107 -117	3.9506 3.3497 ML PRESSURE PI 6.8530 4.9773	1.0495 PATION . 664 PL/PN 2.1278 1.5159	0.041496 MERGRY 4NLTY PL/PYF 0.044858 0.060420	0.10781 PL/PTP 0.22046 0.15697	1.3500 X/DMAX -1.9070 -3.0330				
137 142 14001×100 AVIT-UPRIT -107 -112 -122	3.9506 3.3497 ML PRESSUAF PI 6.8530 4.9773 4.7771	1.0495 PATENT CO PL/PN 2.1270 1.5159 1.4714	0.041496 MEAGEN - IM, ET PL/PYF 0.044858 0.060470 0.058683	0.10781 PL/PTP 0.22046 0.15697 0.15246	1.3500 X/DMAX -1.0970 -1.0300 -1.0920				
137 142 140017400 AVIT HIPRO -107 -112 -122 -127	3,9506 3,3497 ML PACSSUAF PI 6,4510 4,9773 4,7773 4,7773	1.0495 P41195 FG4 PL/Pn 2.1278 1.5159 1.4714 1.0778	0.041496 MEROPE - 4NE FT PL/PYF 0.04615R 0.060470 0.060470 0.062986	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11168	x/DMAX -1-9676 -20300 -1-9690 -1-9690				
137 142 	3.9506 3.3497 ML PACSEURE PI 6.4570 4.9773 4.7371 4699 3.746	1.0495 PATION . FEE PL /PR 2.1278 1.5159 1.4714 1.0778 1.1961	0.041496  PL/PYF 9.094858 0.060420 0.059699 0.047986 0.047702	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11168 2.12393	x/DMAX -1.9010 -1.0010 -1.0010 -1.0010				
137 142 140013400 AVIT HIPRIT -107 -112 -127 -127 -147	3.9506 3.3497 ML PACSSUAF P1 6.8530 4.9773 4.7371 4699 3.5636 1.347	1.0495 PATENT - FEE PL/PH 2.1278 1.5159 1.4714 1.0778 1.1961 1.2405	0.061496 PL/PYF 0.094858 0.060470 0.056492 0.047702 0.047702 0.047702	0.10781 PL/PTP 0.22046 0.15467 0.11168 7.12383 7.12383	1.3500 X/DMAX -1.0970 -1.0070 -1.0000 -1.0000				
137 142 AVIT LIPE II -117 -127 -127 -137 -147 -152	3.9506 3.3497 ML PACSSUAF P1 6.4530 4.9773 4.7371 4699 3.340 3.4299	1.0495 P41195 F64 P4 /Pn 2.1270 1.5159 1.4714 1.0778 1.1961 1.2495 1.0654	0.041496  PL/PYF 0.094858 0.050470 0.050697 0.047702 0.047702 0.042489	0.10781 PL/PTP 0.22046 0.15647 0.15246 0.11168 2.12363 2.14781 7.11039	x/DMAX -1.9676 -10.00 -1.0070 -1.0070 -1.0000 -1.0000				
137 142 ••••••••••••••••••••••••••••••••••••	3.9506 3.3497 ML PRESSURE PI 6.8530 4.9773 4.7371 4699 3.3436 1.347 3.4299	1.0495 PATENT - FEE PL /PR 2.1278 1.5159 1.4714 1.0778 1.1961 1.9495 1.0654 1.0654	0.061496  PL/PYF 0.086858 0.460420 0.057420 0.047486 0.047742 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11148 7.12393 7.1781 7.11039 0.11039	1.3500 X/DMAX -1.0970 -1.0070 -1.0000 -1.0000				
137 142 ••••••••••••••••••••••••••••••••••••	3.9506 3.3497 ML PRESSURE PI 6.8530 4.9773 4.7371 4699 3.3436 1.347 3.4299	1.0495 PATENT - FEE PL /PR 2.1278 1.5159 1.4714 1.0778 1.1961 1.9495 1.0654 1.0654	0.041496  PL/PYF 0.094858 0.050470 0.050697 0.047702 0.047702 0.042489	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11148 7.12393 7.1781 7.11039 0.11039	x/DMAX -1.9676 -10.00 -1.0070 -1.0070 -1.0000 -1.0000				
137 142 ••••••••••••••••••••••••••••••••••••	3.9506 3.3497 ML PRESSURE PI 6.8530 4.9773 4.7371 4699 3.3436 1.347 3.4299	1.0495 PATENT - FEE PL /PR 2.1278 1.5159 1.4714 1.0778 1.1961 1.9495 1.0654 1.0654	0.061496  PL/PYF 0.086858 0.460420 0.057420 0.047486 0.047742 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11148 7.12393 7.1781 7.11039 0.11039	x/DMAX -1.9676 -10.00 -1.0070 -1.0070 -1.0000 -1.0000				
137 142 AVIT MPRII -107 -117 -127 -127 -147 -149 -152 -157 >ADDITION	3.9506 3.3497 ML PACSSUAF P1 6.4530 4.9773 4.7771 4699 3.4299 3.4299 3.4299	1.0495  PATION FOR 2.1270 1.5159 1.4714 1.0778 1.1961 1.2495 1.0654 1.0654	0.041496  PLPPF 0.0946858 0.060470 0.656689 0.047702 0.042489 0.042489 0.042489 0.042489	0.10781 0.22046 0.15647 0.15246 0.11168 7.12393 7.1771 7.11039	1.3500 x/DMAX -1.9670 -1.0070 -1.0070 -1.0000 -1.0000 -1.0000				
137 142 >40047400 AVIT MIRES -107 -117 -127 -127 -137 -147 -152 -157 >60017100	3,9506 3,3497 ML PACCEURE PI 6.9500 4.9773 4.7371 6699 3,536 3,34799 3,4299 101 PRESSUPE	1.0495 PATION FOR PL/PN 2.1278 1.5159 1.6714 1.0778 1.1961 1.0454 PATION FAI	0.041496  PL/PYF 0.044858 0.040470 0.047986 0.047702 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15647 0.15246 0.11168 7.12383 7.11039 0.11039	X/DMAX -1-0476 -1-0476 -1-0470 -1-0470 -1-0470 -1-0400 -1-0400 -1-0400				
137 142 AVIT UPPR -107 -112 -127 -127 -147 -149 -152 -157 AVD UPPO -159 -157	3.9506 3.3597 ML PRESSURE PI 6.8510 4.9773 4.7371 6699 3.6299 3.4299 3.4299 1AI PRESSUPE PI 3.6299 3.6299	1.0495  PATION FAI  PL /PN  2.1278  1.5159  1.6714  1.0778  1.1961  1.0654  1.0654  PATIOS FAI  P/PN  1.0654  1.0654	0.041496  PLPPF 0.0946858 0.060470 0.656689 0.047702 0.042489 0.042489 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11168 7.12383 7.11039 0.11039 PI/PTP 0.11039 C.11039	X/DMAX -1-9010 -10300 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
137 142 140413   100 AVIT   100 III   110 II	3.9506 3.3597 ML PRESSURE PI 6.8510 4.9773 4.7371 6699 3.6299 3.4299 3.4299 1AI PRESSUPE PI 3.6299 3.6299	1.0495  PATION FAI  PL /PN  2.1278  1.5159  1.6714  1.0778  1.1961  1.0654  1.0654  PATIOS FAI  P/PN  1.0654  1.0654	0.041496  PLPPF 0.046458 0.04074986 0.047707 0.042489 0.042489 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11168 7.12383 7.11039 0.11039 PI/PTP 0.11039 C.11039	X/DMAX -1-9010 -10300 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
137 142  AVIT TIPE -117 -117 -127 -127 -127 -137 -149 -152 -157  AVD WIPD -159 -159 AVD WIPD AVD WIPD	3.9506 3.3497 ML PACSSUAF PI 6.8530 4.9773 4.7371 4699 3.4299 3.4299 3.4299 3.4299 3.4299	1.0495  PATION FAI  PLOTO 1.5159 1.4714 1.0778 1.19415 1.0654 1.0654 1.0654 1.0655 PATION FAI  PATION FAI	0.041496  PL/PYF 0.04485R 0.040470 0.04770 0.04770 0.042489 0.042489 0.042489 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15657 0.15246 0.1168 2.12393 2.10781 2.11039 0.11039 0.11039 C.11039	X/DMAX -1.9970 -1.0070 -1.0070 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
137 142 >40013400 AVIT MIRED -107 -112 -127 -127 -147 -152 -157 >600117100 >600117100	3.9506 3.3497 ML PARESTURE PI 6.95 10 4.9773 4.7371 4699 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299	1.0495  PATION FAI  PATION FAI  1.0495 1.0654 1.0654 1.0654 1.0654 1.0654	0.041496  PL/PYF 0.046458 0.060420 0.056683 0.047702 0.042489 0.042489 0.042489 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15697 0.15266 0.11168 7.12393 7.1771 7.11039 0.11039 PI/PTP 0.11039 C.11039	X/DMAX -1-9070 -1-0070 -1-0070 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000				
137 142 1400 13 100 AVIT MIRED -107 -112 -127 -127 -137 -149 -152 -157 >AND MIRED AVID MIRED AVID MIRED -167 -172	3.9506 3.3497 ML PRESSURE PI 6.8530 4.9773 4.7371 4699 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299	1.0495  PATION FAI  PATION FAI  1.5159 1.4714 1.0778 1.19415 1.0654 1.0654 1.0654 1.0654 1.0654 1.0654 1.0654	0.041496  PL/PYF 0.044658 0.060420 0.05869 0.047702 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11168 2.12393 2.16781 7.11039 0.11039 PL/PTP 0.11039 C.11039 PL/PTP 0.11039 C.11039	X/DMAX -1.9970 -1.0070 -1.0070 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
137 142  AVIT TIPE -147 -117 -127 -127 -127 -137 -149 -152 -157  >ANDITION AVD WORD -159 -157  AVD WORD -159 -157  AVD WORD -169 -179	3.9506 3.3497 ML PRESSURE PI 6.8530 4.9773 4.7371 4699 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299	1.0495  PATION FAI  PATION FAI  1.5159 1.4714 1.0778 1.19415 1.0654 1.0654 1.0654 1.0654 1.0654 1.0654 1.0654	0.041496  PL/PYF 0.046458 0.0403470 0.047407 0.047409 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489	0.10781 PL/PTP 0.22046 0.15697 0.15246 0.11168 2.12393 2.16781 7.11039 0.11039 PL/PTP 0.11039 C.11039 PL/PTP 0.11039 C.11039	X/DMAX -1-9070 -1-0070 -1-0070 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000				
137 142 140013400 AVIT MIRED -107 -112 -127 -127 -137 -142 -152 -157 >APRITION AVD MORD -15? -157 >PROSTTION AVD MORD -16.7 -172	3.9506 3.3597  ML PRESSURE PI 6.95 NO 4.9773 4.7371 6699 3.340 3.4299 IAI PRESSUPE PI 3.6299 3.6299 3.6299 3.6299 3.6299	1.0495  PATION FAI  PLANT FAI  1.0495  1.0778  1.1961  1.0654  1.0654  1.0654  1.0654  1.0654  PATION FAI  PATION FAI  PATION FAI  PATION FAI  PATION FAI  PATION FAI	0.041496  PL/PYF 0.046458 0.0403470 0.047406 0.047407 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489	0.10781  PL/PTP 0.22046 0.15697 0.15246 0.11168 7.12393 7.11039 0.11039 0.11039 0.11039 0.11039 0.11039	X/DMAX -1-9070 -1-0070 -1-0070 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000				
137 142  140012100  AVIT MIRED -107 -112 -127 -127 -147 -147 -152 -157  >ADDITION AVIT MIRED -167 -177 -177 -177 -177 -177 -177 -177	3.9506 3.3497 ML PRESSURE PI 6.8530 4.9773 4.7371 4699 3.8299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299	1.0495  PATION FEE  M /PN 2.1278 1.5159 1.4714 1.0778 1.1941 1.0654 1.0654 1.0654 1.0654 1.0654 1.0654 1.0654 1.0654 1.0654	0.041496  PL/PYF 0.044658 0.060470 0.656683 0.047986 0.047107 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489	0.10781  PL/PTP 0.22046 0.15467 0.15246 0.11168 7.12383 7.14761 7.11039 0.11039 0.11039 0.11039 0.11039 0.11039 0.11039	X/DMAX -1-9910 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000				
137 142  140013100  AVIT MIRED -107 -112 -127 -127 -137 -142 -152 -157  >ADDITION AVIT MIRED -169 -169 -167 -172  AVIT MIRED -167 -172  AVIT MIRED -167 -172  AVIT MIRED -167 -172  AVIT MIRED -172  AVIT MIRED -187 -187	3.9506 3.3497  ML PRESSURE PI 6.9530 4.9773 4.7371 6699 3.4299 3.4299  IAI PRESSUPE PI 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299 3.4299	1.0495  PATION FAI  PLANT FAI  1.0495  1.0778  1.1961  1.0654  1.0654  1.0654  1.0654  1.0654  PATION FAI  PATION FAI  PATION FAI  PATION FAI  PATION FAI  PATION FAI	0.041496  PL/PYF 0.046458 0.0403470 0.047406 0.047407 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489 0.042489	0.10781  PL/PTP 0.22046 0.15697 0.15246 0.11168 7.12393 7.11039 0.11039 0.11039 0.11039 0.11039 0.11039	X/DMAX -1-9070 -1-0070 -1-0070 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000				

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MASA-LEH I	s erectes	STAR VALUE	97/37/79	CADDELL	REC 10/07/79	02:37:32.875	FAC 9M6X1	PG# C034	100 14 100 1059
DAND IT ION	AL PRESSURE	PATTOS	IMAPY PLUG						
								2.3	
AND HUBD	PL	PL/PI)	PL/MTF	PL/PTP	X/DMAX				
32	14.759	4.5770	0.19397	0.42AA1	0.43200				
37	7.5719	2.3702	9-995634	9-55501	0.53000				
47	13.368	4.3°18	0.17412	0.40584	0.62903				
.57	9.9441	3.0841	0.12396	0.27194	0.72700				anglesser - magam magaman angaman anakan - magampan mina
>40011104	AL PRESSUPE	PATIOS . FL	CW SPLITTEP I	. P.					
AVD HORD	PL	PI /PO	PL/PTF	PL/PTP	X/DMAX				
62	11.331	3.5140	0.14125	0.32522	J.42200				
<u>£7</u>	7.9423	2. 4631	2_ £95094	0.23076	0.67000	and the second s			and the second of the second of the second
>ADDITION	NL PRESSURF	RATIOS . FL	N SPLITTER C	.0.			e e demonstration of the second secon		
AVD WORD	PL	PL/PO	PL /PTF	PL /PTP	X/DMAX .				
77	32.335	13.028	0.4930#	0.93951	J. 5 JR00				
92.	16.299	5. Q548	0.23319	0.47359	0.58300				
97	3.4745	1.0775	0.943312	0.19095	J. 6 70UO				
SADD ET TON	LL PRESSURÉ	RATIOS . FJ	CCTCP SHEDUD	in the Bills Made there is	<del>-</del> - / /	and the second second	er redendar, salatilar vedjer, allas date vu apid		· • · ·
AND MUND	PL	FL / 90	PI /PTF	PL/PTP	X/DPAX	-			
107	6-9356	2.1106	0.294836	0.19774	0.62400			A	-
11?	4.9373	1.5002	2-040299	0.14055	J. 630UJ	<del></del>		20.00	
122	4.7373	1.4599	0.058674	9-13676	0.96300		<u> </u>	CA SE	
127	3.4745	1.0775	9.043312	0.10095	1-9400			AV	
127	4.2327	1.2590	9. 150245	9.11711	1.2200			6	
142	3.6549	1.1335	3_045569	0.10619	1.3500	*	, the	<b>S</b>	** *
>40017 F004	+ POESSION	441195 - FA					HA AN	_	
רפחשוועו	PL	<b>9</b> (/Pf)	PI /PTF	PL /PTP	X/DMAX		X,3		
-107	6.9056	2.1106	0.094836	2.19774	-1-9630		· 9		
• •	4.4373	1.5002	0-040299	0.14055	-1.0000	• • •	and the same of th		*** * * * **
-117	4.7379		0.058676	2.13676	-1.0000				
-122	4745	<u> 1.4598</u> 1.3775	0.047312	3.10095	-1.0090				<del></del>
-127	4.3397	1.2500	0.050245	0.11711	-1.0000				
-14?	1.45	1.1335	0.050245	0,17619	-1.0000	*		rancasian e management e a	
-152	3.4214	1.7636	0.642750	0.099643	-1.0000				
-157	7.4344	1.2651	0.047917	0.000780	-1.0000	•	and the second of the second o	maga ina ina daga ang ang ang ang ang ang ang ang ang	
>10017109	L PRESSIPE	RATION FAI	" "FTTLE FLAP						
IVO ሣጣዚባ	PI	PI /PI	M 1016	PL /PTP	Y/DMAY	=		• •	
-167	3.4294	1.0636	× 0.042753	0.099643	-1.0000				
-157	3.4344	1.065)	3-047812	0.0997#9	-1.0000		· · · · · · · · · · · · · · · · · · ·		
>10011 104	L PRESSURF	* STYPK . 29	DES SHETTER	nestinu					
AND MUSA	PL /	Pt /Pf)	PI / PTF	PI /PTP	K\DMAA	•			
-1 / 7	3.414	1.9651	0.742812	050789	-1.0000				
-172	1	1.0651	0.942412	0.055789	-1.0000	¥			
					- LOUVIN				٠ - ١٠ - ١ - ١٠ - ١ - ١ - ١ - ١ - ١ - ١
Skošit fori	M OPESSIDE	PATING . BO	DES SIBELIO (	OCATION -					
ב אפנו חעם	r)	PL / PO	PI / PTF	PI /PTP	Aydava	- i	•		
197	3.9956 3.3295	1.2391	0.045908	0.11-99	-1.0330 -1.0330				
		1.2158	0.342971	0.11391					

	4451-1 FW1	5 PRFL [4]	IMARY DATA	07/07/19	C400E11	PEC 10/07/75	02:38:15.959	FAC 8X6X1	//w/ /4 PG4 C834 NPG 1069	
)	>4nn111nn	AL PRESSUPE	PATINS . PF	LHAFY PLUG	-				and the state of t	
	AVD HOPD	PI	PI / PO	ሚ /የፕኖ	PL /PTP	X/DHAX				
	37	17.134	5.3270	0.21325	0.47774	0.43200				
	37	6-7531	2.7574	0.1101#	0.22102	0.53000				
	47	16.294	5.04.28	0.20767	9.49654	3.62900				
	52	11.469	3.5654	0.14274	0.28633	J. 72700				
	>ADDITION	AL PRESSURE	RATIOS . FLO	DW SPLITTER I	.D.					
	DRUM GAV	_PL	PL /PO	PL /PTF	PL /PTP	x/n=ax			•	
	67	13.159	4.0913	2.16378	0.32853	0.42200				
	67	9.2033			0-22976	0.42200				
	01	746922	2.8613	C-11454	W-22710	Vebiteet	····			
	>40017 10%	AL PRESSURE	PATINS . FLO	OW SPLITTER C	.p.		***		*	
	AVD WOPD	P1,	PI /PII	PL /PTF	PI /PTP	X/DMAX		and the second s		
	77	32.426	13.901	0.49356	0.Rg957	9.50800			•	
	<b>R2</b>	16,339	5,0799	0.20325	0.40792	0.58300			<del></del>	
	a5	3.4724	1.0795	0.043216	0.096690	0.67000				
-	Senul I fue	AL PRESSURE	PATINS . EJI	ECTOR SHACIO	The second second	TO THE TOWNS OF THE PERSON OF	er a seminar e e e e e e e e e e e e e e e e e e e		ing and the second seco	
	AYD HORD	PI	Pt /P1	PL /PTF	PL /PTP	X/DMAX	- A 1242-00	e i i de especial de la companya della companya de la companya della companya del	entimientegithers - appropries on an institute on the second	
	107	6-9266	2.1224	0.094960	0.17043	U. 62400			*	
	11?	4. 9544	1.5792	0.060416	0.12119	0.43000				
	122	4.7142	1.4656	0.05%71	0.11769	0. 96000				
	127	3.4775	1.0*11	0.043279	0.086815	1.0900			- And the state of	
	137	4.4499	1.3831	0.055369	0-11107	1.2200				
	147	4.1134	1.2789	9.051193	0.16269	1-3500				
$\overline{}$	- NUDITION	M-ARESSURE	******							
~	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			• • • • •	61 (919	* (7)		and the same and the same		
~	AVE MORT	PL	PL /PIT	PL / PTF	PI /PTP	X/D##		olin i rapid daminin and i ya ∰		
~	4VI WORN -107	PL 6-9266	M /PN 2-1224	PL / PTF 0. 084960	0.17043	-120000				
~	AVP WORN -107 -117	PL 6-9266 4-8544	M /PR 7-1224 1-5992	P[ / PTF 0. 084940 0. 063416	0.17043 0.12119	1.0000		and the same of th		
_	AVI WORN -107 -117 -127	PL 6.9266 4.8544 4.7142	M /PR 7-1224 1-5992 1-4656	P[/PTF 0.084960 0.063416 0.05867[	0.17043 0.12115 0.11769	-1.0000 1.0000 -1.3000				
_	AVI WORN -107 -117 -127 -177	PL 6.9266 4.8544 4.7142	M /PR 7.1224 1.5092 1.4656	PI / PTF 0. 084960 0. 063416 0. 058671 0. C43279	0.17043 0.12119 0.11769 0.086915	-1.0000 -1.0000 -1.0000		•		
_	AVN WORN -107 -117 -122 -177 -137	6.9266 4.8544 4.7142 3.4775 4.29	M /PA 2.1224 1.5092 1.4656 1.0811 1.3831	PI / PTF 0.054940 0.063416 0.058671 0.643279	0.17043 0.12119 0.11769 0.086915 0.11107	-1.0000 -1.0000 -1.0000 -1.0000				annin frankrisioni
_	AVI MORN -107 -117 -122 -127 -137 -142	6.9206 4.8544 4.7142 3.4775 4.399	M /Pn 2.1224 1.5992 1.4656 1.0811 1.3831 1.2799	PI / PTF 0. 084940 0. 05:3416 0. 05:8671 0. C43279 0. C55349 0. 05:1193	0.17043 0.12115 0.11769 0.006915 0.14107	-1.0000 1.0000 -1.0000 -1.0000 -1.0000	· · · · · · · · · · · · · · · · · · ·			anton Good and the
_	AVM MORN -107 -117 -122 -177 -137 -142 -152	6.9266 4.8544 4.7142 3.4775 4.29	M /PA 2.1224 1.5092 1.4656 1.0811 1.3831	PI / PTF 0.054940 0.063416 0.058671 0.643279	0.17043 0.12119 0.11769 0.086915 0.11107	-1.0000 -1.0000 -1.0000 -1.0000	· · · · · · · · · · · · · · · · · · ·			anto Colombia
_	AVI WORN -107 -117 -117 -127 -137 -142 -157 -157	PL 6. 9206 6. 8544 6. 7142 7. 4775 4. 639 4. 1134 3. 4374 3. 4326	PI/PH 7.1224 1.5992 1.4656 1.9811 1.3831 1.2799 1.0671	PI/PTF 0.0849A0 0.063416 0.058671 0.043279 0.0553A9 0.051193 0.042719	0.17043 0.12115 0.11769 0.086915 0.14107 0.19269 0.085690	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	AVI WORN -107 -117 -127 -127 -147 -145 -167 -167 -167	PL 6. 9206 4. 9544 4. 7142 3. 4775 4. 939 4. 114 3. 4374 3. 4324 Al PRESSIPE	PI /PT 7.1224 1.5092 1.4656 1.0811 1.3831 1.2799 1.0671 1.0671	PI / PTF 0. 0849A0 0. 063416 0. 058671 0. C43279 0. C53279 0. 051173 0. 042719 0. 042719	0.17043 0.12115 0.11769 0.086475 0.14107 0.10269 0.085690	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AVI WORN -107 -117 -117 -127 -137 -142 -167 -167 -167 -167 -167	PL 6.9266 4.8544 4.7147 1.4775 4.939 4.1134 3.4324 AL PRESSIME	PI /PR 7.1224 1.5092 1.4656 1.0811 1.3831 1.2799 1.0671 1.0671	PI / PTF  0. 0849A0 0. 063416 0. 058671 0. C43279 0. C553A9 0. 051193 0. 042719 0. 042719	0.17043 0.12115 0.11769 0.086975 0.11107 0.19269 0.085690	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AVD WORN -107 -117 -117 -127 -127 -137 -142 -157 -167 -167 -167 -167	PL 6. 9206 4.8544 4.7142 3.4775 4.039 4.1134 3.4324 AI PRESSIME PL 3.4324	PI /PH ?-1224 1.5392 1.4656 1.9811 1.3831 1.2799 1.0671 1.9671 PATION FAI PATION FAI	P[/PTF 0.0849A0 0.063416 0.058671 0.058671 0.055349 0.055349 0.042719 0.042719 0.042719	0.17043 0.12115 0.11769 0.086975 0.14107 0.10269 0.085690	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	AVI WORN -107 -117 -117 -127 -137 -142 -167 -167 -167 -167 -167	PL 6.9266 4.8544 4.7147 1.4775 4.939 4.1134 3.4324 AL PRESSIME	PI /PR 7.1224 1.5092 1.4656 1.0811 1.3831 1.2799 1.0671 1.0671	PI / PTF  0. 0849A0 0. 063416 0. 058671 0. C43279 0. C553A9 0. 051193 0. 042719 0. 042719	0.17043 0.12119 0.11769 0.086975 0.11107 0.19269 0.085690	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AVI WORN -107 -117 -127 -127 -147 -147 -147 -167  >AND ST INS	PL 6.9266 4.8544 4.7142 1.4775 4.939 4.114 3.4324 3.4324 7.4324 7.4324	PI /PN 7.1224 1.5992 1.4656 1.9811 1.3831 1.2749 1.9671 1.9671 PATION FAI	P[/PTF 0.0849A0 0.063416 0.058671 0.058671 0.055349 0.055349 0.042719 0.042719 0.042719	0.17043 0.12119 0.11769 0.086975 0.11107 0.19269 0.085690 0.085690 0.085690 0.085690	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AVI WORN -107 -117 -127 -127 -147 -147 -147 -167  >AND ST INS	PL 6. 9206 4.0544 4.754 4.775 4.039 4.114 3.4324 7.4324 AT PRESSIDE	PI/PN 7.1224 1.5092 1.4656 1.0811 1.3831 1.2799 1.0671 1.0671 PAYIN: FAI PI/PN 1.0671 PAYIN: FAI PI/PN 1.0671	PI / PTF  0. 0849A0 0.063416 0.058671 0. C43279 0. C553A9 0. 042719 0. 042719 0. 042719 0. 042718 0. 042718 0. 042718 0. 042718	0.17043 0.12115 0.11769 0.086975 0.14107 0.10269 0.10269 0.085690 0.085690 0.085690 0.085690	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AVI WORN -107 -117 -117 -127 -137 -142 -157 -167 -167 -167 -167 -167 -167 -167 -16	PL 6.9206 4.8544 4.7142 1.4775 4.939 4.114 3.4324 3.4324 7.4324 AI PRESSIPE PL 3.4324 7.4324	PI/PH 7.1224 1.5092 1.4656 1.0811 1.3831 1.2799 1.0671 1.9671 PATION, FAI PATION, FAI PATION, FAI PATION, FAI	PI / PTF	0.17043 0.12115 0.11769 0.086975 0.11107 0.19269 0.085690 0.085690 0.085690 0.085690	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	AVID WITH IN W	PL 6. 9206 4.0544 4.754 4.775 4.039 4.114 3.4324 7.4324 AT PRESSIDE	PI/PN 7.1224 1.5092 1.4656 1.0811 1.3831 1.2799 1.0671 1.0671 PAYIN: FAI PI/PN 1.0671 PAYIN: FAI PI/PN 1.0671	PI / PTF  0. 0849A0 0.063416 0.058671 0. C43279 0. C553A9 0. 042719 0. 042719 0. 042719 0. 042718 0. 042718 0. 042718 0. 042718	0.17043 0.12115 0.11769 0.086975 0.14107 0.10269 0.10269 0.085690 0.085690 0.085690 0.085690	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	AND WORN -107 -117 -127 -127 -147 -147 -147 -167  >AND WORN -167  >AND WORN -167  AND WORN -167	PL 6. 9266 6. 9544 6. 7142 7. 4775 4. 1134 3. 4324 3. 4324 7. 4324 AT PRESSIME PL 3. 4324 AT PRESSIME	PI/PH ?.1224 1.5992 1.4656 1.0811 1.3831 1.2799 1.0671 1.0671 PAYINS, FAI PI/PH 1.0671 1.0671 1.0671 1.0671	PI / PTF	0.17043 0.12115 0.11769 0.086915 0.14107 0.10269 0.085690 0.085690 0.085690 0.085690 0.085690 0.085690 0.085690	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	AND WORN -107 -117 -127 -127 -147 -147 -147 -167 -167 -167 -167 -167 -167 -167 -16	PL 6.9206 4.0544 4.7142 3.4775 4.079 4.114 3.4324 3.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324	PI /PT  7.1224 1.5992 1.4656 1.0811 1.3831 1.2799 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671	PI / PTF	0.17043 0.12115 0.11769 0.086975 0.11107 0.19269 0.085690 0.085690 0.085690 0.085690 0.085690 0.085690 0.085690	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	AVI WORN -107 -117 -117 -127 -127 -137 -142 -142 -147 -147 -147 -147 -147 -147 -147 -157 -157 -157 -157 -157 -157 -157 -167 -172 -167 -172 -172 -172 -172 -172	PL 6.9266 4.0544 4.0544 4.0544 4.075 4.079 4.1134 3.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7	PI/PN 7.1224 1.5092 1.4656 1.0811 1.3831 1.2799 1.0671 1.9671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671	P[/PTF 0.0849A0 0.063416 0.058671 0.053779 0.055349 0.042719 0.042719 0.042719 0.042719 0.042718 0.042718 0.042718 0.042718 0.042718 0.042718 0.042718	0.17043 0.12115 0.11769 0.086915 0.1107 9.19269 0.085690 0.085690 0.085690 0.085690 0.085690 0.085690 0.085690	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	AND WORN -107 -117 -127 -127 -147 -147 -147 -167 -167 -167 -167 -167 -167 -167 -16	PL 6.9206 4.0544 4.7142 3.4775 4.079 4.114 3.4324 3.4324 7.4324 7.4324 7.4324 7.4324 7.4324 7.4324	PI /PT  7.1224 1.5992 1.4656 1.0811 1.3831 1.2799 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671 1.0671	PI / PTF	0.17043 0.12115 0.11769 0.086975 0.11107 0.19269 0.085690 0.085690 0.085690 0.085690 0.085690 0.085690 0.085690	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

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**山本郷州大学等**とい、大学を持ちを発展できませた。 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1921 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1

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4454-1 FHIS	PRFLIMI	HARY DATA	97/07/79	CADRELL	REC 13/07/79	92:40:27,495	FAC BYEKE	PG# C034	RDG 1061
>699171094	L_PRESSUPE	PATINS . PP	IMARY PLUG			- Marie Marie de la companio del companio del companio de la companio del companio de la companio del companio de la companio della companio de la companio de la companio de la companio de la companio della companio	n e temperatur name o un orden o		en eggenegen om av de a som den o
IAU AULL	PL	<b>የ</b> ፤ / ኮባ	PL/PTF	PL/PTP	X/IMAX				
32	12.377	2.7125	0.164f€	6.42745	0.43200				
37	6.33?3	1.9465	0.004337	9.22411	0.53000				
47	11.432	3.5142	0.15687	0.4041	0.42600				
52	A. 2643	2.5435	J_11262	0.25259	u. 72700		·	<del>,</del>	
AND! TECOA<	L PRESSURE	RATIOS . FLO	OW SPLITTER 1.	. O.			-		
LAD MULD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX			-	•
<b>4</b> 2	9.3002	2 <b>.</b> 65 69	0.12680	0.32517	J.42200				
£7	6,5123	2.0)19	<u> </u>	0-23049	0.67000		····		
>#POITIONA	L PRESSUPE	RATIOS . FLO	PW SPLITTER C	D.					·
MD AUBO	PL .	PL/PO	PL/PTF	PL/PTP	X/DMAX				
77	29.863	9.1799	7.40716	1.0570	0.50800				
*2	14.973	4.5782	9.22306	0.52713	0.58300				
97	3.5125	1.0798	0.947891	0.12432	0.67000				
ANDITIONA	L PRESSIRE	RATIOS . EJI	ECTOP SHARRIN				ு ப்படுப்ப ஆடி ஊர்க்க மத் <del>அன்</del> றுப்பில் வி		
AND WORD	PL	PL /PD	PI /PTF	PL /PTP	X/DMAX		and the second s	د د م ما سالومو موداند	
197	6.2319	1.9157	0.254968	0.22957	0.62400				
112	4,429?	1.3615	0.9603#9	0.15676	U-93000				
122	4.3399	1.3746	0.058759	0.15251	0.96000				
127	3.4975	1.0751	0.C476 M6	0.12379	1.0500		and the second s		
137	3.5075	1.0782	0.047923	0.12414	1.2200				
142	3.0516	0.93898	0.041607	0.10701	1.3500		· · · · · · · · · · · · · · · · · · ·	or other termination of the con-	
>400 ( T TONA	- mercunt	ALTING - FRI	FEEDY INCT						
WINDER	ři.	PL/PD	PL/PTF	PL /PTP	X/044X		•	market er er i degege i juner den Wielen i i	<b>.</b>
-107	6.2319	1.9157	0.08%969	0.72057	-1,0000				when the control of t
-112	4.4792	1.3615	0. 040389	0.15676	2.0000				
-122	4.3397	1.3746	0.058750	0.15251	-1.0000				
-127	3.4975	1.0751	0. 047696	0.17379	-1.0000				
-1 77	3.6075	1.07*2	0.047923	0.12014	-1.0000				
-142	3.2536	0.93808	0.041607	0,10801	-1.0000	•			
-152	3.4624	1.0544	0.047298	0.12255	-1.0000				
-1 5 7	3.4626	1.0644	0.047239	0.17755	-1.0900				
APPLITIONA	PRESSIME	PATINE . FAT	402715 4140						
	rt	PL/PT	AL/PTF	PL /PTP	X/D#AX				
רקוא מען	3.4624	1.0644	3.947299	0.12255	-1-0000				
		1-0649	8 C472CB	9.12255	-1.0000		The second second second	ul.	-
LVN HAPT -157 -157	2.4624								
-157 -157	3.4674	PATINE , 29	UER SIMPLE	JUN TUN					
-157 -157 >89911 [898	PPESSIPE								-
-157 -157 >29911109A IVO HOPO	2.4524   DPESCHPE   PI /	PI / PI	PL/PTF	PL IPTP	K/DMAX			. at the	-
-157 -157	7.4624   PPESCHPE   PI   3.4624	PI / PO 1.2659		PL /PTP 12272	K/D#AK -1.0000 -1.0000				• •
-157 -157   SEPOIT MUN IVO WOPO -167	2.4624 PI 3.4674	Pr / Pri 1. 2659 1. 0659	PL/PTF 0.047276	PL /PTP 12272 0.11277	-1.0000	· · ·			-
-157 -157 -26911 (IPA 100 MOPO -167 -172 -389011 (PH)	PI 3. 4674 PI 3. 4674 PI 7. 6674 PI PESSIPE	M / MA 1.2659 1.0659 PAYINS , 30	PL/PTF 0.047276 0.047276 DEG SHPFUN TO	PL /PTP 12272 0.1927?	-1.0000 -1.0000				
-157 -157 -2670]T [MWA -147 -172	2.4624 PI 3.4674	Pr / Pri 1. 2659 1. 0659	PL/PTF 0.047276 0.047276	PL /PTP 12272 0.11277	-1.0000				-

>t.	JAPPILT I O	PRESSIRE	PATINS_E PRI	MARY PLUG	and the second s	£			validations for responsible sources of the contract	
AVD	หกดบ	PL	PJ / P-/7	PL/PTF	PL /PTP	X/DMAX				
72		13.531	4, 1570	0.19475	0.42761	0.43200		·		
37		7. 3595	2.1713	J. C96386	0.22309	0.53000				
47		12.931	3.9619	1.17587	0.40706	0.62900				
52		2-1373	2.9104	0-12476	0.28675	0.72700				
. >A!	PAPOLITIC	PPESSURE	RATIOS . FLO	CW SPLITTEP 1	.0.					
AVD	40×0	PL	PL / PO	PL/PTF	PL /PTP	X/DMAX				
45		10.799	3.1944	0.14100	0.32861	J <b>.</b> 42200				
67.		7.2748_	2_2376	O_ Cº 9326	0_22585	0.67000				******
>4"	JAPOLT LO	PRESSUPE	RATIOS . FLO	NW SPLITTER O	.0.		•			
	WORD .	PL.	PL /PO	M /PTF	PL /PTP	X/DMAX				
77		29 <b>.</b> 827	9.1741	0.40724	0.94256	J.50800				
02		14.767	4,5729	2.22259	0.4658?	0.50300				
97		3.5079	1.0790	0.047895	0.11096	J. 670 <b>00</b>				
>Ar	ואריון דן פו	PRESSIME	RATIOS , FJ	FETCH SHPCUS	V 400	_ /	e e a une deservación de la company de la co			
~ <b>V</b> D	Musu	PL	PL/PO	PL /PTF	el /PTr	X/DPAX			· ••· •	
19	, <u></u>	6.2381	1.9095	0.084762	0.19619	J.62400				
112	)	4.4049	1.354F	0.050141	0.13020	U. R3000				
127	?	4.2596	1.3194	0.058567	0.13556	J. 96000				
127	•	3.4729	1.0743	0. 547690	0.11038	1.0900				
121		3.6783	1.1314	0.0 6221	9.11624	1-2200				
148	}	3.3576	1.0327	9.45743	0.13610	1.3500				
<"	<del>917 (948</del> )	POFFERINE	****** + ***							<del></del>
AVE	MU 6 J	PL	P) /P()	PL /PTF	PL /PTP	×/DMAX				
-107		6.2)#1	1.4795	0.094762	0.19419	-1 .9000				
-112		4.4349	1.3548	0.060141	0.13920	71.0000				
-12		4.2896	1.3194	C- C58567	0.13556	-1.0000				
-12		374353	1.0743	0.1476.90	0.1103	-1.0000				
-13	,	3.6743	1.1314	0. 350?21	0.11474	-1.0000				
-14	1	3.3576	1.0327	0.045843	0/010	-1.0000				
-153	•	3.4629	1.0651	0.047279	0.10943	-1.0000				
-12.	•	3.4574	1.04.36	7. 7.77211	0.13927	-1.0000	•			
	DIT TOWAL	perssipe	FATING FAI	NETTIE FLAR						-
	MUND	οį	P1 /PD	M /OTF	PL /PTP	X/DHAX				
-157	•	3.4623	1.9651	Q-1)4727C	0.10943	-1.0000		. = .		
-15	•	3.457#	1.063	0.067211	0.10977	-1.0000				
>21	OFF TOHAL	PPFSSIJRF	ग्राप्टर क	DEC SHEODY	OCATION					
	AL.D.D	m /	PI /PO	M /PTF	MATE	x/DMAx				
-16		3.4()	1.3651	1].047279	0.10043	-1.0000				
-17	•	3 16.34	1.0651	0.047779	3-100	-1.0000	•			
>41	itt fried	PARKEINE	PATING . PO	DEG SHREUD E	PATERIN					
AVO	WAY	PI	Pt /PO	PI / PTF	PI /PTP	YATOMA				
	<i>-</i>	3.9338	1.2199	0.053710	0.17431	-1.000				
-12	•									
-1077 -157	•	3.8537	1.1457	0.052616	0.12170	-1.0000				

CONTRACTOR OF STREET

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7 8.9557 7.4565 0.11055 0.22172 0.53000 77 14.901 4.5751 0.2752 0.45677 3.62500 2 13.478 3.2157 0.14102 0.23655 0.72700  20 11.000 P.	MAS A-L FU I	S PPELS=	IHAPY DATA	97/97/79	CADDETT	REC 10/37/79 02:41:56.399	FAC BROXE	PGF C034 PBG 1063
15.537	SAUGIT ION	1 PRESSIPE	PATINS . PP	MARY PLUG				entroppe en la gran a la companio de la companio del la companio de la companio del la companio de la companio del la companio de la companio del la com
15.537	WP WEED	PI	91 / 90	CI / PT F	01 /PTP	X /DMAX		
7	72		4. 7902					
14.941 4.5541 0.22422 0.45977 3.62600  22 13.478 3.2162 0.14302 0.22659 0.72700  ADDITIONAL PRESSURE RATIOS , FLOW SPLITTER 1.0.  D MOPD PL PLYPO PLYPTF PLYPTP NYDWAY  7 8.3861 2.5757 3.11447 0.22968 0.4000  ADDITIONAL PRESSURE RATIOS , FLOW SPLITTER 1.0.  D MOPD PL PLYPO PLYPTF PLYPTP NYDWAY  10 MOPD PL PLYPO PLYPTF PLYPTP NYDWAY  12 14.521 4.5767 0.22968 0.4000  ADDITIONAL PRESSURE RATIOS , FLOW SPLITTEP 0.0.  D MOPD PL PLYPO PLYPTF PLYPTP NYDWAY  2 14.521 4.5767 0.22950 0.40913 0.50000  ADDITIONAL PRESSURE RATIOS , FJECTOP SEMPOUD  D MOPD PL PLYPT PLYPTF PLYPTF NYDWAY  10 MOPD PL PLYPT PLYPTF PLYPTF NYDWAY  10 MOPD PL PLYPT PLYPTF NYDWAY  10 MOPD PL PLYPTP PLYPTP NYDWAY  10 MOPD PL PLYPTP NYDWAY  1	27							
2 13-478 3-2182 0.14302 0.28459 0.72700  ADDITIONAL PRESSURE RATIOS FLOW SPLITTER 1.P.  D 40PD PL PL/PO PL/PTF PL/PTF 1/PPAY  2 11.044 3.4090 0.16358 0.32824 0.42200  7. 8.1861 2.5787 3.11645 0.42200 0.61000  ADDITIONAL PRESSURE RATIOS FLOW SPLITTEP 0.D.  D 40PD PL PL/PO PL/PTF PL/PTF 1/PPAY  2 14.231 4.5767 0.23740 0.45911 0.58900  2 14.231 4.5767 0.23740 0.45911 0.58900  2 14.231 4.5767 0.23740 0.45911 0.58900  D 40PD PL PL/PTP PL/PTP N/PPAX  ADDITIONAL PRESSURE PATIOS, FJECTOP SHROWD  D 40PD PL PL/PTP PL/PTP N/PPAX  ADDITIONAL PRESSURE PATIOS, FJECTOP SHROWD  D 40PD PL PL/PTP PL/PTP N/PPAX  ADDITIONAL PRESSURE PATIOS, FJECTOP SHROWD  D 40PD PL PL/PTP PL/PTP N/PPAX  ADDITIONAL PRESSURE PATIOS, FJECTOP SHROWD  D 40PD PL PL/PTP PL/PTP N/PPAX  ADDITIONAL PRESSURE PATIOS, FJECTOP SHROWD  D 40PD PL PL/PTP PL/PTP N/PPAX  ADDITIONAL PRESSURE PATIOS, FJECTOP SHROWD  D 40PD PL PL/PTP N/PPAX  ADDITIONAL PRESSURE PATIOS, FJECTOP SHROWD  D 40PD PL PL/PTP N/PPAX  ADDITIONAL PATIONAL PATION	47							
D   NOPD   PL   PL/PO   PL/PTF   PL/PTF   Y/DPAF   2. 11.046   2.5757   3.11447   0.22908   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.42200   0.	.52							and the state of t
2 11.094 3.600 0.16558 0.2724 0.42200 27 8.1861 2.2757 1.11447 0.22908 0.61000  APDITIONAL PRESSURE RATIOS . FLOW SPLITTEP 0.D.  10 WIPD PL	MOI TIGGA<	AL PRESSURE	RATIOS , FLO	W SPLITTER I	.n.			
7. 8.1861 2.5177 3.11447 0.22908 0.67000 APOITIONAL PRESSURE RATIOS , FLOW SPLITTER 0.0, 10 MORD PL MI/PD 4.7567 0.47590 0.48990 0.50900 0.2 14.931 4.5767 0.22340 0.40913 0.58900 0.2 3.5082 1.0775 0.647886 0.99008 0.67000 0.48990 0.50900 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.670000 0.670000 0.670000 0.670000 0.670000 0.670000 0.	ND ACED	PL.	PL/PO	PL/PTF	PL/PTP	X/DPAX		
7. 8.1861 2.5177 3.11447 0.22908 0.67000 APOITIONAL PRESSURE RATIOS , FLOW SPLITTER 0.0, 10 MORD PL MI/PD 4.7567 0.47590 0.48990 0.50900 0.2 14.931 4.5767 0.22340 0.40913 0.58900 0.2 3.5082 1.0775 0.647886 0.99008 0.67000 0.48990 0.50900 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.67000 0.670000 0.670000 0.670000 0.670000 0.670000 0.670000 0.	62	11.084	3.6009	0.16358	0.32824	4.42200		
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5?	מחשר מע	Pt	91 / PT	PETE	PI /PTP	×/DMAX		
57 3.46PL 1.0652 0.047339 0.094988 -1.0000 ADDITIONAL PRESSURE PATION . 20 DEG SHRODD LOCATION DI WORD PL PL/PC PL/PTF W/PTP X/DWAX 67 3.46BL 1.3652 9.347339 0.394988 -1.0000 77 3.46BL 1.0652 9.347339 0.09498P -1.0000 ADDITIONAL PRESSURE EXTINS . RO DEG SHROUD LOCATION DI WORD PL PL/PC PL/PTF PL/PTP X/DWAY 3.3463 1.2031 0.053435 0.10330 x.10000	152	3.46.81			• • • •	· · · · · · · · · · · · · · · · ·		
NOPTO PI, PL/PC PL/PTF N/PTP N/DNAN  7.7 3.468] 1.3652 9.347339 0.354988 -1.3000  2.0317 [031] PPFSSSIRE RATIOS , RO DEG SHRCUD INCATION  TO WIDD PL  PL/PC PL/PTP N/DNAN  2.33463 1.2021 0.052435 0.10220 1.0000	157							
7.7 3.448) 1.3652 9.367339 7.364988 -1.3600 72 3.4481 1.0652 9.367339 0.304989 -1.0000 20317 [0] PPESSIRE RATIOS , RO DEG SHRUD INTATION  O MORD PL PLYPD PLYPTE PLYPTE X/DEAV		AL PRESSIPE	PATION . 25	ned sherba i	NCATION .			
7.7 3.448) 1.3652 9.367339 7.364988 -1.3600 72 3.4481 1.0652 9.367339 0.304989 -1.0000 20317 [0] PPESSIRE RATIOS , RO DEG SHRUD INTATION  O MORD PL PLYPD PLYPTE PLYPTE X/DEAV	>40311104	PI	Pt /PC	PI / PTF	N /PTO	Y/DMAY	A 10 A 10 A	
77 3.4441 1.0652 7.047339 0.03498P -1.0000  20017 10111 PPFSSIRE RATIOS , RO DEC SHRUD INCATION  ON WIDOW PL PLAPO PLAPATE PLAPATE X/DRAY								
0 WIDT PL PL/PO PL/PTF PL/PTP X/NAX	Aù MULU						* **	
92 3 9143 1 2021 0 052425 0 19220 -1 3 20	>AP3[₹]P4 VB WPPB 167 177	3.448	1.00.25		_			and the second s
92 3 9143 1 2021 0 052425 0 19220 -1 3 20	VN WOPN 167 172	3.44.81		ก็คดี รัฟหักบูกิ โ	PEATION .			
A 19 AN TO THE MODILIAL AND THICK - FOR THE	VN WOED 167 177 >&6717 [64	1.44A) 3.44A) 100FSSVIRE	RATIOS . PO			******		
47 3.4139 1.1739 0.052126 0.17459 -1.0000	VN WOEN 167 172 SÄÄÄTTÄÄY VN WOEN	1.44AA 3.44AI II PPESSIRE	RATIOS , RO	M \u_t	PL/PTP			

•	MASS - FW 15	9051 141	MARY DATA	97/57/79	CADDELL	PEC 10/07/79	A2+42+32 743	FAC 84441	ACH	ROW PT
	AL / 4 - 1 + M 1/	PP-1 141	AND DESIGNATION	977:1774	CHIRIFEE	WEI. 10/01/19	Uz incicze inc	FAC BYEFT	PCP C934	PPG 1864
	>#nn111grid	C.PRESSIME	PA*175 . J _PP1	MAPY PLUS	and agree to a substitute of the larger of	a to a suppossible conformal design of	water and the same			
	AVD WORD	nę	ሚ /የብ	PL/PTF	P[ /PTP	7/D48 X				
	52	19.652	3.2988	0.16436	0.47444	J.43200				
	27	5.5912	1.7316	0.046276	0.22395	0.53000				
	47	19.151	3.1439	3. 15464	0.40660	1.62933				
	52		2. 2597	0.11208	0.29354	J. 727JJ				
_						7816190	to the control of the			Marine de la Marine de la companione de la
	>ADDITIONS	IL PRESSURE	RAVIOS . FLO	M SPLITTER I	. D.					
	WAL MUSD	PL	Pt /PO	PL/PTF	PL/PTP	x/DMAX				
	62	8.2745	2.5410	9.12669	9.32862	0.422 <b>9</b> 9				
	67	5,7416	1.7702	0.075594	9-22997	0.67999				
~	>400 ET 10NA	L PRESSURE	PATEOS . FLO	W SPLITTER D	. D					
	AVO HOPS	PL	PL / P1	PL /PTF	PL/PTP	X/DMAX		*		
	77	26.501	P. 2076	0.4985	1.0415	0.50000		· · · · · · · · · · · · · · · · · · ·		
	92	13.153	4,0735	0.23296	0.52683	9.58300				
_	97	3,4877	1.0492	0.053418	0.13970	0.67400		<del></del>		
	>ANDITENNA	PRESSIME	PATING . FJF	CYCE SHPOIN			-	Z www.s. appears a sales on spins of	ser andriani, , ,,,	<b>.</b>
	AVD WORD	PL	PL / PO	PL /PTF	PL /PTP	x/DMAX				
				0.084499	0.21934					
		<u>5.4760</u>	1-6960			0. <u>624<b>00</b></u>				
٠.	112	3.9015	1.2349	9. 360233	0.15635	0.53000				
٠.	122	3.7993	1.1732	g.05P455	0.15174	0.91909		***	*	***
	127	3.4627	1.9724	3.053631	0.13069	1.0900				
	137	3. 3919	0. 95759	0. C47711	0.12344	1.2500				
	142	2.6711	0.83346	7,941576	0.10779	1.3500				
-				FACAR TAG 57						
_	<del>&gt;400 7  0</del> 00		<del></del>							
_					Ö1 /PTP	X COM ME		ra sama da la carres	to the second se	
<b>*</b>	AND WIPD	PL	91 /90	PL/PTF	PL/PTP	X/DM/A		A second section of	temple are - <b>a_am</b> er	
•	APO WIPT	PL 5.4760	91 / 90 1 • 6960	PL /PTF 0.094499	0.21934	-36000			and a second of the second of	• · · •
•	ATQ WIPT -107 -112	PL 5.4760 3.9035	91 / PO 1 - 6960 1 - 2389	PL / PTF 0.094499 0.060233	0.21934 0.156.5	-1.0000 1.0000		e e e e e e e e e e e e e e e e e e e		
-	ATO WIPTI -107 -112 -12?	PL 5.4760 3.9035 3.7893	PI /PI 1.6960 1.2399 1.1732	PL/PTF 0.094499 0.060233 0.058655	0.21934 0.156.5 9.15174	-1.7000 1.7000 -1,0000				nagagaananan ara sa sassannan ake -
-	AVQ WIPTI -107 -112 -127 -127	PL 5.4760 3.9035 3.7893 3.4627	01/00 1.6960 1.2989 1.1732 1.0724	PL/PTF 0.094499 0.050233 0.058655 0.053431	0.21°34 0.156.5 0.15174 0.1394	-1.0000 -1.0000 -1.0000				
_	APQ WIPTO -107 -112 -127 -127 -137	Pt. 5.4760 3.9035 3.7813 3.4627 3.9019	M / PO 1.6960 1.2289 1.1732 1.0724 0.95759	Pt / PTF 0.094499 0.050233 0.058655 0.053431 0.067711	0.21934 0.156.5 0.15174 0.1384 0.1286	-1.0000 -1.0000 -1.0000 -1.0000				
_	Arg yerry -107 -112 -112? -127 -137 -142	PL 5.4760 3.9035 3.7813 3.4627 3.1019 2.6011	M /Pn 1.6960 1.2289 1.1732 1.0724 0.95749 2.93346	PL/PTF 0.94499 9.969233 0.058655 9.053431 0.647711 0.641526	0.21934 0.156.5 0.15174 0.1384 0.1284 0.12779	-1.5000 -1.5000 -1.5000 -1.5000 -1.5000		A		
-	APQ WIPTO -107 -112 -127 -137 -142 -152	PL 5.4760 3.9035 3.7893 3.4627 3.1919 2.6931 3.4626	M / PG 1.6960 1.2289 1.1732 1.0724 0.95789 0.93346 1.0652	PL/PTF 0.094499 0.096233 0.058455 0.053431 0.647711 0.041526 0.053122	0.21934 0.156.5 0.15174 0.12845 0.12384 0.10779 0.13789	-1.0000 1.9000 -1.9000 -1.9000 -1.0000 -1.0000				
_	APQ WIPTO -107 -1127 -127 -137 -142 -152 -157	PL 5.4760 3.4035 3.7893 3.4627 3.4627 3.4676 3.4476 3.4476	M / Pn 1.6960 1.2289 1.1732 1.0724 0.95789 2.93346 1.3452 1.0646	PL/PTF 0.944499 9.969233 9.058455 9.053431 9.947711 3.041526 9.053162	0.21934 0.156.5 0.15174 0.1384 0.1284 0.12779	-1.5000 -1.5000 -1.5000 -1.5000 -1.5000				
-	AND WIPTI -107 -112 -127 -127 -137 -142 -152 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.919 7.6931 3.4426 3.4376	91/80 1.6960 1.2289 1.1732 1.0724 0.95789 0.93346 1.3442 1.9646	PL/PTF 0.094499 0.096233 0.059655 0.053631 0.047711 0.041526 0.053045	0.21934 0.156.5 0.15174 0.1393 0.12394 0.10779 0.13769	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AND WIPTI -107 -112 -127 -127 -137 -142 -152 -157 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.4627 3.4626 3.4626 3.4626	PI /PO 1.6960 1.2989 1.1732 1.0724 9.95749 9.93346 1.3442 1.9646 PATIO FAR	PL/PTF  0.094499 0.094499 0.059455 0.053431 0.047711 0.041526 0.053122 0.053045	0.21934 0.156.5 0.15174 0.12394 0.12394 0.12399 0.13769	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	APQ WIPD -107 -112 -127 -127 -137 -142 -152 -157 >APDST (NYA) AVIT WIPD -152	PL 5.4760 3.9035 3.7893 3.4627 3.4627 3.4676 1. PPESSUPE	PATITION FAME	PL/PTF 0.0944499 0.060233 0.058455 0.053631 0.0647711 0.0641526 0.0531045 MOZZJE F14P PL/PTF 0.053127	0.21934 0.156.5 0.15174 0.13845 0.12384 0.12384 0.13789 0.13789	-1.0000 1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000				
_	AND WIPD -107 -112 -127 -127 -137 -142 -152 -157 -157 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.919 2.6931 3.4476 3.4376	PI /PO 1.6960 1.2789 1.1732 1.0724 9.95789 9.91346 1.3442 1.9646 PA YION FAN PL/PO 1.9662 1.9666	PL/PTF 0.0944499 0.060233 0.058455 0.053431 0.047711 0.041526 0.053122 0.053045 1 WOZZIE FLAP PL/PTF 0.053127 0.053127	0.21934 0.156.5 0.15174 0.12845 0.12384 0.10779 0.13769 0.13769	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AND WIPD -107 -112 -127 -127 -137 -142 -152 -157 -157 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.919 2.6931 3.4476 3.4376	PI /PO 1.6960 1.2789 1.1732 1.0724 9.95789 9.91346 1.3442 1.9646 PA YION FAN PL/PO 1.9662 1.9666	PL/PTF 0.0944499 0.060233 0.058455 0.053631 0.0647711 0.0641526 0.0531045 MOZZJE F14P PL/PTF 0.053127	0.21934 0.156.5 0.15174 0.12845 0.12384 0.10779 0.13769 0.13769	-1.0000 1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000				
-	AND WIPD -107 -112 -127 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.4626 3.4376 PPESSIPE PI PPESSIPE PI PPESSIPE	PI /PT 1.6960 1.2789 1.1732 1.0724 0.95789 0.93346 1.3642 1.0646 PATITO FAN PL/PT 1.0662 1.0662 1.0666 PATITO FAN PL/PT	PL/PTF 0.094499 0.060233 0.058655 0.053631 0.0547711 0.053122 0.053045 PL/PTF 0.053127 0.053145 DEG SHUPTR 11	0.21934 0.156.5 0.15174 0.13847 0.12384 2.19779 0.13789 0.13769 PL/PTP 0.13789 2.13769	1.9000 1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000				
- -	AND UNPO -107 -112 -127 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.919 7.6931 3.4476 3.4376 I PPESSIPE NI 3.4426 PPESSIPE PI 3.4426	PL/PR 1.6960 1.2289 1.1732 1.0724 0.95789 2.93346 1.3452 1.0646 PATION FAR PL/PR 1.0662 1.9666 1.9666	PL/PTF 0.094499 9.960233 0.058655 9.053631 9.0647711 3.0647711 3.0647712 9.053122 9.053045 PL/PTF 0.053127 9.053145  DEG SHPCIM 10 PL/PTF 0.053127	0.21934 0.156.5 0.15174 0.12875 0.12884 0.10779 0.13769 0.13769 PL/PTP 0.13769 nration	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
- -	AND WIPD -107 -112 -127 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.4626 3.4376 PPESSIPE PI PPESSIPE PI PPESSIPE	PI /PT 1.6960 1.2789 1.1732 1.0724 0.95789 0.93346 1.3642 1.0646 PATITO FAN PL/PT 1.0662 1.0662 1.0666 PATITO FAN PL/PT	PL/PTF 0.094499 0.060233 0.058655 0.053631 0.0547711 0.053122 0.053045 PL/PTF 0.053127 0.053145 DEG SHUPTR 11	0.21934 0.156.5 0.15174 0.13847 0.12384 2.19779 0.13789 0.13769 PL/PTP 0.13789 2.13769	1.9000 1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000				
-	AND WIPT -107 -112 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.4626 3.4426 3.4376 PPESSIPE PI 3.4428 3.4376 PPESSIPE PI 3.4426 3.4326	PATION FAN  PATION FAN  PATION FAN  PATION FAN  PL/PO  1.0642  1.0646  PATION FAN  PL/PO  1.0662  1.0662	PL/PTF 0.094499 9.960233 0.058655 9.053631 9.0647711 3.0647711 3.0647712 9.053122 9.053045 PL/PTF 0.053127 9.053145  DEG SHPCIM 10 PL/PTF 0.053127	0.21934 0.156.5 0.15174 0.13847 0.12384 0.12384 0.13789 0.13769 PL/PTP 0.13789 0.13769	1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
	AND WIPT -107 -112 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 5.4760 3.4035 3.7893 3.4627 3.4626 3.4626 3.4626 3.4626 3.4626 3.4626 3.4626 3.4626 3.4626	PI/PT 1.6960 1.2289 1.1732 1.0724 0.95789 0.93789 0.93346 1.3652 1.9666 PATITO FAM PI/PT 1.9662 1.9662 1.9662 1.9662 1.9662	PL/PTF 0.074499 9.960233 0.058655 9.053431 9.0647711 3.0647576 9.053122 9.053045 PL/PTF 0.053127 9.53045 DEG SHUPPR 0.053127 0.053127 0.053127	0.21934 0.156.5 0.15174 0.12875 0.12384 0.10779 0.13769 0.13769 0.13769 0.13769 0.13789 0.13789	-1.0000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000				
	AND WIPD -107 -112 -127 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 5.4760 3.9035 3.7893 3.4627 3.4626 3.4626 1. PPESSIPE PI 3.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.4426 1.442	PL/PN 1.6960 1.2789 1.1732 1.0724 0.95789 2.93346 1.3452 1.9646 PATITO FAM PL/PN 1.0662 1.9662 PATITO JA62 1.9662 PATITO JA62 1.9662 PATITO JA62 PATITO JA62	PL/PTF 0.0944499 0.060233 0.058455 0.0536431 0.0641526 0.053165 0.053165 0.053127 0.053127 0.053127 0.053127 0.053127 0.053127 0.053127	0.21934 0.156.5 0.15174 0.12875 0.12384 0.10779 0.13769 0.13769 0.13769 0.13769 0.13769 0.13789 0.13789	1.9000 1.9000 -1.9000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	AND WIPT -107 -112 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 5.4760 3.4035 3.7893 3.4627 3.4626 3.4626 3.4626 3.4626 3.4626 3.4626 3.4626 3.4626 3.4626	PI/PT 1.6960 1.2289 1.1732 1.0724 0.95789 0.93789 0.93346 1.3652 1.9666 PATITO FAM PI/PT 1.9662 1.9662 1.9662 1.9662 1.9662	PL/PTF 0.074499 9.960233 0.058655 9.053431 9.0647711 3.0647576 9.053122 9.053045 PL/PTF 0.053127 9.53045 DEG SHUPPR 0.053127 0.053127 0.053127	0.21934 0.156.5 0.15174 0.12875 0.12384 0.10779 0.13769 0.13769 0.13769 0.13769 0.13789 0.13789	-1.0000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000 -1.9000				

	MASS-1 FM1	C 0011111	INAPT DATA	07/37/79	CAODELL	PEC 13/07/79 0	12-64-37 844	FAC 946X1	PS4 C036	PDG 1945
			-		CASSIFII	FEC 10/0/// 0	12 - 44 - 32 - 300	FAC 140AS	7-5 - C - 03-0	-1.4 1007
-	- Swool a fea	al, Passine	enting . PPI	TAPY PLUG.		t a tracina de la composición dela composición de la composición dela composición de la composición de	- Maria - I	the state of the s		
-	SAU MOEU	PL	ነሳ / ነሳ	PI /PTT	PL /PTP	X/DMAK				
	32	11.044	7.678)	1.19425	9.47651	0.43200				
	77	6.2434	1.7231	J. C7631*	J.22296	3.53939				
_	47	11.439	3. 53 22	0.17600	0.46740	0.629))				
	52	3_1536	2.5237		0.29137	D. 72700				
_						D. 12.00		The second state of the second	Parallel and the Control of the Cont	estimated and a second
	MOI TECCA	AL PRESSUPE	PATIOS . FLO	W SPLITTER I.	. D.					
	AND HUND	PL	PL/PO	PL/PTF	PL/PTP	Y/DMAY				
	62	9.1966	7.8444	0.14172	0.32806	9.42700				
-		£_52?7	1.9889	2,299099_		0-67000	manage as a series of the seri			
_	MOS TERGAS		PATINS . FLO	W SPLITTEP C	- D.					
	AVD WOPD			PL/FTF		X/DMAX				
		PL	PL/PN		PL/PTP				•	
	77	26.577	9.2135	0.40924	7.94770	0.50900				
		13,139	4.06.2	2.29270	0.46521	0.56300	Control of the Contro			
	د 2	3.4793	1.0772	0.053672	0.12424	0.67900				
	MOT TECHN	AL PRESSURE	PATINS , FJF	CTOR SHEDUD	* •					
`	AVD WPPD	Pt	PL /PG	PL /PTF	PI /PTP	X/DMAX	* *			
		5,4723	1.6944	2.295523	0.19542	J-62500				
	112	3.3938	1.2775	0.060163	0.13976	J. #3000				
_										
	122	3.7846	1.1710	0. 65#3#6	0.13515	0.96000				
	127	3.459)	1.0710	0.053362	0.12352	1.0900				
	137	3.2496	1.9359	0.050117	0.11601	1.2230		The second second	ake a company of the	
	142	2.9533	0.91433	0.04557	0.10545	. 1.3500				
	C SADOLT SON	or the	******	<del></del>						
	AVILADED	Pl	<b>ም</b> ር / ምብ	PI /PTF	M /PTP	* /D#A *		•	· • • • • • •	
	-107	5.4723	1.6044	0.9*4423	0.19542	-A.JOOO				
	-112	3.4998	1.2075	601000	0.13974	-1.0000				TT V
-		3.7855	1.1710	U_C52366	0.13515/	-1.0990				
	-127	3.4591	1. 3713	0.053362	0.12357	-1-0000				
		4593								
	-1 -7	3.3686	1.0059	0. (59117	0.1601	-1.0000				
	-1°7 -14?	3.9686 2.0590	0.91433	0.045557	0.1601	-1.0000 -1.0000				
	-1°7 -14? -152	3.9486 2.9539 3.4289		0.045557	0.1601	-1.0000				
	-1°7 -14?	3.9686 2.0590	0.91433	0.045557	0.1601	-1.0000 -1.0000	* * * * * * * * * * * * * * * * * * *		and the second of the second o	
,	-127 -142 -152 -157	3.9486 7.9539 3.4299 3.4299	0.91433	0.045557 0.052899 9.352899	0.11601 0.10545 0.12245	-1.0000 -1.0000 -1.0000				
yan .	-127 -142 -152 -157	3.9486 7.9539 3.4299 3.4299	0.91433 1.0617 1.0617	0.045557 0.052899 9.352899	0.11601 0.10545 0.12245	-1.0000 -1.0000 -1.0000			•	
ум. ,	-127 -142 -152 -157 >400111000	3.9486 2.9590 3.4289 3.4289	0.91433 1.0617 1.0617	0.045557 0.052899 13.052899 13.052899 M /PTF 0.352899	0.1601 0.10545 0.12245 0.12245	-1.0000 -1.0000 -1.0000 -1.9000				
,,	-127 -142 -152 -157 >40011110N	3.9486 7.0539 3.4289 3.4289 11 PRESSIME	0.91433 1.9617 1.0617 PATERS FAR	0.045557 0.052899 0.052899 NOTE FLAP	0.1601 7.10545 7.12245 0.12245	-1.0000 -1.0000 -1.0000 -1.0000				
,	-127 -142 -152 -157 >400 HT HON 440 HOND -157 -157	3.9486 2.0539 3.4289 3.4289 11 PRESSIME P1 3.4289 7.4299	0.91433 1.9617 1.9617 PATINS . FAN PL/PN 1.9617	0.045557 0.052899 9.052899 NO721 FLAP N /PTF 0.352899 10.057899	0.1601 7.10545 7.12245 0.12245 9.12245 9.12245	-1.0000 -1.0000 -1.0000 -1.0000				
-	-127 -142 -152 -157 >400 HT HON 440 HOND -157 -157	3.9486 2.0539 3.4289 3.4289 11 PRESSIME P1 3.4289 7.4299	0.91433 1.0617 1.0617 PAY(n) FAN PI / Pn 1.0617 1.0617	0.045557 0.052899 9.052899 NO721 FLAP N /PTF 0.352899 10.057899	0.1601 7.10545 7.12245 0.12245 9.12245 9.12245	-1.0000 -1.0000 -1.0000 -1.0000				
- -	-127 -142 -152 -157 >4001710N4 440 40P0 -152 -157 >4001710N4	3.9486 7.0539 3.4299 3.4299 3.4299 3.4299 2.4799 2.4799	0.91433 1.0617 1.0617 PATINS, FAN PL/PN 1.0617 1.0617 1.0613 PATINS, 72	0.045557 0.052899 9.952899 NO721 FEAP M /PTF 0.352899 0.052899 NEG SHPPDQ LF	0.1601 9.10545 9.12245 9.12245 9.12245 9.12245 9.12245	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
,	-127 -142 -157 -157 -157 -157 -157 -157 -250 1110 4040	3.9486 2.0539 3.4289 3.4289 3.4289 7.4789 7.4739	0.91433 1.0617 1.0617 PATINS FAN PLAN 1.0617 1.0617	0.045557 0.052899 9.952899 NOTE STAP NOTE J.J52899 N.052899 N.052899	0.1601 9.10545 9.12245 9.12245 9.12245 9.12245 9.12245	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
,	-127 -142 -157 -157 -157 -157 -157 -157 -240-111074 -440 HOP 0	3.9486 2.0539 3.4289 3.4289 3.4289 7.4739 21 PRESSIME PL 3.4289 7.4739	0.91433 1.0617 1.0617 PATINS, FAN M/PN 1.9617 1.0617	0.045557 0.052899 9.052899 9.052899 0.352899 0.052899 0.052899 0.052899	0.1601 9.10545 9.12245 9.12245 9.12245 9.12245 9.12245 0.12245 0.12245	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
-	-127 -142 -152 -157 -157 -157 -157 -157 -157 -167 -167 -172	3.4249 3.4249 3.4249 3.4249 3.4249 3.4249 3.4249 3.4249	0.91433 1.0617 1.0617 PATINS FAN M / PN 1.9617 1.0617 1.9617 1.9617 1.9617	0.045557 0.052899 9.052899 9.052899 0.052899 0.052899 0.052899 0.052899	0.1601 0.10545 0.12245 0.12245 PI /PTP 0.12245 0.12245 0.12245 0.12245 0.1245	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
- -	-127 -142 -157 -157 -157 -157 -157 -240 HOPD -167 -172 -172 -172	3.9486 7.0539 3.4289 3.4289 3.4289 91 3.4289 21 PRESSIRE PL 3.4289 3.4289 1 PRESSIRE	0.91433 1.0617 1.0617 PATERS FAN M / PR 1.0617 1.0617 1.0617 1.0617 1.0617 1.0617	0.045557 0.052899 9.052899 9.052899 0.052899 0.052899 0.052899 0.052899 0.052899	0.1601 0.10545 0.12245 0.12245 0.12245 0.12245 0.12245 0.12245 0.12245 0.1245	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
-	-127 -142 -152 -157 -157 -157 -157 -157 -157 -167 -167 -172	3.4846 7.4539 3.4249 3.4249 3.4249 7.4739 21 PRESSIRE PL 3.4249 7.3349 1 PRESSIRE	0.91433 1.0617 1.0617 PATINS FAN M / PN 1.9617 1.0617 1.9617 1.9617 1.9617	0.045557 0.052899 9.052899 9.052899 0.052899 0.052899 0.052899 0.052899	0.1601 0.10545 0.12245 0.12245 PI /PTP 0.12245 0.12245 0.12245 0.12245 0.1245	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

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MASA-LEW		INSRY DATE	07/07/79	CADCELL	PEC 10/07/79	02:45:03.233	FAC BROKE		on 14 G 1666
>anatitus	AVÎ BBEZZINDE	PATENS , PP	1430Y PENG		e				
AU NURU	PL	21 / PG	PI /PTF	PL /PTP	T /000 A T			The same of the sa	
3.2	13.456	4. 2844	9-21347	0.42713	X/D™AX -0.4328J				
37	7.2120	2.2399	0-11111	0.22732	0.53000				
47	13.795	4.1111	0. 20443	0.40985	0.42500				
52	9,3435	2.0)96	3.14452	U-2E917	J. 72700				
NADDET IDE	IAI BACCCIME				Verziev		- management of the second of		
	WE WESSIME	KATI'95 . FL	CW SPLITTER I	. D.					
AL HUBU	PL	PL/PO	PL / PTF	PL/PIP	X/DMAX				
62	10.657	3.2754	0.16419	0.32853	0.42200				•
6.7	7.7476	2.3228	9.11574	0.22958	J. 67900				
>40011104	AL PRESSUPE	PATIOS . FL	OV SPLITTER O	o Do					
VD WORD	PL					=		÷ #	
77	76.592	M /PC P-2225	PI/PTF	PL/PTP	X/DMAX				
92	13.14)		0.40069	0.81974	0.50000		• • •		
· · · · · · · · · · · · · · · · · · ·	3.4890	4,9755 1,9788	0.29306	0.40630	ŷ, 5 <b>0</b> 300				
•	3041.47	A si i F F F F F F F F F F F F F F F F F	0.053754	0.10756	0.67000				-
ADDET FOR	AL PRESSIPE	RATIOS . FJI	ECTOP SHPOUD	No Million I dan u	*	*** ** *	The state of the s	Manager of the second of the s	
ID WOOD	PL	Pt /PG	PI /PTF	PI /PTP	Y/DMAY			**	
107	5.4886	1.6971	9.094569	0.16920	Q.¢2400				
lla	7.9151	1.2104	0.060317	0.12069	0.83000				
122	3.7994	1.1749	0.058541	0.11714	0.96000				
27	7.4690	1.0726	0.053445	0.10f 94	1.0900			remaining the second second	
137	3.5842	1.1083	0.055221	0-11049	1.2200				
47	3.3196	1.0761	0. C51128	0.10230	1.2500	* * * * * * * * * * * * * * * * * * * *		•	
40011104	N PRESSIPE	44195 , FOI	FACON IN ET.						
neny n	- _{Pl}	PL /27	_	1711 Universit					
07	5.4886	1.6971	PL /PTF 0.084560	PL /PTP	X/DMAX		•		<del>v</del> • • •
12	3.9151	1-2106	0.060317	0.16950	-1.0000				
22	3.7999	1,1749	0.058541	0-12069	-1.0000				
27	\$693	1.0724	0.053445	<u> 2.11715</u>	-1.0000				
37	3. 3042	1.1293	0.0557445	0.1069	-1.0000				
42	3.31	1.3261	0.651129	0.11049	-1-0000				
<b>67</b>	3.4439	1.0649	0.053040	0.45230	-1.0000				-
£7 *	3. \$439	1.0649	0.05.0ed >	0.10616	-1.0000 -1.0000				
				0.10010	-1.0000				
AUDIT BOW	II DEECLIPE	PATINE FIN	KOTTLE FLAP						
በ <b>ህ</b> ርዮብ	Pl	PI /PI	JA 1977	PL /PTP	KANNAX				
57 <b>57</b>	3.4439	1.0549	0.057059	0.19616	-1.0000				
~,	2.4439	1.0549	D C23 CEO	0.10616	-1.0000		THE MEN W.		
CDD   1 1986	if bucklibe	PATION . 20	OF C SHOTTO IT	CATION					
D MUDD	Pt /	PL /P1	M /PTF	VL/PTP	X/D9ÁX			,	
4.7	3.4789	1.0533	6.052981	010601	-1.0000				
77	3.50	1.0549	3.053659	0.10616	-1.0000	**		***	
እስካችተ ተገካ <u>ታ</u>	PRESSION	ATTOS TAN	DFG"SHECUD"(A	•					
				111111					
חשפע ח	PL	Pt /Pr)	PI /PTF	PL/PTP	XJMHAX			-	
	7.4744	1.1827	0.058927	9.11791	-1.0300				
9.7	3.7300	1-1470	0.057151	0.11435	~1.03Q0				

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>Ann17_Ir		"INAPY DATA E patins _{.a.p}	07/97/79 P148PV DLUC	CvDuE11	REC 10/07/79 03:30:	49-104 FAC 8X6X1 PGM C034 PDG 1067
			ea mask, legging ,		and the second of the second o	
AND MUND	9 E	PL/PD	OL/PTF	PL/PTP		The second section will be second sec
	22.243	1.5703	0.78434		X/DMAX	The second secon
37	17.913	1,2576	9.30779	0.53864	0.43200	
47	19.343	1.2730		0.43136	0.53000	
52	11.767	2.83.072	7.71176	0.43603	J. £290J	
			0-20332	0.28455	0. 72700	
>ADDIT to	NAL PRESSUPE	PATEDS . FL	CW SPLITTEP	t.D.		***
AVD WORD	PL					
67	13.758	ci \ btJ	PL/PTF	PL /PTP	X/DMAX	
_67		0.97176	0.23777	0.33315		
	9.4457	Q.66684_	Q. 16333	0.22874	3.42700	
>#DOITING#<	WAL PRESSURE	PATIOS . FI	TH SPLITTER		0.67000	
			A SETTIFE (	P• P• _		
AVD HUPD	PL	PL / PO	PL/PTF	<b>5</b> 4 45 55		The state of the s
77	25.034	1.7673		PL/PTP	X/DMA x	
⁹ Z	13.36R	0.94372	0.43255	0.60621	0.50900	· · · · · · · · · · · · · · · · · · ·
0.7	14.199		n. 23097	0.32371	Q-58300	
		1.3)16	9.74515	0.34357	U. 67300	
>anoit in	AL PPESSIME	RATIOS . FJ	FTTCD SUBSIM		3.0.009	The second secon
			COLLE SHELDE			And the second of the second o
AVD WOPD	Pί	PI /PI	PLOPTE	04 4		
197	12.222	J. 96296		PI /PTP	X/DMAX	and the control of th
112	12.277	7.86 [87	C-21118	0.29597	0-62400	•
122	12.232		0.21092	7.25561	J. 83000	
127	14.153	0.86357	0.21136	0.29621	0.96000	
137		7.99915	0. 24454	0.34772		
142	12-617	9 <b>.89</b> 976	0-21801	0.30554	1-0900	and the control of th
• • •	12.947	0.91406	9.22372	0.31343	1.2200	
>4H-) [7 104	M- ARECCURE	AATIOS , SOE			1.3500	
			ERCON TOPET			
•						
ני אניה עמי	PI	PI /PO			7	
Ent word		PI /PO	PI /PTF	PL /PTP	X/DMAX	
107 PORT	PI	PI /PO 9-86286	P1 /PTF 0.21116	0.25597		
ฟก หาคา 117	Pt 12.272 12.207	PI /PH 1-86286 11-86181	91 /PTF 0.21118 0.21092		-!.0000	
107 117 112	Pt 12-272 12-207 12-232	PI /PO 9-86286 0-86180 9-86357	0.21118 0.21092 0.21136	0.29597 0.29561	-!-0000 -1-0000	
107 117 112 122	Pt 12.272 12.207 12.232 14.153	PI /PO 9-86286 0-86189 	91 /PTF 0.21118 0.21092	0.25597 0.29561 0.29621	-!.0000 -1.0000 1.9000	
VII VORO 107 112 122 127 137	PI 12-272 12-207 12-232 14-153 12-017	PI /PO 1-86286 0-86180 2-85357 1-39915 J-89076	91 /PTF 0.21118 0.21092 0.21136 0.2 454	0.29597 0.29561 0.29621 0.34272	-!.0000 -1.0000 -1.0000	
Vn ungn 107 117 122 127 137 142	PI 12.272 12.207 12.232 14.153 12.017 12.934	PI /PO 9-86286 0-86189 	P1 /PTF 0.21118 0.21092 0.21136 0.2 454 0.21891	0.29597 0.29561 0.29621 0.34272 0.30554	-!.000 -1.000 -1.000 -1.0000 -1.0000	
Vn ungn 107 117 122 127 137 142 157	PI 12.272 12.207 12.232 4.153 12.017 12.932 14.183	PI /PO 1-86286 0-86180 2-85357 1-39915 J-89076	P1 /PTF 0. 2111A 0. 21092 0. 21136 0. 2 454 0. 21891 0. 773/2	0.25597 0.29561 0.29621 0.34272 0.30554 0.32553	-!.000 -1.000 1.000 -1.000 -1.0000 -1.0000	
Vi ung n 107 117 122 127 137 142 157	PI 12.272 12.207 12.232 14.153 12.017 12.934	PI /PP 1-86 286 0-86 189 2-86 357 1-99 15 0-89 076 1-91 496 1-97 13	P1 /PTF 0-21118 0-21092 0-21136 0-2-454 0-21891 0-723/2 9-2450	0.29597 0.29561 0.29621 0.34272 0.34273 0.31553 0.31553	-!.000 -1.000 -1.000 -1.0000 -1.0000 -1.0000	
VN UNRA 107 117 122 127 137 142 157	PI 12-2-72 12-2-97 12-2-32 14-153 17-917 12-917 14-183 14-178	M /PO 9-86286 0-86189 9-86357 9-9915 0-89076 1-9313 1-0339	91 /PTF 0.21118 0.21092 0.21136 0.2 454 0.21891 0.73/2 0.2450 0.2450	0.25597 0.29561 0.29621 0.34272 0.30554 0.32553	-!.000 -1.000 1.000 -1.000 -1.0000 -1.0000	
VN UNRA 107 117 122 127 137 142 157	PI 12-2-72 12-2-97 12-2-32 14-153 17-917 12-917 14-183 14-178	PI /PP 1-86 286 0-86 189 2-86 357 1-99 15 0-89 076 1-91 496 1-97 13	91 /PTF 0.21118 0.21092 0.21136 0.2 454 0.21891 0.73/2 0.2450 0.2450	0.29597 0.29561 0.29621 0.34272 0.34273 0.31553 0.31553	-!.000 -1.000 -1.000 -1.0000 -1.0000 -1.0000	
VN VNR N 107 117 122 127 137 142 157 0000111093	PI 12-2-72 12-2-97 12-2-32 14-153 17-917 12-917 14-183 14-178	M /PH 1.86286 0.86189 9.86357 1.99915 0.89076 1.91496 1.0339 PATION FAN	0.21118 0.21092 0.21136 0.2 454 0.21891 0.773/2 0.2450 0.2450	0.29597 0.29501 0.29621 0.34272 0.30554 0.34343 0.34333	-!.000 -1.000 -1.000 -1.0000 -1.0000 -1.0000	
VI VIRA 107 112 122 127 137 142 157 MODITIONS	PI 12.272 12.207 12.232 14.153 17.017 12.947 14.183 14.178	PI /PD 1.86286 0.861PD 2.86357 1.29915 1.99076 1.91496 1.0339 PI /PD	0.21118 0.21092 0.21136 0.2 454 0.21891 0.73/2 0.2450 0.2450 0.24407	0.29597 0.29561 0.29621 0.34272 0.30554 0.34753 0.34345 0.34333	-!.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
VI VIRA 107 112 122 127 137 142 157 MODITIONS	PI 12.2.22 12.207 12.232 14.153 12.017 12.942 14.103 14.178 1 0000000000000000000000000000000000	PI /Pn 7.86286 0.86180 9.86357 9.86357 9.9915 3.89076 9.91496 1.0713 1.0739 PATION FAN PI /Pn 1.0713	0.21116 0.21092 0.21092 0.21136 0.2 454 0.21891 0.77372 0.2450 0.24407 NOZZIE KAP	0.29597 0.29561 0.29621 0.34272 0.30554 0.34753 0.34345 0.34333	-!.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
VN VNR N 107 112 127 137 142 157 0000111093 00 VNP N 57	P( 12.2.22 12.207 12.232 14.153 12.017 12.932 14.163 14.178 1 0000000000000000000000000000000000	PI /PN 7-86286 0-86180 9-86357 9-99976 3-91496 1-0713 1-0739 PI /PN 1-7717 1-0709	0.21118 0.21092 0.21136 0.2 454 0.21891 0.733/2 0.2450 0.24407	0.29597 0.29561 0.29621 0.34272 0.30554 0.34343 0.34343	-!.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
VID VIDEO 117 117 112 127 137 142 157 157 167 167	P( 12.2.22 12.207 12.232 14.153 12.017 12.932 14.163 14.178 1 0000000000000000000000000000000000	PI /PN 7-86286 0-86180 9-86357 9-99976 3-91496 1-0713 1-0739 PI /PN 1-7717 1-0709	0.21118 0.21092 0.21136 0.2 454 0.21891 0.733/2 0.2450 0.24407	0.29597 0.29561 0.29621 0.34272 0.30554 0.34343 0.34343	-!.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
VID VIDEO 117 117 117 117 117 117 117 117 117 11	P( 12.2.22 12.207 12.232 14.153 12.017 12.932 14.163 14.178 1 0000000000000000000000000000000000	PI /PN 7.86286 0.86180 9.86357 9.99915 3.89076 7.91406 1.0713 1.0739 PATION FAN PI /PN 1.0713 1.0709	0.21110 0.21092 0.21136 0.2 454 0.21891 0.77372 0.2450 0.24407 NCZZLE FAR 0.74596 0.24407	0.29597 0.29561 0.29621 0.34272 0.30554 0.34343 0.34343	-!.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
107 117 112 122 127 137 142 157 157 2400111043 157 250 MORD	PI 12.272 12.207 12.207 12.232 4.153 17.017 12.937 14.183 14.178 1 PRESSUPE N 14.183 14.179 PRESSUPE N 14.183 14.179	PI /PN 7.86286 0.86180 9.86357 9.99916 3.91496 1.0713 1.0739 PI /PN 1.7713 1.0709 ATION . FAN PI /PN PI /PN PI /PN	0.21110 0.21092 0.21136 0.2 454 0.2 456 0.2 450 0.2450 0.24407 NCZZLE FLAP 0.74506 0.74506 0.74506	0.29597 0.29561 0.29621 0.34272 0.30554 0.34345 0.34333 PL /PTP 0.34345 0.34333	-!.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
200 HORD 107 117 117 1122 127 137 142 157 157 2400111093	P( 12.272 12.207 12.207 12.232 14.153 17.017 12.907 14.163 14.179 1 PRESSURE R 14.179 1 PRESSURE R 14.179 1 PRESSURE R 14.179 1 PRESSURE R 14.183 14.183	PI /PN 7.86286 0.861PN 9.86357 7.99915 3.89076 7.91496 1.0339 ATION FAN PI /PN 1.0339 ATION FAN PI /PN 1.0309 ATION FAN PI /PN 1.0309	0.21110 0.21092 0.21136 0.2 454 0.21891 0.77372 0.2450 0.24407 NCZZLE FAR 0.74596 0.24407	0.29597 0.29561 0.29621 0.34272 0.30554 0.3453 0.34333 PL /PTP 0.34333	-!.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
VID WORD 107 112 122 127 137 142 157 157 24001710N3 157 20 WORD 67 72	PI 12.2.22 12.207 12.232 14.153 17.017 12.947 14.163 14.179 1 PRESSUPE R 14.163 14.179 1 PRESSUPE R 14.163 14.173 14.163 14.163 14.163 14.163 14.163	PI /PPO 1.86286 0.86180 2.86357 9.29915 0.89076 1.9713 1.0739 PATION FAN PI /PPO 1.7713 1.07309 PT /PPO 1.7713 1.0713 1.0713	01 /PTF 0.21116 0.21072 0.21072 0.21136 0.2 454 0.21871 0.7372 0.2450 0.74407 PT /PTF 0.24506 0.24506 0.24506	0.29597 0.29561 0.29621 0.34272 0.30554 0.34345 0.34345 0.34333 PL/PTP 0.34345 0.34333	-!.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000	
VID WORD 107 112 122 127 137 142 157 157 24001710N3 157 20 WORD 67 72	PI 12.2.22 12.207 12.232 14.153 17.017 12.947 14.163 14.179 1 PRESSUPE R 14.163 14.179 1 PRESSUPE R 14.163 14.173 14.163 14.163 14.163 14.163 14.163	PI /PPO 1.86286 0.86180 2.86357 9.29915 0.89076 1.9713 1.0739 PATION FAN PI /PPO 1.7713 1.07309 PT /PPO 1.7713 1.0713 1.0713	01 /PTF 0.21116 0.21072 0.21072 0.21136 0.2 454 0.21871 0.7372 0.2450 0.74407 PT /PTF 0.24506 0.24506 0.24506	0.29597 0.29561 0.29621 0.34272 0.30554 0.34345 0.34345 0.34333 PL/PTP 0.34345 0.34333	-!.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
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NO MORD  107  112  122  127  137  142  157  >	PI 12.2.22 12.207 12.232 14.153 17.017 12.947 14.163 14.179 1 PRESSUPE R 14.163 14.179 1 PRESSUPE R 14.163 14.173 14.163 14.163 14.163 14.163 14.163	PI /PN 7.86286 0.86180 9.86357 9.29915 0.89076 7.91496 1.0733 1.0733 1.0733 1.0733 1.0733 1.0733 1.0733 1.0733 1.0733 1.0733 1.0733	0.21116 0.21092 0.21136 0.2 454 0.21691 0.77372 0.2450 0.24407 NOZZLE FLAP 0.74506 0.74506 0.24506 0.24506	0.29597 0.29501 0.39554 0.34272 0.30554 0.3455 0.34333 PL/PTP 0.34333 CATION QL/PTP 0.34345 0.34345 0.34345	-!.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000	
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200 HORD 107 117 112 127 137 142 157 157 200 HORD 157 200 HORD 67 72 200 HORD 67 72 200 HORD 67 72	P( 12.2.22 12.207 12.232 14.153 12.017 12.942 14.163 14.178 1 0000000000000000000000000000000000	PI /PN 7.86286 0.86180 9.86357 9.99976 3.99976 3.91406 1.0339 PATION FAN PI /PN 1.0309 ATION 90 PI /PN 1.0313 1.0313 ATION 90 PI /PN 1.0313 1.0313	PI / PTF 0.21110 0.21092 0.21136 0.2 454 0.21891 0.773/2 0.2450 0.2450 0.74506 0.24607  PI / PTF 0.24506 0.24506 PI / PTF 0.24506 PI / PTF 0.24506 PI / PTF 0.24506	0.29597 0.29561 0.29621 0.34272 0.30554 0.34345 0.34345 0.34333 PL/PTP 0.34345 0.34333 CATION PL/PTP	-!.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
107 117 112 122 127 137 142 157 157 20011110N3 157 20011110N3 67 72 20011110N3	PI 12.2.22 12.207 12.232 14.153 17.017 12.943 14.178 1 PRESSUPE R 14.183 14.179 1 PRESSUPE R 14.183 14.179 1 PRESSUPE R 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 14.183 1	PI /PN 7.86286 0.86180 9.86357 9.99915 0.89076 7.91496 1.0713 1.0739 PI /PN 1.0713 1.0713 1.0713 1.0713 1.0713 1.0713 1.0713 1.0713 1.0713 1.0713 1.0713	01 /PTF 0.21110 0.21092 0.21136 0.2 454 0.21891 0.77372 0.2450 0.74407 PT /PTF 0.24596 0.24696 FG SHRCHIN INC	0.29597 0.29501 0.39554 0.34272 0.30554 0.3455 0.34333 PL/PTP 0.34333 CATION QL/PTP 0.34345 0.34345 0.34345	-!.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000	

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NASA-EEHI	S 28FL [4]	MARY PATA	07/07/79	CADRETT	REC 10/07/79 03:32:17.2	### ### ### ### ### ### ### ### ### ##
>4991T109	INT PRESSURE	PATIOS . PRI	MAPY PING			
		·				The state of the s
IVO HODO	PL	PI / PO	PL/PTC	PE /PTP	X /DMAX	
32	71.737	1.5477	7.34111	0.53949	0.43200	
3.7	17.4/10	1.2421	C-27367	0.43274	) <b>.</b> 53900	<i>!</i>
47	17.41)	1.2570	0.27694	0.43753	7.62900	•
.52	11.696	11. RZ547	J. 19197	2.29769	_ 3.72700	The first term of the state of
>400171004<	IAL PRESSURE	PATTOS . FLO	M SOLITTEP I	1.0.		
NO HORD	PL	PI /PO	PLIPTE	PL/PTP	X/DMAX	
62	13.577	0.95826	9.21113	0.33386	0.42200	
97	2,3296	0,65629	0.14475		J.67C00	
>40717100	Al POFSSIPE	RATIOS . FLO	w spiltten r	·- D-		
					•	· · · · · · · · · · · · · · · · · · ·
VD WORD	PL	PI /PN	PL/PTF	PL/PTP	X/DMAX	
77	27.753	1.9585	0.43151	0.68235	0.50800	
# Z	13,322	2, 94025	0.20716	0.32758	0.58300	
92	14.198	1.0013	0.22062	0.34887	0.67000	
>APPITION	AL PRESSIME	RATIOS , FUE	CTCP SHPPUD		ير مستقديد و د م يو	
	•	PI /P(1		01 (0.70	Danie Di Communication de la Communication de	and the second s
VD WOPO	PE		P1 / P7F	OL /PTP	X/DMAX	
107	12.1.76	0.85938	0.18934	0.29941	0.62400	
112	12.176	0.85938	0.18934	0.29541	0.83000	
122	12,196	7.86905	0.18959	0.29966	0.56000	The second to the second termination of the
127	14.159	0.99927	0.22015	0.34813	1.0900	
137	12.512	0.88304	0.19455	0.30765	1.2200	and the second of the second o
147	12.947	0.99670	0.19977	0.31590	1.3500	
-40014 lov	M PRESCURE	44105 - 600	FORDY THET			
VI HUD U	PŁ	የኒ / የባ	PL/FTF	PL /PTP	X/DMAX	The transfer of the second sec
107	12.174	0.85934	0.18934	0.25941	-1.0000	
	12.176	() P533R	9.19534	0.29941	-X.0000	THE REPORT OF THE PARTY OF THE
		0.99922 0.99922	2.1905)	0.29966	-1.0000	
122	13-196		0.27015	0.34*13	-1.0000	
127	14.159					
127	12.512	O. 89304	0.19455	0.39765	-1.0000	and the second s
122 127 127 127	14.159 12.512 12.965	0.89304 0.93570	0.12277	590 آجون	-1.0000	
122 127 137 147 152	14.159 12.512 12.682 14.199	0.89304 0.93573 1.9013	0.19977 0.77962	0.2[590 3.34887	-1.0000 -1.0000	
122 127 127 142 152	14.159 12.512 12.965	0.89304 0.93570	0.12277	590 آجون	-1.0000	
122 127 127 142 152 157	14.159 12.512 12.662 14.189 14.199	0.89304 0.93573 1.9013	0.19977 0.72962 0.27067	0.21590 3.34887 0.34887	-1.0000 -1.0000	
122 127 127 147 152 157 2601[7][08	4.159 12.612 12.622 14.199 14.198	0.89304 2.93573 1.0013 1.0013	0.12077 0.72062 0.22062	0.21590 3.34887 0.34887	-1.0000 -1.0000 -1.0000	
122 127 127 147 152 157 >ADDIT TON	12:-159 12:-112 14:-149 14:-149 14:-149	0.89304 2.93573 1.0013 1.0013 PATION FAR	0.19977 9.72962 0.22062 F NOZZLE FIAR	0.21590 3.34887 0.34887	1.0000 -1.0000 -1.0000	
122 127 127 142 142 152 157 >ADDIT TON VO MORD	4-159 12-512 12-612 14-189 14-188 Pt 14-188	0.89304 0.93573 1.9013 1.9013 FATION FAR 91/PD 1.0013	0.12077 0.72062 0.22062 1 MOZZLE FLAN	0.2159G 3.34887 0.34887 Pt /PTP 0.34887	*/DMAY -1.0000	
117 127 127 127 147 147 157 2457 2457 2457 2457 2457	12:-159 12:-112 14:-149 14:-149 14:-149	0.89304 2.93573 1.0013 1.0013 PATION FAR	0.19977 9.72962 0.22062 F NOZZLE FIAR	0.21590 3.34887 0.34887	1.0000 -1.0000 -1.0000	
122 127 147 147 157 157 2ADTT TON VO MORT	12-137 12-122 12-144 14-148 14-148 14-148 14-148 14-148	0.89304 0.93573 1.9013 1.9013 FATION FAR 91/PD 1.0013	0.12077 0.72062 0.22062 0.22062 0.22062 0.22062	0.159G 3.34887 0.34887 Pt /PTP 0.34887 0.34887	*/DMAY -1.0000	
122 127 147 147 152 152 157 200 HOPD 157 157	12-137 12-122 12-144 14-148 14-148 14-148 14-148 14-148	0.89304 2.93573 1.9913 1.9913 PATTON FAR 9L/PO 1.9913	0.12077 0.72062 0.22062 0.22062 0.22062 0.22062	0.159G 3.34887 0.34887 Pt /PTP 0.34887 0.34887	*/DMAY -1.0000	
122 127 147 147 157 157 200 HOPO 157 157 157	12.159 12.12 12.12 14.149 14.149 14.148 14.148 14.148 14.148 14.148	0.89304 0.93573 1.0013 1.0013 FATION FAR 9L/PD 1.0013 1.0013 1.0013 1.0013	0.27062 0.27062 0.27062 0.27062 0.27062 0.27062 0.27062	0.259G 3.34887 0.34887 0.34887 0.34887	1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
122 127 147 147 157 157 200 MOPO 157 2400 IT IOP WO MOPO 167	12-159 12-12 12-12 14-149 14-149 14-146 14-146 14-146 14-146	0.89304 0.93573 1.9013 1.9013 PATION FAR 91/PD 1.9013 PATION - 20	0.19077 0.77062 0.27062 0.27062 0.27062 0.27062 0.65 SHPDOM I	0.159G 3.34887 0.34887 0.34887 0.34887	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
122 127 147 147 157 157 200 HOPD 157 200 HOPD 167 177	# 159 12-512 12-62 14-199 14-199 14-198 14-198 14-198 14-199 14-199 14-199	0.89304 2.93573 1.9013 1.9013 1.9013 PATION FAR 91/PO 1.9013 PATION - 20 PATION - 20 1.9010	0.19077 0.77062 0.27062 0.27062 0.27062 0.27062 0.27062 0.77054 0.27054	0.159G 3.34887 0.34887 0.34887 0.34887 0.34887 0.34887	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
122. 127 147 147 147 157 157 200 UNPO 157 157 200 UNPO 167 177 177 200 UNPO 207 207 207 207 207 207 207 207 207	12.159 12.12 12.632 14.189 14.188 14.188 14.188 14.188 14.188 14.188 14.188 14.188 14.188 14.188 14.188	0.89304 2.93573 1.9013 1.9013 1.9013 PATION FAR 2/PD 1.9013 PATION . 20 PATION . 20 PATION . 20	0.19077 0.77062 0.27062 0.27062 0.27062 0.27062 0.27062 0.77054 0.77054 0.77054	0.159G 3.34887 0.34887 0.34887 0.34887 0.34887 0.34875 0.34875	-1.0000 -1.0000 -1.2000 */DMAY -1.0000 -1.0000 -1.0000 -1.0000	
122 127 147 147 157 157 2457 157 2457 247 247 247 247 247	12.159 12.12 12.12 12.12 14.199 14.198 14.198 14.198 14.198 14.198 14.198 14.198 14.198 14.198 14.198 14.198 14.198	0.89304 0.93573 1.9013 1.9013 PATTON FAR 01/PO 1.9013 PATTON 20 1.9010 1.9010 1.9010 1.9010 1.9010 1.9010 1.9010	0.19077 0.77062 0.27062 1.W077LE FLAD 0.27062 0.27062 0.77063 0.77054 0.27054 0.27054	0.2159G 3.34887 0.34887 0.34887 0.34887 0.34887 0.34887	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
122. 127 147 147 147 157 267 200 HOPD 167 157 200 HOPD 167 177 277 200 HOPD 167 177	# 159 12-512 12-62 14-189 14-189 14-186 14-186 14-196 14-197 14-197 14-193	0.89304 0.93573 1.0013 1.0013 1.0013 1.0013 1.0013 1.0010 1.0010 1.0010 1.0010 1.0017	0.19077 0.77062 0.27062 1.27062 0.27062 0.27062 0.77062 0.77063 0.77054 0.27054 0.27054 0.27054	0.34887 0.34887 0.34887 0.34887 0.34887 0.34887 0.34887	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
122. 127 127 142 152 152 153 VO WOPD 155 157 VO WOPD 167 177 177 VO WOPD 167 177 VO WOPD 177 V	PI 14-193 14-179	0.89304 0.93573 1.9013 1.9013 PATTON FAR 01/PO 1.9013 PATTON 20 1.9010 1.9010 1.9010 1.9010 1.9010 1.9010 1.9010	0.19077 0.77062 0.27062 0.27062 0.27062 0.27062 0.67062 0.77054 0.77054 0.77054 0.77054 0.77054	0.2159G 3.34887 0.34887 0.34887 0.34887 0.34887 0.34887	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	

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>+>>17.17.1691	. 22555105	P*1105 . PR1					
22 1 1 1 1 1 1 1 1		e interpretation			· · · · · · · · · · · · · · · · · · ·	i de la la pagina più parti desaria di 1920 i	morphone des comitats and conditions of defer to taking a terminal property of the
INU MUBU	PI	PĮ / PD	PL/PTF	~L /P TP	<b>米/印牌各发</b>	7	
37	21.545	1-5227	0.37257	0.53867	G.43200	•	
37	17.314	1. 22 27	9.74347	0.43271	9 <b>.53006</b>		
47	17.513	1.7375	7.74614	5.4775A	J. 62430		
.52	12.128	<b>).</b> 65006		0.30059	J. 72730		
PROFITEGRA	L PPESSUPE	PATIOS . FLO	W SPLITTER I	.D.			
WD WORD	PL	PL/PO	PL/PTF	PL/PTP	y/DHAK		
£2	13.342	0.94394	U.18757	1.37247	J.42200		
<u> </u>	<u> 7.1659</u>	0.64779	0.12685	0.22906	0-67000		Mary and Transaction of the Control
MOI TICOA	L PPESSUPE	PATIOS . FLO	W SPLITTER O	- 9-		a yanga d	
IAD HOBU	PL	PL/PD	PL/PTF	PLIPTP	F/DMAF		
77	30.419	7-1640	9.43942	0.76520	9.50500		
F2	14.659	1.0353	0.20592	0.36609	0,50300		
97	14.174	1.0017	0.19425	0.35422	a.e.7000		
SADDITIONS	E PRESSUPE	PATINS . FJF	CTEP SHEDING		terior y to the window of	The same of the second	en and the second of the second of
IVD VORD	PL	PI / PG	PL /PTF	P1 /P1P	Y/DMAY		<del>-</del>
107	_12.353	0.85395	0.16985	0.30196	0.62400		
112	12. 369	0.85289	7. 16964	0.30159	D-93000		
122	12.1/19	9-65572	9-17029	U. 30259	G. 96 390		
127	14.139	0.49725	0.19875	0.35334	1.0900	· · · · · · · · · · · · · · · · · · ·	to the part of the contract of
137	12.438	9-87905	0-17495	0-31084	1.2200		
142	12.753	3.90133	0.1792#	0.31771	L. 3510	de la la communicación de la	the control of the co
>40017 JCH	- sectime	<u> </u>	CACON 10152				
AL MUND	PL .	PL / PT	PI /PTF	PE /PTP	I/DMAX	والمستقد والم والمستقد والمستقد والمستقد والمستقد والمستقد والمستقد والمستد	مع المدار والأهاب المعاد المهدالية المهدالية المعادية والمعادية وا
137	12-083	0.85395	ű. 14985	0-30196	-1-9000	•	*
iiz 🔪	12.768	0.8528G	0.16964	0.30159	-3. 1300		and a state of the segrence of the second of
122	12.179	J. #5572	2.17029	0.30259	-1.0290		
127	14.179	0.99925	0.19875	0.35774	-1.0000	· · · · · · · · · · · · · · · · · · ·	<del></del>
127	12-638	0.8790*	9.17485	3.319-4	-1.0000		
147	12.753	7.90133	9-17978	0,2(471	-1.0000	a an arrangement	was a ser and an error of the contract of
167	14.164	1.0010	0.19419	7.35397	-1.0000		
157	14.1/9	1.9916	n.ingia			war and a reference	and the second of the second of
				0.35439	-1.0000		
אריון דורינגל	i beeclibe	BUILDS FAR	**************************************				
YO VERO	Pf	PI / Pf i	PIPTE	PL /PTP	Y/DMAY	- Anne	**
167	14.244	1.9010	X 0. 13910	0.35397	-1.0000		
1=7	14.169	1.0015	19019	0.75406	-1.0000	•	••
>40 71 ¥ 1096	PPFSSIPF	1110 . 20	DEG SHEETING T	PEATION			
	PL /	PE / PO	74 / PT F	Q1 /07P	*/D#AX	e namen e e e e	
AU Muba	14.159	1-0014	9.1951#		-1.0000		
		1-0019	7.19617	n*3253 32706	-1.0000		
iyn wnpn ·167 ·172	14.284						
167		Petine , 40	Dec siprim T	PERTIPE	\		
·167 ·172		PETINE . 40			EMAR		
-167 -172 -280 317 1090	DOES (1905		NEG TIPETIN T M/STE 3.13046	PL/PTP	x/max -1.00mg		

7	NA SA-I FW	s section	IHAPY DATA	07/67/79	TESCOAS	REC 13/07/79	C3:35: 31.192	FAC ENGXI		1070
	>tūn jā Ind	al poeceilar	PATIOSDPI	MADA WERE					THE PERSON NAMED IN THE PE	
-	AVD MOED	PL	PJ /PG	M /PTF	PL /PTP	y/DMAY				
	37	21.147	1.4974	9.27161	0.53911	0.43700				
	37	17.735	1.2722	G-21#23	J.432F3	J.53JUB				
_	47	17.210	1.7167	0.22685	0.43505	0.62500				
	52	11.429	2.89652		29037	0.7270ú	The second secon			
^ ,	>ADDIT IDN	AL PRESSUPE	PATIOS . FLO	W SPLITTEP	r. D.					
	AVD HOPT	PL	PL/PO	PL/PTF	PL/PTP	X/DM4X				
	42	13.109	0. 92674	0.16823	0.33366	0.42200				
		9-0012	0.63635	2-11551	0-22911	J_67000		·····		
	>400111004	AL PRESSUPE	PATIOS . FLO	W SPI ITTER I	P. D.					
		. PL	PL/PN	Pt / PT F	PL / PTP	y/DMAX			narra r	
_	77	73.417	2.3625	0.42885	0.25059	0.50500				
_	92	16.030	1.1332	2.22571	0.49401	<u> </u>				
	92	14.154	1.0314	0.19177	0.36053	0.67030				
	>Anni Tinn	AL PRESSUPE	MATTUS . FJE	CALA ZHOUND		<b></b>		an include the second s		
$\widehat{}$	AVP WOFD	PL	PL /PD	PE / PTF	PL /PTP	X/DPAY				
_	107	11.053	<u> </u>	9.15211	0.30171	<u> 9.62409</u>				
	112	11.403	9.83444	0.15147	0.30043	).#3000				
3	127	12,003	0.84959	0.15404	0.30553	3 <b>,</b> 96000				
	127	14.124	13,00952	J. 19126	0.35951	1.0900				
	137	12.319	9. 870A7	0.15709	0.31355	1.2200				
	147	12.534	0.89315	0.16213	0.37157	1.3500				
-	-	AL BRESSIME	MATTOS , FO	ERCON INCT						
	AVE HEPE	PL	PI / PO TO	PI /PTF	PL /PTP	X /DHA Y		•		
	-107	11.853	0.23798	0.15211	0.30171	-1.0000				
	-11?	11.803	0. 73444	0.15147	0.30043	-2.1000				-
	-127	12.073	1). P4859	0.15494	0,30553	-1.0000				
	-127	14.174	0.99952	J. 19126	0.35051	-1.3000				
	-127	1 319	0.87087	0.15805	0.31255	-1.0000				
	-142	12.6	0.80315	0.16213	0.2157	-1.0200	*			
	-152	14-150	1.0)10	0.19171	0.36040	-1.3000				
	-157	14.159	1.0010	0.1-171	0.76040	-1.0000				
	>40717108	AL PRESSURE	PATER . FAR	HOTTLE FLA	P					** **
	AVO HORD	Pl	PI./PI	INTE	PL /PTP	x/PMAX	•	no e e entre e e entre e e e e e e e e e e e e e e e e e e	and the second s	-
	-157	14.159	1.0310	0.19171	0.36940	-1.0000				
-	-1=7	i4.159	1.0010	19171	0.76040	-1.0000		The second secon	•	
	>A991710N	AT PRESSIPE	PATIOS , 20	LEC SHOUND	OCATION					
-	AVD HOPD	•1 /	94 / 90	PI /PTF	PE /PTP	X/DMAX			make and make a significant of	•
	-167	14.158	. 1.0010	2-19171	26040	-1.3000				
_	-177	14/64	1.0026	0.18164	0.34027	-1.0000				
	>2071110	P	PATING . AO	HER SHERMA	TOTATION -					
_	AVD HOPD	PI	P[ / P'')	OF L	PL /PTP	XAMAX				
	-192	14.174	1.0735	0.12714	0.36129	-1.0300				
	167	14.174	1.0025	0.18214	0.34129	-1.0000				
	<b>-</b>	170177	1011111	17-17-51"	134 25 17 7	-1.0000				

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91E <b>3</b>	7LE 1	ver				DAM RE		rtno M	n <b>yze</b>	MONEL C				Mark days days	and the same of th		•
FLI	GHT F	PHOITI		·····		SIJOFO					•		***************************************				
		CNFISH				01								The same of the sa	no de un c <b>umung</b> de gayran actes <del>antiques ac</del> tes gay	alika sahirin na anang sa	
-		MOZZLE LTTEZ	P. 13()			SPEET !											
	HQ71					SHIPT						Market III I					
		LPNST															
£ .3F	र इंग्लि	IMPEL	DPENING														
							andre e										
*85	al i	TF/PTP	PTF/PC	PTP/PN	OMEGA	bli/blt	rof	CDP	CF1	FTAL E	TALLINT	CFPL	CFP?	F <b>9</b>			
371 1.	96.4	2.30	19.75	8.57	0.100	0.134	1.003	0-979	0-9749	0.9749	0.5781	0_9781	0.9786				
572 1.	957	2.32	22.08	9,53	0.000	C.132	1.004	0.091	2.9832	0.9802	0.9930	0.0830	0.9835	1.4942	· · · · · · · · · · · · · · · · · · ·		
373 1. 374 1.		2.32		10.70							0.9853						
377 1.		2.33		11.64							0.9856						
974 1.	960	2.33	24.04	10.72	0.070						C. 9879					***************************************	
079 1.		2.31	22-18		0.000						0.9467						
383 1. 381 1.		2.31		12.62							0.9844						
387 1.		2.31									0. 0445						
743 1.		1.99		10.03							0.9962						
)84 1.   995 1.		2.31 2.31	19.67		0.014						0.9847						
484 T.	959	2.50	19.89	7.66	0.070	0.133	0.472	0.980	0. 9943	0.9812	0.9847	7, 0074	3,9483	1.5000			
C87 1.		2.00		11-14							0.9890				The second secon		
DAR 1.		2.31	22.46	9.72	0.019						0.9973						
107 1.	<b>56 1</b>	2.03	24.48	12.46	0.016						0.000						
3°L 1.		2.33		10.67							0.9931						
093 1.		2.59	24.64	13.53	0.379						0.9941						
796 1.	559	2.33	77.34	11.75	0.019						0. 9974						
195 1.		2.69		10.52							0.9921						
396 l. 097 l.		2.32 2.60		12.87							0.9912						
Jea I.		2.33		12.87							0. 9929						
Joe 1.		2.33		11.60							0.9935						
199 1.		2.32	24.41 22.41	13.71	0.019						0.4922						
132 1.		2.31	19.56		0.019						0.9962						
	_								•						•		

a graph statements in the second of

	4427-( EA1	S PPFLIM	INARY DATA	36/19/79	CADDETI	REC 10/11/79 03:33:24.247 FAC RN6H1 PGM CR34 ROG 1971
-	" > You I k I w	AL PRESSURE	PATIOS . PRI	MAPY PLUG		
	AVD HOFD	PL	PE / PO	PL /PTF	PL /PTP	X/DMAX
	32	12.341	7. 1950	0. LA709	C.43106	0.43200
	37	6.5331	1. 9566	0.000047	0.22620	0.53000
	47	8.7479	2.4702	0.12504	0.28811	0.62900
	52	9.2729	2.4777	0.12542	0.289 +7	0.72700
	>ADDITIONAL	AL PRESSURE	RATIOS . FLO	W SPLITTEP 1	. 0.	
	AVD WOPD	PL	PL / PO	M /PTF	PL/PTP	X/DMAX
	42	9.3925	7.8130	0.14240	0.32808	0.42200
	47	6.5931	1.9746	0.005957	0.23030	0.67000
	>+natt tun		PATIOS , FED			
			•			
	AVE HERD	PL	PI /PN	PL/PTF	/PL/PTP	X/OMAX
	77	26.851	P. 0416	0.49707	0.937#9	0.50800
	P?	13.235	3, 96 38	9,20065	0.46230	0.58300
	e.5	3.5823	1.0729	0.054311	0.12513	0.67000
	>ADDITION		RATTOS . EJF	CTOP SHPOUR	· · · · · · · · · · · · · · · · · · ·	
	AVD HORD	PL	PL /PD	PL/PTF	PIZPTP	X/DMAX
	107	3.9825	1.1927	0.060379	0.13911	0.62490
	112	3. 9275	1.1763	0.059544	0.13719	0.83000
	1.72	3.8475	1.1523	0.056331	0.13439	0.56000
	127	3.5723	1.2629	0.054159	0.1247#	1.0700
	127	3.2621	g. 0769A	0.949456	0.11395	1.2700
		1.2171	0.96350	0.047774	0.11237	1. 3500
	14?	70 28 18	ひってのごつひ	£.0 0.4 £ 1 1.4	A# 1 15 31	*****
					V411231	
_	-1	nt-2025/497	****** ***	<del>( 0.007 - 1.44 * *</del>		
~	VALUE LANG	PL	PL/PO	PL/PTF	ej /ete	x roman
~	avi voku	PL 3.9825	PL/PN 1.1927	PL/PTF 0.060378	Pi /P†P 0.13911	x/nmixt .
_	AVI UNEN -107 -112	PL 3.9825 1.9275	PL/PN 1.1927 1.1763	PL/PTF 0.060378 0.059544	PI /PTP 0.13911 0.13719	X/NM3/X -1 5000 1.0000
~	AVI UNEN	PL 3.9825 1.9275 3.8675	PL/PN 1.1927 1.1763 1.1523	PL /PTF 0. 060378 0. 059544 0. 059331	0.13911 0.13719 0.13719	X/DM3A -1.5000 -1.0000 -1.0000
_	AVN YORD -107 -112 -122 -127	PL 3.9825 1.9275 3.8675	PL/PD 1.1927 1.1743 1.1523 1.0699	PL /PTF 0. 06037N 0. 059544 0. 059331 0. 054159	0.13911 0.13719 0.13639	X/Dmixt -1 5000 1.0000 -1.0000 -1.0000
_	AVI UNEN	PL 3.9825 1.9275 3.9675 5773 3.4621	PL/PN 1.1927 1.1763 1.1523	PL /PTF 0. 060378 0. 059544 0. 059331	0.13911 0.13719 0.13639 0.13639 0.12634	X/DM3A -1.5000 -1.0000 -1.0000
_	AVN YORD -107 -112 -122 -127	PL 3.9825 1.9275 3.8675	PL/PD 1.1927 1.1743 1.1523 1.0699	PL /PTF 0. 06037N 0. 059544 0. 059331 0. 054159	0.13911 0.13719 0.13719	X/Dmixt -1 5000 1.0000 -1.0000 -1.0000
_	AVI MORN -!n7 -!n7 -112 -122 -127 -127	PL 3.9825 1.9275 3.9675 5773 3.4621	PL/PD 1.1927 1.1743 1.1523 1.0699 0.97698	PL/PTF 0.060378 0.059544 0.0595431 0.054159 0.049456	0.13911 0.13719 0.13639 0.13639 0.12634	X/DM34 -1-3000 -1-0000 -1-0000 -1-0000 -1-0000
_	AVI YORN -107 -112 -122 -127 -127 -142	PL 3. 9825 1. 9275 3. 9675 3. 9675 3. 9273 3. 92171	PL/PD 1.1927 1.1743 1.1523 1.0699 0.97698 0.94356	PL/PTF 0.06037R 0.059544 0.059331 0.054159 0.04945 0.0494774	0.13911 0.13719 0.13639 0.12639 0.12637	x/nmix -1-2000 -1-0000 -1-0000 -1-0000
	AVT YORN -!07 -!12 -!27 -!27 -!27 -!42 -!67	PL 3. 9825 1. 9275 3. 8675 3. 8675 3. 21 3. 21 3. 5473 3. 5473	PL/PD 1-1927 1-1763 1-1523 1-3659 0-97698 0-96350 1-9624	PL/PTF 0.06037R 0.059544 0.059331 0.054159 0.04945 0.049774 0.053780 0.053780	0.13911 0.13719 0.13439 0.12437 0.12437 0.1237 0.12391 0.12391	X/DMAX -1.5000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	AUT 11000 -107 -107 -127 -127 -127 -127 -152 -152 -157	PL 3. 9825 1.9275 3.9675 5.773 3.1621 3.2171 3.5673 3.5673	PL/PN 1-1927 1-1763 1-1523 1-3659 0-97698 0-96356 1-9624 1-9624	PL/PTF 0.06037R 0.059541 0.054159 0.04456 0.04477 0.0537R0 0.0537R0	0.13911 0.13719 0.13719 0.13439 0.12474 0.12474 0.12391 0.12391 0.12391	X/Dmid -1.5000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	AUT VIORO -107 -112 -127 -127 -127 -142 -162 -167 510777 1740	PL 3. 9825 1. 9275 3. 8475 1. 5773 3. 4621 3. 2171 3. 5473 1. 5473	PL/PD 1-1927 1-1763 1-1523 1-3659 0-97698 0-96350 1-9654 1-9624 PATICS FAN	PL/PTF 0.06037R 0.059544 0.059544 0.059545 0.044159 0.049456 0.048774 0.053780 PINTYLE FLAP	0.13911 0.13719 0.13739 0.13439 0.12474 0.11495 0.11237 C.12391 0.12391	X/OMAX -1.5000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	AUT 11000 -107 -107 -127 -127 -127 -127 -152 -152 -157	PL 3. 9825 1.9275 3.9675 5.773 3.1621 3.2171 3.5673 3.5673	PL/PN 1-1927 1-1763 1-1523 1-3659 0-97698 0-96356 1-9624 1-9624	PL/PTF 0.06037R 0.059544 0.059544 0.059541 0.054159 0.049456 0.048774 0.053780 PINZZIJ FLAP PL/PTF 0.053780	0.13911 0.13719 0.13719 0.13439 0.12474 0.12474 0.12391 0.12391 0.12391	X/NMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	AUT UNEN -107 -112 -127 -127 -127 -142 -162 -167 -167 -167 -167 -167	PL 3. 9825 1. 9275 3. 9675 3. 9675 3. 9673 3. 9673 3. 9673 4. PRESSIRE PL 3. 5473	PATION FOR PLANT PARTIES FAN PARTIES	PL/PTF 0.060378 0.059544 0.059544 0.054159 0.049456 0.048774 0.053780 PHOYYLF FLAP PL/PTF 0.053780 0.053780	PI /PTP 0.13911 0.13719 0.13439 0.12474 0.12495 0.12391 0.12391 0.12391 0.12391 0.12391	X/0mid -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	AND TORN -107 -112 -127 -127 -127 -142 -162 -167 -167 -167 -167 -167	PL 3.9825 1.9275 3.9625 3.9675 3.5673 3.5673 3.5673 3.5673 4. PRESSIME PL 3.5673 3.5673	PATINA FOR PATINA PATIN	PL/PTF 0.06037R 0.059544 0.059544 0.057931 0.054159 0.049456 0.048774 0.053780 PHOTEL PLAP 0.053780 0.053780 0.053780	0.13911 0.13719 0.13739 0.12474 0.12474 0.1237 0.12391 0.12391 0.12391 0.12391	X/N#AX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
_	### ##################################	PL 3. 9825 1.9275 3.9475 5773 3.9475 3.9473 3.9473 3.5473 41 PRESSIRE PL 3.5473 41 PRESSIRE	PAYING FRANCE PAYING PAY	PL/PTF  0.06037R 0.059544 0.059341 0.054159 0.0494%6 0.049774 0.053780 PL/PTF  PL/PTF  PL/PTF	PI /PTP 0.13911 0.13719 0.13439 0.12474 0.12391 0.12391 0.12391 0.12391 0.12391	X/DMAX
_	AVITY (PM) -107 -112 -127 -127 -127 -142 -162 -167 -167 -167 -167 -167 -167	PL 3. 9825 1. 9275 3. 9675 3. 9675 3. 7773 3. 3. 21 3. 21 73 3. 5473 3. 5473 41 PRESSIME PL 3. 5473 41 PRESSIME	PATION FAN PL/PN 1-1927 1-1763 1-1523 1-3659 0-97698 0-96350 1-9624 1-0624 PATION FAN PL/PN 1-0624 PATION 20 PL/PN 1-9639	PL/PTF 0.060378 0.059544 0.059544 0.059541 0.054159 0.049456 0.048774 0.053780 PL/PTF 0.053780 DEC SIMPLOM 1 PL/PTF 0.053780	PI /PTP 0.13911 0.13719 0.13439 0.12474 0.12497 0.12391 0.12391 0.12391 0.12391 0.12391 0.12391	X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	### ##################################	PL 3. 9825 1.9275 3.9475 5773 3.9475 3.9473 3.9473 3.5473 41 PRESSIRE PL 3.5473 41 PRESSIRE	PAYING FRANCE PAYING PAY	PL/PTF  0.06037R 0.059544 0.059341 0.054159 0.0494%6 0.049774 0.053780 PL/PTF  PL/PTF  PL/PTF	PI /PTP 0.13911 0.13719 0.13439 0.12474 0.12391 0.12391 0.12391 0.12391 0.12391	X/0mid -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/0MAX
	AVITY (PM) -107 -112 -127 -127 -127 -142 -162 -167 -167 -167 -167 -167 -167	PL 3. 9825 1.9275 3.9675 3.9675 3.7673 3.5673 3.5673 3.5673 7.5673 41 PRESSURE PL 3.5473 7.5473 1.5473 1.5473	PATION FAN PL/PN 1-1927 1-1763 1-1523 1-3659 0-97698 0-96350 1-9624 1-0624 PATION FAN PL/PN 1-0624 PATION 20 PL/PN 1-9639	PL/PTF 0.06037R 0.059544 0.059341 0.054159 0.0494%6 0.0537R0 0.0537R0 PL/PTF 0.0537R0 DEG SIMPTUM PL/PTF 0.053R56 0.053R56	PI /PTP 0.13911 0.13719 0.13439 0.12478 0.12495 0.12391 0.12391 0.12391 MCAYINH N/PTP 0.12408 0.12408	X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	AVITY IN AVI	PL 3. 9825 1.9275 3.9675 3.9675 3.7673 3.5673 3.5673 3.5673 7.5673 41 PRESSURE PL 3.5473 7.5473 1.5473 1.5473	PATINS - FOR PATINS - RO	PL/PTF 0.060378 0.059544 0.059544 0.059541 0.054159 0.0494%6 0.048774 0.053780 0.053780 0.053780 0.053780 0.053780 0.053856 0.053856	PI /PTP 0.13911 0.13719 0.13439 0.12474 0.12495 0.12391 0.12391 0.12391 0.12391 0.12391 0.12391 0.12391 0.12391	X/Nmax -1,5000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000
	AUTO UNEN	PL 3. 9825 1. 9825 1. 9275 3. 8475 3. 8475 3. 2173 3. 5473 3. 5473 41 PRESSURE PL 3. 5473 41 PRESSURE PL 3. 5473 41 PRESSURE PL 3. 5473 41 PRESSURE	PL/PN 1-1927 1-1763 1-1523 1-3699 0-97698 0-96356 1-0624 1-0624 FAYINS FAN PL/PN 1-0624 FAYINS - 20 PL/PN 1-0639	PL/PTF 0.060378 0.059544 0.059544 0.059541 0.054159 0.049456 0.049774 0.053780 0.053780 0.053780 0.053780 0.053780 0.053856 0.053856	PI /PTP 0.13911 0.13719 0.13439 0.12474 0.12495 0.12391 0.12391 0.12391 PI /PTP 0.12391 MCATYINA PI /PTP	X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	AVIT (1996) -107 -112 -127 -127 -127 -127 -142 -142 -142 -147 -147 -147 -147 -147 -147 -147 -147	PL 3. 9825 1.9275 3.8475 1.5723 3.3421 3.2171 3.5473 3.5473 41 PRESSIME PL 3.5473 2.5473 41 PRESSIME PL 3.5473 3.5525 3.8523 3.8523	PAYING FOR PL/PD 1.1927 1.1743 1.1523 1.3659 0.97698 0.96350 1.0624 PAYING FAN PL/PD 1.0624 1.0624 1.0624 1.0639 PL/PD PL/PD PL/PD	PL/PTF 0.060378 0.059544 0.059544 0.059541 0.054159 0.0494%6 0.048774 0.053780 0.053780 0.053780 0.053780 0.053780 0.053856 0.053856	PI /PTP 0.13911 0.13719 0.13439 0.12474 0.12495 0.12391 0.12391 0.12391 0.12391 0.12391 0.12391 0.12391 0.12391	X/Nmax -1,5000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000

Antinosis-

4A SA -1 EW [ 9	c butfin	THAPY PATA	04/10/79	CADOFII	PEC 10/11/79	03:34:39.759	FAC 97681	PGH C034	RNG 1072
****************	41 PPESSUPE	PATIOS , PP1	MAPY PLUG						
ነለሁ ሳሁኔታ				D: /ATA	X/DMAY				
190 30P9 - 32	P[	P( /P1	PL/PTF	PI /PTP					
47 77	13.436	4.1164	0.18647	0.43212	0,43200				
	7.2938	2.1691	0.09#257	0.22770	0.53000			and the second of the second o	
£7	9.7415	7.7494	0.17455	0.26862	0.67900				
52	9.2665	2.7569	0.12488	0.28941	0. 7270)	Harry Control of the			
>AODITION	LL PRFSSIMF	PATINS . FEE	OW SPLITTER I	. D.			<del>-</del>		and the second second second second
מקחני הע	Pl	PL/PO	PI /PTF	PL /PTP	x /DMA x				
62	10.532	3.1333	3.14193	0.32892	0.42200		A SECTION ASSESSMENT	NAME OF TAXABLE PARTY AND ADDRESS OF TAXABLE PARTY.	
67	7.3909	2, 1989	0, 099606	0.23083	0.67000	***************************************	Variation of the latest and the late		
SAND ET FORK	L PRESSIME	PATINS . FLO	W SPLITTER P	.0.	*				
VO VORD	Pl	PL/PG	PL/PTF (	PL /PTP	X/DMAX				
77	30.58Å	9, 0995	0.41220	0.95523	0.50800		and compare an in the property of the party	e and all company of a section of the company of the company of	tion of the second seco
97	14.92I	4.4391	0.20109	0.46600	0.50300				
27	3.6076	1.6743	3.540621	0.11268	0.67000	<del></del>			
SANDIT INN		RATIOS . FJE			Maria de la compania		pur pro		v nenemen versussiaanskussiaania (iii - ne
					The second second second	where the same and the same and			
AU AULU	PL	PL /PI)	PI / PTF	PL/PTP	X/DMAX				
137	4.5000	1.3414	0.060764	0.14081	0.62400				
113	4.4437	1.3720	0.059847	0.13878	J. 83000			<del></del>	
127	4.3486	1.2937	0.058605	0.13501	0.96000				
177	3,5978	1.0704	0.048486	0.11236	1.0900				
137	3.652	1.0867	0.945225	0.1140	1-2200		alan engle and religion his religion was different to the control of		
147	3.6178	1.0763	0.944756	0-11299	1.3500				
restated	H-brescher	****	to the last to			***************************************			
be much	Pl	PL / PG	"PI_/PTF"	" PI /PTP	×/DHAY				
103	4.5059	1.3414	0.969764	U.140#1	-1.0000		•		
112	4.4437	1. ?220	0.059887	0.13878	-1.0300	same a comment.			
132	4.3496	1. 2937	0.054605	0.13581	-1.0000				
127	3.5078	1.0704	7.348476	1.11236	-1.0000				
137	3.4529	1.0867	0.749228	0.11600	-1.0000				
14?	3.6174	1.0763	0.048756	0.1150	-1.0000		The same of the sa		
14: 152	3.5727	1.0629	0.04#149	3-11158	-1.0000				
196 157	3.5727	1.0629	0.048149	0.1115#	-1.0000		To the second se		
	AT PRESSURE		HUSZIE FLAN			<u> </u>			
NAUN GRI	of	PI /PII	F( /PTF	PL/PTP	X/DHAX		The state of the s		
-157	3.5727	1.0629	X 0.049149	9.11150	-1.0000				
157	3.5727	1.9629	3 UT WI TO	0.11158	-1.0000	**	The state of the second control of the secon		
	II PRESSURE	PATER . 21	गम्द उसलेका ग	TEXTION		7			
SANTITING		91 /911	PI /PTF	EI /PTF	X/DMAX		ي المعادية	contact the process from the contract of the c	The same of the sa
	Pŧ	/ (FI / FI)		0-11158	-1.3000				
ሁስ ሣጣቀብ	PL 3.5722		7.368140	V-44 6 1 75					
LVN YNPN -1f7	3.5722	1.7629	7.348149 0.048149	0.1 N.50	~1.0700				
LVA 4MPA -167 -177	3.5727 3.5727	1.7629 1.7629	0.048149	0.1715m	-1.0000				
LVN 40PN -167 -172 -3ANDITINU	3.5727 3.5727	1.7629 1.7629		0.1715m	-1.0900				
LVA 4MPA -167 -177	3.5727 3.5727	1.7629 1.7629	0.048149	0.1715m	-1.0000 x/MAX	- 1	. SEPARA NA MARINE PROPERTY AND A THE CONTRACT OF	and a second of the second of	Names and the second se
IVO YOPO 167 177 SAUDITION IVO YOMO	3.5727 3.5777 WESSINE	1.7629 1.7629 RATINS . *5	0.048149 DEG SIMMOD E	0.1745s	x/DMAX				
VA 40PA 167 172 SAMBITINA VA 40PA	3.572 <i>3</i> 3.5 <i>2</i> 27 W PPESSURE	1.7629 1.7629 RATHIS = #9 PL/PO	0.048149 NEG SIMORRI ET PL/PTF	0.1345# ************************************					

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Assets the con-

NOSA-LFWIS	. batfini	MARY DATA	0e/10/79	CADDELL	PFC 10/11/79 03	:35:58.690	FAC MEST	PGM C034	New 15 RPG 1073
>40011 [74/	H PRESSURE	RATIOS , PRI	MARY PIUG						
	•								
AND HUBD	PL	PI / PO	ME / PTF	PL/PTP	X/DMAX				
?2	15.54A	4.6199	0.18604	0.43197	7.43200				
17	9.15A1	2.4241	0.097615	C-22ff5	0.53000				
47	10.259	3.3780	0.12795	0.28779	J.62900				
. 52	10.403	3.093#	0.12454	0.24914	0,72700				
>ANDITIONA	IL PRESSUPE	PATINS , FLD	W SPLITTEP T	. D.	-				and the second s
AVD WORD	PL	PI /PO	PI /PTF	PL /PTP	X/DMAX	- · · · · · · · · · · · · · · · · · · ·			
45	11.024	3.5133	0.14148	0.32 <b>85</b> 0	0.42200				
	R.2892	2,4627	0. 799171	0.23027	0.67000				
>Anni Tinuk	IL PRESSURE	PATINS , FLO	M SPLITTER D.	•D• , , , , , , , , , , , , , , , , , ,					Mark A et al. (Automorphis State Control of the Con
40PD	PL	PL /PO		PL/PTP	X/DMAX				
7-	34.261	10.180	0.40995	0.95187	0.50000				
R2	16.798	4. 9912	0.20099	0.46668	0.583 <b>00</b>				
92	3.6094	1.0725	0.943197	0.10028	0. 67000				
>400 IT 1094	L PRESSIME	RATIOS , EJĒ	CTOR SHROUD	* · =	and the second s				
VD WORD	PL	PI,/PI)	PL /PTF	PL/PTP	X/DMAX				
107	5.9863	1.5112	0.060856	0.14130	0.62400				
112	5.0159	1.4904	0.060019	0.13936	Q. 83000				
122	4.9058	1.4577	0.058700	0.13630	0.96000				
127	3.6944	1.0710	0.043127	0.10014	1.0900	***			
137	4.1033	1.2143	0.049058	0.11391	1-2200				
142	4.0699	1.2093	0.048699	0.11307	1.3500				
_		14102 - CO	-						
_							-de-aleman alika kirak a salapa pan pendembelan salah salah		
ane o	PL	M /PO	PI /PTF	PL /PTP	X/OMAX		•		
107	5.0850	1.5112	0.060856	9-14130	-1-0500				
112	5. 1159	1.4904	0.060018	0.13936	-1.0000				
122	4.9058	1.4577	0.258702	0.13630	/-1.0000				
177	26344	1.0710	0.043127	U- 10015	-1.0000				
127	4.1000	1.2183	0.049058	0.11341	-1.0000		· professional and a second contract of the s		
	4.0490	1.2093	0, 048698	0,21307	-1.0000				
152	3.5943	1.0650	0.042888	0.099582	-1.0000				
157	3.5743	1.0650 1.0636	0.042888 0.042828	0.059443	-1.0000 -1.0000				
157 157	3, 5703	i.0636							
157 157 540 51 <b>7 (</b> 044	3, 5703	i.0636	0. C42 #2#						
157 157 SANSYY <b>TOU</b> A VO WORD	3. STO3	1.0636 PATTON FAN	0. C42 #2# HC771E FI 40	0.059443	-1-0000 X/04AX				
-152 -157 545 71 <b>7 764</b> WO WORD -152	3. 5793 L MRESSURE (	PATION FAN	0. C42 828 H0771E FLAD	0.059443 Pl /PTF	-1.3000				
157 340 117 1044 WO WORD 157	3. 5703 L PRESSURE ( PI 3.5943	1.0636 PATER FAN M /PR 1.9650 1.0536	0. C42 #2# HP771E FLAP 1.PTF 0.042888	0.059443 Pt /PTF 0.099582 0.099443	-1.3390 x/pmAx -1.3900				
-  67 -157 	3.5703 IL PRESSIME PI 3.5843 1.5793	1.0636  PATION FAN  PLAN  1.9650 1.0636  RATUR , 20	0, C42 #2# HC771E F1 AP 1 /PTF 9, 9478## 0, 942 #2# DFG CHPTON TI	0.059443 Pt /PTF 0.099582 0.099443	#/DMAX -1.0000 -1.0000				
157 340 317 TONA VO WORD 157 157 340017 TONA VO WOPD	3.5703  IL MRESSURE  PI 3.5743 7.5793  IL MPESSURE	1.0636  PAYTON FAN  PL/P0  1.0650  1.0636  RAYUM 20	O. C42 #2#  HP771E TI AP  1 /PTF  0. 042 #2#  DFG CH#PDG TI  PL/PTF	P1 /PTF 0.099582 0.099443 PCATYON	#/DMAR -1.0000 -1.0000				
157 360 117 TOMA 1400 MORTI 157 360 177 TOMA 140 MOPO 167	3.5703 IL PRESSIME PI 3.5843 1.5793	1.0636  PATION FAN  PLAN  1.9650 1.0636  RATUR , 20	0, C42 #2# HC771E F1 AP 1 /PTF 9, 9478## 0, 942 #2# DFG CHPTON TI	0.059443 Pt /PTF 0.099582 0.099443	#/DMAX -1.0000 -1.0000				
-157 -157 -157 -150 -150 -157 -157 -167 -167	3.5703 IL PRESSURE PI 3.5793 IL PRESSURE PI 3.5793 3.5793	1.0636 PAYTON FAN PLAND 1.0650 1.0636 PLAND 1.0636 1.0650	O. C42 828  HP771E FLAP  1/PTF O. 142 888  DFG SIPPIDE TI  PL/PTF O. 142 828	P1 /PTF 0.099582 0.099443 PTAYYON 1 /PTP 0.099443 0.099582	#/DMAX -1.0000 -1.0000 X/OMAX -1.6000				
AVD WORD -157 -157 ->AAAATTTANA AVD WOPD -167 -172 ->ABATTTTAN	73.5703  PI 3.5843 7.5793  II PPECCURE  PI 3.5793  II PPECCURE  PI 7.5793  7.5743	1.0636  PAYTON FAN  PL/PO 1.0650  RAYIN 20  PL/PO 1.0650  FAYTON RO	0. C42 #2#  HP771E F1 AP  1 /PTF 0. 142 ### 0. 142 ###  DFG SIPPIDE T1  PL /PTF 0. 142 ### 0. 142 ###  DFG SIPPIDE T1	0.059443 P1 /PTF 0.049582 0.069443 PCAYION 1 /PTP 0.099443 0.049582	#/DMAX -1.0000 -1.0000 #/DMAX -1.0000				
-157 -157 -157 -150 -150 -150 -157 -157 -167 -167 -167 -167 -172	3.5703  IL PRESSURE  PI 3.5843 7.5793  IL PRESSURE  PI 3.5793 3.5443  IN PRESSURE	1.0636  PATION FAN  PLAN  1.9650  1.9650  PLAN  PLAN  1.9650  PATION FATION  PLAN  P	O. C42 828  HC771 F F1 AP  I /PTF O. 942888  DFG SIPPUR TI O. 942828 O. 942888  DEG SIPPUR TI PL /PTF O. 942888	0.059443  P1 /PTF 0.099582 0.099443  PTAYINN  1 /PTP 0.099443 0.099582	#/DMAX -1.0000 -1.0000 #/DMAX -1.0000				
-157 -157 -157 -150 -150 -157 -157 -2400111044 -167 -167 -240311104	73.5703  PI 3.5843 7.5793  II PPECCURE  PI 3.5793  II PPECCURE  PI 7.5793  7.5743	1.0636  PAYTON FAN  PL/PO 1.0650  RAYIN 20  PL/PO 1.0650  FAYTON RO	0, C42 #2#  HP771E F1 AP  1/PTF 0, 142 ### 0, 142 ###  DFG SIPPIDE TI  PL/PTF 0, 142 #2# 0, 142 ###  DFG SIPPIDE TI	0.059443 P1 /PTF 0.049582 0.069443 PCAYION 1 /PTP 0.099443 0.049582	#/DMAX -1.0000 -1.0000 #/DMAX -1.0000				

					را با به تعالیم از این این از این
Ners-I ENS	5 PRF1 [4]	INARY DATA	06/10/79	CADDEII	REC 10/11/79 03:36:58,636 FAC 89681 PGS C036 PRG 1076
SAPOITION	AL PRESSIME	PATINS . PPI	MARY PLUG		
			7,4,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7		
AVD HOPD	Pl	Pf / PG	PL /PTF	PL /PTP	K/DPAK
32	17.267	5.134R	0.18559	0.43117	0.43200
37	4.0451	2.6898	0.097222	0.22584	0.53000
47	11.510	3.4728	0.12371	0.28738	0.62900
52	11.545	3.4391	0.17430	0.28875	0.72700
>ADDITION	AL PRESSIRE	PATIOS . FLO	M ZM LAAEN Î	• P•	The second secon
AVD HORD	FL	PI / P/)	PL /PTF	PL /PTP	X/DMAX
£2	13.149	3.9193	0.14133	0.32831	9.42209
67	9.2051	2.7374	0.098941	0.72984	0.67000
>Windle find	AL PRESSURE	RATIOS , FLO	M PACTALEM IN	• 1/•	Service Control of the control of th
AND HUBBI	PL	PL /PII	PL / PTF	PLIPTP	X/DMAX
77	37.620	11.107	0.49436	0.93930	U. 50NU3
P2	18.706	5.5627	0.20106	0.46705	0.5830G
3	3.6075	1.0724	0. 73 8774	0.090073	0.67000
MODITION	il Dafécime	PATINS . FJF	Prof. Supplied.		
AVD WORD	PĹ	PL /PO	PL/PTF	PL/PTP	K/OMÁX
197	5.6441	1.6784	0.060666	0.14092	0.62400
712	5.5740	1.6576	0. 050013	0.13917	0.63000
122	5.4589	1.6734	0.058676	0.13630	3. 96000
127	3.6175	1.0754	0.038883	0.090323	1.0900
137	4.5583	1.3555	0.04#99	0.090325	
142	4.5283	1.3466	0.048673	0.11306	1.2200
<b>4. *</b> €	マッフとおう	1. 3400	U+194F0 15	U+11390	50 - 77W
<del>&gt;145(17</del> 04)	-	PRINC - COR	EVIEW INTEX		
AND MUSEU		M / PO	PI / STE	5i 7615 "	¥/m6¥
	"F[" "	M /FO	PL/PTF	PL7PTP "	T/MAX
-107	5.6441	1.6784	0.060666	0.14092	-1.9900
-107 -112	5.6441 5.5740	1.6784	0.060666 0.050913	0.14092 C.13417	-1.9099 -1.9600
-107 -112 -172	5.6441 5.5740 5.4589	1.6784 1.6576 1.6234	0.060666 0.059913 0.058676	0.14092 C.13417 0.13630	-1.900 -1.900 -1.000
-107 -112 -122 -127	5.6441 5.5740 5.4589	1.6784 1.6576 1.6234 1.0758	0.060666 0.050913 0.058676 0.038883	0.14092 C.13417 0.13630 0.090323	-1.0000 -1.0000 -1.0000
-107 -112 -172 -177 -127	5.6441 5.5740 5.4589 -AIY5 4.5683	1.6576 1.6576 1.6234 1.0758 1.3555	0.060666 0.059913 0.058676 0.058676 0.058683 0.048995	0.14092 C.13417 0.13630 0.040323	-1.000 -1.000 -1.0000 -1.0000
-107 -112 -172 -177 -127 -142	5.6441 5.5740 5.4589 6175 4.7583 4.5234	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466	0.060666 0.054913 0.058676 0.058676 0.048995 0.048973	0.14092 C.13417 0.13630 0.040323	-1.000 -1.000 -1.000 -1.000 -1.000
-107 -112 -172 -177 -127 -142 -152	5.6441 5.5745 5.4589 6175 4.1583 4.5234 3.5724	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.0624	0.060666 0.054913 0.058676 0.058676 0.048995 0.048673 0.038398	0.14092 C.13417 0.13630 0.090323 0.11381 C.11366 0.489198	-1.000 -1.000 -1.000 -1.000 -1.000 -1.000
-107 -112 -172 -177 -127 -142 -152	5.6441 5.5740 5.4589 6175 4.7583 4.5234	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466	0.060666 0.054913 0.058676 0.058676 0.048995 0.048973	0.14092 C.13417 0.13630 0.090323	-1.000 -1.000 -1.000 -1.000 -1.000
-107 -112 -172 -177 -137 -142 -152 -157	5.6441 5.5745 5.4589 6175 4.1583 4.5234 3.5724	1.6784 1.6576 1.6234 1.9758 1.3555 1.3466 1.9624	0.060666 0.054913 0.058676 0.058676 0.048995 0.048673 0.038398	0.14092 C.13417 0.13630 0.090323 0.11381 C.11366 0.489198	-1.000 -1.000 -1.000 -1.000 -1.000 -1.000
-107 -112 -172 -177 -127 -142 -152 -157	5.6441 5.5740 5.4589 5.4589 4.5274 3.5724 3.5724 AT PRESSIME	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.9624 1.9624	0. 06C6A6 0. 074913 0. 075676 0. 074843 0. 044995 0. 04671 0. 038796 0. 038799	0.14092 C.13417 0.13630 0.090322 0.11341 0.11366 0.489198	-1.000 -1.000 -1.000 -1.000 -1.000 -1.000 -1.000
-107 -112 -127 -137 -137 -142 -152 -167 -167	5.6441 5.5740 5.4589 5.4589 4.5234 3.5724 3.5724 AT PRESSIRE	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.9624 1.9624 PAYITIC FAN	0.06C6A6 0.050913 0.056676 0.056676 0.048683 0.048995 0.048671 0.038398 WNOZEF FREP	0.14092 C.13417 0.13630 0.090322 0.11341 0.11364 0.089198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-107 -112 -177 -177 -137 -142 -152 -157 -157 -157 -157	5.6441 5.5740 5.4589 4.754 4.5234 3.5724 3.5724 7.5724 7.572510F	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.0624 FAYING FAN	0.06C666 0.050913 0.058673 0.048673 0.048673 0.048999 0.038398 NITVZEF EXER	0.14092 C.13417 0.13630 0.090322 0.11361 0.11366 0.769198 0.085198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-107 -112 -177 -177 -137 -142 -152 -157 -157 -157 -157	5.6441 5.5740 5.4589 5.4589 4.5234 3.5724 3.5724 AT PRESSIRE	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.9624 1.9624 PAYITIC FAN	0.06C6A6 0.050913 0.056676 0.056676 0.048683 0.048995 0.048671 0.038398 WNOZEF FREP	0.14092 C.13417 0.13630 0.090322 0.11341 0.11364 0.089198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-107 -112 -127 -127 -137 -152 -157 -157 -157 -157 -157	5.6441 5.5740 5.4589 4.754 4.5234 3.5724 3.5724 7.5724 7.572510F	1.6784 1.6576 1.6234 1.0758 1.3555 1.3666 1.9624 1.9624 PAYITIS FAN PL/PT 1.9624 1.3624	0.06C666 0.050913 0.058673 0.048673 0.048673 0.048999 0.038398 NITVZEF EXER	0.14092 C.13417 0.13630 0.090322 0.11341 0.11365 0.085198 0.085198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-107 -112 -177 -137 -137 -147 -152 -157 -157 -157 -157 -157 -157	5.6441 5.5740 5.4589 7.175 4.5683 4.5274 3.5724 7.5724 7.5724 81.5724 81.5724	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.0624 VAYING FAN PL /PO 1.0624 1.1624	0.06C666 0.050913 0.058676 0.058676 0.048673 0.048673 0.038398 0.038398 0.038398	0.14092 C.13417 0.13630 0.090322 0.11361 0.11366 0.769198 0.085198 PL/PTP 0.089198 0.085198	-1.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-107 -112 -177 -127 -142 -152 -152 -157 -157 -157 -157 -157 -157 -157 -157	5.6441 5.5740 5.4589 -6175 4.5234 3.5724 3.5724 7.5724 7.5774 4.5774 3.5774 4.5774	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.9624 1.9624 1.9624 PAYING FAN PL/PN	0. 06C666 0. 050913 0. 058673 0. 048673 0. 048673 0. 048673 0. 038398 0. 038398 0. 038398 0. 038398	0.14092 C.13417 0.13630 0.090322 0.11361 0.11366 0.489198 0.089198 PL/PTP 0.089198 0.089198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-107 -112 -122 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	5.6441 5.5740 5.4589 5.4589 4.523 4.523 3.5724 7.5724 7.5724 41 PRESSIME PI 3.5774	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.9424 1.9624 PAYING FAN PLAN PLAN PLAN PLAN PLAN PLAN PLAN PL	0. 06C6A6 0. 050913 0. 058676 0. 078883 0. 048995 0. 048671 0. 038799 0. 038799 0. 038799 0. 038799 0. 038799 0. 038799	0.14092 C.13417 0.13630 0.090322 0.11361 0.11365 0.089198 0.089198 0.089198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000
-10.7 -112 -1.27 -1.27 -1.47 -1.52 -1.57 -1.57 -1.57 -1.57 -1.57 -1.57 -1.57 -1.57 -1.57	5.6441 5.5740 5.4589 5.4589 4.5234 3.5724 3.5724 7.5724 7.5724 7.5724 7.5724 7.5724 7.5724	1.6784 1.6576 1.6234 1.7758 1.3555 1.3466 1.9624 1.9624 1.9624 PAYING FAN PI /PN 1.9639 1.9639 1.9639	0. 06C666 0. 050913 0. 058673 0. 048673 0. 048673 0. 038398 0. 038398 0. 038398 0. 038398 0. 038452 0. 038452 0. 038452	0.14092 C.13417 0.13630 0.090322 0.11361 0.11366 0.089198 0.089198 0.089198 0.089198 0.089198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-107 -112 -177 -127 -142 -152 -152 -157 -155 -157 -157 -157 -157 -157 -157	5.6441 5.5740 5.4589 5.4589 4.523 4.523 3.5724 7.5724 7.5724 41 PRESSIME PI 3.5774	1.6784 1.6576 1.6234 1.7758 1.3555 1.3466 1.9624 1.9624 1.9624 PAYING FAN PI /PN 1.9639 1.9639 1.9639	0. 06C6A6 0. 050913 0. 058676 0. 078883 0. 048995 0. 048671 0. 038799 0. 038799 0. 038799 0. 038799 0. 038799 0. 038799	0.14092 C.13417 0.13630 0.090322 0.11361 0.11366 0.089198 0.089198 0.089198 0.089198 0.089198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000
-107 -112 -127 -127 -137 -142 -152 -157  AVD WOPD -152 -157  > FOOTY FOR	5.6441 5.5740 5.4589 5.4589 4.5234 3.5724 3.5724 7.5724 7.5724 7.5724 7.5724 7.5724 7.5724	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.9624 1.9624 1.9624 1.1624 1.1624 1.1624 1.1624 1.1624	0. 06C6A6 0. 050913 0. 058676 0. 078883 0. 048995 0. 048673 0. 038798 0. 038798 0. 038798 0. 038798 0. 038798 0. 038798	0.14092 C.13417 0.13630 0.090322 0.11361 0.11362 0.085198 0.085198 0.085198 0.085198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000
AVD WOPD -152 -157 >ATOTT FOR AVD WOPD -16" -172 "SAMET TOR AVD WOPD	5.6441 5.5740 5.4589 6.175 4.5274 3.5724 7.5724 7.5724 6.5724 6.5724 6.5724 6.5724 6.5724 6.5724 6.5724 6.5724	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.0624 PAYING FAN PL /PO 1.0624 PAYING PA PAYING PA PAYING PA 1.0639 1.0639 1.0624	0. 06C666 0. 057913 0. 058676 0. 078883 0. 048995 0. 048671 0. 038398 0. 038398 0. 038398 0. 038398 0. 038398 0. 038398 0. 038452 0. 038452	0.14092 C.13417 0.13630 0.090322 0.11341 0.11366 0.085198 0.085198 0.089198 0.089198 0.089198 0.089198	-1.0000 -2.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000
-107 -112 -127 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	5.6441 5.5740 5.4740 5.4740 5.4744 3.5724 3.5724 7.5724 7.5724 81 PRESSIRE PI 3.5774 3.5724 81 PRESSIRE	1.6784 1.6576 1.6234 1.0758 1.3555 1.3466 1.9624 1.9624 1.9624 1.1624 1.1624 1.1624 1.1624 1.1624	0. 06C6A6 0. 050913 0. 058676 0. 078883 0. 048995 0. 048673 0. 038798 0. 038798 0. 038798 0. 038798 0. 038798 0. 038798	0.14092 C.13417 0.13630 0.090322 0.11361 0.11362 0.085198 0.085198 0.085198 0.085198	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000

•		PATINS , PRI				
WAU MUBU	PL	M /PN	PL/PTF	PI /PTP	CAMAX	
32	17.177 8.9984	5.1140 2.5730	0.18544 0.097143	0.4 3203 0.72632	0.43200 0.53300	
37 47	11.439	3.4055	0.997143	0.28779	0.62900	entropy was subject to the entropy of such the same succession in probability succession. He was a side size to the
52	11.499	3,4234	0.12414	0.28921	0.72700	
NUI 11004<		PATINS , FIG				
AVD WORD	PL	ም /ምገ	PI /PTF	PL/PTP	I/DMAX	
12	13.044	3.8952	0.14124	0.32907	0.42200	g
67	9.1585	2.7766	3.008871	0.23035	9,67000	
>ADDITIONA	AL PRESSIRE	PATINS . FLO	W SPLITTER C	. n.		
AVD HOPD	Pt	PL/PO	PI /PTF	PI /PTP	I/DMAX	
77	36.910	10.989	0.39846	0.92832	0.50800	
82	14.612	5.5410	0.20092	0.46R11	0.58300	
e7	3.6344	1. 3731	0.038911	0.090654	3.67000	
>AD311 EGN	AL PRESSURE	PATENS . FUE	CŤCR SHROUĎ			
AVN HOPR	ří ····	PI /PO	PL/PTF	PL /PTP	I/OMAX	
1:07	5.6165	1.6721	0.040633	0,14126	J. 62400	
112	5.5464	1.6513	0.059877	0.13950	0.83000	
172	5.4313	1.4170	0.058634	0.13660	Q. 96000	
127	3.6144	1.3761	0.030019	0.090905	1.0900	
13"	4.5304	1.3448	0.048934	0.11795	1.2209	
142	4.5004	1.3398	0-048584	0.11319	1.3500	
	AL PACKSING	ALHAC . FOR	ENOW INTER			
AVITUAPO	Pt	Pt /PO	PL /PTF	PL /PTP -	C/DMA T	•
-107	5.6165	1.6721	0.060633	0.14126	1.9630	
-112	5.5464	1.6513	0. 055877	0.14950	¥:0000	
-127	5.4313	1.6170	0.058634	0.13660	1.0000	
-127	300144	1. 5*61	7.334014	0.340205	1.0000	
-127	4.7204	1.3488	0.048908	0.11345	1.0000	
-14?	4.533	1.3396	0.048594	0.1(319	1.0600	
-152	3.5743	1.0641	0.038587	0.089898	1.0000	
-157	307793	1.0641	9.93874	איימיים נייני	1.0900	
>30011 PM	NI PRESSIME	PATITIS FAR	HOTTIF PLAN			
AAU AUBL	ol	PI /PD	WIPTE	PL/PTP	MAX	
-152	3.5743	1.0641	<b>₩</b> 0.038587	0.089898	1.0000	
-157	3.5743	1.0641	030507	G. GRORON	-1.0003	
うとうつぎますり	AI BPFCCIBF	PATTON . 20	nea shead t	PATION		
AVD HOPO	PL	PL / PO	PI /PTF	AT 15.15	ear in the same of	e, di carata agusta de la terraminata esperantata. Combinante un principio de combina de la carata de la carata
-167	3.5743	1.0541	0.038597	32Guouau	1.0000	
-177	3.5743	1.0641	0032527	O. Oronon	1.0000	
``\$477} <b>T</b> TY	AT MESSIBE	PATTING , NO	OFG SHPPOPTI	DEATION -		and the state of t
AVD HOPP	PI	PL/PO	PI /PTF	PI /PTP	Now x	
-132/	3.1237	7. 52098	0.033722	U-078565	1.0090	
-124	3.1899	0. 94936	0.034425	0.040202	1.0000	a na principala usuga <b>nilibi sabaran</b> namba na menganya manda pari musu n <del>api ni napisahi.</del> Al <del>i Ministrati na manda nilahi.</del> Ministrati
CODITION 5	* muddibed	TUPHST PAPAN	FTroc		•	
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										Row 18	
	4658-1 FU 15	<b>BBEITM</b>	ATEG VRAME	26/19/79	CARRETT	PEC 10/11/7	o 07:41:24.837	FAC 9X6X1	PG4 C034	PNG 1078	
	>#001*104	IT DBESSIPE	PATENS . PRE	MARY MIIG						·····	
~	AVD POPD	PI	PI /PO	PI /PTF	PI /PTP	X/DMAX					
	27	15.570	4.6757	0.19538	0.43144	0.43200				<b>≠</b>	
_	37	P. 1928	2.4374	J. "976A7	U-22734	0.53000					
	47	10.357	3-0951	0.12764	0.28775	0.42900					
-		1-1-4-72	3.0985	0.12414	0.28900	0.72700					
^	>APPLIT TO PA	L PPESSIPE	PATINS . FEM	u SPLITTER I.	. n.				Committee and the committee of the commi	Print	
	TAU HUBU	PI	PI /PO	PI / PTF	PL/PTP	X/DMAX					
<b>^</b>	47	11.812	2.51.94	9.14100	0.32816	0.42209	** * 1	and the second s			
_	£7	P.2878	2.4697	0.798936	0.23025	9.67000					
^	>AOOTT FONA	I PRESSIME	PATINS . FIM	SPLITTER O	. D.		* * · · · * /· · · · · · · · · · · ·				•
	TAU AUNU	PL	PL/PO	PL/PTF	PL/PTP	X/IMAX					•
•	77	33.454	9.9648	0. 39936	0.92941	0.50800					
	P2	16.763	4.9933	0.29911	0.46572	U.58300	•				-
-	- 42	3,5912	1.0647	0.042870	0.09769	U.67000			<del></del>		
	>ADDITIONA	L PPFSSUPE	PATINS , EJE	CTC# SHPNUN	÷		a garante de mario de la compansión de l	all the second s	The state of the s		
<b>.</b>	****		er 100 ·	M 4075		# 40m Au					
	AVR MOPO 107	PL 5.0771	PL/PT 1.5123	Pt /PTF 1). 960t 38	PL /PTP 0-14105	X/8MAX 0.62400					•
-	ii	4.1971	1.4985	0.050657	0.13683	0.02400			<del></del>		
	122	4.8970	1.4587	0.058458	0.13605	0.96000	-		,		•
	127	3.5962	1.0712	0.042929	0.099908	1.0930					
	197	4. 3865	1.2172	0. C487P3	0.11353	1.2200					
	147	4.1515	1.206#	J. 0487€<	0.11256	1.3500	The second secon			<del>,</del>	•
_		-	WWW. FOR								
	/						-				
	Baun MAN	Pt	PL/PII	PL/PTF	PI /PTP "	x/hmā x		•			
	-101	5. 1771	1.5123	0.06060R	0.14105	-1.0000					
	-112	4.9971	1.4985	0.059653	0.13863	-1.0000					
_	-122 -12*	4.9073	1.4597	0.058458 0.042976	0.13605	-1.0000 -1.0000					
	-137	4.3865	1.2172	0.0427/3	0.11303	-1.0000					
	-142	4.1576	1.276#	0.048365	0.14256	-1.0000					
	-157	3.5661	1-0622	0.042571	399074	-1.0000					
	-1=7	3.5561	1.06 22	0.042571	3.099074	-1.0000		and only a reflect and an experience of the second			
-											-
	>EUD IT IUNT	I PRESSIME	PETITY FAR	MULTIF FEED	-						
	AVP HPPD	PL	PL/PD	MIPTE	PI /PTP	X ADMEX		a makany makanda magagagaga daday pambaga kababa		to ai - 1981; y-yapanganana apartambi - 4i	
	-152	3.5661	1.0627	×0.042571	0.099074	-1.0000					
	-157	3.5461	1.0422	0.042571	0.099074	-1. 3000					•
	···· >End14 lude	3#17244F	<b>RATION . 20</b>	TE SHIEDELL	DEAVION						
-			/	* ***		u #64 = 4					
	AVD UCRE -157	PL 3.5661	M /F9 1.0627	7[/PTF J.042571	0200074	X/DMAX -1-0000					
	-17?	1.551	1.0627	C-042511	0. 094935	-1.0000					
_	* 4 * 4		T & Charles		100.00	- 10 0000					_ }
 ت	TPPTT10CRC	KEESSIME.	**************************************	११ तास्त्रामार तस	UCTAINS	\	· · · · · · · · · · · · · · · · · · ·				
	AVD WODE	PI	PI /P7	PL / PTF	PL /FTP	x your x			<del></del>		3
	-197	3-1608	0.94150	0.037732	0.087813	-1.0052					
•	معز-	3.2204	0.9593#	0.038449	0.049481	-1.0000		1			
	Scotten 5	* weddibed	THEUST DADAM	FFERS			•				
	-	· · ·									

	"AS/ -1 5HTS	BULL INS	P'PPY PATA	36/10/79	CAPPELL	REC 10/11/79	03:42:24.803	FAC ANANI	PS4 C034	PRG 1679
		l buckellbt l			- 1 - 1					· · · · · · · · · · · · · · · · · · ·
_			•					- <del> </del>		······································
	ያካ የያሳ አጥርብ	P[ 13.350	PI /PII	el /etr	PI /PTP	X/DMAX		Applications of the second of		
	37	13.750	4.1475	7. 19701	0.43125	0-43200 2-53000	•			
-		7.3479	2.1866	3.098594	0.22736	0.53000				• · · · · · · · · · · · · · · · · · · ·
	47	0.3317	2. 7696	0.12489	7.29798	0.67400				
	5?	9,3317	2.7785	0.12524	0.28850	J. 72700				
~	AND 11002<	PPESSIRE F	ATINS . FEE	W SPLITTEP I	. n.				a kanan gara a lagar a lagar	and an opposition of a special state of the contract of the co
	AVD MUPD	PI	PI / PO	PL/PTF	PL /PTP	# ADMA W				
*	67	10,590	3.1531	0.14219	0.32786	0.42200				
	67	7.4389	2. 2149	0.039=73	G. 23030	9.67799				
-				W SPLITTER C						
					•		nort Maria normani en altragamente	e (parametra migrito e emispagagas e entre appar (gr. entre e e	andre contempo is	anders de l'Artes e autoriste l'annéel (agrante : l'artes plus especial)
	TAU MUSD	Pl	PL/PO	PL/PTF	PL /P TP	X/DMAX				
	77	79,746	A. F6 86	0.39988	0.92215	0.5000				
		14.913	4.4403	0.20021	0.46169	0.58700				
	e 2	2.5913	1.0643	0.047215	0.1111c	0.67000				
	>ennit inna	L PPESSUPE I	PATINS , FJI	CTOR SHADOD	A 1 May 1 May 1				and the second s	nak in sing and a sing of a second relative production of the second sec
~	ልህበ ህግጽብ	PI	PI /PI	M /PTF	PL /PTP	7/0-AX	i an ann i a contra accessor			
	107	4.5060	1. 3417	0.060495	0.13950	0.62400				
_	- <del>172</del>	4.4413	1.3223	0.059623	0.13749	0.83000				
$\overline{}$	172			0.058348						
		4.3461	1.2940		0.13455	0.96000			-	and the second s
	127	3.5863	1.0478	0.048148	0. [1103	1.0900				
	137	3.6663	1.0916	9.949727	0.11351	1.2200				and the second section of the section o
	142	7.6213	1.0792	0. 4F6ĮR	0.71211	1.3500	_			
			ATION TO	CACO INCL						
								apada ga may mada aya dadanada iya	en skri <del>geniskiske se jegykryk en sk</del> ri <del>ski</del> j s <del>ees</del>	
	WALL HUB II	PI	PL/PN	PL /PTF	PL /PTP	Y/DHAY		•		
	-107	4.5369	1.7417	2.060495	0.13050	-1.00ho	<del></del>	AND THE PROPERTY OF THE PROPER		
	-117	4.4410	1. 3273	J. 059623	0.13749	-1.05.00				
	-177	4.3461	1.2940	0.050748	0.13455	-1.0000				
	-127	5863	1.0678	0.048148	0.11103/	-1.0000				
	-137	3.8643	1.0916	0. C49222	3.1137	-1.0000				
	-147	3.62	1.0782	0.048618	0.1/211	-1.0000				
	-152	3.5664	1.0619	0.047880	#.1 1041	-1.0000				
	-157	1.5614	1.0604	0. 647813	0.11076	-1.0000		· · · · · · · · · · · · · · · · · · ·		
	- CANDITINUAL	[\$& <u>c</u> &&]#EI		MITTELL ALLE						
						3 mm1		· August 6 mary range graduation représente augustion	on the second second second second	
	AVD HEED	Pl	M /PO	PERTE	PI /PTP	X VOWER				
	-157	3.5664	1.0619	O. 347000	0.11041	-1.0000	<b></b>	a pro an experience and the constitution of th		
	-1=7	3.5614	1.0604	8 347A13	3.11026	-1.0006				. —
			TATTOS . 20	ताहद दाम्लीका र रात	TETTON					<u> </u>
_	AVD WOED	<b>Pl</b> /	PI /PN	OL /PTF	DI IPTP	X/DMAX			and the second s	name of the second
	-167	3.5664	1.0619	0.047880	M1041	-1.0000				
_	-177	3.5614	1. 3604	0.047913	0.11026	-1.0900			and the same of th	grand gracing in the state from grands or the Co
-									•	
	Zanul Alunas	MARKELINE. A	ETTIC . NO	<u>तस्य उपन्तातः । ।</u>	TEAT TON					
•	AVD HOPE	6.	m /84			J				
		PI	PL /PA	PL /PTF	PI /PTP	XXMMXX				
	-182	3.1364	0.93367	0.042130	9.397103	-1.0000		a se an an a san a agus sa an an ann an an an an an an an an an a		
J		₹.2364	J. 95471	0.043049	3.399770	-1.0000				
	Scarton 5	, MEASUPED T	THPHST PAPAR	it alb c		•				
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								y magnetive of \$100 direct NV and		
							and the second s		the state of the s	

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NASS-LEWI	c LbEf In	INTER DETA	06/19/70	CAPPELL	PFC 10/11/79	93:43:3% 203	FAF RX6XI	<del>-</del>	Tod 15 Ing 1009
101 F1C12	ICL PHESSIME	PATENS . PF	Tabba bing		reg veningemen verdage i digelenge og i				
<b>ስ</b> ቤ ትህቤ <u></u>	Pl	<b>PI /</b> የባ	M /PTF	P[ /PTP	XAMAX				
• •	12. 372	3.6759	7.1RE69	0.43103	7.43700				
37	6.5219	1.9440	3.609730	1.22765	0.53000		**		
4.7 6.7	8.2475 8.7675	2.45#4 2.4643	0.12485 0.12516	3.26826 0.28856	9-62900				
					7.72700				
	Mf ball 221me	BRAINS . VE	CM SPLITTER I				de comme e comme de	And the second second second second	many restricts and their explanation of the control
AD MUBU	PL	PL /PN	PI /PTF	PL/PTP	X/DMAY		and the first of the second se		rations and the second of the second
FZ F7	9.3976 6.5919	2.8912	0.1422 <b>6</b> 0.0997 <b>9</b> 0	0.32846	0.42200				
		1.0649		0.23040	0.67000	<del></del>			
>#Lot A low	IAL PRESSURE	PATIOS . FLO	OM SPLITTEP C	• P•	resonance some		- Anna de California de la compansión de		The state of the s
AU NUEU	PL	PL/PD	PL/PTF	PL/PTP	X/DHAX				
77 22	26.389	7.8660	0.39949	0.92735	0.50000				
A2 \$2	13.247 - 5946	1.0715	0.20054 0.054416	0.46300	0.58300 0.67000				
_	_		*	Ve 1/204	U0 T FOUU				
SAPPET EON	AL PRESSUPE	PATINS . EJI							
daun uk	PL	PL / PD	PI /PTF	PI JPŤP	X /DMAX	and the second of the second o	en armere approximately received any fragmentary against		
10;	3.9700	1.1934	0. C60944	0.13476	0.62400				
113	3.9299	1.1714	0. 059493	0.13736	0. #3000				
[27 [77	3.8499 3.5796	1.1476	0.059281 0.054189	0.13456	0.960 <b>90</b> 1. <b>0</b> 9 <b>06</b>				
137	3.2392	2.06553	0.044036	0.11322	1.2200				
14?	3.2197	0.95658	0.048582	0.11217	1.350C	ranco de la companya			
<del>lantit fal</del>	AL PAPERDAR	ALTIAC - FAI	FRANK INCE						
טן אניא טוא	rt ·	<b>ቅ</b> ር / ቦሽ	PL /PTF	PI /PYP	X / fm Ax				
107	3.9700	1.1834	0.060099	0.13876	-1.0300				
!12	2.9299	1.1714	0.059493	0.11726	-1.J050			<del></del>	
127	3.8499	1.1476	J. C5#2#1	C.13456	-1.0000				
27	3. 7462	7.0670	0.754189	3.12511	-1.5000				
137 142	2.2392	0. 95658 0. 95658	0.049036 0.048582	0.113/2	-1.0000				
152	3.5596	1.9613	U. C53896	0.12441	-1.0000 -1.0000				
ا جُ	3.5446	1.3625	7.053962	6.12459	-1.0030				
-			HP77LE FLAF						
					42 8000 24				
19 8569 152	rt 3.5596	m /PA	Q. 057886	% /PTP 0.12441	x/DNAx -1.3900				
	3.5646	1.0425	0.057062	0.17459	-1.0000			and the second control of the second control	
177	-								
-			•		21 0010 x 00		بمالة الرجيسات يوووونون والرواء		
አሉንጎ <b>የየ ሰ</b> ኞቹ		10E	PL /PTF	PLIPTP	X/DMAX -1.0000				
- 5 ዶ ኃጎ <b>የየ ያ</b> ሾች VD - ሣርተርር	Pi /	/ PT /PT	0.052004						
- ራዶኃጎ <b>የየዘ</b> ሾጭ የበ ሣርተር L67	PI 3.5596	1-96 19	0.0538% 0.053962	0.12441			-		
- 6 ዶ ግጎ <b>የየ (ሸ</b> ፄ / በ - ህብተ በ ( ዶ የ L የ ግ	PI 3.5596 3.5566	1.9619	0.057962	3-13050	-1.6000				
5 #35   T   MW 90   400 0 167 177 5 #83   T   MW	# paladibe 3.220 3.220 bi	1.9619 1.9625 Patyns , no	०-०५१९४१ त्रम्यानाम्य	0.13050	-1.0300				
0 4000 0 4000 167 177 0 40317 [P4	PI 3. 5596 3. 5566 AL PRESCRIPE	1.06.10 1.06.25 PATTOS NO PL/PO	0.057962 DEG KIMPHIN TI PL/PTE	3.13050 HETITIA Pl /PTP	-1-0000				
157 542217 [7] 542217 [7] 642 167 172 542217 [7] 64217 [7]	# paladibe 3.220 3.220 bi	1.9619 1.9625 Patyns , no	०-०५१९४१ त्रम्यानाम्य	0.13050	-1.0300				

486 f-4 EM4	< PPF1 141	THAT'S TATA	06/10/79	CADDETS	REC 10/11/79	07:52:21.691	FAC AVENS	PG# 1934	NOC 1991
ንልሳሳ <u>ት</u> ፣ የሳኅ	AL COESSIME	****** * PR	MAPY MUG	as managed in a process of the	d a super-contractor representation of a special	· ·			
AVO UCED	r.į	PI 7 PO	PL/PYE	PI /PIP	X/DMAX				
27	19.221	5.44KR	3.144.55	3.43174	0.43200				
77	0,5570	7. 4550	0.657782	0.22631	0.53000				
47	12.112	3.4705	J. 12403	3.29659	1.62900				The second of th
	12.192	3,6444	0,12482	G.ZMARA	0.72700				
MOT TTECAK	AL PRESSURE	RATIOS . FLE	NE SPEETTER E	. D.	_		on all one of MATER's agree participal are in the	معاصونات الاناساء أمانا ورد مواهد	······································
AVD WORD	Pi	Pt /WD	PL /PTF	PL/PTP	X/DMAX				
63	13.647	4.1392	0.14176	0.32609	2.42200		to a so the second widole sugar to announcement the		description of the second section of the section of the second section of the section of the second section of the sec
ě Ť	9,7013	2. 8999	0.099318	0.27486	3.67000				
MOT TECHN	AL PRESSURE	PATINS . FLE	W SPLITTEP C	. 0.					
AVP WEED	Pi	PL /PO	PL/PYF	PL /PTP	X/DMAX				
77	30.046	11.615	0.30701	0.92049	0.50000		to the second of the control of the	to spanning on all to streets to Figure at	ements to the constant of the
P.7	19.601	5.8592	0.20067	0.46443	0.58300				
	7.5834	1.0703	0.036656	0.004838	0.61000				
						يوال المنافق ا	The same of the sa	er salapanter (1988) e 180 e e - Arresto Marie (1884) e 1884 e e e e e e e	na da mi interactivama garapettiki interactivativa i isisiste et
>800 ( T (0M)	IL PRESSIME	RATIOS . FJF	CTOR SHEELIN						
AVO HOMB	ΡΊ	PL/PD	PL /PTF	PI /PTP	X/BMAX	THE THE THE STATE OF THE STATE	AND when the service is a service approximately all the service of approximation and the service of the service	Million - specification and the control of the cont	in description of some appears only resonant to the entire some govern
1:)7	5.9133	1,7672	0.060<40	0.14011	0.62490				
117	5. R4R3	1.7487	0. C59F74	0.13857	0.83000				
125	5.7331	1.7138	0.058696	0.13585	0.96000				
127	3.5854	1.0716	0.036708	0.084956	1.0900	a 1990 de la meranda agraçada	<ul> <li>— in proper year year of agreemant and interesting only office of</li> </ul>		and the second section of the second
137	4.7971	1.4346	0.049112	0.11367	1.2200				
147	4.7670	1.4259	0.04R805	0.11295	1.3500	The state of the second of the second	and the same of the suppression for the stage of the same of the s	Personal Control of the Property of the Personal Control of the Personal Contr	make the special programmer than the state of the state o
CHARTINE	n-setting-	tatios , for	ENDOK TALET			.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
AVILLED	ei -	PL/Ph	PL/PTF	PI /P (P	X/DAAX	er om de gegendene i "Lancer v. v. i somme.	The same was the same of the s	Notes and the second se	and the second s
-107	5.9133	1.7677	2.062540	0-14011	-1.9000		-		
-112	F.#4#3	1.7482	0.055874	0.13857	-1.0000	or the second of	entropy and the second		and the second s
-122	5.7331	1.7138	0.058696	0.13585	-1.0000				
-127	4456	1.0717	0. (3/ 709	0. 0A4 95	-1.0000				
-12' -13'	4.1071	1.4343	0.049112	0.11267	-1.0400				
-142	4. 7674	1.4750	0. 648875	0.11295			/ w		لدين الهواج والمتعلقينينينينية فتتستعيم يهامير
-147 -157	3.5454	1.0598			-1.0000				
-157 -157	3.5454 3.5454	1.0598	0.036255	0.094087	-1.0000		r e un de describe de la confederación (región describeración)		and the transferred names and address of the second second
			0.034298	6.084007	-1.0000				
Straff find	il beestier	BATIFIC FAR	- WALLES	<del></del>	intermittent on a security of the artificial teaching and a security of	ATTENDED TO SECTION AND ASSESSMENT OF THE SECTION ASSESSMENT OF THE SE			
AVP HEPTS	Pŧ	M / PO	TE / PTF	P1 /P7F	X/DHAX		naka ingga sa rawa wa ingga kangangana angka	the second line which is not in the second state of the second se	an
-1*?	3.5454	1.0598	0.036298	3-084007	-1.0000				
-1 . ,	7.5454	1. 1502	30536564	0.964307	-1.0000		in a ser major se sale adapt majority ballet e selectivo	The same state of the same of	- or some some some some some some some
₩ስት ተተረካለ< ¨`	if beloding	FRYS . 20	HER SIMPLE	PETTIN					
AVP HIPP	•1 /	PI /PN	M /PTF	W 1070	X/INIAN		. I in a summary of the company of the original states of	transport and the second	and the second special property and the second seco
-367	3.5454	1.0594	0.036298	0200001	-1.0000				
-172	3,06.4	1.0508	0.036299	0-03-603	-1.0000		<ul> <li>11. So Service all recover appropriate positions of confer or restable</li> </ul>	Marian grade	um may in indeplete ying ngan in object producered /Bertine (America) in real
	N BOESSIPE	******* ***	तार राम्यकार	PEATION -					
አያካላቸ <b>ተ</b> የሳይሀ				-					
						and the second of the second of the second	The same of the sa	THE BELLINGS IN HE SEE THE LONG THE T	and the control of th
AVO WOT	PI	PL / PG	PE /PTF	PL /PTP	X JOHNER	1 2 4 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	and the second section of the second purpose of the second	Berthal Belle and the second of the second o	and the same of th
	P  3.264# 3.1844	ም / የቤ ዓ. 946ዓ5 ዓ. 95 <i>2</i> 94	Pt /PTF 0.032401 0.032606	PL /PTP 0.0769R9 0.075464	1.0030 -1.0030	and the second and a second	oran de la large de l'Amedia perde d'Amedia Amedia (1971) Million	Berg magazingscar and soci to compare on a	and the state of t

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	IS PPFLIM	IMARY DATA	05/19/79	CARPELL	REC 10/11/79 03:54:40,576 FAC 9X6X1 PG* C034 PDG 108
					nen san fran . a
TOUR LE TUN	VAL PRESSURE	PATINS . PP	MARY PLUG		
ሰ ላቦዋ በ	PL	Pt 790	PI /PTF	PI /PTP	X/DMAX
7	14.444	5.5301	0.18700	0.43129	0.43206
7	9.6589	7. RR 34	0.097927	J.22586	0.53000
7	12.273	2.6599	0.12443	0. 28/ 99	0.62900
,	12.343	3.6808	0.12514	0.28863	0.72700
10011104	MAL PRESSURE	RATIOS_+_FLO	W SC ITTEP, I	• D•	and the second s
กษาคา	PL	P1 / PO	PL/PTF	PL /PTP	x/DMAX
?	14.067	4.1949	0.14262	0.32894	0.42200
7	0.8289	2.9310	0.099651	0.22984	0.67000
INDIT ION	IAL PRESSURE	RATINS . FLO	W SPLITTER O	• 0•	
า พุทธภ	Pt	Pt / PC	PL/PTF	PL/PTP	X/SMAX
7	39.093	11, 555	0.39625	0.91391	0.50800
•	10.783	5.4994	0.20057	0.46260	0.58300
<u> </u>	3, 5968	1.0726	0.036467	0.084107	0.67000
	=================================				
NIST TEN	TADZZANT JAN	RATTOS . FJE	CTTR SHPOUR		
า พถตก	Pį	PI /PO	PI /PTF	PL /PTP	X/MAX
)7	5.9584	1.7768	0.060410	0.13933	0.62400
12	5,9034	1.7604	0.059852	0.13804	0.83000
, ,	5.7833	1.7246	0.058635	0.13524	0.96000
77	3.6169	1.0786	0.0=6670	0.094575	1.0900
7	4.9573	1.4486	0.049251	0.11359	1.2700
2	4.82.4	1.4397	0.044547	0.11249	1, 3500
	4811E 1	40-4121	40 046.341	A0 1 1 4 4 4 4	50 · FOV
100 T T 100	-	441105 <b>-</b> FOE	ENDON THEFT		
Muou	PL	PI /PO	PE/PTF	PL 7P TP	x/044x
Huou	PL 5.9584	PI /PO 1.7768	PE/PTF 0.060410	0.13933	-1 <del>- 20</del> 000
Muou	PL 5.9584 5.9034	Pi /P7 1.7768 1.7664	PE/PTF 0.060410 0.055952	0.13933	-1,0000 -1,0000
Huou St.	PL 5.9584 5.9034 5.7833	PI /PD 1.7768 1.7664 1.7246	PE/PTF 0.060410 0.055952 0.05865	0.13933 0.13664 0.13524	-1,4000 -1,0000 -1,0000
Hue d	PL 5.9584 5.9634 5.7833	PI/PO 1.7768 1.7664 1.7246 1.0786	PE/PTF 9.060410 0.055952 0.05865 0.036670	0.13933 0.13604 0.13524	-1,0000 -1.0000 -1.0000
Whon 2.7	PL 5.9584 5.9634 5.7833 3.6168 4.578	PI / PT 1.7768 1.7664 1.7646 1.0786 1.4486	PE/PYF 9.060410 0.055852 0.05865 0.036670 0.049251	0.13933 0.13604 0.13524 0.084574 0.11259	-1,0000 -1,0000 -1,0000 -1,0000
Whon	PL 5.9584 5.9034 5.7833 3.6168 4.578 4.878	PI / P7 1.7768 1.7664 1.7246 1.0776 1.4486 1.44397	PL/PYF 0.060410 0.05942 0.05863 0.036670 0.049251 0.048947	0.13933 0.13664 0.13524 0.084574 0.11259 0.11289	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000
Whon	PL 5.9584 5.9634 5.7833 3.6168 4.578 4.678 3.5768	PI / PT 1 · 7768 1 · 7664 1 · 7246 1 · 0746 1 · 4486 1 · 4397 1 · 00666	PE/PTF 0.060410 0.055952 0.05863 0.036670 0.049251 0.048947 0.036264	0.13933 0.13664 0.13524 0.08457 0.11559 0.11289 0.083639	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000
Whon	PL 5.9584 5.9034 5.7833 3.6168 4.578 4.878	PI / P7 1.7768 1.7664 1.7246 1.0776 1.4486 1.44397	PL/PYF 0.060410 0.05942 0.05863 0.036670 0.049251 0.048947	0.13933 0.13664 0.13524 0.084574 0.11259 0.11289	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000
wnon 17 17 17 17 17 17 17 17	PL 5.9584 5.9634 5.7833 3.6168 4.8578 4.8778 3.5768 7.5768	PI/PO 1.7768 1.7664 1.7246 1.0786 1.4486 1.4397 1.0666	PE/PTF 9.060410 0.055942 0.05863 0.036670 0.049251 0.048947 0.036264 0.036266	0.13933 0.13664 0.13524 0.08457 0.11559 0.11289 0.083639	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000
שומים שו ביר מים שומים ש	PL 5.9584 5.9634 5.7833 3.6168 4.578 4.678 3.5768 7.5768	PI / PT 1.7768 1.7664 1.7664 1.7246 1.0746 1.4486 1.4397 1.0666 1.0666	PE/PTF 0.060410 0.056452 0.05863 0.036670 0.049251 0.049251 0.046264 0.036264	0.13933 0.13604 0.13524 0.08457 0.11269 0.11269 0.083639 0.363639	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
# HOOD 27 27 27 27 27 27 27 27 27 27	PL 5.9584 5.9634 5.7833 3.6168 4.578 4.678 3.5768 7.5768	PI / PT 1.7768 1.7664 1.7246 1.0746 1.4486 1.4397 1.0666 1.0666 RATIOS FAN	PE/PTF 9.060410 0.056952 0.05863 0.036670 0.049251 0.048947 0.036264 0.036264	0.13933 0.13604 0.13524 0.03457 0.11259 0.11269 0.087639 0.087639	-1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000
# non 27 27 27 27 27 27 27 27 27 27 27 27 27	PL 5-9584 5-9634 5-7833 3-6168 4-6578 4-6778 3-5768 7-5768 PP 550RE	PI/PO 1.7768 1.7664 1.7664 1.7246 1.0748 1.4486 1.4397 1.0666 1.0666 RATION FAN	PE/PTF 9.060410 0.055452 0.05865 0.036870 0.049251 0.048947 0.036264 0.036264	0.13933 0.13604 0.13524 0.08457 0.11359 0.1289 0.083639 0.083639	-1,0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
# HOOD 27 27 27 27 27 27 27 27 27 27	PL 5.9584 5.9634 5.7833 3.6168 4.578 4.678 3.5768 7.5768	PI / PT 1.7768 1.7664 1.7246 1.0746 1.4486 1.4397 1.0666 1.0666 RATIOS FAN	PE/PTF 9.060410 0.056952 0.05863 0.036670 0.049251 0.048947 0.036264 0.036264	0.13933 0.13604 0.13524 0.03457 0.11259 0.11269 0.087639 0.087639	-1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000
37 17 17 17 17 17 17 17 17 17 17 17 17 17	PL 5.9584 5.9634 5.7833 3.6168 4.578 4.678 3.5768 7.5768 PPESSURE PI 2.5768	PI / PT 1.7768 1.7664 1.7664 1.7246 1.0746 1.4397 1.0666 RATIOS FAN PL / PT 1.0666 1.0666	PE/PTF 0.060410 0.056452 0.05863 0.036670 0.049251 0.048947 0.036264 0.036264 NNY/IF FLAP 0.036264	0.13933 0.13604 0.13524 0.1352 0.11259 0.11269 0.087639 0.087639 0.087639 0.087639	-1,0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
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7.7	13.027	4.3145	0.71543	0.42095	0.43230		. =		
77	7.7513	2.2773	0.11781	0.27659	0.53000				
• 7	5.2972	2.8771	0.14279	9.29677	3.67700			and the second second	
-7	4.3277	7.8994	3.14441	0.20031	u. 72760				
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Ment Linear	I PPFSSIME	PATIOS . FI	NW SPLITTER I	-D-					
WE WELL	PE	PL / PG	S4 /PTF	PL /PTF	E/DMAX				
£7	13.693	3.2945	0.16415	0.37739	0.42200				Company of the Compan
1.7	7.4414	2.3052	0.11521	0.27977	0.67300				•
			OM SPLITTER C		-		The second of the second second	and the second s	and the second s
AU AUBL	<b>&gt;</b> 1	PI / PO	PLYPTE	PL /PS	X/DMAX				
77	25. 354	4. 339I	0.40027	0.79831	0.50800	gaperia series i series de caracteria			
• 7	12.948	4. 02 34	0.75109	0.46103	0.58300				
6.7	3.4374	1.3449	0.053220	0.10614	0.67960	<u> </u>			
>4931110W	L PRESSURE	PATIOS . FJ	ËCTOP SHPRYO	* * * * * * * * * * * * * * * * * * * *			. The special	A	and the second s
ልህ ግርፍህ	PL	PL/PD	PL/PTF	PL /PTP	X/DMAX	and the second of the second	Break or come a stratily a which the has a province a second		anders of the same and the same
197	3.5931	1.2029	0.060118	0.11950	0.62400				
112	3.4399	1.1227	0.055421	0.11851	0.83000				
122	3.7479	1.1611	3.05#026	0.11573	0.96000				
177	3.4375	1.0533	0.053142	0.10599	1.0900	and the second of the second o			
127	3.5927	1.1099	3.055448	0.11063	1.2200				
147	3.5226	1.3913	2. 054537	0.10877	1.3500				
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anen a	Pi	PL /PÓ	PL/PTF	PL/PTP	x/neax				
מפרע עיי	Pi 3.5831	P( /Pf) 1+2329	PL/PTF 3.36911#	0.11990	-1.0000				
11? 1-7	PI 3.5831 3.8380	P( /PN 1-2329 1-1990	PL/PTF 3.06011# 0.059421	0.11990	-1.0000 -1.0000	7			
117 117 177	P1 3.4831 3.8380 3.7479	P( /PN 1.2329 1.1990 1.1611	PL/PTF 3.369118 0.059421 0.059025	0.11990 0.11851 0.11573	-1.0000 -1.0000 -1.0000				
117 117 127	Pi 3.5831 2.8380 3.7479 3.6325	P( /Pn 1.2729 1.1990 1.1611 1.3633	PL/PTF 7.36011# 0.059421 0.059025 7.053142	0.11990 0.11851 0.11573 0.10599	-1.0000 -1.0000 -1.5000	7			
1-7 11:2 1:27 1:27 1:27	PI 3.4831 2.8380 3.7479 3.6325 3.427	P( /Pf) 1.2729 1.1990 1.1611 1. W 33 1.1790	PL/PTF 7.36011# 0.054421 0.05427 0.053142 0.05546#	0.11990 0.11851 0.11573 0.10599 0.11063	-1.0000 -1.0000 -1.0000 -1.0000	7			
Vi unen 1-7 112 127 127 127 127	PI 3.5831 2.8380 3.7479 3.4375 3.427	P( /Pn 1-2729 1-1990 1-1611 1-3-23 1-1790 1-2913	PL/PTF 7.36011R 0.05421 0.05402F 0.053145 0.0546R 0.054537	0.11990 0.11851 0.11573 0.10599 0.11063 0.10637	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
117 117 127 127 127 127 147 142	P1 3.5831 2.8380 3.7479 3.4375 3.4377 1.6724 3.4225	9( /Pf) 1-2729 1-1690 1-1611 1-3633 1-1700 1-2913 1-2632	PL/PTF 3.36011R 0.054421 0.05402F 0.053142 0.054537 0.052987	0.11990 0.11851 0.11573 0.10599 0.11063 0.1097	-1.0000 -1.0000 -1.5000 -1.5000 -1.0000 -1.0000				
117 117 127 127 127 127 147 142	PI 3.5831 2.8380 3.7479 3.4375 3.427	P( /Pn 1-2729 1-1990 1-1611 1-3-23 1-1790 1-2913	PL/PTF 7.36011R 0.05421 0.05402F 0.053145 0.0546R 0.054537	0.11990 0.11851 0.11573 0.10599 0.11063 0.10637	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 117 127 127 127 147 142 142 142	PI 3.5831 3.8380 3.7479 3.4325 3.4327 3.4225 3.4225	9 /P0 1.2329 1.1890 1.1611 1. 33 1.1300 1.3013 1.3632 1.3632	PL/PTF 3.36011R 0.054421 0.05402F 0.053142 0.054537 0.052987	0.11990 0.11851 0.11573 0.10599 0.11063 0.10977 0.10569	-1.0000 -1.0000 -1.5000 -1.5000 -1.0000 -1.0000				
107 117 117 127 127 127 127 142 142 142 142	PI 3.5831 3.8380 3.7479 3.4325 3.4225 3.4225	9 /P0 1.2329 1.1890 1.1611 1. 33 1.1300 1.3013 1.3632 1.3632	PL/PTF 3.36011R 0.054421 0.05462F 0.053142 0.054537 0.052937 0.052937	0.11990 0.11851 0.11573 0.10599 0.11063 0.10977 0.10569	-1.0000 -1.0000 -1.5000 -1.5000 -1.0000 -1.0000				
VI WINE IN 117 117 127 127 127 127 127 127 127 127	PI 3.5831 3.8380 3.7479 3.4375 3.4377 1.5724 3.4225 3.4225 7.4225	PL /PD 1-2329 1-1690 1-1611 1-3633 1-1360 1-3913 1-3632 1-3632 PAYIOS FEI	PL/PTF 7.36011R 0.059421 0.059421 0.0593142 0.05546R 0.054537 0.052987 0.052987	0.11990 0.11851 0.11573 0.10599 0.11063 0.10927 0.10569	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
117 117 117 127 127 147 142 142 142 142 142 142 142 142 142 143 144 144	91 3.5831 2.8380 3.7479 3.4375 3.4377 1.5724 3.4225 3.4225	9 /P0 1.2329 1.1490 1.1611 1.3633 1.1390 1.3913 1.3632 1.3632	PL/PTF 3.36011R 0.054421 0.05462F 0.053142 0.054537 0.052937 0.052937	0.11990 0.11851 0.11573 0.10599 0.11063 0.1097 0.10568	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
Vi unen 11-7 11-7 12-7 12-7 12-7 14-2 14-2 14-2 14-7 Vinniffinie Vinuen 15-2 14-7	PI 3.4731 2.8380 3.7479 3.4375 3.4225 3.4225 3.4225 3.4225 3.4225 3.4225	PAYING FEI	PL/PTF 7.36011R 0.059421 0.059421 0.0593142 0.05546R 0.054537 0.052987 0.052987	0.11990 0.11851 0.11573 0.10599 0.11063 0.10599 0.10568	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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_	AND HERD	PI	P( / P/)	PI /PTF	CI /PTP	× /DMAX				~	, T
	37	11.268	3.6614	3.10677	9.43077	1.43700					
		6.3412	1-9430	0.0006)	J. 72874	J. 53500					
	37	A. 2377	7.4497	0.12496	0.23821	3.62500		-			•
	47 52	A.0377	2.4513	0.12525	0.24911	0.72700					
_		7:22:11				a and Edward Tolk sections	<del></del>				_
-	APPLITICESC	PPFSSIIPE	PETIOS . FLOW	SPLITTE T.	n.						
			- 100	PL /PTF	PL/PTP	x/DMAX					
	AVD MEDD	PI	PL/PG			3.42290					
	62	9.1327	2.7940	0.14252	0.32872	0.67000					
	_ e7	6.4113	1.9614	0.10005	0.23076	2001907					
	APOTT FORC	PRESSUPE	RATIOS . FLOW	SPLITTEP C.	.0.						
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	<b>ጀ</b> ላሁ ሳህት <i>ቤ</i>	PI	PF /PN	PI /PTF	PL/PTP	X/DMAX					
	77	25. +24	7.8697	0.42144	0.92568	0.50800					
	47	12.918	3. 95.21	9.29169	0.46496	0.58300					
	- <del>5</del> ?	1.4933	1.06.47	0.054516	0.12577	3.67000					•
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	107	3.8738	1.1951	0.066457	0.13943	J.62400					
_	111	3.4337	1.1729	0. 055828	0.13799	2.43000					_
-			1.1438	0.058344	0.13456	0.96000					
¥	127	3.7346 3.49#3	1.0672	0.654437	0.12555	1.0500	A				_
	127	3.477 3.1478	0.96302	0.049124	0.11330	1.2290					
	127 142	7.1225	0.95536	0.049734	0.11240	1.3500					
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-	- STEAT LIBRA	ARECCIAE.	11105 FOE	ACCOUNT OF THE							4
			PL /PO	PL /PTF	PI /PTP	¥/DHÀ¥			···		
	TAILTIN	PL			0.13943	-1-000					
	-107	3-4738	1.1851	0.060453		21.0000	معاديد مناهد المسالم الماسيد				
	-117	3.4337	1.1724	0.05924	0.13799	-1.0000					-
	-17?	3.7386	1.1430	0.058344		-1.0000					
-	-177	2 4 43	1.0672	0.054437	0.12555	-1.0000					
	-127	3.770	0.96302	0.049124	0.11210					<del></del>	
	-147	3.123	0.95536	0.048734	0.11240	-1.0000					
	-152	3.4733	1.0626	0.054203	0.12591	-1.0000					(
	-,5*	3.4733	1-3676	6.054703	0.12531	-1.0000					•
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-	AVE HEFF	PI	PI /PO	/PTF	PL /PTP	X/DMYX					
	-157	3.4733	1.05.26	Q. 254223	0.12591	-1.0000					
_	-157	3.4733	1.9675	0.054203	0.17571	-1.0000					`
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_	AUD HEPT	Pt /	PI /P7	PL / PTF	PLATE	X/DMAX					
	-167	3.4793	1.0641	0.054281	0.12519	-1.3000					
u	-1 77	3.5433	1.3626	0.054203	0.12	-1.0000	,				,
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•	אברא טא	P1	P# / PO	PL /PTF	P1 /PTP	XAMOX					
		7.0176	0.92319	0.047093	0-15861	-1.3030					
	-: 1	7.1777	3.94004	0.047952	0.11060	-1. 1070					•
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37	12.090	7.7118	0.19647	7.43702	0-43200	
37	1495.4	1.9674	0. 598588	0.22726	0.53000	a kanagan kara in in mana menangan menangan menangan menangan menanggan menanggan menanggan mengan mengan menan
47	A-3741	? <b>.</b> 48 ??	0.12479	J. 28757	J•62900	
5?	A. 0881	2, 4952	0-12485	0.29792	9.72790	
>607171094	AT PRESSURE	PATIOS . FLO	W SPLITTER I	.0.	****	
VO HOPD	PI	PL/PN	PL/PTF	PE /PTP	X/DMAX	•
£2	9.2138	2.4711	0.14223	0.32800	0.42200	
67	6.4517	1.9824	0.099592	0.27967	0.67000	
POT TECOM	AL PRESSIRE	RATTOS . FLO	W SPLITTER D	. D.		
ላቦ ዛባቦם	PI	PI /PO	PI /PTF	PL /PTP	H/DMAH	
77	26.094	9.017R	0.47279	0.92889	0.5J800	
82	13.075	4.0176	0.20193	0.46545	0.58300	
07	3.4780	1.0687	0.053689	0.12361	0.67000	
>40017100	AL PRESSURE	PÁTINS , FJE	CTOP SHROUN		e des es esta comença e e com de deservir de	
ላሁ ሳሀኑብ	PL	PL / PO =	PL/PTF	PL /PTP	X/DMAX	
107	3.9137	1.2026	0.060414	0.13932	0.62400	
112	3. 9736	1.1903	J. C5 5795	0.13790	0.83000	
11 <i>6</i> 122	3.7785	1.1610	0.057377	0.13451	0.96000	•
	3.4630	1.0641	0.053457	0.12424	1.0900	
127 137						
L: ' 14?	3.1976 3.1475	0. 97791 2.96714	0.04912# 9.94#5#7	0.11329	1.2200	
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<del>&gt;=0011-104</del>	**************************************	PTIOC - COL	+41474-144-EX			
AURLOU	ԲԷ	PL/PO	PI /PTF	PI /PTP	X/DMAX	•
137	3.9137	1.2026	0.060414	0.1393?	-1.0000	
112	3.8736	1.1993	0.059795	0-13790	-1.000	
1?7	3.7785	1.1610	0.058327	0.13451	-1.0000	
127	34630	1.0641	0. 153457	0.12325	-1.0000	
137	3.1476	9.97791	0.049129	0.113/9	-1.0000	
142	7.1475	0.96714	0.048587	0 21225	-1.0000	
157	3.4570	1.0410	0.057302	1.12292	-1.0000	
	3.45R0	1.3625	0.053390	0.12310	-1.0000	
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-	AL PRESSIDE	RATIOS FAH	HOTTLE FLAD	······································		
ን ልዕንተት ነጥ! የ		PL/PO	NAVOLE FLAD	PL /PTP	Y/BMÀX	
። ያልስኝ <b>ያየ ነ</b> ሾቹ. Vn. ነጥቦስ	PI	PL /PI	LIPTE			
- 5 <u>8的<b>5</b>  </u> †   何月 VD - 110PD 152				PL/PTP 0.12292 0.12310	*/BMAX -1.0000 -1.0050	
5&85 <b>(† )</b> 69. Vn. 1000 157 157	PI 2,4530 3,4540	PL /PO 1.0610 1.0625	0. (533n?	0.12297	-1.0000	
SANTIT IMA. VN. 40PN 157 157 SANTITIMA	PI 3.4530 3.4590 AI DAESSIME	PL/PG 1.0610 1.0625	0. (53302 20053302 DEG SHROWN 11	0.12292 0.12310	-1.0000 -1.0030	
SANTIT IMA. VN. YOPN 157 157 SANTITIMY. VN. YOPN	PI	PL/PO 1.0610 1.0625 PATION 20	O. CS330? 25053363 DEG SHROUNCE	0.12297 0.12310 TEATTON	-1.0000 -1.0050	
- SÃÑŌ[Ŧ]ÑÑ, VN 'YMPN 157 157 SÃÑŌ[Ŧ]ÑŸ VN 'YMPN 167	PI 3.4530 3.4540	PL/PG 1.0610 1.0625 PAYER . 20 PL/PG 1.0625	O. 053393	0.12297 0.12310 0.12310 0.12310	-1.0000 -1.0000 x/pmax -1.0000	
SANSTT IMI, VN 4/NPN 157 157 SANSTTIMU VN 4/NPC 167	PI 3.4530 3.4540 AI BESTIME	PL/PO 1.0610 1.0625 PAYING 20 PAYING 20 PAYING 20 1.0625 1.3625	PI / PTF 0. (5330? 0. (5338) DEG SHROUPL (18 PI / PTF 0. (53380)	0.12297 0.12310 CATTON 1.791P 0.32310 C.12310	-1.0000 -1.0050	
SANSTT IMI, VN 4/NPN 157 157 SANSTTIMU VN 4/NPC 167	PI 3.4530 3.4540 AI BESTIME	PL/PO 1.0610 1.0625 PAYING 20 PAYING 20 PAYING 20 1.0625 1.3625	O. 053393	0.12297 0.12310 CATTON 1.791P 0.32310 C.12310	-1.0000 -1.0000 x/pmax -1.0000	
. SANSET INFA. VN 'UNPN 157 157 >ANSETTINA VN 'UNPN 167 177 SANSETTINA	PI 3.4530 3.4540 AI BESTIME	PL/PO 1.0610 1.0625 PAYING 20 PAYING 20 PAYING 20 1.0625 1.3625	DEC SHRUMENTO O. 053383 DEC SHRUMENTO O. 053383 DEC SHRUMENTO	0.12297 0.12310 NEATION PLATE 0.12310 C.12310	-1.0000 -1.0000 x/nmax -1.0000 -1.3600	
7 5455[7 [64] VD 1000 157 157 2655[7 [64] VD 1000 167 177 2455[7 [64] VD 1000	PI	PL/PO 1.0610 1.0625 PAYING . 20 PL/PO 1.0625 1.3625 PAYING . NO	PI / PTF  0. C5330?  0. C53303  DEG SHROWELL  PI / PTF  0. C53303  DEG SHROWELL  PI / PTF	0.12297 0.12310 TEATION PL/PTP 0.12310 C.12710N PL/PTP	-1.0000 -1.0000 x/max -1.0000 -1.0000	
VD (INPD 157	PI 2.4530 3.4540 AC BAESSINE PI 3.4530 PRESSINE PI	PL/PG 1.0610 1.0625 PAYING . 20 PM /PG 1.0625 1.3625	DEC SHRUMENTO O. 053383 DEC SHRUMENTO O. 053383 DEC SHRUMENTO	0.12297 0.12310 NEATION PLATE 0.12310 C.12310	-1.0000 -1.0000 x/nmax -1.0000 -1.3600	

	PRFLIM	INARY DATA	06/10/79	CADDELL	PEC 10/11/79 04:30:21,094 FAC AX6X1 PGM C034 RDG 1086
SAPORT INNA	PPFSSUPF	PATINS . PRE	MARY PLUG	··	
AVD HOPD	PL	PI / PO	el /ete	PI /PTP	X/DMAX
32	17.718	1, 2933	0.16559	0.47966	0.43200
37	5.4825	1.7460	0.087792	0.227RQ	0.53700
47	7.1631	2.2310	0.11067	0.25715	0.62900
52	7.1781	2.2356	0.11090	0.28775	0.72700
		RATIOS . FLO			
					x/(max
AVP MOPT	PL	በዚ / የተነ	PL/PTF	PL/PTP	
62 67	0.1783	7.5129	0.17635	0.32764	0.42200
	5.7376	1.7630	0.0FR642	0.23000	1.67000
IAMOIT LOUS C	PRESSURF	RATINS . FLO	M SPI ITTER C.	• n _•	
AVD WOOD	PL	PL /PI	Pt /PTF	PL /PTP	X/DMAX
77	26. 373	A.0113	0.40281	1.0452	0.50800
P 2	13.052	4. 0105	0.20165	0.52322	0.58300
97	3.4759	1.06 90	0.053701	0.13034	0.67000
>enait tuant	PRESSIPE	FATINS . EUF	CTCR SHROUD		
AND HUND	PL	PL / PO	PL/PTF	PL /PTP	X.DHAX
107	3.9063	1.2003	0.060351	0.15659	0.62400
112	3.9663	1.1880	0. 055732	0.15499	<b>ს.</b> ჩ3ენც
127	3.7762	1.1603	0.058340	0.15138	0.96000
127	3.4709	1.0665	0.053624	0.13914	1,0900
137	2.8653	0.68042	0.044768	0.11486	1, 2200
142	2.9153	0.86504	0.043404	0.11286	1.3500
	BECCURE	BATTAR FOR	STONY INC.		
			· · · · · · ·	PI /PTP	XZDMAX
AVI HOPD	PL	PL /PN	PL/PTF	PI /PTP	X/DMAX
AVI HOPO	PL 3.9063	P( /PT) 1.2003	PL/PTF 0.060351	0.15659	-1 <b>.</b> 2 <i>6</i> 00
AVI MOPO -107 -112	PL 3.9063 3.8663	PE /PTI 1.2003 1.1570	PL/PTF 0.060351 0.059733	0.15659	-1.0600 -X.0000
AVI MOPO -107 -112 -123	PL 3.9063 3.8663 3.7762	PL /PD 1.2003 1.1690 1.1603	PL/PTF 0.060351 0.059733 0.058340	0.15659 0.15499 0.15138	-1.0600 -1.0000 -1.0000
AVI MOPO -107 -112 -122	91 3.9063 3.8663 3.7762 2.4779	M /Ph 1.2003 1.1690 1.1603	PL/PTF 0.060351 0.054733 0.058340 0.058340	0.15659 0.15499 0.15138 0.13914	-1-3600 -1-0000 -1-0000
AVI HOPD -107 -112 -122 -127 -127	91 3.9063 3.8663 3.7762 2.4739 2.4653	M /PN 1.2003 1.1690 1.1603 1.7665 0.88042	PL/PTF 0.060351 0.059737 0.059340 0.0593674 0.044268	0.15659 0.15499 0.15138 0.13614 0.11578	-1.0600 -1.0000 -1.0000 -1.0000
AVI HIPTI -107 -112 -122 -127 -127 -127	91 3.9063 3.8663 3.7762 2.4739 2.4653 2.813	PE /PT 1.2003 1.1670 1.1603 1.7665 0.88042 0.96504	PL/PTF 0.060351 0.059737 0.059737 0.0573674 0.044268 0.043494	0.15659 0.15499 0.15130 0.13614 0.11676	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000
AVI MOPD -107 -112 -122 -127 -127 -147 -152	PI 3.9063 3.8663 3.7762 2.4739 2.4653 2.41 3 3.4609	PI /PD 1.2003 1.1670 1.1603 1.7665 0.85042 0.8504 1.9634	PL/PTF 0.060351 0.059737 0.059340 0.0593674 0.043494 0.043494 0.053469	0.15659 0.15499 0.15138 0.13914 0.11676 0.11296	-1.9600 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
AVI HIPTI -107 -112 -122 -127 -127 -127	91 3.9063 3.8663 3.7762 2.4739 2.4653 2.813	PE /PT 1.2003 1.1670 1.1603 1.7665 0.88042 0.96504	PL/PTF 0.060351 0.059737 0.059737 0.0573674 0.044268 0.043494	0.15659 0.15499 0.15130 0.13614 0.11676	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000
4V MOPD -107 -112 -122 -127 -127 -142 -152 -157	91 3.9063 3.8663 3.7762 2.4779 2.4673 2.4679 3.4679	PI /PD 1.2003 1.1670 1.1603 1.7665 0.85042 0.8504 1.9634	PL/PTF 0.060351 0.054737 0.058340 0.074266 0.044266 0.043494 0.053469 0.052469	0.15659 0.15499 0.15138 0.13914 0.11676 0.11296	-1.9600 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
AVI MOPD -107 -112 -122 -127 -127 -142 -152 -152 -157 >}001T15VAL	PL 3.9063 3.8663 3.7762 3.4779 2.4653 2.463 3.4609 7.4609 PPF55IIME	PI /PT 1.2003 1.1670 1.1603 1.7665 0.88042 0.96504 1.0634 1.0634 PI /PT	PL/PTF 0.060351 0.059737 0.059367 0.0593674 0.04268 0.04268 0.053469 0.053469	0.15659 0.15499 0.15138 0.13614 0.11296 0.11296 0.11296 0.13874	-1.3600 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0030
AVI MOPD -107 -112 -127 -127 -127 -142 -152 -152 -157	91 3.9063 3.8663 3.7762 3.4739 2.9653 2.91 3.4639 7.4639	M /Ph 1.2003 1.1670 1.1673 1.7665 0.88742 0.85764 1.0634 1.3634 PAYINS. FAN	PL/PTF 0.060351 0.054737 0.058340 0.058340 0.044268 0.043494 0.053469 0.052469	0.15659 0.15499 0.15138 0.13614 0.11296 0.11296 0.13874 0.13874	-1.3600 -X.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0030
AVI MOPD -107 -112 -122 -127 -127 -142 -152 -152 -157 >}001T15VAL	PL 3.9063 3.8663 3.7762 3.4779 2.4653 2.463 3.4609 7.4609 PPF55IIME	PI /PT 1.2003 1.1670 1.1603 1.7665 0.88042 0.96504 1.0634 1.0634 PI /PT	PL/PTF 0.060351 0.059737 0.059367 0.0593674 0.04268 0.04268 0.053469 0.053469	0.15659 0.15499 0.15138 0.13614 0.11296 0.11296 0.11296 0.13874	-1.3600 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0030
AVI MOPD -107 -112 -122 -127 -127 -142 -152 -157 >700 T1594[ AVD WOPD -152	PL 3.9063 3.8663 3.7762 2.4739 2.4639 PPFSSIINE PL 3.4639	PI /PT 1.2003 1.1670 1.1603 1.7665 0.887042 0.84504 1.3634 PI /PT 1.7634 1.0634	PL/PTF 0.060351 0.059737 0.059340 0.0593674 0.043494 0.053469 0.053469 NCYYEF LAP P/PTF 0.053469 0.053469	0.15659 0.15499 0.15138 0.13914 0.11296 0.1296 0.13874 0.13874	-1.3600 -K.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0030
AVI WOPD -107 -112 -122 -127 -127 -147 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 3.9063 3.8663 3.7762 3.4779 2.4779 2.913 3.4609 PPFSSIIPE PL 3.4609 PPFSSIIPE PL 3.4609	PI /PT 1.2003 1.1870 1.1603 1.1603 1.27665 0.88704 2.0634 1.2634 RAYINA FAV	PL/PTF 0.060351 0.059737 0.059340 0.0593674 0.044269 0.043494 0.053469 0.053469 0.053469 DFG SHROND IT	0.15659 0.15439 0.15138 0.13614 0.1256 0.1266 0.13874 0.13874 0.13874 0.13874	-1.3600 -X.0000 -1.0000 -1.0000 -1.0000 -1.0030 X/DMAX -1.0000 -1.0000 -1.0000
AVI MOPD -107 -112 -127 -127 -147 -147 -152 -157 -157 -157 -157 -157 -157 -157 -167	PL 3.9063 3.8663 3.7762 3.4739 2.913 3.4609 PPFSSIINE PL 3.4609 PPFSSIINE PL 3.4609 PPFSSIINE	PI /Ph 1.2003 1.1670 1.1603 1.7665 0.88042 0.84504 1.0634 1.3634 PAYINS FAN PI /Ph 1.0634 1.0634 PAYINS 20 PI /Ph 1.0634	PL/PTF 0.060351 0.059737 0.059340 0.0593674 0.043494 0.053469 0.052469 NICYTEFIAP DEG SHROND U	0.15659 0.15439 0.15138 0.13614 0.1296 0.1296 0.13874 0.13874 0.13874 0.13874	-1.3600 -X.0000 -1.0000 -1.0000 -1.0000 -1.0030 X/DMAX -1.0000 -1.0000 -1.0000
AVI WOPD -107 -112 -122 -127 -127 -147 -152 -157 -157 -157 -157 -157 -157 -157 -157	PL 3.9063 3.8663 3.7762 3.4779 2.4779 2.913 3.4609 PPFSSIIPE PL 3.4609 PPFSSIIPE PL 3.4609	PI /PT 1.2003 1.1870 1.1603 1.1603 1.27665 0.88704 2.0634 1.2634 RAYINA FAV	PL/PTF 0.060351 0.059737 0.059340 0.0593674 0.044269 0.043494 0.053469 0.053469 0.053469 DFG SHROND IT	0.15659 0.15499 0.15138 0.13614 0.11296 0.11296 0.13874 0.13874 0.13874	-1.3600 -X.0000 -1.0000 -1.0000 -1.0000 -1.0030 X/DMAX -1.0000 -1.0000 -1.0000
AVI MOPD -107 -112 -127 -127 -147 -147 -152 -157 -157 -157 -157 -157 -157 -157 -167	PL 3.46/19 3.46/19 3.46/19 PPF55IJPE PL 3.46/19 PPF55IJPE PL 3.46/19 3.46/19 3.46/19 3.46/19 3.46/19 3.46/19	PI /Ph 1.2003 1.1670 1.1603 1.7665 0.88042 0.84504 1.0634 1.3634 PAYINS FAN PI /Ph 1.0634 1.0634 PAYINS 20 PI /Ph 1.0634	PL/PTF 0.060351 0.059737 0.059340 0.053674 0.04269 0.043494 0.053469 PL/PTF 0.053469 DEG SHROND IT	0.15659 0.15495 0.15138 0.13614 0.11296 0.11296 0.13874 0.13874  PI /PTP 0.13874  PT ITINN PI /PTP 0.13874 0.13874	-1.3600 -X.0000 -1.0000 -1.0000 -1.0000 -1.0030 X/DMAX -1.0000 -1.0000 -1.0000
AVI MOPD -107 -112 -127 -127 -127 -142 -152 -157 -157 -157 -157 -157 -167 -167 -167 -167 -167 -17	PL 3.46.19 PPFSSIPE	M /Ph 1.2003 1.1870 1.1603 1.7665 0.88704 0.96504 1.0634 1.0634 1.0634 PAYION . 20 PLAYION . 20 PLAYION . 20 PLAYION . 20 PLAYION . 20	PL/PTF 0.060351 0.059737 0.059340 0.053674 0.04269 0.043494 0.053469 PL/PTF 0.053469 DEG SHROND IT	0.15659 0.15499 0.15138 0.13614 0.1296 0.1296 0.13874 0.13874 0.13874 0.13874 0.13874 0.13874 0.13874	-1.3600 -X.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
AVI MOPD -107 -112 -127 -127 -147 -147 -152 -157 -157 -157 -157 -157 -157 -157 -157	## 3.9063 3.8663 3.7762 3.4779 2.4779 2.4739 3.4609 ### 3.4609 ### ### ### #### ####################	PI /PT 1.2003 I.1670 I.2003 I.1670 I.1670 I.1673 I.7655 O.87042 O.84504 I.7674	PL/PTF 0.060351 0.059737 0.059340 0.059340 0.043494 0.053469 0.053469 0.053469 DFG SHROND U	0.15659 0.15499 0.15138 0.13614 0.1296 0.1296 0.13874 0.13874 0.13874 0.13874 0.13874 0.13874	-1.3600 -X.0000 -1.0000 -1.0000 -1.0000 -1.0030 X/DMAX -1.0000 -1.0000 -1.0000
AVI MOPD -107 -112 -127 -127 -127 -142 -152 -157 -157 -157 -157 -157 -167 -167 -167 -167 -167 -17	PL 3.46.19 PPFSSIPE	PI /Ph 1.2003 1.1670 1.1670 1.1603 1.7665 0.88042 0.86504 1.0634 1.0634 1.0634 1.0634 PAYTON . 20 PI /Ph 1.0636 PAYTON . 20 PI /Ph 1.0650 PETITS . 80	PL/PTF 0.060351 0.059340 0.059340 0.05369 0.043494 0.053469 0.053469 DFG SHROND II PL/PTF 0.053469 0.053469 DFG SHROND II PL/PTF	0.15659 0.15499 0.15138 0.13614 0.1296 0.1296 0.13874 0.13874 0.13874 0.13874 0.13874 0.13874 0.13874	-1.3600 -X.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000

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MASA-LEWIS	PP [] 99	INAPY DATA	06/10/79	CVDDETT	PFC 10/11/79	9 04:10:43.867	FAC ANGRE	PG4 F934	Run 18 PNG 1297
אוימן דן ממזכ	A BEESSHEE	PATING + OPT	MARY PEUG.	*					
A40 - 4000	Pt	P4 / PC	PL/PTF	PI /PTP	X /DMA X				
32	15.533	4.8965	0.21520	7.43158	3.43200			****	
37	P.1732	7. 5710	0.11291	0.27636	7.53000				
47	19.359	3.1361	J. 14311	3.286 BC	0.62500		* · · · · · · · · · · · · · · · · · · ·		war or a re-
52	10.399	3.2075		0.29890	J. 72700				
_"	10,549	*• Z**!2	_ he te .ac _	V. 2 - 2013 V	0.15100				
>ADDITIONA	N PRESSUPE	PATIOS . FLO	r chfittem i	. n.					**************************************
AVD WOPD	PŁ	P( /P1	PL/PTF	PL/PTP	X/DWAX				
62	11.469	2.6699	2. 1f 397	0.32871	0.42290				
67	R. 2933	2.5580	0.11457	0.2296F	J.6700J				
> FOOTT TONK	AL PPESSURE	RATIOS . FLO	N SPLITTER C	• O•					
AVD HOPD	Pt	PL/#N	PL /PTF	PI /PTP	X/DMAK				
77	29.334	9.0634	0.40595	0.81380	0.50800				
	14.593	4.5013	0.20161	0.40417	0.58300				
92	3,4692	1.0701	0. 647929	0.096081	0.67000				· · · · · · · · · · · · · · · · · · ·
		PATINS , FJF				<del>-</del>			
		-		<u> </u>		AND THE STREET OF THE STREET O			
AVB WOPD	PL	PI /PN	PL/PTF	PI /PTP	X/DMAX				
107	4.3953	1.3526	9.060584	0.12145	0.62400				
112	4.3353	1.3372	7. C5C893	0.12007	0.43000				-
127	4.2251	1.3932	0.358371	0.11792	3. 96300				
127	3.4642	1.9685	0.047859	0.095942	1.0900				
127	4.0199	1.2399	0.055536	0.11133	1.2200				
14?	3.9549	1.2198	0.054637	0.10953	1.3500				
1 TOOLS	i settine	avilor - ton	FACOV INTER						
AVP MUBU	PL	Pt / PO	Pt / PTF	PL /PTP	X/DMAX	, i e server a la l			
-107	4.3853	1.3526	2. 263584	0.12145	-1,000		•		
		1.3372	0.044643 0.100144	0.12007					<del></del>
-112	4.3353								
-127	4-2251	1.3032	0.058371	0.11702	-1.0000	· . · · · · · · · · · · · · · · · · · ·			
-127	3.4642	1.0435	0.047859	7.095542	-1.000r;				
-137	4.01.99	1.2399	9.055536	0.13133	-1.0000				
-142	3.050	1.2199	0.054637	0-10053	-1.0000				
-157	3.4442	1.0623	0. C4 75 82	N. 095289	-1.0000				
-157	3.4493	1.7639	0.047651	0.095526	-1.0000	a series to the contract of th			
SABOT* (PRA	IL PRESSUPE	PATING FOR	NAZTIE FLAD						
ብዛግት በላል	PL	P1 / P0	PIPTE	PL/PTP	ZAMAR .				
-152	3.4442	1.0623	0, 6475 #2	0.095388	-1.0000				
-157	3.4492	1.0639	047651	0.095528	-1.0000				
		PATION . 20 1							
	II. PEFTINE								
WAS MUSU	PI	M /Pr	PI / PTF	QI /PTP	X/DHAX				
-167	3.4497	1.0639	0.047651	y Gazz SY	-1.0000				
-177	3.49/2	1.0639	1-947651	0.396*26	-1.90GU				
~~************************************	HESSIDE	PATIOS , NO I	DEC SHRIPUT T	neattea -					
	-								
מפחני חים	PL 2 0004	PI / PD	nl/prf	PI /PTP	XYMAX	_			
102	2.9996	0.92181	3.C41288	0.082769	-1.0000				
-1°2									
-197 -197 Coffee 5	3. 23.96	7.93725 THEIST PARAM	9.941979	0.084156	-1.0000				

Age   Color						Rev 15
AUTH UND   P    P    P    P    P    P    P	MASS-1 FM1	S PRFE 14	INCPY DETA	06/10/79	CARRELL	REC 10/11/79 04:11:50.904 FAC RNANT PGM C034 RDG 1008
17	∑¥00 L± LUA	AL_PRESSURE	PATINS . PPI	MAPY PLUG	·	
77 7.1248 2.271 0.29413 0.27195 0.53000 77 0.0479 2.7027 0.1244 0.2800 0.12700 79 0.0429 2.7029 0.12440 0.2800 0.12700 79 0.0429 2.7029 0.12440 0.2800 0.12700 2400 MOND PL	AVD HOPD					
27						
72					0.22705	
DAPPHI FORM   PRESSURE PAYIOS   FIRM SPEITTER   1.0	•			0.13414	0.28725	0.62900
AVD MOND PL 71 10,314 1,1743 0,1417 0,27276 0,42200 72 10,314 1,1743 0,1417 0,27276 0,42200 73 10,314 1,1743 0,1417 0,27276 0,42200 74 10,314 1,1743 0,1417 0,27276 0,42200 75 10,314 1,1743 0,1417 0,27276 0,42200 75 10,314 1,1743 0,1417 0,40734 0,40704 76 10,4071 0,40734 0,40734 0,40805 0,50800 77 1,1017 0,417 0,4171 0,4734 0,40734 0,40806 0,50800 78 1,417 0,4171 0,40734 0,40734 0,40806 0,40170 79 1,417 1,7087 0,7087 0,1618 0,40805 0,1618 0,40700 79 1,417 1,7087 0,7088 0,1618 0,40806 0,4018 0,40806 0,4018 0,40806 0,4018 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0,40806 0		9.0589	2.7990	0.12449	0.28804	0.72700
17 7,2738 2,2734 0,29247 0,29276 0,42000  2AOTH TOWAL PRESSURE PATINS , FLOW SPITTER C.D.  AND WIRD PL MYND PL/PTE PL/PTE X/DMAX  AND WIRD PL MYND PL/PTE D. 0,40531 0,03782 0,50800  12 14.677 4.5313 0,20146 0,46541 0,59800  22 14.677 4.5313 0,20146 0,46641 0,59800  23 14.677 4.5313 0,20146 0,46641 0,56612 0,58800  2AODITIONAL PRESSURE PATINS , EJECTOR SHPOUD  AND WIRD PL MYND MYNTE MYPTE X/DMAX  AND WIRD PL MYND MYNTE MYPTE X/DMAX  1107 4.4125 1,4623 0,60560 0,14015 0,62400  1117 4.31574 1,4647 0,04680 0,14015 0,62400  1117 4.31574 1,10703 0,547897 C,11011 1,0500  1127 3,4667 1,10703 0,547897 C,11011 1,0500  1137 3,4660 1,1012 0,64640 0,11230 1,2200  1142 3,5144 1,0910 0,64640 0,11230 1,2200  1152 4,4125 1,4623 0,60560 0,1105  1171 4,4125 1,4623 0,60560 0,14015 1,6000  1172 4,4125 1,1023 0,66460 0,11230 1,2000  1173 4,4125 1,1023 0,66460 0,11230 1,0000  1174 1,102 0,64640 0,646740 0,14015 1,0000  1175 1,4417 1,0000 0,646740 0,11230 1,0000  1176 1,4500 1,1012 0,66460 0,11230 1,0000  1177 1,4617 1,0000 0,646740 0,11230 1,0000  1179 1,4617 1,0000 0,646740 0,11230 1,0000  1170 1,4617 1,0000 0,646740 0,11230 1,0000  1171 1,4617 1,0000 0,646740 0,11230 1,0000  1177 1,4617 1,0000 0,646740 0,11230 1,00000  1177 1,4617 1,0000 0,646740 0,11230 1,00000  1177 1,4617 1,0000 0,646740 0,11230 1,00000  1179 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,00000  1170 1,4617 1,0000 0,646740 0,11230 1,000000  1170 1,4617 1,0000 0,646740 0,11230 1,000000  1170 1,4617 1,0000 0,646740 0,11230 1,00000000000000000000000000000000000	>ADDITIONAC	AL PRESSUPE	PATIOS . FEE	W SPLITTEP I	. O.	and the state of t
77 7,238 2,2336 3,299287 0,22876 0,67000  >ANDITIONAL PRESSURE PATING, FIRM SHITTER C.D.  77 79,577 9,161 0,40531 0,93782 0,50800  92 14,677 4,5313 0,29146 0,46615 0,587649 0,10019 0,67000  >ANDITIONAL PRESSURE PATING, FIRM SHPRUD  ANDITIONAL PRESSURE PATING, FIRM SHPRUD  107 4,125 1,1673 1,00605 0,10015 0,62400  112 4,3674 1,1063 1,00605 0,13856 0,14015 0,62400  112 4,3674 1,1129 0,00671 0,13856 0,83000  112 4,2574 1,1129 0,00671 0,13856 0,83000  112 4,2574 1,1129 0,00671 0,13856 0,83000  1137 3,4667 1,1010 0,0247887 C,11011 1,0900  1177 3,4667 1,1010 0,0247887 C,11011 1,0900  1177 3,4667 1,1010 0,048780 0,11128 1,2000  1177 3,4667 1,1010 0,048780 0,11128 1,2000  1177 3,4667 1,1010 0,068781 0,11128 1,2000  1177 3,4667 1,1010 0,068781 0,11128 1,2000  1177 3,4667 1,0010 0,068781 0,13056 1,0000  1177 3,4667 1,0010 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,13056 1,0000  1177 3,4667 1,0000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0,068781 0,10000 0	AVD WORD	PI.	PL / PO	PL/PTF	PI /PTP	K/DMAX
AND TITIONAL PRESSURE PATIOS , FILM SPLITTEP P.D.  AND WINDS 77 79-527 9-1161 0.40531 0.93782 0.50800 12 14-677 4-5313 0.20146 0.40531 0.93782 12 3.4567 1.0667 0.36744 0.10979 0.67000  >ANDITIONAL PRESSURE PATICS , EJECTOR SHAPOUGO  AND WIND PL N/PR PIPET PATICS , EJECTOR SHAPOUGO  1107 4-4125 1.3623 0.00554 0.10053 0.42000 1112 4-3674 1.3169 0.058731 0.13550 0.42000 1121 4-3674 1.3169 0.058731 0.13550 0.40000 1122 4-2576 1.3169 0.058737 0.13550 0.40000 1123 3-4667 1.0703 0.247887 C.11011 1.0500 1124 3-3668 1.1012 0.058848 0.11233 1.3500  1147 3-4647 1.0703 0.247887 C.11011 1.0500 1157 3-4647 1.0703 0.247887 C.11011 1.0500 1167 4-4125 1.3623 0.000509 0.11202 0.0000  AND WINDS PL NORTH RESSURE PATICS POSTATOR NITE PLANE PATICS POSTATOR NITE PATICS PLANE PATICS PATICS PLANE PATICS PATIC	62	10.314		0.14157	0.32758	0,42200
AVID WIRD PL 77		7.213A	2.2334	0.399297	0.22976	J.67000
77	MUI TECON	AL PRESSUPE	PATINS . FIR	W SPITTER P	. D.	a de la composição de l
77	AVD HORD	PL	Pt / PO	PL/PTF	PL /PTP	x/max
122 14,677 4,5313 3.20146 0.46615 3.58000  >ADDOLLIONAL PRESCURE PATICS , EJECTOR SHAPOUD  AVENUADD PL M/PT PL/PT PL/PT X/DRAX  AVENUADD PL M/PT PL/PT PL/PT X/DRAX  117 4,4125 1.3623 3.66682 0.13556 0.46600  117 4,4125 1.3629 3.66682 0.13556 0.46600  117 3.4667 1.3703 0.247847 C.11011 1.0600  117 3.4667 1.3703 0.247847 0.11233 1.3500  ***ANT TOPP PL M/PT PL/PT PL/PT PL/PT X/DRAX  AVENUADD PL M/PT PL/PT PL/PT PL/PT PL/PT Y/DRAX  AVENUADD PL M/PT PL/PT PL/P						
27 3.467 1.0677 0.347449 0.10979 0.67000  >ADDOITIONAL PRESSURE PATICS . EJECTOR SHPOWD  AVE WORD PL 107 4.4625 1.3623 3.069569 0.14015 0.62400  112 4.3674 1.31469 0.054807 0.13956 0.43000  112 4.3674 1.31469 0.054807 0.13906 0.40000  117 3.4666 1.3012 0.064800 0.11010 1.09200  117 3.4666 1.3012 0.064800 0.11010 1.09200  118 3.4666 1.3012 0.064800 0.11010 1.09200  119 3.4666 1.3012 0.064800 0.11010 1.09200  110 4.4625 1.3623 0.060569 0.14015 1.00000  240313140044 ANCECUMA AUTOC FORFATON LILEY  AND TOPD PL 117 4.3624 1.3464 0.069570 0.14015 1.00000  117 4.4625 1.3623 0.060569 0.14015 1.00000  117 4.3624 1.3464 0.069571 0.13866 1.00000  117 4.3624 1.3464 0.069571 0.13866 1.00000  117 1.3960 1.1012 0.068900 0.12029 1.00000  117 1.9960 1.1012 0.068900 0.1223 1.00000  117 1.9960 1.1012 0.068900 0.1223 1.00000  118 1.9970 0.067900 0.10015 1.00000  2401311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067241 0.10031 1.00000  2501311101111 1.0026 0.067312 0.10031 1.00000  2501311101111 1.0026 0.067312 0.10031 1.00000  2501311101111 1.0026 0.067312 0.10031 1.00000  2501311101111 1.0026 0.067312 0.10031 1.00000  250131111111 1.0026 0.067312 0.10031 1.00000  2501311111111 1.0026 0.067312 0.10031 1.00000  25013111111111 1.0026 0.067312 0.10031 1.00000	92					
AVE WERD PL MI/PD PI/PT PI/PT X/DRAX  107 4-8125 1-16-23 3-069569 0-14015 0-62400  112 4-3676 1-1129 0-058-71 0-13506 0-64000  127 3-667 1-0703 0-25757 C-11011 1-0500  137 3-666 1-1012 0-0646-60 0-1129 1-2200  147 3-5566 1-1012 0-0646-60 0-1129 1-2200  147 3-5566 1-1012 0-0646-60 0-1129 1-2200  147 3-5566 1-1012 0-0646-60 0-1129 1-2200  147 3-5566 1-1012 0-0646-60 0-1129 1-2200  147 3-5566 1-1012 0-0646-60 0-1129 1-2200  147 3-5566 1-0646 0-06567 0-14015 1-2200  147 3-5566 1-0661 0-06567 0-14015 1-2200  147 3-5674 1-0675 0-06757 0-14015 1-2000  147 3-6674 1-0675 0-06757 0-12000 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-0600 1-06000 1-06000 1-06000 1-06000 1-06000 1-06000 1-06000 1-06000 1-06000 1-06000 1-06000 1-06000						
107	>ADDITION	AL PRESSURE	PATIFS - EJE	CTOP SHPOUR		
107	440 4000	<u>.</u>		AT 4545**	- 2. 2. 2. 2.	F TO THE RESIDENCE OF THE PROPERTY OF THE PROP
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137   3.5668   1.1012   0.C4840   0.11233   1.3500						
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-107	Limited	A ASE CEUME	AATIOS . FOR	FACOL ILLEY	<del></del>	
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-127 4.667 1.0763 0.757547 0.15016 -1.0000 -127 1.7668 1.1012 0.048660 0.1229 -1.0000 -1-12 1.536 1.0919 0.048548 0.11233 -1.0000 -1-12 1.536 1.0919 0.048548 0.11233 -1.0000 -1-152 1.4417 1.076 0.047241 0.10031 -1.0000 -157 3.4417 1.076 0.047241 0.10031 -1.0000  SPROTYTICKET PRESSURE RETURN FAR HITTITY FURP  AVO MORD PL 1.0676 0.047243 0.10031 -1.0000 -1-52 3.4417 1.0676 0.047243 0.10031 -1.0000  SERDITICKET PRESSURE PRIVING TO THE SUPPLY TOWNEY  AVO MORD PL 9/PD M/PT 1/PTP X/DMAY -1-52 3.4467 1.0676 0.047243 0.10031 -1.0000  SERDITICKET PRESSURE PRIVING TO THE SUPPLY TOWNEY -1-12 3.4467 1.0641 0.047312 0.10647 -1.0000  STOCKET PL 9/PD M/PTF N/PTP X/DMAY -1-12 3.4467 1.0641 0.047312 0.10647 -1.0000  STOCKET PRESSURE PRIVING TO THE SUPPLY TOWNEY -1-12 3.4467 1.0641 0.047312 0.10647 -1.0000						-)-6000
-127	-112			O. C59882	0.13856	1.0000
-127 1.786.8 1.012 0.04860 0.12.29 -1.0000 -142 1.536 1.0019 0.04860 0.12.29 -1.0000 -143 1.536 1.0019 0.04860 0.12.29 -1.0000 -157 3.4417 1.076 0.047243 0.10011 -1.0000 -157 3.4417 1.076 0.047243 0.10011 -1.0000  -28037777048[ PPF5SUPF RATIOS FAW NU7717 FIRP  AVO MORD PL FL/PD 1/PT PL/PTP X/DWAY -152 3.4417 1.0676 0.047243 0.10001 -1.0000 -157 3.4417 1.0676 0.047243 0.10001 -1.0000 -157 3.4417 1.0679 0.047243 0.10001 -1.0000 -157 3.4417 1.0679 0.047243 0.10001 -1.0000 -15037777041 PRFSSUPF PATIOS 70 DEG SUPPON INCATION  AVO MORD PL PL/PD M/PTF NL/PTP X/DWAY -10.2 3.4467 1.0641 0.047312 0.10647 -1.0000 -177 3.4467 1.0641 0.047312 0.10647 -1.0000 -179 3.4467 1.0641 0.047312 0.10647 -1.0000						-1.0000
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-140	-1 2 7		1.1012	0. 648960	0. LF 29	-1.0000
-157 3.4617 1.0676 0.C47243 0.1031 -1.0000  SENDATY WORKS PERSTAPE BAYING FAW NOTTH FLAP  AVO WORD PL FL/PC 1/071 PL/PTP M/DWAW -152 3.4617 1.0676 0.047243 0.1031 -1.0000 -157 3.4617 1.0679 0.047243 0.1031 -1.0000  SENDATY POWER PRESSURE PRAYING 70 DEC SUPPLY INCATION  AVD WORD PL PL/PC PL/PC M/PTP	-147	3.536	1.0919	0.048548		
SANGYTYONAL   PRESSURE RAYING   FAM NOTTO FLAD   AVO 4000   PL   PL/PC   1/P71   PL/PTP   X/DMAX    -1-2   3.4417   1.0626   0.067243   0.10031   -1.0000    -1-57   3.4417   1.0621   0.047243   0.10031   -1.0000    -1-70   3.4417   1.0621   0.047243   0.10031   -1.0000    -1-70   3.4461   1.0641   0.047312   0.10047   -1.0000    -1-70   3.4467   1.0641   0.047312   0.10047   -1.0000    -1-70   3.4467   1.0641   0.047312   0.10047   -1.0000    -1-70   3.4467   1.0641   0.047312   0.10001    -1-70   2.0962   3.02505   3.041129   0.000164   -1.0000    -1-70   3.0463   3.04651   0.041129   0.000164   -1.0000						
AVD HORD PL PLYPE , 70 DEC SHPTON TOTAL TONAN  AVD HORD PL PLYPE PRYPE , 70 DEC SHPTON TOTAL TONAN  -16.7 3.4467 1.0641 0.047312 C.10947 -1.0000  -17.7 3.4467 1.0641 0.047312 C.10947 -1.0000  -17.7 3.4467 1.0641 0.047312 0.10647 -1.0000  -17.7 3.4467 1.0641 0.047312 0.10647 -1.0000  -17.7 3.4467 1.0641 0.047312 0.10647 -1.0000	-157	3.4417	1.0f 76	1.547243	0.10931	-1.0000
-1-2 3.4417 1.0626 0.047243 0.10931 -1.0000 -1-57 7.4417 1.0626 0.047243 0.10931 -1.0000  SENSITIONAL PRESSURE PRIVAC., 20 DEC SHPERM INCATION  AVD MCPD PL PLAND PLAND PLAND PRIVACY PRIVACY PRIVACY PLAND PRIVACY PR	250 <b>334.4</b> 04	N [ PPF 5 S()PF	HEAL SULLER	MITTIE FLED		
-1-7 3.4417 1.0676 0.067243 0.10931 -1.0000 -1-57 3.4417 1.0676 0.067243 0.10931 -1.0000  >ENDITIONAL PRESSIME PRIVING , 20 DEG SHPTON INCATION  AVD HOPD PL PL/PD M/PTF NI/PTP X/DMAY -1-7 3.4461 1.0641 0.047312 0.10647 -1.0000  >1-70 3.4467 1.0641 0.047312 0.10647 -1.0000  >1-70 3.4467 1.0641 0.047312 0.10647 -1.0000  >1-70 3.4467 1.0641 0.047312 0.10647 -1.0000	AVO HORD	Pŧ	FL/PC	MINTI	PL /PTP	Y/DMAY
-157 7.4417 1.0624 0.047243 0.10031 -1.0000  SENSITY INVEST PRESSURE PRYSES, 20 DEG SHPFOR INCATION  AVO HOPD PL PI/PO PI/PTP X/DMAN -16.7 3.4467 1.0641 0.047312 0.1047 -1.0000 -172 3.4467 1.0641 0.047312 0.1047 -1.0000  S13317 INVEST PRESSURE PRISTOS, RO (NEG SHPFOR INCATION  AVO HOPD PL PI/PO PI/PTP Y/DMAN -102 2.9962 3.02505 3.041179 0.095164 -1.0000						
AVD MCPD PL PI/PD PI/PTP X/DMAX -16.7 3.4463 1.0641 0.047312 0.10447 -1.0000 -177 3.4467 1.0641 0.047312 0.10467 -1.0000  S10011   PHI STORE PATIONS , NO (NEC SINCUS INVATION  AVD MCPA PL PI/PD PI/PTP X/DMAX -107 2.9962 0.02505 0.041179 0.005164 -1.0000						
-16.7 3.4467 1.0641 0.047312 C310947 -1.0000 -172 3.4467 1.0641 0.047312 0.10647 -1.0000  S10017   PHOTO PI PI PI / PO PI / PTP P	SENSITION	IT PRESSIBE	PZ 1995 . 20	HE SHE THE	OCATION	
-16.7 3.4467 1.0641 0.047312 C.10947 -1.0000 -177 3.4467 1.0641 0.047312 0.10647 -1.0000  S17717   PHI PI	AVD WEED	PI	PI / PO	M /PTE	91 /910	A WAY.
-17" 1.0641 0.047312 0.10647 -1.0000  >171711   PRINT   PRESSIME PRINTS ; NO THE SIMILIO THERTIPM  AVO WORD PL PL/PO PL/POT PL/P						
247717   PRESSIME PATIOS , NO DEC SINCUS TOTATION  AVO MOST DE PE/PO PE/PTP S/DES  2.99/2 2.99/2 2.92505 2.041179 0.045164 -1.0040						
AVO MEN PI PI/PO PI/PTF PI/PTP Y/MAX -107 2.99/2 7.07505 7.041179 0.705164 -1.0000	**************************************		PRT105 . 80	-		
-107 2.09/2 7.02505 7.041129 0.005164 -1.0000	_					
7000 T 37130 0 17010 C 13030 C 13030 C						
7.0463 7.94051 0.041816 0.096754 -1.00000 ACTITUE 5 , MEASURED THRUST PARAMETERS	-107/					
STOTILE 5 . MEASURED THRUST PARAMETERS	سمز-				0.096754	4 -1.0000
	Virginia 5	. MEASUPED	THRUST PARAM	t & Luc		

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	SETTION	If boEssibe	RATIOS . PP I	MARY PLUG				
	AVM WMPN	PI	<b>PI /</b> PO	PL/PTF	PI /PTP	X/OMAX		
	3?	12.071	3. 7265	0.16590	0.43068	J. 43200		
	37	6.3891	1.9725	0.087811	0.22797	0.53000		
	47	P. 0650	7.4890	0.110A4	0.29776	0.62400		
	57	P.0750	2,4091	0.11126	0.28884	J. 72703		
$\widehat{}$	>4701111044	I PPESSIPE	PATIOS . FLO	W SPLITTEP L	. n.			i de la compansa del compansa de la compansa del compansa de la co
	AVO WODD	Pl.	PL/PO	M /PTF	PI /PTP	X/DMAX		
<u>~</u> .	67	9.2304	7. 2404	0.12645	0.32827	0.42200		
		6.4592	1,9941	0. C48774	0.23047	0.67000		
	>427111004	IL PRESSUPE	PATIOS , FLO	W SPLITTEP O	.n.			Company of the compan
	AVD WORD	PI	<b>ም</b> ር / ምብ	PI /PTF	PI /PTP	X /DMA X		
	77	29.455	9, 3935	0.40483	1.0510	0.50000	and the second s	
	A2	14.455	4.5244	0.20142	0.52290	0.58300		
•	G?	3.4613	1.0686	0.047572	0.12350	J. 67000		
	>AODIT ION	L PRESSIÑE	PATIOS . EJF	CTOP SHPIND		æ.		
	AVD HEPD	PL	PL/PG	PL / PTF	PL/PTP	X/DMAX		
	1.97	4.4024	1.3591	0.060506	0.15709	0.67400		
-	112	4.3523	1.3437	0.055818	0.15529	0.83000		
	122	4.2572	1. 3128-	7. 358442	0.15172	0.96000		
	177	3.4563	1.0670	0.047503	0.12332	1.0430		
	137	3.2710	0.90440	0.744269	0.11493	1.2200		
	142	3.1759	·), 98:34:1	0.047649	0.11332	1.2500		
-	C Propinion	-	14105 - FOE	troom Inter				
	AVE HOP D	PL	PI /PI	PL /PTF	PL /PTP	X/DHAY		
	-10-	4.4:374	1.3591	0.060596	0.1570F	-1,0000		
	-117	4.3523	1.3437	0.059819	0.15529	1.0000		
	-122	4.2522	1.3126	0.058442	0.15172	-1.0000		
•	-177	3.4563	1.0670	0.047503	0.12332	-1.0000		
	-137	395510	0. 97440	0. 344269	0.11493	-1.0000		
	-147	3-13-65	9.08949	9.763669	0,11332	-1.0000		
	-157	3.4413	1.0.24	0.047296	0.12279	-1.0000	****	
	-157	7.4413	1.0624	0.067295	0.12279	-1.0000		
•	שחו דורה לכ"	I PRESSIBE	PATINE, CAN	HOZZLE FLAP				
	AVD HOPD	PL	PL/PIT	AL IPTE	PL /PTP	K/DMAX.	····	
	-152	3.4413	1.0626	0.047796	0.12279	-1.0000		
-	-1 = 7	1.4413	1.0624	14 77 04	6.12279	-1.0000		The state of the s
	SINOTTINN	L PRESSURE	13 yrk - 20	ा तुम्लक्षर <b>उ</b> न्न	NPAY IPM			
-	מערו ווחפט	PL /	PL /PI	PL/PTF	PI /PTP	x/DHAX	·	
	-1+7	3.4915	1.0674	0.047296	0.12270	-1.0000		
J	-177	3,0413	1.0624	0.047296	0.18510	-1.0000		W 10 to the page about a gire off to the season of the
	עימודדומרגל	PRESSIBE	PATTOS . 40	NEC SPECIM TI	**************************************			
_	AVO AVEO	Pl	PL/PN	PL /PTF	PI /PTP			ay pagga a pipa gagg gal maja dan kabasanahkada iba ana Madalah da Sharahada ki basanah da sa ana da sa ana da
	-19-4-11	2.0057	7.97484	9.041177	0.19689	ANDOX -1-		
	7	1. 3457	7. 6403A	0.041863	0.13867			واهم الموادد ا
	SCOTIFE F		THRIST PARAM		0.1 2967	-1.0000		
				3 ¥ -3		a a		La
	•			197			0.3	, and the second of the second

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414 C A 4 E1/ **	005154	INARY CATA	16 # 10 # 70	CADDE	BEC 13/11/70 0/11/110 00	Roy I	-
かんてなーI FWIS		BHARY DATA	)f / 19/79	CAPRE11	PEC 10/11/79 04:14:12,09	FAC #4641PGM CQ34 RNG 10	r-0
>600111004	I PRESSIME	CATIOS . PPI	AYEA SI NO				
AVD UPPD	թլ	PI /PG	PI / PTF	PI /PTP	H/DMAH		
32	17.469	5.3604	7.21546	0.43006	0.43200	The state of the contract of t	
37	9.166R	2.8133	9.11397	0.22569	0.53000		
47	11.621	3.5662	0.14234	0.28612	0.67900	The state of the s	
52	11.696	3.5962	0.14415	0.28772	0.72700		
>^^0111044	IL PRESSURE	PATINS . FLE	₩ SPLITTEP 1.	n.			
AVD WOPD	•	PL / PO	PL / PTF	PL /PTP	X\UaVX		
	PL 13.371	4.0816		0.32746			
62 67	9.3368	2. A560	0.16406 0.11479	0.22913	0.42200 0.67000		
					0-67-100		
>APPET FORM	E PRESSURE	PATIOS . FLO	W SPLITTEP O	.ņ.			
AND MUND	PL	PL / I'M	PI /PTF	PL /PTP	X/DMÁX		
77	32.801	10.766	0.40459	0.00757	J. 50800		
<b>P</b> 2	16.284	4.9970	0.200RS	0.40001	0.58300		
92	3.4942	1.0492	0.042577	0.075782	0. 67000		·
NOT TERRAS	L PRESSIPE	RATERS FJE	CTCP SHPOUD	- · · · · -			<del></del>
VO WORD	ěl.	Pi / PO ***	M /PTF	PL /PTP	X/DMAX		<del></del>
107	4.9304	1.5038	0.060445	0.12065	0.62400		
115	4.8404	1.4854	0. C59704	0.12065	J. 8300)		<del></del>
122	4.7303	1.4516	0.058346	0.11646	0. 96000		
127	3.4893	1.0707	0.043039	0.08505	1.0900		
137	4.5101	1.3849	0.055631				
142	4.4401	1.3625	0.054766	0.11104 0.10932	1.2200		
•							
7 100 11 1000	T BRECENOE	* 1 T 105 + FM	+ water - 164 E +		<del></del>		
יז פונות עואו	PL	PL /PIT	PL/PTF	Pi /PTP	x/549x	•	
-107	4.9034	1.5038	D. C60445	0.12065	-1 0200		
1112	4. 94.14	1.4854	0.059704	0.11517	1.0000		
-177	4.7333	1.4516	0.058346	0.11646	-1.0000		
-127	4R93	1.0707	0.043039	0.085965	-1.0000		
-137	4.74.01	1.3840	0.055631	0.11/04	-1.0000		
-147	4.447	1.3625	0.054766	9/10432	-1.0000		
-152	3.4592	1.0615	0.04266	0.085166	-1.0000		
-157	1.4642	1.0631	0.04273	0.685289	-1.0300		<del></del>
SANSTY INVA	C PRESSURE	HAT PRITTER	FLAP		· · · · · · · · · · · · · · · · · · ·		
ND MUNU .	PI	PI /PO	PL/PTF	PE /PTP	R70MAX		<del></del>
-152	3.4592	1.9615	D. 642668	0.085166	-1.0000		
157	3.4642	1.0631	03042730	0.085280	-1.0000		
SEGULT TUNK	f_bbE241bE	PATEN . 20	DEG SHPOMET	CATION			
ומט אינטו	PI /	PI /PO	PL /PTF	N./PTP	K/DMAX	o na como una que <mark>que que escalaciones deles en el encuención de la composição de la compo</mark>	
-167							
-167 -173	3.4692	1.0431 1.0415	0.042730 0.04266#	0.085166	-1.0000		
-1 -:		1.0011	7. V1/05"	0.000/00	-1.0000		
עירו דוחרוג	TARIPPART T	PATING . RO	THE SHPTIMENT	CEALUM	<u> </u>		
	0.4	AL 460		D1 4055			
חיושע חעו	P1 3.0338	P[ / PO	PI /PTF	PI /PTP	XAIMAX		
	~ _(1) { 575	0.57097	0.637429	0. 374692	-1.000		
-1 °2' 1 P 7	3.0799	0.94480	0.037976	0.375801	-1.0000	por a company of the	

						RON 15
	MASA-LEWIS	PRFL [4]	IMPRY DATA	06/10/79	CADDFII	REC 10/11/79 04:15:39,669 FAC 91611 PGT C034 RDG 1991
	>400 t tone					
	such i i i i i i i i i i i i i i i i i i i	F LAI 770AL	PATIOS . PE	IMARY PLUG		
	AVD MORD	PL	PI / PO	PL/PTF	PL /PTP	x/DMAX
	17	15.003	4.5969	0.18509	0.43063	0.43200
	37-	7.9171	2.4243	0.097611	0.22711	9-53000
	47	10. 303	7. ∪€ 49	0.12349	2.28712	3.62500
	52	10.048	3.0787	0.12396	0.29841	0.72700
_						
	>APPIT IONAL	L PRESSUPE	RATIOS . FLO	IN SPLITTER I	• 0•	
	AVD HOED	PL	PI /PO	, PL/PTF	PL/PTP	X/OMAX
	62	11.413	3.4970	0.14080	0.32769	0.42200
	67	8.0072	2.4534	0.098783	0.22983	0.67000
-						
	>ADDIT TONAL	L PRESSURE	RATIOS , FLO	ON SPLETTER O	. D.	
	445 4656	•	en 400	m 4877		T COMP
	AVD MUKD	PL	Pt /Pfi	PL/PTF	PL /PTP	K/DMAX
	77	32.655	10.006	9.47286	0.93732	0.50890
	- <del>62</del>	16.252	4.47 98	0.20050	0.46650	0,58300
	42	3.4831	1.0672	0.042971	0.099978	0.67000
	SAPRITICHAL	L PRESSUPE	LE . SOITAR	FCTCR SHPOIN		
	**** *****					
	AVO MORO	PL	PI /P()	PL/PTF	PL /PTP	1/0mAx
_	107	4.8948	1.4999	0.060396	0.14050	0.62400
	117	4. 9348	1.4814	0.059645	0.1 2877	0-83000
	127	4.7296	1.4492	0.05#349	0.13576	0. 96000
	127	3.4831	1.0672	0.042971	0.09997#	1.040
	137	3.9287	1.2030	0. 348468	0.11277	1.2700
	142	3-9137	1.1992	0.94#297	0.11234	1.3500
~	C-149011 IB444	PACSTURE	****** + ***	IFARRY SALFT		
			المناسعين عوالا		<u> </u>	
	TALLAURU	PL	PL / PO	PL/PTF	PI /PTP	1/may
	-107	4.8948	1.4798	0.060386	0.14050	-1,000
	-112	4.834R	1.4R14	0.059845	0.13477	1.0000
_	-12?	4.7296	1.4492	0.058349	0.13576	<b>-1.0000</b>
						-1.0000
			1.0672	0. 642971	C. 099934	
	-137	3.9297	1.2939	9.048468	C.13217	-1.0000
	-137 -143	3.9297	1.2939	9.048468 9.048282	0.11277	-1.0000 -1.0030
	-137 -143 -152	3.9297 3.9138 3.6631	1.2939 1.1992 1.0611	9.048468 9.048282 9.042724	0.11217 0.11234 0.099403	-1.0000 -1.0030 -1.0000
	-137 -143	3.9297	1.2939	9.048468 9.048282	0.11277	-1.0000 -1.0030
	-137 -143 -152 -157	3.9131 3.9131 3.6631 3.6631	1.2939 1.1992 1.0611 1.0611	9.048468 9.048282 9.042724	0.11217 0.11234 0.099403 0.099403	-1.0000 -1.0030 -1.0000
	-137 -143 -152 -157 >ADATY (CHA)	3.9297 3.9138 3.6631 3.6631 PRESSURE	1.2739 1.1092 1.0611 1.7611	9.049468 9.048282 9.042724 0.042724	0.11277 0.11234 0.099403 0.099403	-1.0000 -1.0000 -1.0006
	-137 -14? -152 -157 -157 -157 -157	3.9497 3.9138 3.6631 3.6631 PRESSUPE	1.2736 1.1997 1.0611 1.0611 PATINS FAR	9.048468 9.048282 9.042724 0.042724 HARZEE FLAP	0.11277 0.11234 0.099403 0.099403	-1.0000 -1.0000 -1.0006
-	-137 -142 -152 -157 -157 -157 AVD SUPD -157	7. 197 7. 9137 3.4631 7.4631 PAFSSUPE PL 3.4631	1.2736 1.1097 1.0611 1.7611 FAT[05 FAR PI /PO 1.0611	9.048468 9.048282 9.042724 0.042724 1 402215 FLAP 0.042724	0.1234 0.099403 0.099403	-1.0000 -1.0030 -1.0000 -1.0006
	-137 -14? -152 -157 -157 -157 -157	3.9497 3.9138 3.6631 3.6631 PRESSUPE	1.2736 1.1997 1.0611 1.0611 PATINS FAR	9.048468 9.048282 9.042724 0.042724 HARZEE FLAP	0.11277 0.11234 0.099403 0.099403	-1.0000 -1.0000 -1.0006
~**	-137 -142 -152 -157 -157 -157 -157	3.4631 3.4631 3.4631 PRESSIDE PL 3.4631 3.4631	1.2736 i.1097 1.0611 i.7611 PATINS FAR PI /PN 1.0611 1.3612	9.04468 9.042724 9.042724 9.042724 1 MOZZLE FLAP PLAP 0.042724 75.642724	0.11237 0.11234 0.099403 0.099403 71 /FTP 0.099403 0.099403	-1.0000 -1.0030 -1.0000 -1.0006
~**	-137 -142 -152 -157 -157 -157 -157	3.4631 3.4631 3.4631 PRESSIDE PL 3.4631 3.4631	1.2736 1.1097 1.0611 1.0611 FATINS FAR PL/PN 1.0611 1.3611	9.048468 9.048282 9.042724 0.042724 1 402215 FLAP 0.042724	0.11237 0.11234 0.099403 0.099403 71 /FTP 0.099403 0.099403	-1.0000 -1.0030 -1.0000 -1.0006
-	-137 -142 -152 -157 -157 -157 -157	3.4631 3.4631 3.4631 PRESSIDE PL 3.4631 3.4631	1.2736 i.1097 1.0611 i.7611 PATINS FAR PI /PN 1.0611 1.3612	9.04468 9.042724 9.042724 9.042724 1 MOZZLE FLAF PLAF 0.042724 75.642724	0.11237 0.11234 0.099403 0.099403 71 /FTP 0.099403 0.099403	-1.0000 -1.0030 -1.0000 -1.0006
	-137 -152 -157 -157 -167 -167	3.4631 3.4631 3.4631 3.4631 3.4631 3.4631 PRESCIPE	1.2736 i.1097 1.0611 1.7611 PATIOS FAR PLOG11 1.3612 RATES . 70 PLOG11 1.0611	9.04468 9.042724 9.042724 9.042724 1 NOZZIF FLAF 1 /PTF 0.C42724 TREG SHIFTING II PI /PTF 9.042724	0.11234 0.099403 0.099403 0.099403 0.099403 0.099403 0.099403	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	-137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	3.4631 3.4631 PRESSIDE PL 3.4631 3.4631 PRESSIDE	1.2736 1.1097 1.0611 1.7611 FATINS FAR PLANT FAR 1.0611 1.3611 FATINS . 70 PLANT . 70	9.048468 9.042724 9.042724 1.042724 1.402215 FLAP 0.042724 7.642724 7.642724 7.642724	0.11234 0.099403 0.099403 0.099403 0.099403 0.099403	-1.0000 -1.0000 -1.0006 -1.0006 -1.0000 -1.0000
	-137 -142 -152 -167 -167 -167 -167 -167 -167 -167 -172	7. 0131 3.4631 3.4631 PAFSSIME PL 3.4631 3.4631 PMFSSIME PL 3.4531 PMFSSIME	1.2736 1.1092 1.0611 1.0611 1.0611 1.0611 1.3612 PATENTS . 70 PI /PII 1.0611 1.0611 1.0611 1.0611 1.0611	9.048468 9.048282 9.042724 9.042724 1.40221 FLAP 0.042724 7.642724 THEG SHAPFIRE 11 P1 / PTE 9.042724 0.042724	0.11234 0.099403 0.099403 0.099403 0.099403 0.099403 0.099403	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	-137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -167 -167 -172	7. 0131 3.4631 3.4631 PAFSSIME PL 3.4631 3.4631 PMFSSIME PL 3.4531 PMFSSIME	1.2736 1.1092 1.0611 1.0611 1.0611 1.0611 1.3612 PATENTS . 70 PI /PII 1.0611 1.0611 1.0611 1.0611 1.0611	9.04468 9.042724 9.042724 9.042724 1 NOZZIF FLAF 1 /PTF 0.C42724 TREG SHIFTING II PI /PTF 9.042724	0.11234 0.099403 0.099403 0.099403 0.099403 0.099403 0.099403	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	-137 -142 -152 -157 -167 -167 -167 -167 -167 -167 -167 -16	7. 0131 3.4631 3.4631 PAFSSIME PL 3.4631 3.4631 PMFSSIME PL 3.4531 PMFSSIME	1.2736 1.1092 1.0611 1.0611 1.0611 1.0611 1.3612 PATENTS . 70 PI /PII 1.0611 1.0611 1.0611 1.0611 1.0611	9.048468 9.048282 9.042724 9.042724 1.40221 FLAP 0.042724 7.642724 THEG SHAPFIRE 11 P1 / PTE 9.042724 0.042724	0.11234 0.099403 0.099403 0.099403 0.099403 0.099403 0.099403	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	-137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	7. 0131 3.4631 3.4631 3.4631 3.4631 3.4631 PRESCIPE PL 3.4531 PRESSIBE	1.2736 i.1097 1.0611 1.7611 PAYINS FAR PI /PN 1.0611 1.3632 PAYINS . 70 Pi /PN 1.0611 1.0611 1.0611	9.04468 9.042724 9.042724 9.042724 1 NOZZIF FLAF 10.042724 10.042724 10.042724 10.042724 10.042724 10.042724	C.1177 0.11234 0.099403 0.099403  MI /PTP 0.099403  MIAYIMA 0.099402 0.099402 0.099403	-1.0000 -1.0006 -1.0006 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
***********	-137 -142 -152 -157 -167 -167 -167 -167 -167 -167 -167 -16	7. 1.9131 3.4631 3.4631 7.4631 3.4631 7.4631 7.4631 7.4631 7.4631 7.4631 7.4631 7.4631 7.4631	1.2736 i.1097 1.0611 1.0611 PATINS FAR M /PN 1.0611 1.3611 PATINS . 70 M /PN 1.0611 1.0611 1.0611	9.04468 9.042724 9.042724 1.042724 1.407215 FLAP 1.407215 FLAP 1.407215 FLAP 1.4072724 1.62724 1.62724 1.62724 1.62724 0.042724 0.042724 1.665 SHIPTUT TI	0.11234 0.099403 0.099403 0.099403 0.099403 0.099403 0.099403 0.099403 0.099403	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000

RON 13

MASA-LEW	IZ OKEFT.	ያቸለዋሃ ካልቸል	06/11/75	CARRETT	PEC 10/11/79 94:16:29.898	FAF 8X6X1 PG F034 PNG 1092
>٨٦٠١٢ [3	INT PRESSURE	PATIOS . PPI	MARY PLUG		the special designs and the special special states and the special spe	
AVO HOED	PL	of Auto	PL / PTF '	PI /PTP "	X/DM&X	
37	13.465	4-1755	0.16605	0.43047	9.43200	مسهرين والمساوية
3.7	7.1794	2.1783	0.097677	0.22729	), 53600	
47	A. 975)	7.7561	0.11093	0.28757	0.62500	ட்ட நாக்கிய படிகள் கண்டகள் கணியணுக்கில் அன்றும் விகையான முறுக்கிறும் கணிய மறிய வருக்கிறும் வரிய கணிய முறுக்கிற கணிய
52	0.0233	2.7637	0.11124	0.28837	0.72700	
>400   1 / 10*	ANT BEZZIME	PATIOS , FLO	W SPLITTER I	.0.	•	and the second of the second o
AVD HORD	PL	PL / PO	PI /PTF	PI /PTP	X/DMAX	
62	10.250	7.1406	9-12641	0.32770	0.42200	No. 1 (CAS) TO CAMPAIN SERVICE CONTRACTOR OF THE PROPERTY OF T
67	7.1944	2. 2713	0. CR8602	0.22969	0.67000	
>AnntTine	IAL PRESSUPE	PATIOS . FLO	W SPLITTER F	• D•		
AVO WORD	PL	PL/PO	PL /PTF	PL /PTP	X/DMAX	
77	32.689	10.016	0.49313	1.0451	3.50800	and the second second contract the second of
82	16.273	4.9861	0.20069	0.52026	3.58300	4
- 65	3.4915	1.0667	0.042935	0.11130	0.67000	
>A70 IT tOt	IAL PRESSIME	PATIOS . FJE				
					A DESCRIPTION OF THE PROPERTY	
TAU MUBD	PL	PL/PN	PL /PTF	PI /PTP	X/DMAX	
107	4.8979	1.5007	0.060434	0.15459	0.62400	
11?	4.0329	1.4808	0. 055401	0.15451	0.07000	
122	4.7178	1.4455	0.058182	0.15083	0.96000	
127	3.4915	1.0667	0.042935	0-11130	1.0900	
137	3.5716	1.0943	0.644047	9.11418	1.2299	
147	3.5365	1.0936	0.043615	0.11306	1.3500	
-	AL BAFCEUSE	evalue - coa	CADON THIEF			
AND HOPD	PĹ	PL/PÑ	<b>?L/PTF</b>	of /ptp	x/0nAx	
-107	4.4979	1.5007	9.060404	0.15659	-1_0000	•
-112	4.4329	1.4404	0.059601	0.15451	1.0000	
-122	4.7178	1. 4455	0.058182	0.15043	-1.0000	
-127	3,4915	1. 66.67	0.037177	0.11136	-1.0000	
-137	3. 116	1.0943	0.044047	0.11-16	-1.6000 -1.6000	
-142		1.0836	0.043615			
-15?	3.4665	1.3621	0.04275)	0.11306	-1.0000	
-157	3.4645	1. 16.21	0.042750	0.110#2	-1.0000 -1.0000	and the second and the second
				A+ 1 IAu5	-1.0000	
~~ 54n7JT for	IVE BEEZZIEE	RAYING FAR	F14P	· · · · · · · · · · · · · · · · · · ·		
TAU HUEU	PE	MI/PO	DI /PTF	PI /PTP	X/DMAX	, april process of the contract of the contrac
-15?	3.4465	1.0621	0.042750	0.11082	-1.0000	
-187	3.4665	1.36.21	0.042750	0.11042	-1.0390	and the second s
ምነ የተሰብጸኛ	INT PRESSURE	RAYMS . 20	DEC SHADO	HEATTON		
	rı /	PI /PO	PL / PTF	RI JPTP	K/DMAX	
AVO HODA	3.4654	1.0521				
AVD ৮ባዮቦ		1.0637	0.042750 ).0422[2	0.110A2 0.110AA	-1.0000 -1.0000	age cape of the control of the contr
-147						
-167 -172	3.5/15					
-147	3.5/15	PATTINS . PO	तहरू दक्षितिकार	reating		
-167 -172	3.5/15	P7 TYNS ; FO	PI / PTF	PL/PTP	карцах	
-147 -177 -3207171100 AVD WOMD -197	2.6/15 UP PPFSSUPF				v/huan -1-0/hua	
-147 -177 -277 	7./15 UM PRESSURE PL 3./1309 3.1910	Pt /PO	PI / PT F 0. 03 73 79 ). C3 7996	PL / PTP		

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~	4853-1 FH15	P9F1, 141A	ARY DATA	04/10/79	CADDELL	RFC 10/11/79	De:18:72.134	FAC 94643	PG# C934.	. buc 1043
,	APOITTONA .	i bekzenbe i	ATENS a PRI	MAPY PLUG		in . As come you are had referenced requires apprehiment or processes and	aggyang kanadinan sa kanaga digunak nagan da Adamaga kaya Manada da	Free print and the company of the contract of	en de la companya de	
$\overline{}$	AVD HOPD	PL	PL / PD	PL/PTF	PL /P1P	X/DMAX				
	3,7	19,422	5.8164	0.21236	0.42986	0.43200		20 12 11 AM	e niversa. I i su i a deservición de servición de la servición	water water to the control of the co
	37	9.8544	3.0452	0.1111#	0.22505	0.53000				
$\hat{}$	47	12,524	3.8793	0.14131	0.28603	2.62900			to a contract of the second section of the section of the second section of the section o	territoria de la compressa de
	52	12.549	3. 6907	0.14204	C.28752	0.72700				
_						V* 12.190				
^	>40017 10%	L PRESSIMF #	INTERS , FLE	W SPLITTER I	an.			100 - Marie	a supplier and the supplier of	manufic the one operationmentalized the ground out
	AVD HORD	P1	PL / PO	PL/PTF	PI /PTP	x/DMAX				
	£?	14.369	4.4473	3.16212	U. 37#16	3.42 <b>20</b> 0	-			
	67	10.029	1.0943	0.11316	0.22905	3.67000				
			ATING . FIE	W SPLITTER O		Annual Square State St. of Township of Square Special State St. of St. o				
							m m , where ever a	an erge de desse Marines (April 1980) est de distribuiro	un appendix non constructive and the designation of the second section of the second section of the second second section of the se	graph <del>thallian a magaing ag i prige to it latte</del> i rija v
	TAD MUAD	PL	PL /PO	PL/PTF	PL/PTP	X/DMAX	g in managers of a seguine of the con-			ويورا الراء الراء فيستخطع والوارونية والماكورة والموارقة
	77	35, 593	10.996	0.49147	0.81265	9. 50 <b>00</b>				
	P2	17.933	5.5176	9.29129	0.40726	0.56300		···		
	92	3.4550	1.0476	0.0.4481	0.078903	0.67600				
	>407111044	PRESSIRE P	ATINS , FJE	EČTIM SHPININ	· · · · · · · · · · · · · · · · · · ·	r - rapropii sebi ga, seda rapro	No. 4. American in the state	<ul> <li>Conjugació y contrô el le men permito i que transmituación de la conferencia.</li> </ul>	nog <del>alistica (anales negatione) es est</del> e e <del>stilles diffica (cas</del> e etc. esc	igggebings of the edition of the state of th
~	AVD HERD	PL	Pt. /Pñ	PL/PTF	PL/PTP	X/DMAX	يستهد منتز بالمداد يهداه منطوحات			
	481) MURII 197	5.3721	1.6601	0.060610		0.62400				
	112	5. 3220	1.6446	0.060046	0.12269	0.83000				
3	172	5.1919	1.6344	0.058579	0.12174	0. 96020				
•	127						and the second of the second	man in the second secon		haratheanters - Patricul - enthancemental and the con-
		3.4750	1.0738	0.039207	0.079361	1.0900				
	137 147	4.4716	1.5116	0.055189	0.11171	1.2200	and the second	and the second second second second		and the second s
	-	4.4165	1.4884	7.054342	0.11000	1.3500				
	/	POESSION O								
	TAUKUBU	PL	PL/PG	PL/PTF	PL/PTP	X/OMAK		•		
	-107	5.3721	1.6601	0.060610	0.12269	-1,0000				
-	-113	5.3223	1.644	0.969946	0.12154	1.0200		1 Trans. 188 1995 197 Manager Landson College 198		THE PARTY OF THE PROPERTY OF THE PARTY OF TH
	-127	5.1919	1.2044	0.058578	0.11057	-1.0000				
-	-127	4150	1.0730	0. 030207	0.0793/1	-1.0000				
	-137	4.7916	1.5116	0.055149	0.11171	-1.0000				
	-147	4. 9185	1.4986	0.054342	9/1000	-1.0000	and the second of the second o	The second secon	The second secon	And the second s
	-123	3.4449	1.0645	0.034848	0.078675	-1.0000				
	-157	3.4399	1.0630	0.028813	0.078560	-1.0006	a a consess	non videoscopus (merides <u>promi</u> se <del>escale</del> el 19 fro	the state of the s	
	े इंटिंग्स गिर्मी।	PRESSIPE P	ATTORY FAR	I WATELE FLAR	THE RESERVE OF THE PERSON OF T	Minima /				
•	ልህባ ሦርነድብ	PE	M /P0	AIRTE	PL /PTP	X/DMAX		والإستان والأساء المستعدم الأساء	The state of the second section of the section of the second section of the section	ganganan any ata by ganga palas. In albania – albania, in isi i
	-15.	3.4449	1.0645	NABREO .O	0.078675	-1.0000				
÷	-177	3.4300	1.0639	2230011	0.078560	-1.0220		r ≠ ranger = ==	ter organization and constitution of the const	gangari i dipini di daga 15. Sangangan dipini di manandan daga
	> ተባሳተየ የሰዛል	DEFTTMET	ATUS . 70	तहर सम्बद्धाः	neatenn	m. ye w mayyo we i q <del>the rest frame to the continue</del>				
Ų	ሊዋቦ ፈብዮክ	PL /	PL / PO	PL/PTF	Q1 /PTP	X/DMAX			and the second s	- May Mark Milly and a Mark of the control of the c
	-147	1.4333								
U	-17? -17?	3.4349	1.0430 1.)614	0.074911	0.27444	-1.0000 -1.000		المعاصف وهداده المحاسب المعارب الم	en a anno de dispulso e estre este este	Company of the control of the control of the control of
			रक्रालंड क्रा	ner simetin T			and the second s			
-										
۔ ن									the control of the major term in the design of the	and the second s
<u> </u>	AVE MOTOR	PL	Pt / Pf)	PL/PTF	PL /PTP	r Program				
<u>-</u>	-187		P( /P/) 	PL/PTF 0.034123	Pt /PTP 0.069070	* 71max -1 - 01ma				
~ س		PL 3, 3244 3, 3735		PL / PT F 0. 034123 0. 034744	Pt /PTP 0.069070 0.070378	# Prese -1 - 0000 -1 - 9030		سان سسخت د د	gen be belogue a	age to the second of the second

•							How 16
,	AVET-LENIA	; PRFLIM	INEPY DATA	06/10/79	CADDETT	REC 10/11/79 04:19:35.227	FAC BYEFT PGH C034 PNG 1044
	>enniting	LL PRESSIME	PATINS . PRI	HAPY PLUG	چا الا <del>مام المام /del>		
	AVD HIPD	PL	PL / PO	PI /PTF	PL /PTP	х /гінд х	
	32	16.396	5.0647	0.18524	0.43114	0.43200	en la companya da mangantan da m
	27	F.6160	2.6614	n. C97344	0.22656	C. 53000	
	47	19.935	3.3778	0.12355	0.28754	0.62900	் ஆண்டாயார் என பழும்பாணப்பட வருக்காளியும் உள்ள குடிய <del>முக்கும் ஆட்டியும் மறும் முற</del> ்கும் ஆண்டும் ஆண்டும் ஆண்டும் இரும் இரும்பது இரும்பது
	52	10.785	3, 3033	7.12411	0.24886	3.72790	
_	>ADDIT EDN	N PRESSURE	PATINS . FLO	W SPLITTER I	.n.	* (	
	AVD WORD	Pl	PI /PN	PL/PTF	PL /PTP	Y/DMAX	t mine the second of the secon
	67	12.479	3.8548	0.14099	0.32815	J.42200	i de i degra que acción como la como a que experior as delaceres que el apropriorio com este este aperior que
	67	8.7510	2. 7931	0.097869	0.23011	0.67000	
-			RATIOS , FLO				
							en e
	VAU MUBU	P1	PI /PII	PI /PTF	PL /PTP	Y/OMAX	and the state of t
	77	35.461	10.954	0.40064	0.43245	o. 50 <b>00</b> 0	
	<u> 82                                   </u>	17.795	5.4967	0.20105	0.46792	0.58300	
	c.3	3.4546	1.0571	0. 639031	0.090840	0.67900	<b>₩</b> £
	>ADDITERNA	it pressime	PATINS , FUE	CTC# SHACUD		i destruit de la companie de la comp	OF PEGNAL
	AVD HOPD	Pl	PL/PO	ML/PTF	PI /PTP	X/DMAX	
	107	5.3607	1.6559	0.060565	0.14096	0.62400	<i></i>
_	117	5.3007	1.6373	0. 054697	0. 13978	0, 83000	
	122	5-1836	1.6707	0.058531	0.13623	0.56000	<b>6</b> 6
	127	3.4696	1.0717	0. (30233	0.091235	1.0900	The second control of
	137	4.3102	1.3314	0. 049657	0.11334	1.2200	
	142	4.2452	1.3237	0.049414	0.1126R	1.3500	
					0000	•••	ই ট
<	-> TOUTS TOW	f weering	ALUCK , EC	EACHS THEFT			₹8
	NURD HURD	PL	PL/PN	PL/PTF "	PI /PTP "	x/IMpil	- — жүндө жануыбыр — жүмүндө жанабардан жанабан. Жан <b>жара</b> мдандандандандандан жаны коммендик жанадан жана
	-107	5.3637	1.6559	0.060565	0.14096	-L/1000	
	-112	5.3307	1.6373	O.CSSAAT	~ ∂. 1393£	1.0000	
	-127	5-1806	1.6003	0.058531	0.13623	-1.0000	
	-127	3.4606	1.0717	0. 2342 00	0.091285	-1.0000	
	-127	4.41 72	1.3314	0.048657	0.12534	-1.0000	
	-147	4.7762	1.3237	7.048414	Gel 1268	-1.0000	THE RELEASE OF THE PARTY OF THE
	-1*7	3.4396	1.0425	0.038861	0.090446	-1.0022	
	-1 = 7	7.4396	1.0625	0.038863	0.090446	-1.0000	sie ser sager in gest in gest deltwick in mentaliste in delt is der rapper andere mentaliste seidel andere Sager (1400). Alle der deltwick in the second of
	Santit inda	C PPFSSUPE	PATTING . FAR	MOTTLE FLAP	·		
	<b>ጀ</b> ለው ለቤ <b>ս</b> ሁ	οį	PL /PI	MIPTE	PI /PTP	X/DWAX	on a comment of the second
	-1*2	3.4396	1.0625	0. 038861	0.050446	-1.0000	
	-157	3.4396	1.0625	338861	<b>0.090446</b>	-1.0000	ை நார் காற்றும் குறிய நாரும் குறிய குறிய காறிய இது முறிய முறிய குறிய குறிய குறிய குறிய குறிய குறிய குறிய குறிய குறிய நார்கள்
	SAPOIT INV	I BECCOME	RATERS . 20	DEC SHERWIT	NETTON -		
	AVE HORD	Pl /	P1 /P0	PL/PTF	<b>PLIPTP</b>	X/DMAX	والمراجعة والمراجعة والمستردة والمراجعة والمنطقة والمستراجعة والمستراجعة والمستراجعة والمستراج والمراجعة والمستراجعة والمستراء وال
	-167	3.4394	1.0525	0.038861	D90446	-1-0000	
	-177	3.5576	1.0625	0.038861	0.640446	-1-0000	
	יוויחו דורריול	PPFS5IME	स्वरागद 🔭 स्व	ור כושיטה זו	HERRING -		
			ምር / ኮብ	PI /PTF	M /PTP	XAMAX	and the state of t
	AVE ICE	PI					
	103	-			0.078598	~1.00 <b>00</b>	
		P( 3.0343 3.3503	0. 92 800 9. 94530	0.037947	0.078598	-1.0000 -1.0000	and the second s

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$\infty$

										Run 18	•
~	VASA-FEBS		INARY DATA	06/10/79	CADDETT	REC 10/11/79	04:20:23,143	FAC REST!	PG4 C935	PDG 1095	*
	>ขอบ1±เบิศ	L PRESSUPE	PATTOS E PPT	HARY MUG							
$\overline{}$	AVD WEED	PI	PI /PI)	Pt /PTF	PL /PTP	X/DMAX					
	37	14.773	4.5340	7.16562	0.43115	0.43200					
_	37	7.7696	2.3846	0.047105	0.27675	0.53900					
	47	9.4598	3.0261	0.11054	0.28775	0.62909					
-	<u> </u>	9,8978	3.0353	0.11088	0.28863	0.72700					
	PROFESSIONS	L PRESSUPE	RATIOS , FLOR	W SPLITTEP E	. n.				compared the same of the contract of the contr	Marine	•
	AVD WOPD	PL	PL / PO	PL / PTF	PL /PTP	X/DMAX					
	£2	11.235	3.4480	0.12595	0.22788	0.42200			- again delicate de la large dels a cambrilles a la sed	and the description of the second of the sec	
	67	7.8797	2,4183	0.088339	0.22996	0.67000					••
-											
	NAUI AIGUR<	IL PRESSIME	FATIOS , FLO	e SPLITTER D	.D.					description of the contraction o	•
	AVP WOPD	PL	<b>የ</b> L / የባ	PL / PTF	PL /PTP	X/DMAX					
	77	35, 743	10.970	0.40071	1.0431	0.50800				The state of the s	
	87	17.936	5.5348	9.29109	0.52346	0.58300					
_	97	3.4770	1.0671	0. 038981	0.10147	0.67300					
	>400141044	L PRESSURE	RATIOS , EJEC	CTCR SHPOUD		•		the Marian steel or the Marian Marian Company of the Company of th	Outstadingen produces, described organic - Training - T		
~	****					A A LALEND THE				- Standard Street Broad Broad Standard	
•	AVD WORD	PL	Pt /PO	PL/PTF	PL /PTP	X/DHAX					-
_	107	4,3036	1.6553	0.040469	0.15741	9.62400					_
_	117	5.3486	1.6415	0.055763	0.15600	0.43000					
	127	5.2135	1.6771	0.058449	0.15215	0.96000					
	127	3.4070	1.0702	0.635093	0.10177	1.0990					
-	177 147	3, 9374	1.2054	0.044143	0.11491	1.22:00				Marine and the second of the s	
	14	3.8874	1.1931	U. 1143577	0.11345	1.3500					
-	<	t PRFSSIPF	PATINS - FFR			—			<del></del>		_
		<u></u>									.•
	AVIT WORD	PI	PL/PG	M /PTF	PL /PTP	X/PMAX		•			
	-127	5.3936	1.6553	0.06046	0.15741	-1.0000			a algorithm and the state of th	approximate and the second sec	_
	-115	5.3496	1.6415	0. 059943	0.15609	-1.1000					•
-		5.2135	1.6301	0.756449	0.15215	1.0000					
	-127	4170	1.0702	G. 039093	0.15177	-1.0000					_
	-137	3.3474	1.2004	0.044143	0.11541	-1.0000					
	-147 -157	3.4623	1.1931	0.043582	0.1/345 10104	-1.0000					
	-157	3.4569	1.0625	0.039812 0.039756	0.10000	-1.0000				ga, no construir aggrega e quantita de la constitución de la constituc	
	-1-17	304304	1.3610	U. U. W. 770	0.13074	-1.0000					
-	AND THEF VC	PRESSIRE	PATIOS FAN	HATTE FLAN					····		
-				/					Manage arrange that a visit of the second order of the second or	and the second of the second o	●,
	AVԴ ₩ር₽Đ	PL	PL/P1	/PTF	PL /PTP	X/DMAX					÷
	-15?	3.4629	1.3625	0.030812	0.10104	-1.0000		, ,	The second section of the second section of the second section of the second section s	sande como manifestamente que se ser una requisión con este en effecto com	•
	-157	3.4569	1.7613	D C3H7SK	0.100AC	-1.0010					•
	NOOT TICEN	PERSIME	PATION . 20 1	FE SHP OF T	CATTON	and the state of t					- :
	44D 4200C		/	~ ****	\	ri America	-		ويعاده والمارة والمساو	and the second s	• ;
	AVP WORD	Pl	PI / PG	PL / PTF	1P 1P	X/DMAX					•
	-167 -177	3.4622	1. 3625 1. 9619	0.039812	0510104	-1.0000					
~	-1,	3.4449	1.4610	0. 134756	0. I pava	-1.0000					- i
	פניחז זו ררגל	PARKLINE	T. DR ZOTTAW	प्रदार प्रमहत्त्वता 🔢	TEATTING -						
•	AVO HEAT	PI	<b>መ</b> ረ / ቦን	PI /PTF	PL /PTP	X AMERIKA				and the second s	<b>—</b> i
	-192	3.0215	9. 92732	0.033874	0.088180	-1.0000					
Ł	67	3.0765	0.94422	0.034491	0.089787	-1.2000			112 W 188 I W.	tak transport of the second se	85
			THPIST PARAME		U. UATIN!	10.000					
											<b>,</b>
											-

							Run 15
	AVCV-FEMIZ	. PRE141	HARY DATA	06/10/79	CADDELL	PFC 10/11/79 04:21:30.211	FAC 9X6X1 PGM CQ34
	> NOO IT IONA	1 PPESSUPE	RETINS . PP	MARY PLUG			
	AVA WEPA	P1	የኒ / የብ	PL/PTF	PL /PTP	X/DMAX	
	??	10.106	5 <b>.</b> 55.95	0.19582	0.43133	9. 43200	
	37	9.4829	2.9071	0.097325	0.22591	0.53000	
	47	12.J3R	3.6904	0.12355	0.2867R	0.62900	
	52	12.398	3.7987	0.12416	0.29F21	). 72700	
	ANDIT TONA	L PRESSUPE	PATIOS . FLO	W SPLITTER I	. n.		
	AVO HOPO		F1 400	DE ADTE	PL /PTP	X/DPAX	n de terre e de décide de militaire de décide de la company de la compan
		PL	FI / PO	PL/PTF			
	62	13.792	4.2283	0.14155	0.32858	0.42200	
_	_67	9.6429	2.9561	0.098967	0.22972	0.67000	
	>APPLIT IPPA	L PRESSURE	RATIOS . FLO	W SPLITTER D	.0.		
	AVD WOPD	PL	PI / PO	PI /PTF	PL /PTP	X/DMAX	
	77	38. 729	11.573	0.39749	0.97266	J.5UROD	
	92	19.610	6.0116	0. 20126	0.46717	0.58300	
-	92	3.4840	1.06 11	7.025757	0.083000	0.67000	
							and the control of the second states and the second states are a second states and the second states are an experienced as the second states are an experienced as the second states are as a second state are a
			RATIOS , FJE				
	AAL MUMD	PL	PL/PN	PL/PTF	PL /PTP	X/DMAX	
_	1 37	5.8913	1.8030	0.060361	0.14011	0.62400	
_	112	5.8463	1.7923	0.060002	0.13978	O. 83000	
	122	5.7062	1.7493	0.058564	0.13594	J.96000	
	127	~ 3.5040 ~ <del>~</del>	1.0742	0.035963	0.063477	1.0900	
	177	4.7694	1.4594	0.048857	0.11341	1.2200	
	142	4.7303	1.4531	D. C4P549	0.11269	1.3500	
_	->13614164E	FRUEECHUE	BATTOS . FOR	EFCOV YNLFY			
<					01 /0 /0	VANANT	
	DHUM UAV	PI_ /	Pt /P0	PL/PTF	PL/PTP	K/DMAN	•
	AVIT UNEN -107	PI. 5.8813	Pt /PO 1.9030	PL/PTF 0.060361	0.14011	-1.9600	•
	AVIT UDED -197 -112	PI 5-8813 5-9463	Pt /Pn 1.8030 1.7923	PL/PTF 0.060361 0.060002	0.14011 0.13924	-1.0000 -1.0000	•
	AVIT HORD -107 -112 -122	PI. 5.8813 5.4463	Pt /Pn 1.9030 1.7923 1.7493	PL/PTF 0.060361 0.060002 0.058564	0.14011 0.13924 0.13594	-1.0000 -1.0000 -1.0000	•
	AVIT MORTO -107 -119 -129 -127	Pt. 5-8813 5-9463 5-70	Pt /PO 1.8030 1.7923 1.7493 1.0742	PL/PTF 0.060361 0.060302 0.056564 0.035963	0.14011 0.13929 0.13594 0.093477	-1.0000 -1.0000 -1.0000	•
	AVIT VITRO -107 -119 -129 -127 -137	Pt. 5.8913 5.8463 5.701. 5.701.	Pt /Pn 1.8030 1.7923 1.7493 1.0742 1.4594	PL/PTF 0.060361 0.060302 0.058564 0.035963 0.048857	0.14011 0.13929 0.13594 0.093477 0.11341	-1.0000 -2000 -1.0000 -1.0000	•
	AVIT WORD -107 -112 -127 -127 -137 -142	PI. 5-9913 5-9463 5-701 4-743 4-7434	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4501	PL/PTF 0.060361 0.060002 0.058564 0.035963 0.048857 0.048857	0.14011 0.13924 0.13594 0.093477 0.11341 0.11269	-1.0000 -3.000 -1.0000 -1.0000 -1.0000	•
	AVIT WITH IT -107 -119 -127 -137 -141 -152	PI. 5.8813 5.8463 5.705 4.7524 4.7524 4.7575	Pt /Pn 1.8030 1.7923 1.7493 1.0742 1.4594 1.4501 1.0604	PL/PTF 0.060361 0.063002 0.058564 0.04857 0.04857 0.04859 0.035500	0.14011 0.13924 0.13594 0.093477 0.11351 0.11269 0.002404	-1.0000 -2.0000 -1.0000 -1.0000 -1.0000 -1.0000	•
-	AVIT WORD -107 -112 -127 -127 -137 -142	PI. 5-9913 5-9463 5-701 4-743 4-7434	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4501	PL/PTF 0.060361 0.060002 0.058564 0.035963 0.048857 0.048857	0.14011 0.13924 0.13594 0.093477 0.11341 0.11269	-1.0000 -3.000 -1.0000 -1.0000 -1.0000	
	AVIT UTAN 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-	5. 9913 5. 9463 5. 70 \$ 5743 4. 7494 4. 73 75 3. 4599 3. 469)	Pt /Pf 1. 9/3 30 1. 7923 1. 74 93 1. 07 42 1. 45 94 1. 45 01 1. 06 04 1. 06 35	PL/PTF 0.060361 0.063002 0.058564 0.04857 0.04857 0.04859 0.035500	0.14011 0.13924 0.13594 0.093477 0.11351 0.11269 0.002404	-1.0000 -2.0000 -1.0000 -1.0000 -1.0000 -1.0000	•
	AVIT UTAN 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-107 1-	5. 9913 5. 9463 5. 70 \$ 5743 4. 7494 4. 73 75 3. 4599 3. 469)	Pt /Pf 1. 90 30 1. 7923 1. 7493 1. 0742 1. 4594 1. 4501 1. 0604 1. 0635	PL/PTF 0.060361 0.063002 0.058564 0.035963 0.048857 0.048550 0.035500 0.035603	0.14011 0.13924 0.13594 0.093477 0.11351 0.11269 0.002404	-1.0000 -2.0000 -1.0000 -1.0000 -1.0000 -1.0000	•
	AVIT WITH IN -107 -112 -127 -137 -142 -152 -157 -157 -157 -157	PI. 5.8463 5.70 5.70 4.704 4.704 4.7374 3.4699 3.4699 1.98ESSURE	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4594 1.4501 1.0604 1.0635	PL/PTF 0.060361 0.060002 0.058564 0.035963 0.048857 0.048550 0.035500 0.035603 I HCZYLF ECAP	0.14011 0.1392# 0.13594 0.093477 0.11341 0.14269 0.082642	-1.0000 -V.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	•
	AVITATION N -107 -112 -112 -127 -137 -147 -157 -157 -157	PI 5.8913 5.4663 5.70 574.7 4. 1404 4. 73 74 3. 4597 3. 469)	Pt /Pf 1. 90 30 1. 7923 1. 7493 1. 0742 1. 4594 1. 4501 1. 0604 1. 0635	PL/PTF 0.060361 0.060002 0.058564 0.048549 0.0485500 0.035500 1 HCZYLF ECAP	0.14011 0.1392# 0.13594 0.093477 0.11359 0.11367 0.11269 0.062404 0.082642	-1.0000 -V.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
	AVITYONA  -107 -112 -112 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157	Pt. 5.8463 5.4663 5.701 4.7404 4.7374 3.4590 3.4590 3.4590 3.4590	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4501 1.0604 1.0635 Pt /Pn 1.0604 1.0635	PL/PTF 0.060361 0.063002 0.058564 0.035963 0.04857 0.04859 0.035500 0.035603 HCZ7LF ECAP PL PTF 0.035500 0.035603	0.14011 0.1392# 0.13594 0.093477 0.11341 0.14269 0.082642 PE/PTF 0.082642	-1.0000 -V.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
	AVITATION 1 -107 -117 -127 -127 -137 -147 -157 -157 -157 -157 -157 -157 -157 -15	Pi 5.8413 5.463 5.70 4.73 4. 74.04 4.73 74 3.4590 3.4590 3.4590 3.4590 [PPECCURE	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4501 1.0604 1.0635 RAYINS FAR Pt /Pn 1.0604 1.0635	PL/PTF 0.060361 0.060002 0.058564 0.035963 0.048549 0.035500 0.035603 HCZYLF FEAP 0.035500 0.035500	0.14011 0.13929 0.13594 0.093477 0.11371 0.11371 0.1264 0.082640 0.082642	-1.0000 -V.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
	AVITATION  -107 -117 -127 -127 -137 -147 -157 -157 -157	Pi 5.8413 5.463 5.70 7.4594 4.73 9.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.46	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4501 1.0604 1.0635 RAYINS FAR Pt /Pn 1.0604 1.0635	PL/PTF 0.060361 0.060002 0.058564 0.035563 0.048549 0.035500 0.035603 I HCZ7LF EXAP PL PTF 0.035500 D.035603	0.14011 0.1392# 0.13594 0.093477 0.11354 0.093477 0.11364 0.082642 PE/PTF 0.082642 PE/PTF 0.082642	-1.0000 -V.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	•
_	AVITYONA  -107 -112 -112 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	PI 5.8913 5.9463 5.701 4.574.1 4.7374 3.4597 3.4597 3.4597 3.4597 [PPECCURE	Pt /Pn 1.8030 1.7923 1.7493 1.0742 1.4501 1.4501 1.0604 1.0635 RAYINS FAR Pt /Pn 1.0604 1.0635	PL/PTF 0.060361 0.060362 0.058564 0.058564 0.04857 0.04859 0.035500 0.035603 HCZ7LF ECAP PL/PTF 0.035500 DEG SHREIML	0.1401! 0.1392# 0.13594 0.093477 0.11341 0.14269 0.082642 PL/PTP 0.082642 PL/PTP 0.082642 DIATTIN	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAY -1.0000	
-	AVITATION  -107 -117 -127 -127 -137 -147 -157 -157 -157	Pi 5.8413 5.463 5.70 7.4594 4.73 9.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.4699 7.46	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4501 1.0604 1.0635 RAYINS FAR Pt /Pn 1.0604 1.0635	PL/PTF 0.060361 0.060002 0.058564 0.035563 0.048549 0.035500 0.035603 I HCZ7LF EXAP PL PTF 0.035500 D.035603	0.14011 0.1392# 0.13594 0.093477 0.11354 0.093477 0.11364 0.082642 PE/PTF 0.082642 PE/PTF 0.082642	-1.0000 -V.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
-	AVITATION 1 -107 -117 -117 -127 -137 -147 -157 -157 -157 -157	Pt 5.8413 5.9463 5.70 1 574.1 4.7694 4.73 1 4.7691 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4501 1.0604 1.0635 RAYINS FAR Pt /Pn 1.0635 PAYINS 70 1.0635	PL/PTF 0.060361 0.060362 0.058564 0.058564 0.04857 0.04859 0.035500 0.035603 HCZ7LF ECAP PL/PTF 0.035500 DEG SHREIML	0.14011 0.13928 0.13594 0.093477 0.11371 0.11264 0.092644 0.092642 PE/PTF 0.092642 DEATTION 1/PTP 0.092642 0.092642 0.092642	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAY -1.0000	
-	AVITATION IN THE TOTAL T	Pt 5.8413 5.9463 5.70 1 574.1 4.7694 4.73 1 4.7691 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4501 1.4501 1.0604 1.0635 RAYINS FAR Pt /Pn 1.0604 1.0635 PATINS 70  Pt /Pn 1.0635 1.0635	PL/PTF 0.060361 0.060002 0.056564 0.035963 0.048549 0.035500 0.035603 HCZYLF ECAP PL PTF 0.035500 0.035603 DFG SHRRING TO 0.035603 0.035603	0.14011 0.1392# 0.13594 0.093477 0.11341 0.14269 0.082642 0.082642 P[/PTF 0.082642 0.082642 0.082642 0.082642	-1.0000 -V.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAY -1.0000 -1.0000 X/DMAR -1.0000 -1.0000	
	AVITATION -107 -117 -127 -127 -137 -147 -157 -157 -157 -157 -157 -157 -157 -15	PI 5.8413 5.463 5.70 4.73 14 4.73 14 3.4590 3.4590 3.4590 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4600 3.4600 3.4600 3.4600 3.4600 3.4600 3.4600 3.4600 3.4600 3.4600 3.4600 3.4600 3.4600 3.46000	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4594 1.4501 1.0604 1.0635 PAYINS PAYINS PO 1.0635 PAYINS PO 1.0635 PAYINS PO 1.0635 PAYINS PO 1.0635	PL/PTF 0.060361 0.060002 0.058564 0.048549 0.048549 0.035500 0.035603 HCZYLF ECAP ML PTF 0.035500 D C35603 DFG SHRITING TO PL/PTF	0.14011 0.1392# 0.13594 0.093477 0.11341 0.14269 0.082642 0.082642 DE /PTF 0.082642 0.082642 0.082642 0.082642 0.082642 0.082642 0.082642	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000  X/DMAY -1.0000 -1.0000  X/OMAR -1.0000 -1.0000	
-	AVITATION IN THE TOTAL T	Pt 5.8413 5.9463 5.70 1 574.1 4.7694 4.73 1 4.7691 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690 3.4690	Pt /Pn 1.9030 1.7923 1.7493 1.0742 1.4501 1.4501 1.0604 1.0635 RAYINS FAR Pt /Pn 1.0604 1.0635 PATINS 70  Pt /Pn 1.0635 1.0635	PL/PTF 0.060361 0.060002 0.056564 0.035963 0.048549 0.035500 0.035603 HCZYLF ECAP PL PTF 0.035500 0.035603 DFG SHRRING TO 0.035603 0.035603	0.14011 0.1392# 0.13594 0.093477 0.11341 0.14269 0.082642 0.082642 P[/PTF 0.082642 0.082642 0.082642 0.082642	-1.0000 -V.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAY -1.0000 -1.0000 X/DMAR -1.0000 -1.0000	

				INAPY PATA	06/10/73	CADDELL	PEC 10/11/79 74:22:32.17	A FAC 8X6XI PGM C034 PNG 1097
		250211104	I PRESSIPT	PATINS PP	MARY PLUG			
	$\hat{}$	AVB HOPD	PL	<b>ም</b> ፤ / የባ	ol /ptr	PL /PTP	X FDMAX	
		32	16.179	4. 95 50	0.16549	0.43099	0.43700	் நார் பார் நார்கள் இருந்து இரு இருந்து இருந்து இருந்த
		37	A.5339	2.6367	0.996592	0.22608	0.53000	
	$\sim$	67	10.783	2.3053	0.11930	0.28666	0.62900	The state of the s
		52	10.928	3,3190	0.11076	0.28786	0.72700	
		MODITION	I DRECSIME	PATINS . FEF	N CDI ITTED I			
				* "			•	ஆ ஆக்கு இருக்கு இணையுள்ளது. இது இருக்கு
	_	AVD HUPD	υĹ	PL / PO	Pt /PTF	PL /PTP	X/DMAX	
		A2	12.307	3.7724	0.12589	0.32717	0.42200	
		67	R.6239	2.6435	0.044219	0.27927	0.67600	
		>APPLITIONAC	L PRESSIME	RATIOS . FLE	N SPLITTER P	.n.		
		AVD HOPE	PL	<b>ም</b> / PD	PĮ /PTF	PL/PTP	X/DMAX	
		77	39.747	11.877	0.39637	1.0301	2.50800	. po to the property of the pr
		92	19.659	6. 9761	0.20110	0.52263	0.58300	
		92	3.4984	1.0693	0.035686	0.092740	0.67000	
		SECOLITIONS	1 PRESSIME	PATINS . EJE	FÉTER SUREIM			
60						and the second second	region en en region en en	
$\circ$		SAU MUNU	PL	PL / Pfi	PL / PTE	M /PYP	X/DMAX	
		1)7	5.8992	L. P283	0.060347	0.15643	0.62400	
		117	5.8492	1.7991	0.067047	0.15403	3. 83003	
		127	5.7342	1.7577	0.058659	0.15244	0.9600)	The state of the s
		177	3.5)34	1.0739	0.335839	0.053135	1.0900	
		137 147	4.3238	1.3754	3.C44731 9.043771	0.11495	1.2200	
		-	4.2789	1.3116		0.11375	1.3500	
		Ziant tom	T BECKEUPE	PATION FOR	ERODY INLET			
		ח פחש יועם	PL	PL /PD	PL/PTF	Pt /PTP	X/DMAX	The state of the s
		-107	5.4992	1.4083	0.060347	0.15693	-1900هوا	
		-112	5. 8592	1.7991	0.050040	0.15603	1.0000	
		-177	5. 7342	1.7577	0.058659	0.15244	~1.0000	
		-1 27	34 134	1.7733	0.735939	0.253124	-1.0000	
		-1 >7	4. 32.38	1.3254	0.044231	0.13495	-1.0000	
		-14?	4.7730	1.3116	0. 543771	9/1374	-1.0000	
		-1=7	3.4634	1.7616	0.035439	7.1192775	-1.0000	
		~157	3.4634	1.0616	0.035432	0.392075	-1.0000	
	~	Santi tou	ा <b>। व्यवस्ताहर</b>	PATTOLINE	NOTTE FLAM			
		AVO HOPO	PI	חיין אין	PI /PTF	PI /PTP	x/DMAX	
		-157	3.4634	1.7616	0.235439	0. 352075	-1.0000	
		-157	3.4634	1.0616	3235439	0.092075	-1.0000	in the companion of the
		Stant+taki	, poessibe	PAPENT . 20	DEC SHEET	OCATION		
	<u>.                                    </u>			/	`		w James	, and the second
		ለያው <i>ፈጣ</i> ዎን	٥١	PI /PI	P[ /PTF	979	X/0 ^m 1X	
		-167 -177	3.44.74	1.06 32	0.0354A1 0.035430	0.09229#	-1.0000	The contract the street contract to the street of the contract to the contract
				1.0616			-1.6000	
		מיחו דורדונ	_ PPF5519F	PATINS . HO	कार रामका र	PERTIN		
	•	AVD ATIES	οt	el / ኬህ	PL / PTF	PL /PTP	*/BMAY	La Company of the Com
		-X*,	3.6241	7. 47822	0. 030977	0.090503	-1.0074	و در من من المسلم ا
		-; 07	7.0772	0.94203	3.07147R	0.001701	-1.0100	
	<b>U</b> /	•		THOUST PERAM			•	

										Rut 15
	AUCS - LAI	S PPFE END	HARY DATA	06/10/79	L*uo£11	PEC 10/11/79 04:	:73:17.925	FAC SYENE	PGM CD34	PRG 1098
	>4201T100	AL PRESSIBLE	PATING . PP	MARY PING						
	AVO VOED	PI,	PI /PO	Pt /PTF	PI /PTP	X / DMA X				
	يدن	19.112	5.5466	0.18527	7.43096	0.43200				
	37	0.4707	7.5079	0.094554	0.22555	0.53000				•
	47	12.156	3.6971	0.12333	3.28687	J.6290J				·
_	57	12.111	3.7789	3.12385	0.28817	J. 72700				
	>ANDITIONAC	AL PPESSURE	RATIOS . FLE	N SPLITTER I	. D.					
	AVO WORD	PL	PI /PO	PL/PTF	PI /PTP	X/DMAX				
	£7	13.434			3.32845					
	67	9.6490	4.2772 2.9549	0.141 <i>2</i> 9 0.098792	0.22959	9.42200 8.67000				
	>ADDIT ION	AL PRESSURF	FATIOS . FLO	TH SPLITTER D	, n _*					
	AVD HORD	PL	Pt /Pf)	PL/PTF	PL /PTP	X/DMAX				
	77	3 A. 7 OA	11.854	0.39595	0.97101	0.50800				
	87	19.640	A.0143	0.20090	0.46730	J.58300				
Ī	0)	3.4872	1.0679	0.035671	0.082974	0.67000			·····	····
	SERVITIONS	AL PRESSURE	PATTOS . F.IE	CTOP SHPOUD	<del>-</del> -					
					· · · · · · · · · · · · · · · · · · ·	t garage and the common and the				
	AVD WOPD	PL	PL / PG	PL /PTF	PL/PTP	X/DMAX				
_	137	5. ARIA	1.8012	0.060165	0.13995	0.62460				
_	11.7	5.8519	1.7970	0. C5 0859	0.13074	C.#3000				
	127	5.7218	1.7522	7.05*529	0.13614	0 <b>.</b> 96000				
	127	3.5722	1.0725	0.035824	0.083330	1.0900				
	יין	4.7571	1.4568	0.048661	0.11319	1.2200				
	142	4.7321	1.4491	0.048405	0.11260	1.3500				
Ξ		4 *4F54.p.F	******* ***	-						
`		-4					Application of the contraction o			
	AVILANDE	PL	PL/PO	PL/PTF	PL /PTP	X/DMAX		•		
	-107	5.8818	1.4012	0.060165	0.13995	-1.0000				
	-112	5.4514	1.7920	J. C50459	0.13924	×1.0000				
	-127	5.7219	1.7522	0.058529	0.13614	-1.0030				
	-127	7.5777	1.0725	0.035724	0.083336					
						-1.000c			··	
	-137	4. 1571	1.4568	0.648661	0.11219	-1.0G30				
	-142	4.7374	1.4568	0.648661 0.648465	0 • 1 بر 10 • 0 10 • 10 • 0	-1.0030 -1.6030				
	-14? -15?	4.73X 3.4672	1.456# 1.4491 1.041#	0.648661 0.648465 0.625466	0.11269 0.11269 0.082498	-1.0G30				
	-142	4.7374	1.4568	0.648661 0.648465	0 • 1 بر 10 • 0 10 • 10 • 0	-1.0030 -1.6030				
	-14? -157 -157	4.7334 3.4672 3.4672	1.456# 1.4491 1.051# 1.0618	0.648661 0.648465 0.625466 0.035466	0.11269 0.11269 0.082498	-1.0030 -1.0030 -1.0000				
	-142 -157 -157 -157 -5753 <b>]Y Y</b>	4.73% 3.4672 3.4672 AL DRESSURE	1.456P 1.4491 1.051P 1.0618	0.G48661 0.C484C5 0.C25466 0.035466	0.112/9 0.11260 0.082498 0.082498	-1.0030 -1.0030 -1.0000 -1.0000				
	-142 -152 -157 -5/55 <b>111 Y</b> FFF AVD HOPD	4.7334 3.4672 3.4672 AL DRESSURE PL	1.456P 1.4401 1.041P 1.961B	0.648661 0.64865 0.625466 0.035466 F HOTTE	0.11249 0.11240 0.082498 0.082498	-1.0000 -1.0000 -1.0000 -1.0000				
	-14? -16? -15? -15? -5/50114 \$PSU AVD WOOD -15?	4.7334 3.4672 3.4672 AL PRESSURE PL 3.4672	1.456P 1.4401 1.061P 1.061B PAYION F/F PL/PO 1.0618	0.048661 0.048405 0.025466 0.035466 F HOTTLE FLAP 0.035445	0.11269 0.11269 0.082498 0.082498 Pt /FTP 0.092498	-1.0000 -1.0000 -1.0000 -1.0000				
	-142 -152 -157 -5/55 <b>111 Y</b> FFF AVD HOPD	4.7334 3.4672 3.4672 AL DRESSURE PL	1.456P 1.4401 1.041P 1.961B	0.648661 0.64865 0.625466 0.035466 F HOTTE	0.11249 0.11240 0.082498 0.082498	-1.0000 -1.0000 -1.0000 -1.0000				
	-14? -167 -157 -157 -157 -157 -157	4.7374 3.4672 3.4672 AL DRESSURE PL 2.4672 7.4672	1.456# 1.4491 1.641# 1.0618 PAYION FFF PL/PO 1.0618	0.048661 0.048405 0.025466 0.035466 F HOTTLE FLAP 0.035445	0.1126 0.11260 0.082498 0.082498 Pt /FTP 0.092498 0.082498	-1.0000 -1.0000 -1.0000 -1.0000				
	-142 -157 -157 -157 -157 -157 -157 -157	4.7374 3.4672 3.4672 PL 3.4672 7.4672	1.456P 1.4401 1.061P 1.061B PAYION F/F PI /PO 1.061B	0.048661 0.048405 0.025466 0.035466 F HOTTLE FLAP 0.035466 DFG SHPT DE TO	0.11269 0.11269 0.082498 0.082498 Pt /FTP 0.092498 0.082498	-1.0030 -1.0030 -1.0000 -1.0030 X/DMAY -1.0000 -1.0030				
	-142 -162 -157 -157 -157 -157 -157 -157 -157 -157	4.7374 3.4672 3.4672 PI. 3.4672 2.4672 FL TRESTIME	1.456# 1.4401 1.061# 1.061# PAYION FAP PL/PD 1.061# PAYION - 20	0.048661 0.048405 0.025466 0.035466 F HOTTLE FLAP 0.035445 0.035466 DFG SHPTUE TO PL/PTF	0.11269 0.11269 0.082498 0.082498 0.082498 0.082498	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	-14? -167 -157 -5763]] PAGE  AVO MOPO -157 -157	4.7374 3.4672 3.4672 AC PRESSURE PL 3.4672 7.4672 PL 100ESSURE	1.456# 1.4491 1.641# 1.0618 PAYIDS FAP PL/PD 1.061# PL/PD 1.061#	0.G48661 0.C484CF 0.C25466 0.035466 F HOTTLE FLAP 0.035466 DFG SHPTON TO PL/PTF 0.C35466	0.11260 0.11260 0.082498 0.082498 0.082498 0.082498 773YINN	-1.0000 -1.0000 -1.0000 -1.0000 x/bmay -1.0000 -1.0000				
	-142 -162 -157 -157 -157 -157 -157 -157 -157 -157	4.7374 3.4672 3.4672 PI. 3.4672 2.4672 FL TRESTIME	1.456# 1.4401 1.061# 1.061# PAYION FAP PL/PD 1.061# PAYION - 20	0.048661 0.048405 0.025466 0.035466 F HOTTLE FLAP 0.035445 0.035466 DFG SHPTUE TO PL/PTF	0.11269 0.11269 0.082498 0.082498 0.082498 0.082498	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	-14? -167 -157 -5763]] PAGE  AVO MOPO -157 -157	4.7374 3.4672 3.4672 PL 2.4672 2.4672 7.4672 FL BRESSIME PL 3.4672 3.4672	1.456P 1.4401 1.061B 1.061B PAYIDS F/F PL/PD 1.061B PAYIDS - 20 PL/PD 1.061P 1.061P	0.G48661 0.C484CF 0.C25466 0.035466 F HOTTLE FLAP 0.035466 DFG SHPTON TO PL/PTF 0.C35466	0.11269 0.11269 0.082498 0.082498 0.082498 0.082498 0.082498 0.082498	-1.0000 -1.0000 -1.0000 -1.0000 x/bmay -1.0000 -1.0000				
	-142 -157 -157 -157 -157 -157 -157 -157 -157	4.7374 3.4672 3.4672 AL PRESSURE PL 3.4672 7.4672 PL PRESSURE PL PRESSURE	1.456# 1.4491 1.051# 1.0618 PAYIOS * PAP PL/PD 1.061# 1.061# 1.061# 1.061#	0.048661 0.028405 0.025466 0.035466 F HOTTE FLAP 0.035466 DEG SHPEOUTE 0.035466 0.035466	0.1126 0.11260 0.082498 0.082498 0.082498 0.082498 7771118	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
	-142 -157 -157 -157 -157 -157 -157 -157 -157	4.7374 3.4672 3.4672 PI. 3.4672 7.4672 FL TRESTINE PI. 3.4672 PI. DEFTTINE	1.456# 1.4401 1.061# 1.061# PAYIDS . FAP PL/PD 1.061# 1.061# 1.061# 1.061#	0.048661 0.048407 0.025466 0.035466 F HOTTLE FLAP 0.035466 DEG SHPEDA TE 0.035466 0.035466 0.035466	0.11260 0.11260 0.082498 0.082498 0.092498 0.082498 0.082498 0.082498 0.082498	-1.0030 -1.0030 -1.0030 -1.0030 -1.0030 -1.0030 -1.0030 -1.0030				
÷	-142 -157 -157 -157 -157 -157 -157 -157 -157	4.7374 3.4672 3.4672 AL PRESSURE PL 3.4672 7.4672 PL PRESSURE PL PRESSURE	1.456# 1.4491 1.051# 1.0618 PAYIOS * PAP PL/PD 1.061# 1.061# 1.061# 1.061#	0.048661 0.028405 0.025466 0.035466 F HOTTE FLAP 0.035466 DEG SHPEOUTE 0.035466 0.035466	0.1126 0.11260 0.082498 0.082498 0.082498 0.082498 7771118	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

0854-	-LEWIS PRELIT	MINARY DATA	06/10/79	CADDFII	PEC 10/11/79 04:73:58.035	FAC PX6V1 PGY CD34 RDG 1099
<b>ን</b> ልበብ (	IT IONAL PRESSIPE	E PATIOS . PP	MARY PIUG	almante titting abdange antoniote er	. at Area	
AVn wr	rrn Pt	PL/PN	PI / PTF	PL /PTP	*/DMA*	
32	14.446	5.0791	0.18481	0.43047	0.43200	and the support of measurest surface to be an expensive the measurement of the surface of the su
17	A.6289	2.6649	0.096962	0.22586	0.53000	
67	10.069	3.3475		0.28710	3.62900	The residence of the experience of the company of t
52			0.17376	0.24854	0. 72 700	
	11.774	3,4045	0.12387		0. 12 100	
PENAC	ET IONAL PRESSUPE	FRATERS , FLO	OW SPLITTER L	, n _*		Company of the Compan
AUN WE	TRO PL	PL / P(1	PL/PTF	PL /PTP	X/DMAX	
62	12.533	3.8707	0.14084	0.32805	0.42200	
67	#.7789	2.7112	0.098648	0.22978	9. 67000	
>#0") !	ITIONAL PRESSIRE	PATIOS . FLO	NW SPLITTER N	.0.	Same and the state of the state	
AVD HD	OPO PL	PI / PO	PI /PTF	PL /PTP	X/DMAX	
77	35.397	10.932	0.39775	0.02649	0.50900	
42	17.890	5.5251	0. 20103	0.46827	0.58300	
- 65	3,4610	1.0689	7.038801	0.090589	0.67000	
1008	IT IONAL PRESSURE	RATIOS . FJI	FC TOP SHPOUD	e cama em des	ar is a companient of the second of the seco	de son viruale ses virus en companiones de la companione de la com
AVD WO	10 D#	PL/PD	PL/PTF	PL /PTP	X/DHAX	
	· ·				• •	
107	5.3926	1.6623	0.060495	0.14089	0.62400	
112	5.3226	1.6438	0.759817	0.13932	2.83000	
122	5.2375	1.6087	0.050517	0.13630	0.96000	
177	3.4719	1.0719	0. 035004	0.090951	1.0900	
137	4.3318	1.7378	0.048677	0.11336	1.2200	
142	4.3118	1.3716	0.048452	0.11296	1.3500	
Creat.	FIGNAL PRESCUE	HATIOS , FO	FROM IMES			
AVD	nan Pe	Pt ZPO	PL /PTF	PL /PTP	XZOMAN	
-107	5.3926	1.6623	0.060485	0.14089	-1,000	
			0.059813	0.13932	1.3000	
-117	5.3226	1.643#	0.058517			
			11155.8517	0.13630	/-1. Jugo	
-1??	5.2075	1.6082				
-1 >	\$4713	1.0719	0.039004	0.090851	-1.0000	
-1 27 -1 37	4.713	1.0710	0.039004 0.048677	0.13A3A	-1.0000	
-1 27 -1 37 -1 4 3	4.713 4.718 4.3114	1.0710 1.3378 1.3716	0.039004 0.048677 0.048452	0.13A3A 9.112A6	-1.0000 -1.0000	
-127 -137 -147 -152	4.3418 4.3114 3.4413	1.0719 1.3378 1.3716 1.0627	0.039004 0.048677 0.048452 0.038666	0.11.73A 9.112Ac 0.090065	-1.0000 -1.0000 -1.0000	
-1 27 -1 37 -1 4 3	4.713 4.718 4.3114	1.0710 1.3378 1.3716	0.039004 0.048677 0.048452	0.13A3A 9.112A6	-1.0000 -1.0000	
-127 -137 -143 -152 -157	4.3418 4.3114 3.4413	1.071° 1.3378 1.3316 1.0627 1.3642	0.039004 0.048677 0.048452 0.038666 0.038772	0.11.73A 9.112Ac 0.090065	-1.0000 -1.0000 -1.0000	
-127 -137 -143 -152 -157	4-713 4-718 4-318 3-4417 3-4461	1.0710 1.3378 1.3716 1.0627 1.3642	0.039004 0.048677 0.048452 0.038666 0.038722	0.11/3A 0.11296 0.090065 0.090196	-1.0000 -1.0000 -1.0000 -1.0000	
-1 27 -137 -147 -152 -157 -157	4.318 4.318 4.317 3.4461 3.4461 11109AL PRESSIDE	1.071° 1.3378 1.3316 1.3627 1.3642	0.039004 0.048677 0.048452 0.038666 0.038722 0.038722	0.11/3A 9.112*6 0.090065 0.090196	-1.000 -1.0000 -1.0000 -1.0000	
-1 27 -1 37 -1 47 -1 52 -1 57 -1 57 -1 57	4.713 4.318 4.318 3.4461 3.4461 7109AL BOCCCIDE	1.0710 1.3378 1.3316 1.0627 1.3642 F PATTOS FAP M /PO 1.0627	0.039004 0.048677 0.048452 0.038672 0.038722 0.038666	0.11/58 9.112/6 0.090065 0.050196	-1.0000 -1.0000 -1.0000 -1.0000	
-127 -137 -142 -152 -157 -157 AVD 40 -152 -157	4.318 4.318 3.4461 3.4461 3.4461 7109AL PRESSIDE 11109AL PRESSIDE 11109AL PRESSIDE	1.071° 1.3378 1.3316 1.0627 1.3642 FRYNS FAF M /PN 1.0427 1.0652	0.039004 0.048677 0.048452 0.038666 0.038722 0.038666 0.038666	0.11-58 0.12-6 0.090065 0.050196 P( /PTP 0.290065 0.090156	-1.000 -1.0000 -1.0000 -1.0000	
-127 -137 -142 -152 -157 -157 AVD 40 -152 -157	4.713 4.318 4.318 3.4461 3.4461 7109AL BOCCCIDE	1.071° 1.3378 1.3316 1.0627 1.3642 FRYNS FAF M /PN 1.0427 1.0652	0.039004 0.048677 0.048452 0.038672 0.038722 0.038666	0.11-58 0.12-6 0.090065 0.050196 P( /PTP 0.290065 0.090156	-1.0000 -1.0000 -1.0000 -1.0000	
-127 -137 -142 -152 -157 -157 AVD 40 -152 -157	4.713 4.718 4.318 3.4463 3.4463 7104AL BOCCCIPP 3.4463 17104AL BOCCCIPP	1.071° 1.3378 1.3316 1.0627 1.3642 FRYNS FAF M /PN 1.0427 1.0652	0.039004 0.048677 0.048452 0.038666 0.038722 0.038666 0.038666	0.11-58 0.12-6 0.090065 0.050196 P( /PTP 0.290065 0.090156	-1.0000 -1.0000 -1.0000 -1.0000	
-127 -137 -142 -152 -157 -157 -157 -157 -157	4.713 4.718 4.311 3.4461 3.4461 3.4461 3.4461 1710001 POFSSURE	1.0710 1.3178 1.316 1.3642 1.3642 FPATTOS FAP 01/PO 1.0642 FPATTOS FAP	0.039004 0.048677 0.048452 0.038666 0.0386722 0.038666 0.038666 0.038722 0.038722	0.1145R 0.124C 0.090065 0.090196 P(/PTP 0.290065 0.090196	-1.000 -1.000 -1.0000 -1.0000 */OMÄX -1.0000	
-127 -147 -152 -157 -157 -157 -157 -157 -157	4-713 4-318 4-318 3-441 3-4461 (************************************	1.071° 1.3378 1.3376 1.3627 1.3642  PATING FAP  PLOAPT 1.0642  PATING FAP  PLOAPT 1.0652	0.039004 0.048677 9.048452 0.038666 0.038722 0.038666 0.038666 0.038727	0.11/38 9.112#6 0.090065 0.090196 PE/PTP 0.090065 0.090196	-1.000 -1.000 -1.0000 -1.0000 -1.0000 -1.0000	
-127 -137 -142 -152 -157 -157 -157 -157 -157	4-713 4-318 4-318 3-4417 3-4461 3-4461 3-4463 1410441 BBESSUBS	1.071° 1.3378 1.3316 1.0627 1.0642 FATTO FAP M./PO 1.0642 P170° P1/PO 1.0661	0.039004 0.048677 9.048452 0.038666 0.038722 0.038666 D.038727 DEC SHPCHO IT PL/PTE 0.038666 D.038666	0.1145A 0.1124E 0.090065 0.050196 PE/PTP 0.090065 0.09015E TATTIPH 0.09045 0.09045	-1.0000 -1.0000 -1.0000 -1.0000 x/DMAX -1.0000 x/DMAX -1.0000	
-127 -137 -142 -152 -157 -157 -157 -157 -157 -167 -167 -172	4.713 4.318 4.318 3.4461 3.4461 3.4461 3.4461 17104AI POFCCORE	1.071° 1.3378 1.3378 1.378 1.378 1.0627 1.0642  PATTOS FAP PLOGS PATTOS FAP PLOGS PATTOS FAP	0.039004 0.048677 0.038666 0.038666 0.0386722 0.038666 0.038666 0.038727 0.038666 0.038727	0.1145A 0.112A 0.090065 0.090196 0.290065 0.090196 700196 700196 0.090196	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
127 -137 -142 -152 -157 AVD 4D -157 -157 AVD 4D -167 -172	4.713 4.718 4.318 4.318 3.4463 3.4463 3.4463 1710441 PRESSURE 740 PL 3.4313 3.4313 1710441 PRESSURE	1.071° 1.3378 1.3378 1.378 1.378 1.378 1.0627 1.0642 PATTOS . 70 PLOCATION OF PATTOS . 70	0.039004 0.048677 0.048677 0.038666 0.038666 0.038666 0.038722 0.038666 0.038722 0.038666 0.038722 0.038666	0.1145A 9.112A 0.0900A5 0.090196 0.9900A5 0.090196 7AYTHW 21/PTP 0.099434 0.09945	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
-127 -137 -142 -152 -157 -157 -157 -157 -157 -167 -167 -172	4.713 4.318 4.318 3.4461 3.4461 3.4461 3.4461 17104AI POFCCORE	1.071° 1.3378 1.3378 1.378 1.378 1.0627 1.0642  PATTOS FAP PLOGS PATTOS FAP PLOGS PATTOS FAP	0.039004 0.048677 0.038666 0.038666 0.0386722 0.038666 0.038666 0.038727 0.038666 0.038727	0.1145A 0.112A 0.090065 0.090196 0.290065 0.090196 700196 700196 0.090196	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	

	MASA-I FHIS	PRFE 14	INAPY DATA	06/19/79	CADDELL	REC 10/11/79 04:24:39.976 FAC AX6X1 PGM CO34 PNG 1100
	JAPOTTTOOAC	PPESSIBE	RATIOS . PP1	4A3Y PLUG		
	AVD WEIRD	Pt	PI /PO	PI /PTF	PL /PTP	X/DMAX
	37	14.206	4.6107	0.18585	0.43056	0.43200
	77	7.4372	2.4239	0.097714	0.22637	J. 52000
•	47	9.9474	3.0766	0.12402	0.28733	0.62900
	5.7	9.9774	3.0959	0.12440	0.28820	0.72700
_ <del></del>						
			RATIOS , FLO			
	AVD WORD	PE	PL/PN	PI /PTF	PL/PTP	X/DMAX
	62	11.347	3.5096	0.14148	0.32776	0-42200
	67	7.9572	2.4611	0.099210	0.22984	0.67000
	SADDITIONAL	PPESSUPE	RATIOS , FLO	W SPLITTEP O	•n•	
	AVD HORD	PL	PL/PO	PL/PTF	PL/PTP .	×/DMAX
	77	32.114	9.9324	0.40040	0.92760	0.50800
	82	16.150	4. 9951	0.20136	0.46650	Ů.5 <b>₹</b> 300
	92	3.4643	1.0715	0.043193	0.10006	2, 67060
-	JANNIT INNAL	PRESSIPE	PATIOS . FJE	CTOR SHPOUR		
A	AVD WORD	PL	PL 7 PR	PL /PTF	PL/PTP	X/DMAX
	107	4.8606	1.5033	0.060602	0.14040	0.62400
	112	4.4056	1.4963	0. (49916	0.13001	0. 63000
	122	4.6905	1.4507	0.058481	0.13548	0-96000
	127	3.4643	1.0715	0.047193	0.10006	1.0900
	127	3.9248	1.2139	0.048934	0.11337	1.2200 .
	147	3.4947	1.2046	J. 048559	0.11250	1.3500
$\overline{}$	240211 1004	<b>ABECCIAE</b>	AATIOS , FOR	COUNTY ET		
ì	AVIT HIPD	PĹ	Pt /PO	PI /PTF	PE /PTP	X70HAD
	-107	4.8506	1.5033	0.060602	0-14049	-1,0000
-	-101		1.4863	0.059916	0.13881	1.0000
	-112	4.4356				
-	-112				0.13548	/ -1.0000
-	-112 -122	4.6905	1.4507	0.058481	0.13548	✓ -1.0000 -1.000u
_:	-112 -122 -127	4.6905	1.4507	0.058481	0.13548	-1.0000
	-112 -122	4.6905	1.4507 1.3715 1.2139	0.058481 0.043193 0.048934	0.13548 0.13094 0.1337	-1.0000 -1.0000
	-112 -122 -127 -127 -127 -142	4.6935 4.6643 3.248 3.894	1.4507 1.0715 1.2139 1.2046	0.058481 0.043193 0.048934 0.048550	0.13548 0.10094 0.11737 9.11250	-1.000 -1.000 -1.000
	-112 +122 -127 -127 -127 -147 -152	4.6935 4.4643 3.248 3.8947 3.4393	1.4507 1.0715 1.2139 1.2046 1.0637	0.058481 0.043193 0.048934 0.048559 0.042881	0.13548 0.1009± 0.11537 0.11550 0.259342	-1.000 -1.000 -1.0000 -1.0000
	-112 -122 -127 -127 -127 -142 -157	4.6905 4641 3.248 3.8743 3.4393 3.4393	1.4537 1.9715 1.2139 1.2044 1.9637	0.058491 0.043193 0.048934 0.048550 0.042581 0.042581	0.13548 0.10094 0.11737 9.11250	-1.000 -1.000 -1.0000 -1.0000
	-112 -122 -127 -127 -137 -142 -152 -157	4.6935 4.643 3.248 3.8792 3.4393 3.4393 PRESSUPE	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637	0.058481 0.048934 0.048934 0.048584 0.042881 0.042881	0.13548 0.19094 0.11737 0.11250 0.259342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000
-	-112 -122 -127 -127 -127 -147 -157 -157 -157 -157 -157 -157	4.6935 4663 3.4663 3.8948 3.4393 3.4393 PRESSUPE	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637	0.058481 0.048934 0.048584 0.042881 0.042881 0.042881	0.13548 0.10094 0.11337 0.11250 0.259342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000
-	-112 -122 -127 -127 -142 -157 -157 -34001110000	4.6935 4643 3.248 3.6393 3.4393 700000000000000000000000000000000000	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637 PAYINS FARI	0.058491 0.048934 0.048934 0.048989 0.042881 0.042981 9.042981	0.13548 0.10094 0.1137 0.11250 0.259342 0.099342 PI/PTF 0.059342	-1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000
	-112 -122 -127 -127 -142 -152 -157 -2 Annitional Avn word -152 -157	4.6935 4663 3.4663 3.8942 3.4393 3.4393 PRESCIPE PL 3.4393 3.4393 3.4393	1.4507 1.9715 1.2139 1.2044 1.9637 1.9637 PAYINS FAN PL /PN 1.9637	0.058481 0.048934 0.048580 0.042881 0.042881 0.042881 VNYZI FLAP 01/PTF 2.042881	0.13548 0.10094 0.11/37 0.11250 0.259342 0.099342 PI/PTF 0.059342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000
	-112 -122 -127 -127 -142 -152 -157 -2 Annitional Avn word -152 -157	4.6935 4663 3.4663 3.8942 3.4393 3.4393 PRESCIPE PL 3.4393 3.4393 3.4393	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637 PAYINS FARI	0.058481 0.048934 0.048580 0.042881 0.042881 0.042881 VNYZI FLAP 01/PTF 2.042881	0.13548 0.10094 0.11/37 0.11250 0.259342 0.099342 PI/PTF 0.059342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	-112 -122 -127 -137 -147 -157 -157 -3400171004L AVD WORD -152 -157 -3400171004L	4.6935 4.663 3.463 3.4393 3.4393 PRESSUPE PL 3.4393 3.4393 PRESSUPE	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637 WAYINS, FAN M./PN 1.9637 1.0637	0.058481 0.048934 0.048580 0.048580 0.042881 0.042881 0.042881 NOTEL FLAD	0.13548 0.10094 0.11250 0.1250 0.259342 0.099342 PI/PTF 0.059342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	-112 -122 -127 -127 -137 -157 -157 -157 -2 AND TYTOWAL AVD WORD -152 -157 -2 AND TYTOWAL AVD WORD -147	4.6935 4663 3.4663 3.699 3.6393 3.4393 PRESSIBE PL 3.4393 PRESSIBE	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637 WAYINS FAR PL/PN 1.9637 1.0637	0.058491 0.048934 0.048580 0.048580 0.042881 0.042881 0.042881 0.042881 0.042881	0.13548 0.10094 0.11/37 9.11250 0.259342 0.099342 0.099342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	-112 -122 -127 -137 -147 -157 -157 -3400171004L AVD WORD -152 -157 -3400171004L	4.6935 4.663 3.463 3.4393 3.4393 PRESSUPE PL 3.4393 3.4393 PRESSUPE	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637 WAYINS, FAN M./PN 1.9637 1.0637	0.058481 0.048934 0.048580 0.048580 0.042881 0.042881 0.042881 NOTEL FLAD	0.13548 0.10094 0.11250 0.1250 0.259342 0.099342 PI/PTF 0.059342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
	-112 -122 -127 -127 -137 -157 -157 -157 -2 AND TYTOWAL AVD WORD -152 -157 -2 AND TYTOWAL AVD WORD -147	4.6935 4663 3.4663 3.4742 3.4393 3.4393 PRESSUBE PL 3.4393 PRESSUBE PL 3.4494 3.4494 3.4494	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637 WAYINS FAR PL/PN 1.9637 1.0637	0.058481 0.048934 0.048954 0.048954 0.042881 0.042881 0.042881 DEG SIRRING TY 0.042843 0.042943	0.13548 0.10094 0.11250 0.1250 0.259342 0.099342 0.099342 0.099342 0.099342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
A	-112 -122 -127 -127 -137 -157 -157 -3 ADDITIONAL AVD WORD -157 -3 ADDITIONAL AVD WORD -147 -147 -172	4.6935 4663 3.4663 3.4742 3.4393 3.4393 PRESSUBE PL 3.4393 PRESSUBE PL 3.4494 3.4494 3.4494	1.4507 1.9715 1.2139 1.2046 1.9637 1.9637 WAYINS, FAN MI /PN 1.9637 NATIOS - 20 PI /PN 1.9653 1.9653	0.058481 0.048934 0.048954 0.048954 0.042881 0.042881 0.042881 DEG SIRRING TY 0.042843 0.042943	0.13548 0.10094 0.11250 0.1250 0.259342 0.099342 0.099342 0.099342 0.099342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
A	-112 -122 -127 -127 -137 -157 -157 -3 ADDITIONAL AVD WORD -157 -3 ADDITIONAL AVD WORD -147 -147 -172	4.6935 4663 3.468 3.8948 3.4393 3.4393 PRESCIPE PL 3.4393 PRESCIPE PL 3.4494 3.4494 3.4494	1.4507 1.9715 1.2139 1.2046 1.9637 PATINS FAM PLOG 37 1.0637 PATINS 20 PLOG 37 1.0653 PATINS 31 1.0653	0.058491 0.048934 0.048580 0.048580 0.042881 0.042881 0.042881 0.042881 0.042881	0.13548 0.10094 0.1137 0.11250 0.259342 0.099342 0.099342 0.099342 0.099342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
A A	-112 -122 -127 -127 -137 -157 -157 -3500171000 AVD WOPD -152 -157 -167 -167 -167 -172	4.6935 4.663 3.6742 3.6742 3.4393 3.4393 PRESSUPE PL 3.4393 PRESSUPE PL 3.4494 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRESSUPE PL 3.4444 PRE	1.4507 1.9715 1.2139 1.2044 1.9637 1.9637 PAYINS FAN PL/PN 1.0637 1.0637 PAYINS . 20 PL/PN 1.0653 1.0653 RAYINS . 80	0.058491 0.048934 0.048984 0.048984 0.042881 0.042881 0.042881 0.042881 0.042881 0.042841 0.042841	0.13548 0.10094 0.11/37 0.11250 0.259342 0.099342 0.099342 0.099342 0.099342 0.099342 0.099342	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000 -1.0000

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	4651 <b>-1</b> FV <b>1</b>	5 DD E1 1/41	41 AT VORUS	94/19/7º	CADDELL	RFC 19/11/79 04:25:29.164	FAC 9X6¥1	PG# 1934	Flux 15"
			PATINS , PPI			RIC LIGHT VITE CONTRACTOR	741 7417-1		
	<b>ልሆ</b> ባ ቁርየቦ	PI	ባ / ነባ	PL/PTF	PL /PTP	X/DMA X			-
	32	13.541	4.1824	0.18/63	0.43130	0.43200	*		
	37	7.1574	2.2091	0. 098576	0.22780	0.53000			
	47	9. 3392	7.761A	0.1245R	0.2879	J. 6290J		•	
	^{5,7}	0. )74?	2.8026	0.12506	0.2P901	J.72700			
^	POLITIONA C	AL PRESSURF	PATINS , FLO	W SPLITTEP 1	• N•				r r
	AVD WORD	PL	PL /PD	PL /PTF	Pt /PTP	XZDMAX	د. بست ددد سدد.		
$\hat{}$	6.7	19.315	3.1459	0.14216	0.32854	9.42200			
_	+7	7.2325	2.2338	0.0996#3	0.23036	0.67000		····	
`	>ADDIT TON	AL PRESSURE	RATIOS . FLO	IN SPLITTER D	. n.	the same and the same of the s			
	440 HUBB	PL	PL/PO	PL/PTF	PL /PTP	K/DMAX			
_	77	29.014	4.9612	0.39988	0.92411	2.50800			
_	97	14.597	4.5083	0.20118	0.46491	0.58300			
	92	3.45?2	1.9662	3. 34757R	0.10995	0.67000			
	PROTEGNAC	AL PRESSURE	RATIOS . EJE	CTCR SHROUD					· · · · · · · · · · · · · · · · · · ·
7	AVD HOPD	PI.	PL / PO	PL/PTF	PI /PTP	X/DMAX			
	197	4.3R37	1.3539	0.960419	0.13962	0.62400			
	112	4. 3387	1.3400	9.050796	0.13819	U. 93000			
<u>ن</u>	122	4.2785	1.3060	0.058279	0.1346A	0-96000			
	127	3.4522	1.9662	0.047574	0.10995	1.0900			
~ .	137	3.5623	1.1903	0.049097	0.11346	1.2200			
	147	3.5273	1.0979	0.048545	G. 1121#	1.3500			
_	- >400 11 10W	AL ARESCHAF	AATIOS . FOR	FAPON THEFT					
	VAU, MUBD	PL	PL/PO	PI /PTF	PL/PTP	X/DMAX			
	-137	4.3937	1.3539	0.060417	0.13962	-1-9500			
	-112	4,3347	1.7400	0.950756	0.13819	-1.0000			
_	-127	4.7285	1.3960	0.058278	0.13468	-1.0000			
_	-177	\$4527	1.0662	7.747578	0.10995	-1.0000			
_	-127 -127	3.5623	1.0662	7.747578 9.044057	0.10995	-1.0000 -1.0000			
_	-127 -127 -147	3.5%23 3.5%23 3.5225	1.0662 1.1003 1.0879	0.047578 0.049057 0.048545	0.10995 0.11346 0.11218	-1.0000 -1.0000 -1.0000			
_	-127 -127 -147 -152	3.5523 3.5523 3.5223 3.4371	1.0662 1.1003 1.0879 1.0616	7.747578 9.744057 0.048545 0.047371	0.10995 0.11346 0.11218 0.10947	-1.0000 -1.0000 -1.0000			
	-127 -127 -147 -152 -157	3.5%23 3.5%23 3.5225 3.4371 3.4421	1.0662 1.1003 1.0879 1.0616 1.0631	0.047578 0.049057 0.049545 0.047371 0.047440	0.10995 0.11346 0.17218 0.10947 0.10963	-1.0000 -1.0000 -1.0000	· · · · · · · · · · · · · · · · · · ·		
	-127 -127 -147 -152 -157	3.5%23 3.5%23 3.5225 3.4371 3.4421	1.0662 1.1003 1.0879 1.0616	0.047578 0.046057 0.048545 0.047371 0.047440	0.10995 0.11346 0.17218 0.10947 0.10963	-1.0000 -1.0000 -1.0000			
	-127 -127 -147 -152 -153 -157	3.5%23 3.5%23 3.5225 3.4371 3.4421	1.0662 1.1003 1.0879 1.0616 1.0631	0.047578 0.046057 0.048545 0.047371 0.047440	0.10995 0.11346 0.17218 0.10947 0.10963	-1.0000 -1.0000 -1.0000			
	-127 -127 -147 -152 -157	3.5527 3.5523 3.5227 3.4371 3.4421	1.0662 1.1993 1.9879 1.0616 1.9631	0.047578 9.04067 0.049545 9.047371 1.047449 1 K9771E FIAP 0/PYF 0.047371	0.10995 0.11346 0.1721m 0.10947 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -142 -152 -157 -157 -167 -1600, word	3.6527 3.5323 3.5223 3.4371 3.4421	1.0662 1.1013 1.0879 1.0616 1.0631 RAYIOS FAN	0.047578 9.040057 0.049545 0.047371 1.047440	0.10995 0.11346 0.1721A 7.10947 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -152 -152 -167 -167 -169 -169 -169	25.27 3.5%23 3.5.27 3.4371 3.4421 41 PBFCSID PL 3.4371 3.4421	1.0662 1.1013 1.1013 1.1019 1.0616 1.7631 RAYIOS FAN	0.047578 0.04057 0.047371 3.047440 1 KMYYLE TIMP 0.047371 0.047371	0.10995 0.11346 0.1721m 7.10947 0.10963 PL/PTP 0.10947 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -152 -152 -167 -167 -169 -169 -169	25.27 3.5%23 3.5.27 3.4371 3.4421 41 PBFCSID PL 3.4371 3.4421	1.0662 1.1013 1.0879 1.0616 1.0631 RAYINS FAN PI / PN 1.3616 1.0631	0.047578 0.04057 0.047371 3.047440 1 KMYYLE TIMP 0.047371 0.047371	0.10995 0.11346 0.1721m 7.10947 0.10963 PL/PTP 0.10947 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -127 -152 -157 -157 -152 -157 -153	4527 3.5%23 3.5225 3.4371 3.4421 Al PRESSIDE PL 3.4371 3.4421	1.0662 1.1013 1.0879 1.0616 1.0631 RAYIOS FAN PI / PO 1.3616 1.0631	0.047578 9.040057 0.049545 9.047371 3.047440 1 KMYYLE FLAP 0.047371 0.047449	0.10995 0.11346 0.1721m 7.10947 0.10963 PL/PTP 0.10947 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -147 -152 -157 -167 -167 -167 -167 -169	4527 3.5%23 3.5223 3.4371 3.4421 AI PRESSIDE PL 3.4371 3.4421	1.0662 1.1013 1.0879 1.0616 1.0631 RAYIOS FAN PI/PO 1.0631 RETIDS . 20	0.047578 0.040057 0.049545 0.047371 0.047440 I KOYPLE FLAD 0/PYE 0.047371 0.047449 DEG SHIPOIDS I	0.10995 0.11346 0.1718 0.10947 0.10963 PL/PTP 0.10947 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -127 -142 -152 -157 -167 -167 -167 -167	9. 4527 3. 5823 3. 5223 3. 4371 3. 4421 41 PRESSIRE PL 3. 4371 3. 4421 41 PRESSIRE	1.0662 1.1013 1.0879 1.0616 1.0631 RATIOS FAN PL/PO 1.0621 RETIOS - 20 PL/PO 1.0621	0.047578 0.040057 0.049545 0.047371 0.047440 I KMYTE FIRP D.047371 0.047440 0.047440 0.047440	0.10995 0.11346 0.1718 0.10947 0.10963 PL/PTP 0.10947 0.10963 0.10963 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -127 -147 -152 -157 -167 -167 -167 -167 -167 -167 -17	25.77 3.5%23 3.5.27 3.4371 3.4421 AI PRESSIBE PL 3.4371 3.4421 AI PRESSIBE	1.0662 1.1013 1.0879 1.0616 1.0631 RATIOS FAN PLAND FAN	0.047578 0.048545 0.047371 3.047440 1.047440 0.047440 0.047440 0.047440 0.047440	0.10995 0.11346 0.1718 0.17947 0.10963 PL/PTP 0.13947 0.10963 0.10963 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -127 -152 -157 -157 -157 -157 -157 -157 -157 -167 -167 -177 -177 -177 -177	94527 3.5%23 3.5223 3.4371 3.4421 41 PRESSIRE PL 3.4371 3.4421 41 PRESSIRE	1.0662 1.1073 1.0879 1.0616 1.0631 RATIOS FAN M/PO 1.3616 1.0631 RATIOS . 70 M/PO 1.0631 1.0631	9.047578 9.040057 9.049545 9.047371 3.047440 1.047440 1.047440 0.047440 0.047440 0.047440 0.047440	0.10995 0.11346 0.1721m 7.10947 0.10963 PL/PTP 0.13947 0.10963 0.10963 0.10963 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
	-127 -127 -127 -127 -147 -152 -157 -167 -167 -167 -167 -167 -167 -177	94527 3.5%23 3.5%23 3.4371 3.4421 AI PRESSIDE PL 3.4371 3.4421 AI PRESSIDE PL 3.4571 3.3571	1.0662 1.1013 1.0879 1.0616 1.0631 RATIOS FAN PLAND FAN	0.047578 0.048545 0.047371 3.047440 1.047440 0.047440 0.047440 0.047440 0.047440	0.10995 0.11346 0.1718 0.17947 0.10963 PL/PTP 0.13947 0.10963 0.10963 0.10963	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

	MASA-LEWIS	ውቦ ዲያ <b>የቀ</b> ናጀ	HAPY DATA	26/12/79	CADOF ! 1	PEC 10/11/79 04:26:10.76? FAC 9868] PGM C034 PNG 1102
	>ADDIT ICNA	PRESSUPE	PATINS . PPI	MARY PLUG		
•	AVD WOPD 32 37 47	P( 12+)36 6+3780 8+0530	el /en 3.7231 1.9728 2.4910	PI /PTF 0.14653 0.098825 0.12478	PL /PTP 0.43026 0.22800 0.25786	Y/DMAX Q. 43200 Q. 53000 Q. 62900
	52	<u> 4.2787</u>	7.4987	9.12517	0.29878	0.72700
	ADDIT IONAL	PRESSURE	PATIOS , FLO	W SPLITTER I	. D.	and the second s
-	4VP HOPD 52 67	PL 9.1828 6.4530	PL/PN 2.9494 1.9969	PL/PTF 0.14228 0.C99987	PI /PTP 0.32P27 0.23068	X/DMAX 0.42200 0.67000
	IAPORT TROOK	PRESSIME	RATIOS . FLO	W SPLITTER O	. D.	The second secon
	AVD WORD 77 92 42	PL 25.769 13.201 3.4614	PL /PO 7.970ñ 4.0214 1.070ñ	PL / FTF 0. 30929 0. 20144 0. 053639	PI /PTP 0.92119 0.46476 0.12375	X/DMAX 9.50R00 0.58300 0.67000
	APPRITTORE <	PRESSUPE	RATIOS . EJF	CTOR SHPOHO		
-, 	AVD WORD 107 112	P1 3.4970 3.4520	PL/PN 1.2054 1.1915	Pt / PTF 0.060383 0.059686	PL/PTP 0.13931 0.13770	x/nmax 0.62400 0.83000
•	172 177 137 142	3.7470 3.4467 3.1765 3.1365	1.1652 1.0661 0.98257 0.97019	0.058368 0.053406 0.049219 0.04859	0.13466 0.12327 0.11356 0.11213	0.96000 1.0900 1.2200 1.3500
	<b>Exportations</b>	BARKKIBE	KATION KO	FROM TRUET		
	AVID WIRD -107 -117 -122	nt 3.8970 3.8576 3.7670	M/PN 1.2054 1.1915 1.1652	94 /PTF 0.060383 0.059686 0.058369	#[ /PTF 0.13931 0.13770 0.13466	x/milk -1,5000 -1,0000
******	-127 -137 -142 -152	3.1465	1.0661 0.98257 0.97019	0.053406 0.049219 0.048599	0.12327 0.13556 0.11213	-1.0000 -1.0000 -1.0000
•	-1 = 7	3.4367 3.4417	1.0646	0.053251	0.17246	-1.0000 -1.0000
	Zīvu lā ludīf	PRESSIPE	HATTING FAN	THE TEXT		
U	4Vn Hmen ~157 ~157	PL 3.4367 7.4417	PL/PT 1.3631 1.0556	0.053251 0.053251 0.053229	PL/PTP 0.12286 0.12304	k/DMAX -1.0000 -1.0000
	TANDITI GOVE	14055344u	PATENS . 20	तहर रामगोत्रका	PATITION	
J	AVD UDPT -167 -172	PL 3.4417	PL/PN 1.0646 1.0646	0.053329 0.053329	0.12304 0.12304 0.12304	X/D#AR -1.0000 -1.0003
	SAMBITIONA	DDE221ME	PATTOS . NO	DEC STANDON TO	DEATION -	
<b>-</b>	AVB WORD -1927 -197 >507 (0) 5	Pt 7.9364 3.0514 , HEAGUPEN	PI / PG 0. 936#5 0. 943#7	PL /PTF 0.046428 0.047291	Pt /PTP 0.10712 0.10908	x/max -1.00mg -1.0000

		Rom 16
MACA APINE BREAM MATA CARRE TE CAR	114TH BYAYS - DDDCDAM COS - DDCC - 13-03 TO 11-4-	
"ASA-IEMIS PRELIMINARY DATA CADDE-II FACI		
	and the second s	· · · · · · · · · · · · · · · · · · ·
	e de la companya del companya de la companya del companya de la co	- · · · · · · · · · · · · · · · · · · ·
	NASE EJECTIO NOZZLE IMDOEL C) SINTC CHUISE (NS=.04 NT)	
HOZZLE CONFIGURATION	23mHC (-miss (m3-60m mis	
PPIMARY-NOZZEF PING SPLET	PLUG (RETRACTED)	
	POPPE SPLITTER	
CLAMSHELL PRISETTON		
FIECTOR IN FT OPENING		
Link to the second of the seco	Commence of the commence of th	a management of the second of
ROG MO PTE/PTP PTE/PO PTP/PO OMEGA PTS/PT	F COF COP CF1 ETA1 ETA1, INT CFP1 CFP2 F9	See the second s
1103 1.957 2.32 19.73 8.51 0.000 0.26	2 1.035 0.980 0.9707 0.9707 0.9739 0.9739 0.9744 1.5156	
	2 1.036 0.982 0.9747 0.9747 0.9774 0.9774 0.9779 1.5171	
	3 1.037 0.981 0.9787 0.9787 0.9811 0.9811 0.9816 1.5199	a seeka a a a a a a a a a a a a a a a a a a
	3 1.037 0.981 0.9794 ( 9394 0.9816 0.9816 0.9820 1.5190 17 3.453 0.985 1.0680 1.0680 1.0702 1.0702 1.0706 2.6097	
	2 1.040 0.983 0.9799 0.9799 6.9820 0.4820 0.9824 1.4223	
	4 1.03m 0.9m2 0.9793 0.9793 J.on13 0.9013 0.9017 1.5190	
	3 1.039 0.983 0.9890 0.9890 0.9811 0.9811 J.9816 1.5216 3 1.037 0.982 0.9808 0.9808 0.9832 0.9832 0.9837 1.5225	
1113 1.954 2.31 27.17 9.67 0.000 0.24	3 1.038 0.983 0.9726 0.9726 0.9754 0.9754 0.9759 1.5167	The state of the second control of the secon
	3 1.036 0.900 0.9720 0.9720 0.9752 0.9752 0.9757 1.5188 3 0.973 0.982 1.0081 0.9786 0.9817 1.0112 1.0117 1.5049	
	3 0.975 0.982 1.0062 0.9748 0.9781 1.0095 1.0100 1.5139	
	3 0.974 0.981 1.0093 0.9763 0.9798 1.0128 1.0133 1.5218	
	2 0.973 0.984 1.0123 0.9823 0.9850 1.0150 1.0155 1.5124 4 0.975 0.981 1.0114 0.9794 0.9823 1.0143 1.0148 1.5152	and approximate the strange definition is the approximate to the control of the c
	4 0.974 0.982 1.0109 <b>0.</b> 9790 0.9819 1.0138 1.0143 1.5142	
	- 2.416 A.445 T.ATTA A.4114 A.4404 T.ATA4 T.ATA4 T.426A	a communication of the second
	2 0.975 0.984 1.0124 0.9820 0.9844 1.0148 1.0153 1.5117 2 0.974 0.981 1.0180 0.9854 0.9879 1.0226 1.0210 1.5195	
1174 1.959 7.60 24.72 9.52 0.041 0.24	? 0.974 0.982 1.0151 0.9811 0.9838 1.0174 1.0143 1.5202	
	4 0.974 0.984 1.0162 0.9854 0.9876 1.0183 1.0188 1.5149 4 0.977 0.983 1.0159 0.9831 0.9854 1.0182 1.0187 1.5195	
The second secon	3 0.673 0.982 1.0165 0.5821 0.9845 1.0189 1.0194 1.5183	es a sur un manus como es acomo as un aporte de como como estambiento con como establicado en como establi
1129 1.956 2.32 29.81 12.86 0.039 0.24	4 0.975 0.983 1.0182 0.9851 0.9872 1.0203 1.0207 1.5200	
	4 0.977 0.983 1.3170 0.9824 0.5946 1.0192 1.0196 1.5217 3 3.974 0.983 1.3223 0.9875 0.9897 1.0246 1.3259 1.5267	
	2 0.974 0.985 1.0175 0.9644 0.9865 1.0196 1.9291 1.5198	and the second of the second o
1137 1.956 3.6) 27.45 10.55 0.041 0.24	4 0.973 0.483 1.0212 0.9867 0.9861 1.0237 1.0241 1.5251	
	; 7.974 0.984 1.9148 0.9834 0.9842 1.6141 1.0196 1.5178 4 7.974 0.983 1.0145 0.9837 0.9858 1.0167 1.0171 1.5125	· 1
	4 0.973 0.982 1.0172 0.9867 0.9861 1.0197 1.0201 1.5152	
U 113/ 1.655 2.32 24.74 10.67 0.039 0.24	9 0.975 0.985 1.0137 0.9813 0.9839 1.0162 1.0167 1.5169	
	3 0.975 0.983 1.J183 0.9842 0.9869 1.0210 1.0214 1.5249 3 0.974 0.982 1.0138 0.9802 0.9832 1.0168 1.0173 1.5214	
₩ 1130 1.056 2.31 27.32 9.66 0.036 0.26	2 0.973 0.983 1.0124 0.9804 0.5833 1.0153 1.0157 1.5158	The second secon
1140 1.956 2.01 22.45 11.15 0.937 0.24	3 J.975 D.983 1.0109 D.9808 D.9835 1.0136 1.0141 1.5117	
1141 1.647 2.33 19.01 7.64 0.041 0.74	3 7.571 0.941 1.0132 0.9799 0.9933 1.0166 1.3171 1.5247	n

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TIME THE DREET MINARY DATA CADDE-IT FACILITY RECYL PROGRAM CO34 POGS 1103 TO 1144 P+W RASE FJECTOR NOTZLE (MODEL C) MOTZLE TYPE FLIGHT COMPLTIONS NOTTLE COMPEGNATION SPLIT PLUG ERFTRACTED) PRIMARY-NOTTLE PLUG FLEM SPETTTER ISENTPOPIC SPITTER FAN NOTZEE SHOPT FLAP CLASSIELL POSITION FJECTCE THEFT OPENING PNG MO PTE/PTP PTE/PTO PTE/PTO CHECA PTS/PTE CDF CDP CF1 ETA1 ETA1. INT CFP1 CFP2 1147 1.957 2.30 19.65 #.61 0.039 0.243 0.974 0.983 1.0072 0.975# 0.9791 1.0105 1.0111 1.5150 1147 1.457 2.33 14.67 4.61 0.039 0.243 0.474 0.475 1.0072 0.475 0.474 1.1167 1.0111 1.5150 1147 1.457 2.33 14.67 9.48 0.037 0.243 0.474 0.475 1.0134 0.478 0.478 0.474 1.015 1.0150 1.5047 1144 1.455 2.32 24.77 10.64 0.039 0.247 0.474 0.472 1.0134 0.4810 0.4835 1.0169 1.0164 1.5145

NACY -F EMI	5 PRELIM	INARY DATA	06/10/79	CADDELL	REC 10/13/79 01:33:52.230	FAC BYGX!	PG4 C034 RNG 1103
>/ >/ 17 [ [ ]	AL PRESSIPE	PATINS . PPI	MARY PLUG				
เลย เลย เลย	PI	PI / ቦባ	PL/PTF	"I /PTP	X/DMAX		
37	12.323	3.6730	0.18619	0.43170	0.43200		
37	6.5333	1.0472	0.098711	0.22886	1.53000		
47	A. 3024	2.4119	0.12227	0.28348	0.62909		r ar terrorisers i centerapole from such materialismo e apolici de la colo
52	8.1774	2.4432	0.12395	0.27716	0.72700		
>40011104	AL PRESSUPE	PATINS . FLO	W SPLITTEP I	. n.		-	
AVD HORD	PI	PL /PI	PL /PTF	Pi /PTP	X/DM4X		
62	9.3815	2.7961	0.14174	0.32864	J. 42200		transfer of the second control of the second
67	6.6082	1.9696	0.099844	0.23149	0.42200		
SANDITION			W SPLITTER C				
						. It is treeted to the second and the second	A PARTICIPATION OF THE CONTRACTOR AND
AVD WORD	PL	PL / PO	PL /PTF	PL /PTP	X/DMAX		
77	27.3A2	R. 1611	0.41371	0.95920	0.50800		
P7	13.342	3. 9766	0.20159	0.46738	0.58300		
ζ 5	3.61 87	1.0785	0.054674	0.12676	0. 6700u	·· <del>- · -</del>	
SADDIT ION	AL PRESSUPF	PATINS . FUE	FOTOR SHRINUM		The second secon		
AVD WOPD	Ρŧ	PL/PO	PL/PTF	PL /PTP	X/DMAX		
107	4.4397	1.3230	0.067065	0.15549	0.67400		
117	4.1237	1.2791	0.062305	0.14446	0. 83000	· · _ · _ · _ · _ · · _ · · · · · ·	
122	3.8237	1.1396	0.057772	0.13395	0.96000		
127	3.5987	1.0726	0.054372	0.12606	1.0500	. v. st. 1990. lake - v. 1990. v. g. st. 1980. began began between the st	
137	3.4086	1.0159	0.051501	0.11941	1.2200		
147	3.2986	0.48315	0.049834	0.11555	1.3500		
ZEDITION	AL BRESSURS	AATING , FOR	RECOR THEE				
AVITARD		<b>5</b> 260	' N. 46-P	Pi /PTP	G Physical Communication of the Communication of th		
	P[ 4,4387	PL/P/I	PL /PTF		RIDMAN	•	
-137		1.3230	0.067065	0.15549	-1 1000	and a street was a few or the street was a street with the street was a street was a street with the street was a street with the street was a street with the street was a street wa	
-112	4.1237	1.2291	0.062305	0.14446	1.0300		
-122	3.9237	1.1396	0.057772	0.13395	<u>-1.0000</u>		
-177		1.0726	3.054372	0.12604	-1.0000		
-137	3.2086	1.0159	2.051501	0.11/41	-1.0000		
-142	2.297	0.94315	0. (49839	9/1555	-1.0000		
-157	7.5697	1.0636	0.053919	2-12501	-1.0000		
-157	3. 5777	1.0651	0.053964	0.12519	-1.0000		
\$2001710E	AT PRESSIPE	RATTOS FAR	I HETTLE FLAR				
AVD 4PPD	PI	PL /PO	M 197F	PI /PTP	X/DMAX	The property of the second	in may attivities magel (A. as mygatilital) kirjunesy at dise 1888 tils seggga tilaliya affiliklise. «1884 tilas » (A. m.
-157	3.56.87	1.2636	X0.057919	0.12591	-1.3300		
-1=7	3.5737	1.0451	3.053006	0.12510	-1-0000	W 1 to 1 Million of the April 100 and 100	para international ( T. Salah Calaberra, Apara) . La Salah Salah Salah Salah Salah Marana Salah
Sennitia	11	R 1710 - 70	तहर डामकोष्ट्र	TEATTON			
מקחי חער	01	Pf 7P0	PL /PTF	AL /075	C10E4U		e garante angles a la garante <del>establishe</del> r en en angles e la companya e e en
				PI /PTP	X/OMAX		
-1 + 7 -1 7 ?	3.50.47	1.7636	0.053919 0.053843	0.12484	-1.0090 -1.0000		and the second s
•							
	PPESSIBL	PATTITE WI	DEC CIMINO TO				
ייין דורייאל						The state of the s	The second secon
SANTITING	ՐԼ	PI /PG	Pt /PTF	PI /PTP	X\DMVX		
/	PE 2.1085	M /MG 0.92650	01 /PTF 0.046 967	P <b>i /PTP</b> 0.13889	1/DWAR -1.0000		
AVN UNDA	7.1095		0.046967		1.0000 -1.0000	www.s.	

**************************************	S PPFEIM	THEFT DATA	06/10/79	CADDELL	RFC 10/13/79 C1:35:04-073	FAC MX641	PGM C334 RNG 1134
>40017.00	AL PRESSURE	PETIOS , PPI	MAPY PLUG			* · · · · · · · · · · · · · · · · · · ·	
A.4.2. (101.0		M 400	01 40 10	PI /PTP	¥/IIMAX		
32 ህብባት ርላል	P1	PI /PN 4.1499	PI /PTF 7. 18647	U.43128	J. 43200		and the second s
	13.876		3.098754	0.73120			
? 7	7.3720	2.1978			0.53000		
4.7	9.3659	2.7717	0.17277	0.28280	0.62900		
52	0.1854	?.7572	9.12389	0.28654	3. 72700		
SAPOLT LON	AL PRESSIRF	PATIOS . FIG	W SPLITTER I	. n.			
AVD HOPD	PL	PL / PO	PI / PTF	PL/PTP	X/IMAX		
6.2	10.590	3.1515	0.14161	0.32753	0.42200		The same of the sa
67	7,4070	2.7233	J. 099903	0.23105	3.67200		
>ADDITION	AL PRESSURE	PATIOS . FLO	W SPLITTER C	. 0.			
AV2 4080		m (80	m /atc	PL /PTP	V /DMA V		
AVD MORO	PL 705	PL/PN	PI /PTF		X/DMAX		and the state of t
77	30.709	7.2172	0.41417	0.95791	0.50800		
82	14.934	4.4026	0.20142	0.46586	J. 5 8 3 0 0		
9.7	3.5827	1.0754	0.048321	0.11176	0.67000		
>ADDIT FOR	AL PRESSURE	PATIÑS , FJE	CTOR SHROUN		embroside on a residence of the second		
AVD HOPD	PĹ	PL/PO	PL/PTF	PI /PTP	X/DMAX		
107	4.9978	1.5001	0.067406	0.15590	U. 62400		
				0.14452	0.63000		
112	4.6328	1.3976	0.062484				
177	4.287R	1.2970	0.05783)	0.13375	0.96000		
127	3.5627	1.0694	0.048051	0.11114	1.0900		
137	3.6228	1.1474	0.051558	0.11925	1.2200		
147	3.7027	1.1114	0. 649940	0.11550	1.3500		
CANDITION	M PRECIME		EADON - IN FT			·····	
_							
AVINAD	PI	Pt /Pn · =	PI /PTF	PI /PTP	X/DMAX	•	
AVT UNER	Pl 4 0078	P[ /Pf)	PI /PTF	PL/PTP	X/DHAX	•	راه ۱۹۹۰ م سورسان باز انگلافان و پروی پار و بروی در در میشود در میشود به میشود و بروی به در
-107	4.9978	1.5001	0.067406	0.15590	000 کو 1-	•	
-107 -112	4.9978 4.6328	1.3906	0.067406 0.062484	0.15590	-1,0000 ,0000	•	
-107 -112 -122	4.9978 4.6328 4.2878	1.5001 1.3906 1.2870	0.067406 0.362484 0.057830	0.15590 0.14452 0.13375	-1.0000 -1.0000	• · · · · · · · · · · · · · · · · · · ·	
-197 -112 -122 -127	4.9978 4.6328 4.2878 3.5627	1.5001 1.3906 1.2870 1.0696	0.067406 0.062484 0.057830 0.048051	0.15590 0.14452 0.13375 0.11114	-1,0000 -1,0000 -1,0000 -1,0000	•	
-197 -112 -127 -127 -137	4.9978 4.6328 4.2878 5.627 3.8228	1.5001 1.3906 1.2870 1.0696 1.1474	0.067406 0.062484 0.057830 0.048051 0.051558	0.15590 0.14452 0.13375 0.11114 0.11425	-1,0000 1,0000 -1,0000 -1,0000 -1,0000	•	
-107 -112 -127 -127 -137 -147	4.9978 4.6328 4.2878 5627 3.728 3.732	1.5001 1.3906 1.2870 1.0696 1.1476 1.1116	0.067406 0.062484 0.057820 0.048051 0.051558 0.049940	0.15590 0.14452 0.13375 0.1111 0.11-25 0.1550	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -127 -127 -137 -142 -157	4.9978 4.6328 4.2878 5.5627 3.7228 3.7329 3.5327	1.5001 1.3906 1.2870 1.0694 1.1474 1.1114 1.0604	0.067406 0.062484 0.057830 0.048051 0.051558 0.04943 0.047646	0.15590 0.14452 0.13375 0.1111 0.11425 0.11550 0.11020	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -127 -127 -137 -147	4.9978 4.6328 4.2878 5627 3.728 3.732	1.5001 1.3906 1.2870 1.0696 1.1476 1.1116	0.067406 0.062484 0.057820 0.048051 0.051558 0.049940	0.15590 0.14452 0.13375 0.1111 0.11-25 0.1550	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -122 -127 -137 -142 -157	4.9978 4.6378 4.2878 5.627 3.7278 3.7328 3.5327 3.5327	1.5001 1.3906 1.2870 1.0694 1.1474 1.1114 1.0604 1.0694	0.067406 0.062484 0.057830 0.048051 0.051558 0.04943 0.047646	0.15590 0.14452 0.13375 0.11111 0.1125 0.1159 0.11020 0.11020	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -122 -127 -137 -142 -157	4.9978 4.6378 4.2878 5.627 3.7278 3.7328 3.5327 3.5327	1.5001 1.3906 1.2879 1.0694 1.1474 1.1114 1.0604 1.0604	0.067406 0.262484 0.057830 0.048051 0.048051 0.04940 0.047646 0.047646	0.15590 0.14452 0.13375 0.1111 0.11425 0.1150 0.11020 0.11020	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -127 -137 -137 -157 -157 -157 -157 -157 -157	4.9978 4.6328 4.2878 5627 3.7328 3.7327 3.5327 3.5327 AL PRESSUPE	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0604	0.067406 0.262484 0.057890 0.048051 0.048051 0.04940 0.047646 0.047646	0.15590 0.14452 0.13375 0.11117 0.11725 0.11570 0.11020 0.11020	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -127 -137 -147 -157 -157 -157 -157 -157 -157 	4.9978 4.6378 4.2878 5.627 3.527 3.5327 3.5327 PI 3.5327	1.5001 1.3906 1.2879 1.0694 1.1474 1.1114 1.0604 1.0694 PATION FAM	0.067406 0.262484 0.057893 0.048051 0.051558 0.049443 0.047646 0.047646	0.15590 0.14452 0.13375 0.11114 0.1125 0.11550 0.11020 0.11020	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -127 -127 -137 -137 -157 -157 -157 -157 -157 -157 -157	4.9978 4.6328 4.2878 5627 3.7328 3.7327 3.5327 3.5327 3.5327 3.5327 3.5327	1.5001 1.3906 1.2879 1.0694 1.1474 1.1114 1.0604 1.0604 1.0604 1.0604 1.0604	0.067406 0.262484 0.057890 0.048051 0.048051 0.047646 0.047646 0.047646 0.047646	0.15590 0.14452 0.13375 0.11117 0.11425 0.1150 0.11020 0.11020 0.11020	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -137 -147 -157 -157 -157 -157 -157 -157 -157 -15	4.9978 4.6378 4.2878 5.627 3.732 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0694 PATION FAM PLOOPER FAM	0.067406 0.262484 0.057884 0.051558 0.049043 0.047646 0.047646 0.047646 0.047646	0.15590 0.14452 0.13375 0.11114 0.1125 0.11550 0.11020 0.11020 0.11020 0.11020	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -137 -147 -157 -157 -157 -157 -157 -157 -157 -15	4.9978 4.6378 4.2878 5.627 3.527 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0694 PATION, FAR PLYPO 1.0604 1.0604	0.067406 0.062444 0.057890 0.04051 0.051558 0.04940 0.047646 0.047646 0.047646 DECEMBER OF TOP	0.15590 0.14452 0.1375 0.11114 0.1125 0.11550 0.11020 0.11020 0.11020 0.11020 0.11020	-1,0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -127 -137 -137 -157 -157 -157 -250 TT 100 AVD WORD -167	4.9978 4.6328 4.2878 3.7327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 1 BDESSIDE	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0694 PATION FAM PLOOPER FAM	0.067406 0.262484 0.057890 0.048051 0.048051 0.047646 0.047646 0.047646 D.047646 D.047646 D.047646	0.15590 0.14452 0.13375 0.1111/ 0.11/25 0.1150 0.11020 0.11020 0.11020 0.11020 0.11020	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -137 -137 -147 -157 -157 -157 -157 -157 -157 -157 -15	4.9978 4.6378 4.2878 5.627 3.527 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0694 PATION, FAR PLYPO 1.0604 1.0604	0.067406 0.062444 0.057890 0.04051 0.051558 0.04940 0.047646 0.047646 0.047646 DECEMBER OF TOP	0.15590 0.14452 0.1375 0.11114 0.1125 0.11550 0.11020 0.11020 0.11020 0.11020 0.11020	-1,0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -127 -137 -137 -157 -157 -157 -250 TT 100 AVD WORD -167	4.9978 4.6378 4.2878 5.627 3.527 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327	1.5001 1.3906 1.2879 1.0694 1.1474 1.1114 1.0604 1.0694 PATION, FAR PLANCE, 20 PLANCE, 20 P	0.067406 0.262484 0.057890 0.048051 0.048051 0.047646 0.047646 0.047646 D.047646 D.047646 D.047646	0.15590 0.14452 0.13375 0.11114 0.1125 0.11550 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000		
-107 -112 -127 -137 -137 -142 -157 -157 -157 -157 -167 -167 -167 -167 -172	4.9978 4.6378 4.2878 3.7327 3.7327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 41 BDECSIDE	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604	0.067406 0.262446 0.057890 0.048051 0.048051 0.047646 0.047646 0.047646 D.047646 D.047646 D.047646 D.047646 D.047646 D.047646 D.047646 D.047646	0.15590 0.14452 0.13375 0.1111/ 0.11425 0.1150 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000		
-107 -112 -127 -137 -147 -157 -157 -157 -157 -157 -157 -157 -15	4.9978 4.6328 4.2878 3.7327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604 PAYING . 70 PL /PN 1.0604 1.0604	0.067406 0.262446 0.057890 0.048051 0.048040 0.047646 0.047646 0.047646 D.047646 DFG SIMPRIM TO	0.15590 0.14452 0.13375 0.11117 0.11125 0.11550 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 x/DMAX -1.0000 -1.0000		
-107 -112 -127 -127 -137 -147 -157 -157 -157 -157 -157 -157 -157 -167 -167 -167 -167 -167 -167 -167 -16	4.9978 4.6378 4.2878 3.7327 3.7327 3.5327 3.5327 3.5327 3.5327 3.5327 3.5327 41 BDECSIDE	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604 1.0604	0.067406 0.262446 0.057890 0.048051 0.048051 0.047646 0.047646 0.047646 D.047646 D.047646 D.047646 D.047646 D.047646 D.047646 D.047646 D.047646	0.15590 0.14452 0.13375 0.1111/ 0.11425 0.1150 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020 0.11020	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000		

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* 4 < A = L FW (	S PRFLIM	INAPY DATA	06/11/79	CABRETT	PEC 10/13/79 01:36:33.026	F4C 8Y6X1 PG# CQ34 RDG 1185
SAU SET TON	et PRESSIJPE	RATIOS , PPI	MARY PLUG			
					· a security that comments the security the security of the se	
AND MULD	Pt	PL / PN	PI /PTF	PI /PTP	X/DMAX	சிரும் சி. மி. இரும் கி. மார் ஆம் <b>ம</b> ்றுள்ள அது சார்
4.7	15,426	4.6329	0.18514	0.43170	J. 43200	
77	R. 1 596	2.4506	0.097931	0.22835	0.53000	meno di
47	10.088	3, 3297	0.1210#	0.27231	0.67900	
_ 52	10.238	3.9747	7.12287	0.2 PE 50	9, 72799	
>400141044	L PPFSSIMF	RATIOS . FLO	W SPLITTEP I	. n.		
AVP WOPD	Pl	<b>የ</b> ዚ / የብ	PI /PTF	PI /PTP	X/DMAX	
62	11.721	3. 5202	0.1406R	0.32801	0.47200	Ca mondes Controlle on a service 1960 is no et interes appart to combine apparentage of a paging apparent a service in a service apparent and a service app
67	P. 2545	2.4791	2.099071	0.23100	J. 67:300	
SANSTITON	E PPESSUPE	PATINS . FIG	W SPLITTER O	.0.		
TAU Must	PL	<b>ም</b> ኒ / የብ	PI /PTF	PL /P TP	x/DMAX	
77	34.128	19.250	0.40960	0.95506	).50A00	to a communication of the second communication and the second communication of the sec
R2	16.774	5.0778	0.20132	0.46942	0. 56300	
- 65	1.5961	1.3800	0.04161	0.10064	0.67000	
						s and the second of the second
> thall low	IL PPFSSIPE	PATINS . FJF	ETOP SHPCUD			
WAL MUEL	PL	· /PN	PI / PTF	PL/PTP	X/DMAX	The state of the s
107	5.6309	.6911	0. 67592	0.15758	0.62400	
117	5.2163	5665	C. 062603	0.14597	0.83000	
172	4.4361	1.4524	0.058043	0.13534	0.96000	
127	3.5411	1.0755	0. 042981	0.10022	1.3900	
177	4.2661	1.2813	0.051202	0.11939	1.2290	
142	4.1461	1. 2452	0.049762	0.11603	1.2500	and the second of the second o
- Zentalum		AATING , EC	FACIN INLES			
		***			-	- Taran - Tara
VAUNUEL	PÍ	<b>ቦ</b> ኒ / ቦስ	PL/PTF	PĹ/PTP	N/DHAY	•
-127	5.6139	1.6911	0.947582	0.15758	-1.0000	
-11,	F. 2160	1.5665	0. (624.03	0.14597	-1.0000	The state of the s
-127	4.9361	1.4574	0.058043	0.13534	-1.3000	
-127	A LUII.	1. 3755	0.747941	0.10022	-1.0000	
-137	4.7661	1.2013	0.051202	9.11939	-1.0000	
-142	4.14M	1.7452	0.049762	N. 11603	-1.0006	er or recognition of the state of the st
-152	3.5411	1.3635	0.042501	0.099098	-1.0090	
-157	2.5411	1.3435	0.042501	0.09909#	-1-0000	த் படுகளு , டி சம்பட <del>படித்தில் இடைய முறிய மடிக்கில் இடிப்படுக்கில் இடிப்படுக்கில் செய்யில் மடிப்படுக</del> ்கில் மடிப்படுக்கில் மடிப்படிப்படுக்கி
くとつつままでの)	. विकार रहा है	RATTING FAR	N <i>03739</i> F F140			
AVO WEED	Pt	PL/M)	PL /PTF	PL /PTP	X /DMAY	The second secon
-152	3.5411	1.2635	0.042501	0.09909#	-1.0000	
-157	3.5411	1. 2525	7 C47501	3.079098	-1.0000	and the second of the second o
SPAST TIME	[ nar<<()pr		DEC SHPFOOTI	WALLE OF		
			_		40	gi a marka gara a mana akasa a mahan aka mana mana kasa a sa sa sa mananga Mana Angala.
<b>ት</b> ሂሳ ።ሮይባ	PL	Pt /PD	PI /PTF	AT NO TO	X/DMAX	
-147 -177	3.53/1	1.0620 1.0535	0.042449 0.042591	0.33096958 0.330398	-1.0000 -1.0000	and the second s
ייי אייזדערנע			ስድር ናዘምሮው <u>ተ</u>			
	. re=119#F	A	entral about the 1.	·		
					<b>*</b>	خان بيشان المستقل ال
AVD WED	PI	<b>ኮ</b> ( / ቦሶ	PI /PTF	PL /PTP	x/Defyx	
avn ven		Pt / PM 3. 92 984			-130 <b>0</b> 0	
AVD WED	PI 3.3963 3.1461		M /PTF 0.037159 0.037759	PL /PTP 9.096642 0.088042	-1.0000 -1.0000	e le la

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ሚልባለE FW I	c patila	THEM DATE	9//11/79	CADNETT	PEL 10/13/10	61:37:17.155	FAC MYSYL	PG4	ROW 16 PRG 1196
>thriting	11 PFF5511PF	PATIOS . PPI	MELA DI PIC			-			
INU PUBL	Pf	የኒ/ቦን	PI / PTF	PL /PTP	x/DMAX				
32	17.130	5.1296	J. 18553	0.43169	0.43200				•
37	9,997	2.779F	0.090012	0.22894	J. 5390u				
47	11.148	3.3567	0.12141	0.2874P	3.62990				
52	11.304	7,4048	0,12715	0.28653	0.72700				
MOLITION	AL PPFSSUPF	PATIOS , FEE	W SPLITTEP I	, n.					
IVD WOPD	Pi	<b>ም</b> ር / ቦብ	PL / PTF	PI /PTP	Y/DMAX				
62	12.941	3.8966	0.14094	0.32792	0.42700		*		
e7	9.1147	2.7444	3.099264	0.23096	0.67000				
Stault ton	AL PRESSUPE	PATIOS . FLO	W SPLITTER P.	.n.					
LVD WHEN	P1	PL/PO	PL/PTF	PL/PTP	X/D#AX				
77	37.160	11.195	0.40491	0.94210	0.50#00				_,,
A?	18.494	5.5686	0.20141	0.46R63	J.58300				
97	3.5857	1.0796	0.039050	0.09085P	0.67009				
>4991T199	AL PRESSIME	PATIOS . FJE	CTOR SHEAUÓ		-		THE RESIDENCE OF THE SECOND SE	* ** ** ** ** **	de liagós a la cidadester de cuas. 166
AU MUBU	Pl	Pt / Pri	PL / PTF	PI /PTP	X/DHAX				
107	6.2009	1. 9671	9.067531	0.15712	J.62400				
112	5,7559	1.7331	0.047686	0.14585	0. 8300U				
122	5.3210	1.6721	9.057949	0.13483	0.96000				
17"	3.5A57	1.0796	0.039050	0.090858	1.0900				remain defenders as the management of the second of the se
137	4.71.39	1.4185	3.051305	0.11937	1.2200				
142	4.5759	1.3778	0.049835	0.11595	1.3500		garan and an an and an		The state of the s
>4001F 104	L PECSUAF	****** <b>**</b>	FARRY IN FT						
NA HULD	Pt	PL /PO	PI /PTF	PI /PTP	x/DMA		The second section of the second seco		The state of the s
A. M				0.15712	-1.0000				
	6.2009	1.4671	0.057531		- 10000				
127		1.7331	0.067531	0.14585					and the second s
127	6.2009 5.7559 5.3210				1.0000				ger <del>ianija gitas</del> va ajangja gita se dajanja agai. Dosk izi - ee di alki izi
127 -112 -127	6.2009 5.7559 5.3210	1.7331	0.062686	0.14585	1.0000				
127 112 127 127	6.2009 5.7559 5.3210 3.5857 4.2109	1.7331 1.6021 1.0796 1.4185	0.062686 0.057947	0.14585 0.13483 0.090998 0.11437	1.0000				
127 -112 -127 -127 -127 -147	4.2009 5.7559 5.3210 3.5857 4.2109 4.5109	1.7331 1.6021 1.0796	0.062686 0.057947 0.057947 0.051375 0.051375	0.14585 0.13483 0.090998 0.11437 0.11595	1.0000 -1.0000 -1.6900				
197 112 122 127 127 147	6.2009 5.7559 5.3210 3.5857 4.2109	1.7331 1.6021 1.0796 1.4185	0.042686 0.057949 0.034059 0.051315	0.14585 0.13483 0.09098 0.11737 0.11595 0.089591	-1.0000 -1.0000 -1.0000 -1.0000				
197 -112 -127 -127 -137 -142 -157	4.2009 5.7559 5.3210 3.5857 4.2109 4.5109	1.7331 1.6021 1.0796 1.4185 1.3778	0.062686 0.057947 0.057947 0.051375 0.051375	0.14585 0.13483 0.090998 0.11437 0.11595	1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 127 127 147 157	6.2009 5.7559 5.3710 3.5857 4.1109 4.5759 2.5357 3.5407	1.7331 1.6021 1.0796 1.4185 1.3778 1.0646	0.042686 0.057949 0.051949 0.051315 0.051315 0.049815 0.038506 0.03856	0.14585 0.13483 0.09098 0.11737 0.11595 0.089591	1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 137 142 157 157 5850[7][0]	6.2009 5.7559 5.3210 3.5857 4.2109 4.579 3.5357 3.5407	1.7331 1.6021 1.0796 1.4185 1.3778 1.0646 1.3561 FAYIN FAR	0.062686 0.057949 0.057949 0.051305 0.051305 0.051305 0.051305 0.03850 0.03850 0.03850 0.03850	0.14585 0.13483 0.14937 0.1437 0.1159 0.089591 1.089718	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 127 137 142 157 157 >āñŋ[Ŧ[n]] VB 46-PB	6.2009 5.7559 5.3210 3.5857 4.2109 4.5709 3.5357 3.5407 AL PPPTSURE	1.733i 1.602i 1.079c 1.4185 1.377R 1.064c 1.356i PAYIN FAN	0.062686 0.057949 0.057949 0.051335 0.051335 0.051335 0.03856 0.03856 0.03856 0.03856	0.14585 0.13483 0.14937 0.14937 0.1159* 0.089591 1.089718	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 127 147 157 157 >Anni Tin'i	6.2009 5.7559 5.3210 3.5857 4.2109 4.579 3.5357 3.5407	1.7331 1.6021 1.0796 1.4185 1.3778 1.0646 1.3561 FAYIN FAR	0.062686 0.057949 0.057949 0.051305 0.051305 0.051305 0.051305 0.03850 0.03850 0.03850 0.03850	0.14585 0.13483 0.14937 0.1437 0.1159 0.089591 1.089718	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 127 147 147 157 157 5 Anoff Ing Vo. 40-P.D. 157	6.2009 5.7559 5.3210 3.5857 4.2109 4.579 3.5357 3.5407 AL PRICESURE	1.733i 1.602i 1.079c 1.4185 1.377R 1.064c 1.356i PAYIN FAN	0.062686 0.057949 0.051305 0.051305 0.051305 0.051305 0.03856 0.03856 0.03856 0.03856 0.03856 0.03856	0.14585 0.13483 0.149376 0.14937 0.1159 0.089591 1.089718 Pt/PTP 0.089591 0.089718	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 127 147 147 157 580017 Ing VB 40-PB 157 540017 Ing VB 40-PB	6.2009 5.7559 5.3710 3.5857 4.1109 4.57 9 3.5357 3.5407 AL PRESSIRE PL 3.5357 3.5407	1.7331 1.6021 1.0796 1.4185 1.3778 1.0646 1.3561 PAYIN FAR	0.062686 0.057949 0.057949 0.051335 0.051335 0.03856 0.03856 0.03856 0.03856 0.03856 0.03856 0.03856	0.14585 0.13483 0.1973/8 0.11437 0.1150* 0.089591 1.089718 Pt /PTP 0.089718	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 127 147 147 157 157 5 A 5 O F T T T T T T T T T T T T T T T T T T	# 2009 5.7559 5.3710 3.5857 4.109 4.579 3.5357 3.5407 AL PRESSIRE PL 3.5357 3.5407	1.7331 1.6021 1.0796 1.4185 1.3778 1.0646 1.2561 RAYIN FAR M /PO 1.0646 1.3661 PAYIN 20	0.062686 0.05746 0.051375 0.051375 0.051375 0.23856 0.23856 0.23856 0.23856 0.23856 0.23856 0.23856 0.23856	0.14585 0.13483 0.14937 0.14937 0.1595 0.089591 1.089591 0.089591 0.089718	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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107 112 127 127 127 127 157 157 5869[7][0][1 VB 46-0 B 157 5800[7][0][1 VB 4000 167 167	# 2009 5.7559 5.3210 3.5857 4.2109 4.5709 3.5357 3.5407 AL PRESSIRE PL 3.5357 3.5407 AL PRESSIRE PL 3.5357 3.5407	1.7331 1.6021 1.0796 1.4185 1.3778 1.0646 1.3661 PAYION FAN M/PO 1.0646 1.3661 PAYION 20 PI/PO 1.3661 1.3631	0.062686 0.05746 0.051375 0.051375 0.051375 0.23856 0.23856 0.23856 0.23856 0.23856 0.23856 0.23856 0.23856	0.14585 0.13483 0.12978 0.1297 0.1159* 0.089591 1.089718 0.089591 0.089718 0.089718 0.089718	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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	82	20,209	6.0370	0.66882	0.46654	0.58300			
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	107	6.7648	2.9298	0.22360	0.15617	0.62400			•
	117	6.7896	1.8789	0.70816	0.14520	0.83000			
	122	F. 8194	1.7384	0.19260	0.13435	0.96000			•
	127	3.6.79	1.0408	0.11974	0.0#3522	1.0900		-	The state of the s
	127	5.1691	1.5442	0.17107	0.11933	1.2200			
	142	5.619)	1-4993	0.16611	0.11587	1.3500			
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	-137	5. M91	1.5442	0.17107	0.11923	-1.0000			•
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SEPTITIONS.

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Pt / PO

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VP WPPD         PL         PL/PTD         PL/PTP         X/DMAX           167         3.5539         1.0608         0.036400         0.044201         -1.0000           172         3.5529         1.0608         0.036400         0.074201         -1.0000           540311 [0.000 PESSIPE RAYINS , MO DEG SHREUN THEAVYON         NO MONTO PL         PL/PTP         X/DMAX	
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47	11.807	3.5532	0.12162	0.24222	9. 62930	*-	F T R TOTAL OR ORDER OF THE STATE OF	Market Market of Market Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of t	
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52	13.744	4.1360	0.14157	0.32851	0.42200		****	e i de c <del>ulture</del> de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de suite de s	Married of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the season of the s
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AVD WOPD	PI	PI /PO	PL /PTF	PL /PTP	X/DMAX				
107	6.5588	1.9738	2.567561	0.15077	0.62400				
117	6.0942	1.8740	0.062775	0.14567	0.93000				
1,23	5.6445	1.6986	0.05#143	0.13492	0.96000				
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147	4.6339	1.3925	0.050283	0.11673	1.3500				
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AVII UNPN -107 -117 -122 -127	PL 6.2349 5.7970 5.3570 5797	PI /PI 1.8752 1.7413 1.6090 1.0766	PI / PTF 0.067713 0.067881 0.058103 0.038877	PI /PTP 0.15719 0.14597 0.13488 0.090280	X/DM/X -1.0000 1.0000 -1.0000 -1.0000				
AUDITION AUIT UCPO -107 -117 -127 -137	PL 6.2349 5.7970 5.3570 4.700	PI / PRI 1. 8752 1. 7413 1. 60 90 1. 0766 1. 4286	PI / PTF 0.067713 3.662881 0.058103 0.058103 0.038877 0.051586	PI /PTP 0.15719 0.1459 0.13487 0.0502/0 0.11475	X/DM/A -1 (000 1.0000 -1.0000 -1.0000				
AUDITION  AUDITION  -10° -11° -12° -12° -127 -137 -14°	PL 6.2349 5.7970 5.3570 4.7500 4.6779	PI /PN 1.8752 1.7413 1.6990 1.0766 1.4286 1.1925	PI / PTF 0.067713 3.067881 0.058103 0.038877 0.051596 0.051283	PI /PTP 0.15719 0.14507 0.13488 0.050270 0.11475 0.11475	X/DM/X 0000 1.0000 -1.0000 -1.0000 -1.0000		•		
AVID UPPD -107 -117 -122 -127 -137 -147 -142 -142	PL 6.2349 5.7970 5.3570 4.7570 4.7570 2.5277	PATION - W PI / PO 1.8752 1.7413 1.6940 1.0766 1.4286 1.3925 1.0616	PI / PTF 0.067713 0.067713 0.062881 0.058103 0.038877 0.051586 0.053283 0.028234	PI /PTP 0.15719 0.1579 0.13489 0.050270 0.11475 0.11473 0.098989	X/DM/X -1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000		•		
AUDITION  AUDITION  -10° -11° -12° -12° -127 -137 -14°	PL 6.2349 5.7970 5.3570 5.4570 4.700 4.6770 3.5277 3.5347	PI / PR 1.8752 1.7413 1.60 90 1.0766 1.4786 1.3925 1.0616 1.0631	PI / PTF 0.067713 3.067881 0.058103 0.058107 0.051596 0.053283 0.028234 1.038388	PI /PTP 0.15719 0.14597 0.13487 0.050270 0.11475 0.11673 0.088989 0.389115	X/DM/X 0000 1.0000 -1.0000 -1.0000 -1.0000				
AVID UPPD -107 -117 -122 -127 -137 -147 -142 -142	PL 6.2349 5.7970 5.3570 5.4570 4.700 4.6770 3.5277 3.5347	PI / PR 1.8752 1.7413 1.60 90 1.0766 1.4786 1.3925 1.0616 1.0631	PI / PTF 0. 067713 0. 067713 0. 058103 0. 038877 0. 038877 0. 051596 0. 053283 0. 078388 1. NOVII FIAR	PI /PTP 0.15719 0.14597 0.13487 0.050270 0.11475 0.11673 0.088989 0.389115	X/DM/X -1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AUDITION  AVII UNPN  -107  -117  -127  -137  -147  -147  -167	PL 6.2349 5.7970 5.3570 5.4570 4.700 4.6770 3.5277 3.5347	PI / PR 1.8752 1.7413 1.60 90 1.0766 1.4786 1.3925 1.0616 1.0631	PI / PTF 0.067713 3.067881 0.058103 0.058107 0.051596 0.053283 0.028234 1.038388	PI /PTP 0.15719 0.14597 0.13487 0.050270 0.11475 0.11673 0.088989 0.389115	X/DM/X -1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000		•		
AUDITION  AUTOPO  -107 -117 -127 -137 -147 -147 -147 -167 -167	PL 6.2349 5.7970 5.3570 5.797 4.500 4.6170 3.5277 3.5347	PI / PRI 1. 8752 1. 7413 1. 60 90 1. 0766 1. 4786 1. 1925 1. 06 31	PI / PTF 0. 067713 0. 067713 0. 058103 0. 038877 0. 038877 0. 051596 0. 053283 0. 078388 1. NOVII FIAR	PI /PTP 0.15719 0.14597 0.13489 0.050290 0.11475 0.11475 0.11475 0.098589 0.389115	X/DM/X -1 0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AUDITION  AUTHORY  -107 -117 -127 -137 -147 -147 -167 -167 -260017 [08]	PL 6.2349 5.7970 5.3570 4.7500 4.6770 3.5347	PI / PR 1. 8752 1. 7413 1. 69 90 1. 0766 1. 4286 1. 1925 1. 06 31 PATIOS FAR	PI / PTF  0. 067713  0. 067713  0. 058103  0. 058103  0. 058107  0. 053287  0. 053283  0. 078389  1. NOZZI FIAP	P1 /PTP 0.15719 0.15719 0.13489 0.050280 0.11475 0.11475 0.089115	X/DM/X -1 (000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AUDITION  AUTHORY  -107 -117 -127 -137 -147 -147 -147 -167 -2001T ION  AVE 4000 -167 -167	PL 6.2349 5.7970 5.3570 5.7570 4.7500 4.6777 3.5347 All PRESSURE Pt 3.5297 3.5347	PI / PN 1. 8752 1. 7613 1. 60 90 1. 0766 1. 4286 1. 1926 1. 0616 1. 0631  PATING FAR PI / PN 1. 0616 1. 06 31	PI / PTF 0.067713 0.067713 0.058103 0.058103 0.038877 0.051586 0.053283 0.028234 1.038388 1.07711 FIAP	PI /PTP 0.15719 0.14597 0.13488 0.090280 0.11475 0.11475 0.089115 Pt /PTP 0.089999 0.089115	X/DMAX -1 (0000 -1 0000 -1 0000 -1 0000 -1 0000 -1 0000 -1 0000				
AUDITION  AUDITION  -107 -117 -127 -137 -147 -147 -147 -157 -20017 100  AVE 4000 -157 -157	PL 6.2349 5.7970 5.3570 4.5797 4.7600 4.6770 3.5347 IAI PRESSURE PL 3.5297 3.5347 IAI PRESSURE	PI / PR 1. 9752 1. 7413 1. 60 90 1. 0766 1. 4286 1. 1925 1. 06 31 PATTOS FAR PI / PR 1. 06 16 1. 06 31	PI / PTF 0.067713 3.062881 0.058103 0.038877 0.051586 0.053283 0.028238 1.038388 1.0771 FIAP 0.038334 3.028388	PI /PTP 0.15719 0.14597 0.13488 0.060290 0.11475 0.11673 0.088989 0.088989 0.0889115	X/DMAX -1 (000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVID 17 19 19 19 19 19 19 19 19 19 19 19 19 19	PL 6.2349 5.3570 5.3570 5.3570 4.500 4.6170 3.5297 3.5347 AI PRESSURE PL 3.5297 3.5347 IAI PRESSURE	PI / PRI 1. 9752 1. 7413 1. 69 90 1. 0766 1. 42 96 1. 1925 1. 06 16 1. 06 31 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PRI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PRI / PRI 1. 06 16 16 16 16 16 16 16 16 16 16 16 16 16	PI / PTF  0. 067713  0. 067713  0. 067713  0. 058103  0. 058103  0. 058177  0. 051596  0. 050233  0. 078234  0. 078234  0. 078234  0. 078234  0. 078234  0. 078234  0. 078234  0. 078234	PI /PTP 0.15719 0.15719 0.14597 0.13489 0.090290 0.11475 0.11475 0.098989 0.089115	X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AUDITION  AUTHORY  -107 -117 -127 -137 -147 -147 -147 -157  >thottion -157 -157  AVD RODD -157	PL 6.2349 5.7970 5.3570 5.797 4.7600 4.6777 3.5347 MI PRESSURE PL 3.5297 3.5347 MI PRESSURE PL 3.5297 3.5347 MI PRESSURE PL 3.5297 3.5347	PI / PR 1. 8752 1. 7613 1. 69 90 1. 0766 1. 4286 1. 1926 1. 06 16 1. 06 31 PATING FAR PI / PR 1. 06 16 1. 06 31	PI / PTF 0.067713 0.067713 0.067713 0.058103 0.058107 0.058107 0.051596 0.0503784 0.038384 0.038384 0.038384 0.038384 0.038387 0.038789	PI /PTP 0.15719 0.15719 0.13489 0.090280 0.11475 0.11475 0.0849115 Pt /PTP 0.089115 TEATION	X/DMAX -1 0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVID 17 19 19 19 19 19 19 19 19 19 19 19 19 19	PL 6.2349 5.3570 5.3570 5.3570 4.500 4.6170 3.5297 3.5347 AI PRESSURE PL 3.5297 3.5347 IAI PRESSURE	PI / PRI 1. 9752 1. 7413 1. 69 90 1. 0766 1. 42 96 1. 1925 1. 06 16 1. 06 31 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PRI / PRI 1. 06 16 1. 06 2 3 1 PATTERS FAM. PRI / PRI 1. 06 16 16 16 16 16 16 16 16 16 16 16 16 16	PI / PTF  0. 067713  0. 067713  0. 067713  0. 058103  0. 058103  0. 058177  0. 051596  0. 050233  0. 078234  0. 078234  0. 078234  0. 078234  0. 078234  0. 078234  0. 078234  0. 078234	PI /PTP 0.15719 0.15719 0.14597 0.13489 0.090290 0.11475 0.11475 0.098989 0.089115	X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AUDITION  AUTHORY  -107 -117 -127 -137 -147 -147 -147 -157  >thottion -157 -157  AVD RODD -157	PL 6.2349 5.3570 5.3570 5.3570 4.700 4.700 3.5347 ALI PRESSURE PL 3.5297 3.5347 ALI PRESSURE	PI / PRI 1. 8752 1. 7413 1. 69 90 1. 0766 1. 4286 1. 3925 1. 0616 1. 0631 PATTES Fab. PI / PRI 1. 06 16 1. 06 31 PATTES Fab. PI / PRI 1. 06 16 1. 06 31 1. 06 31 1. 06 31 1. 06 31	PI / PTF 0.067713 0.067713 0.067713 0.058103 0.058107 0.058107 0.051596 0.0503784 0.038384 0.038384 0.038384 0.038384 0.038387 0.038789	PI /PTP 0.15719 0.15719 0.1459 0.13489 0.090290 0.11475 0.11475 0.098989 0.089115  PI /PTP 0.089115	X/DMAX -1 0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVIDATE INV.  AVIDATE INV.  AVIDATE INV.  AVIDATE INV.  AVIDATE INV.  AVIDATE INV.  -167  -167  -167  -167  -167  -167  -167  -177  -177	PL 6.2349 5.7370 5.3570 5.797 4.7620 4.6777 3.5347 MAI PRESSIRE PL 3.5297 3.5347 MAI PRESSIRE PL 3.5297 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI	PI / PR 1. 8752 1. 7613 1. 69 90 1. 0766 1. 4286 1. 1926 1. 06 16 1. 06 31 PAYING FAR PI / PR 1. 06 16 1. 06 31 DAYING FAR PI / PR 1. 06 31 1. 06 31 1. 06 31 1. 06 31 1. 06 31 1. 06 31	PI / PTF 0.067713 0.067713 0.067713 0.058103 0.058107 0.058107 0.053837 0.0781383 0.0781384 0.038334 0.038334 0.038388 0.038388 0.038788 0.038788	PI /PTP 0.15719 0.15719 0.14597 0.13488 0.090280 0.11475 0.11475 0.084915 PI /PTP 0.089115 TETTITM	X/DMAX -1 0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AUDITION  AUTHORY  -107  -117  -127  -137  -147  -147  -147  -147  -147  AVD 4000   PL 6.2349 5.7970 5.3570 4.7500 4.6770 3.5347	PI / PR 1. 8752 1. 7413 1. 60 90 1. 0766 1. 4286 1. 1925 1. 06 31 PATINS FAR PI / PR 1. 06 16 1. 06 31 PATINS FAR PI / PR 1. 06 31 1. 06 31 PATINS FAR PI / PR 1. 06 31 PATINS FAR PI / PR 1. 06 31 1. 06 31 PATINS FAR PI / PR 1. 06 31 PATINS FAR PI / PR 1. 06 31 1. 06 31 PATINS FAR PI / PR 1. 06 31 PATINS FAR PI / PR 1. 06 31 1. 06 31	PI / PTF  0. 067713	PI /PTP 0.15719 0.15719 0.15719 0.13487 0.039020 0.11475 0.11673 0.089115 PI /PTP 0.089115 TAYTON 1/PTP	X/DMAX -1 (000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
AVIDATE INV.  AVIDATE INV.  AVIDATE INV.  AVIDATE INV.  AVIDATE INV.  AVIDATE INV.  -167  -167  -167  -167  -167  -167  -167  -177  -177	PL 6.2349 5.7370 5.3570 5.797 4.7620 4.6777 3.5347 MAI PRESSIRE PL 3.5297 3.5347 MAI PRESSIRE PL 3.5297 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI PRESSIRE PL 3.5247 MAI	PI / PR 1. 8752 1. 7613 1. 69 90 1. 0766 1. 4286 1. 1926 1. 06 16 1. 06 31 PAYING FAR PI / PR 1. 06 16 1. 06 31 DAYING FAR PI / PR 1. 06 31 1. 06 31 1. 06 31 1. 06 31 1. 06 31 1. 06 31	PI / PTF 0.067713 0.067713 0.067713 0.058103 0.058107 0.058107 0.053837 0.0781383 0.0781384 0.038334 0.038334 0.038388 0.038388 0.038788 0.038788	PI /PTP 0.15719 0.15719 0.14597 0.13488 0.090280 0.11475 0.11475 0.084915 PI /PTP 0.089115 TETTITM	X/DMAX -1 0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

				*****					RUN 16
**454~I FW	[5] PRF[[M]	MADA DALV	06/11/79	CADOFII	REC 10/13/7	9 01:43:13.827	ENC AXEXT	PGM . CQ34	_ PNG 1112
AUD I T IUV	IAL_PPESSIME	PATIOS . PPI	TAVBA LFRE						
ላው ጠሩቅሀ	Pt	P  / PO	PI /PTF	PL /PTP	X/DMAX				
32	15.374	4.6295	0.18569	0.43195	0.43200				
77	A.1344	7.4494	0.098246	0.22854	0.53000				
47	19.362	3.0299	0.12153	0.29270	9.62903				
52	10.192	3.0690	0.12310	C.28635	0.72700				
· · · · · · · · · · · · · · · · · · ·	10.172	16 06 70	0.12310		0.72700		- <del></del>		<del></del>
NOT TIONS	INL PPESSURE	RATIOS . FEC	OW SPLITTER 1.	. D _•					
AUND	Pi	Pt / PO	PL /PTF	PI /PTP	X/DMAX				•
2	11.665	3.5126	0-14089	U. 32774	0.42200				
57	8.2793	2.4780	0.099393	0.23171	J.67000				
ADD TERRA	AT PRESSURE	PATIOS . FLE	N SPLITTER D	n_	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s				
						# · # -			
in Authori	PI	PL/PO	Pt /PTF	PI /PTP	X/DMAX				
7	33.147	9.9911	0.40034	0.93128	0.50800				
?	16.682	5.0232	0.2014R	0.46869	0.58300				
2	3.5749	1.0771	0.043203	0.10050	0.67000				
400 F T 1004	AL PRESSIPE	RATIOS . FJF	FOTOR SHROUD						
D WORE	PL	Pt /PO	PL/PTF	PL /PTP	X/DHĀX		<del></del>		
07	5,6063	1.6PA1	0.067712	0.15751	0.62400				
17	5.1915	1.5632	0.062702	7.145A6	0.83000				
77	4.7916	1.4428	0.057873	0.13462	0.96700				
י,	3.5719	1.0756	0.043142	0.10036	1.0900				
37	4.241P	1.2777	0.051232	0.11918	1.2200				
47	4.1314	1.2447	J. 149904	J. 11679	1.3500				
volt for	AL PAF ; TURE	PATION TOP	LAUDA IMIET						
MUBD	Ρ!	PL /PO	PI /PTF	PL /PTP	X/DMAX				
		1.6881	0.067712	0.15751	-1.0000		•		
	5.6063		0.062702	7.14586	1.0200 -				
	5.6063 5.1915	1 64 23							
12	5.1915	1.5632		0 12442 /	_ 1 0000				
!?	5.19[5 \ 4.7916	1.4420	0.057873	0.13462	-1.0000				
12	5.1915 4.7916 4.5719	1.442n 1.0754	0.057873 0.043142	0.10035	-1.0000		***************************************		
12 27 27	5.1915 4.7916 4.7916 4.2418	1.4428 1.0754 1.2773	0.057873 0.043142 0.051232	0.10036	-1.0000 -1.0000				
12 22 77 77 42	5.1915 4.7916 4.7916 4.8618 4.1314	1. 4429 1. 6754 1. 2773 1. 2442	0.057873 0.043142 0.051237 0.049904	0.10036	-1.0000 -1.0000 -1.0005				
12 27 77 42 67	5.1915 4.7916 5.5719 4.2618 4.1314 3.5319	1.4420 1.0754 1.2773 1.2442 1.0635	0.057873 0.043142 0.051232 0.051232 0.049904 0.042658	0.1003 0.14919 0.11609 0.099232	-1.0000 -1.0000 -1.0000 -1.0000				
12 22 27 27 27 42 62 67	5.1915 4.7916 4.8418 4.1314 3.5319	1.442n 1.07% 1.2773 1.2442 1.0635 1.0635	0.057873 0.043142 0.051232 7.049904 0.042658 0.042658	0.10036	-1.0000 -1.0000 -1.0005				
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12 27 37 42 62 62 63 63 64 63 64 64 64 64 64 64 64 64 64 64 64 64 64	5.1915 4.7916 4.7916 4.7619 4.7618 4.1314 3.5319 3.5319 3.5319 3.5319 3.5319	1.4428 1.0784 1.2773 1.2442 1.0635 1.0635 PAYING FAR 01/PN 1.0635 1.3635 1.0635 1.0635	0.057873 0.043142 0.051232 0.051232 0.049904 0.042658 0.042658 0.042658 0.042658 0.042658 0.042658 0.042658 0.042658	0.1003 0.1418 0.11609 0.099232 0.099232 0.099232 0.099232 0.099232 0.099232 0.099232 0.099232	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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12 27 77 47 47 47 47 47 47 47 47 47 47 47 47	5.1915 4.7916 4.7916 4.7619 4.7618 4.1314 3.5319 3.5319 3.5319 3.5319 3.5319	1.4428 1.0784 1.2773 1.2442 1.0635 1.0635 1.0635 1.0635 1.0635 1.0635 1.0635 1.0635 1.0635 1.0635	0.057873 0.043142 0.051232 0.051232 0.049904 0.042658 0.042658 0.042658 0.042658 0.042658 0.042658 0.042658 0.042658	0.1003 0.1418 0.11609 0.099232 0.099232 0.099232 0.099232 0.099232 0.099232 0.099232 0.099232	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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>40017.00	AL PRESSURE	PETIOS , PPI	MAPY PLUG			* · · · · · · · · · · · · · · · · · · ·	
A.42 (101.0		M 400	01 40 10	PI /PTP	¥/IIMAX		
32 ህብባት ርላል	P1	PI /PN 4.1499	PI /PTF 7. 18647	U.43128	J. 43200		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
	13.876		3.098754	0.73120			
? 7	7.3720	2.1978			0.53000		
4.7	9.3659	2.7717	0.17277	0.28280	0.62900		
52	0.1854	?.7572	9.12389	0.28654	3. 72700		
SAPOLT LON	AL PRESSIRF	PATIOS . FIG	W SPLITTER I	. n.			
AVD HOPD	PL	PL / PO	PI / PTF	PL/PTP	X/IMAX		
6.2	10.590	3.1515	0.14161	0.32753	0.42200		The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa
67	7,4070	2.7233	J. 099903	0.23105	3.67200		
>ADDITION	AL PRESSURE	PATIOS . FLO	W SPLITTER C	. 0.			
AV2 4080		m (80	m /atc	PL /PTP	V /DMA V		
AVD MORO	PL 705	PL/PN	PI /PTF		X/DMAX		and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t
77	30.709	7.2172	0.41417	0.95791	0.50800		
82	14.934	4.4026	0.20142	0.46586	J. 5 8 3 0 0		
9.7	3.5827	1.0754	0.048321	0.11176	0.67000		
>ADDIT FOR	AL PRESSURE	PATIÑS , FJE	CTOR SHROUN		embroside on a residence of the second		
AVD HOPD	PĹ	PL/PO	PL/PTF	PI /PTP	X/DMAX		
107	4.9978	1.5001	0.067406	0.15590	U. 62400		
				0.14452	0.63000		
112	4.6328	1.3976	0.062484				
177	4.287R	1.2970	0.05783)	0.13375	0.96000		
127	3.5627	1.0694	0.048051	0.11114	1.0900		
137	3.6228	1.1474	0.051558	0.11925	1.2200		
147	3.7027	1.1114	0. 649940	0.11550	1.3500		
CANDITION	M PRECIME		EADON - IN FT			**	
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AVINAD	PI	Pt /Pn · =	PI /PTF	PI /PTP	X/DMAX	•	
AVT UNER	Pl 4 0078	P[ /Pf)	PI /PTF	PL/PTP	X/DHAX	•	راه ۱۹۹۰ م سورسان باز انگلافان و پروی پار و بروی در در میشود در میشود به میشود و بروی به در در در در در در در در در در در در در
-107	4.9978	1.5001	0.067406	0.15590	000 کو 1-	•	
-107 -112	4.9978 4.6328	1.3906	0.067406 0.062484	0.15590	-1,0000 ,0000	•	
-107 -112 -122	4.9978 4.6328 4.2878	1.5001 1.3906 1.2870	0.067406 0.362484 0.057830	0.15590 0.14452 0.13375	-1.0000 -1.0000	• · · · · · · · · · · · · · · · · · · ·	
-197 -112 -122 -127	4.9978 4.6328 4.2878 3.5627	1.5001 1.3906 1.2870 1.0696	0.067406 0.062484 0.057830 0.048051	0.15590 0.14452 0.13375 0.11114	-1,0000 -1,0000 -1,0000 -1,0000	•	
-197 -112 -127 -127 -137	4.9978 4.6328 4.2878 5.627 3.8228	1.5001 1.3906 1.2870 1.0696 1.1474	0.067406 0.062484 0.057830 0.048051 0.051558	0.15590 0.14452 0.13375 0.11114 0.11425	-1,0000 1,0000 -1,0000 -1,0000 -1,0000	•	
-107 -112 -127 -127 -137 -147	4.9978 4.6328 4.2878 5627 3.728 3.732	1.5001 1.3906 1.2870 1.0696 1.1476 1.1116	0.067406 0.062484 0.057820 0.048051 0.051558 0.049940	0.15590 0.14452 0.13375 0.1111 0.11-25 0.1550	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -127 -127 -137 -142 -157	4.9978 4.6328 4.2878 5.5627 3.7228 3.7329 3.5327	1.5001 1.3906 1.2870 1.0694 1.1474 1.1114 1.0604	0.067406 0.062484 0.057830 0.048051 0.051558 0.04943 0.047646	0.15590 0.14452 0.13375 0.1111 0.11425 0.11550 0.11020	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -127 -127 -137 -147	4.9978 4.6328 4.2878 5627 3.728 3.732	1.5001 1.3906 1.2870 1.0696 1.1476 1.1116	0.067406 0.062484 0.057820 0.048051 0.051558 0.049940	0.15590 0.14452 0.13375 0.1111 0.11-25 0.1550	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -122 -127 -137 -142 -157	4.9978 4.6378 4.2878 5.627 3.7278 3.7328 3.5327 3.5327	1.5001 1.3906 1.2870 1.0694 1.1474 1.1114 1.0604 1.0694	0.067406 0.062484 0.057830 0.048051 0.051558 0.04943 0.047646	0.15590 0.14452 0.13375 0.11111 0.1125 0.1159 0.11020 0.11020	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000		
-107 -112 -122 -127 -137 -142 -157	4.9978 4.6378 4.2878 5.627 3.7278 3.7328 3.5327 3.5327	1.5001 1.3906 1.2879 1.0694 1.1474 1.1114 1.0604 1.0604	0.067406 0.262484 0.057830 0.048051 0.048051 0.04940 0.047646 0.047646	0.15590 0.14452 0.13375 0.1111 0.11425 0.1150 0.11020 0.11020	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -127 -137 -137 -157 -157 -157 -157 -157 -157	4.9978 4.6328 4.2878 5627 3.7328 3.7327 3.5327 3.5327 AL PRESSUPE	1.5001 1.3906 1.2877 1.0694 1.1474 1.1114 1.0604 1.0604	0.067406 0.262484 0.057890 0.048051 0.048051 0.04940 0.047646 0.047646	0.15590 0.14452 0.13375 0.11117 0.11725 0.11570 0.11020 0.11020	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
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77	R. 1 596	2.4506	0.097931	0.22835	0.53000	meno di
47	10.088	3, 3297	0.1210#	0.24231	0.67900	
_ 52	10.238	3.9747	7.12787	0.2 PE 50	9, 72799	
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62	11.721	3. 5202	0.1406R	0.32801	0.47200	Ca mondes Controlle on a service 1960 is no et interes appart to combine apparentage of a paging apparent a service in a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service apparent and a service app
67	P. 2545	2.4791	2.099071	0.23100	J. 67:300	
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77	34.128	19.250	0.40960	0.95506	).50A00	to a communication of the second communication and the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the second communication of the sec
R2	16.774	5.0778	0.20132	0.46942	0. 56300	
- 65	1.5961	1.3800	0.04161	0.10064	0.67000	
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107	5.6309	.6911	0. 67592	0.15758	0.62400	
117	5.2163	5665	C. 062603	0.14597	0.83000	
172	4.4361	1.4524	0.058043	0.13534	0.96000	
127	3.5411	1.0755	0. 042981	0.10022	1.3900	
177	4.2661	1.2813	0.051202	0.11939	1.2290	
142	4.1461	1. 2452	0.049762	0.11603	1.2500	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
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VAUNUEL	PÍ	<b>ቦ</b> ኒ / ቦስ	PL/PTF	PĹ/PTP	N/DHAY	•
-127	5.6139	1.6911	0.947582	0.15758	-1.0000	
-11,	F. 2160	1.5665	0. (624.03	0.14597	-1.0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
-127	4.9361	1.4574	0.058043	0.13534	-1.3000	
-127	A LUII.	1. 3755	0.747941	0.10022	-1.0000	
-137	4.7661	1.2013	0.051202	9.11939	-1.0000	
-142	4.14M	1.7452	0.049762	N. 11603	-1.0006	er or recognition of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the st
-152	3.5411	1.3635	0.042501	0.099098	-1.0090	
-157	2.5411	1.3435	0.042501	0.09909#	-1-0000	த் படுகளு , டி சம்பட <del>படித்தில் இடைய முறிய மடிக்கில் இடிப்படுக்கில் இடிப்படுக்கில் செய்யில் மடிப்படுக</del> ்கில் மடிப்படுக்கில் மடிப்படிப்படுக்கி
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-152	3.5411	1.2635	0.042501	0.09909#	-1.0000	
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	67	10.005	2. 98 RR	0.73113	0.2309A	0.67000			
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	77	39.831	11.830	1.3102	0.91954	0.59 <b>800</b>			The contract of the common terms of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contra
	82	20,209	6.0370	0.66882	0.46654	0.58300			
	0.7	3.6129	1.0793	0.11957	0.083407	0.67000			
	MODITION	AL PRESSIPE	PATIOS . EJ	FCTCR SHPOUR					· · · · · · · · · · · · · · · · · · ·
72	AVD WORD	et .	P( / P()	PÍ /PTF	PL/PTP	X/DMAY			The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
	107	6.7648	2.9298	0.22360	0.15617	0.62400			•
	117	6.7896	1.8789	0.70816	0.14520	0.83000			
	122	F. 8194	1.7384	0.19260	0.13435	0.96000			•
	127	3.6.79	1.0408	0.11974	0.0#3522	1.0900		-	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
	127	5.1691	1.5442	0.17107	0.11933	1.2200			
	142	5.619)	1-4993	0.16611	0.11587	1.3500			
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	-127	6.7649	2.0208	2.22289	0-15617	-1.0000			•
	-i12 \	6.2896	1.6789	J. 20816	0.14520	-1.0000			a en un la rema el mémo el majorio monojo de entre el monojo de la mentión de la majorio de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la mentión de la menti
	-127	5.8194	1.7384	9.19240	0.13435	1.0000			
	-157	A170	I.0404	0.11974	0.0435722	-I .0000			
	-137	5. M91	1.5442	0.17107	0.11923	-1.0000			•
	-147	5.01	1.4293	0.16611	0.11547	-1-2000			The second consists and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second se
	-1*2	9.5628	1.0643	0.11791	Ø6 082251	-1.0000			_
	-157	3.5428	1.0643	0.11791	0.042251	-1.0000			- THE - THE - AREA AND AND AND AND AND AND AND AND AND AN
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117	6.0942	1. 6740	0.062775	0.14567	0.93000				
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-137	5.3000	1.5047	0.051504	0.13/51	-1.0000				
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ላው ጠሩቅሀ	Pt	P  / PO	PI /PTF	PL /PTP	X/DMAX				
32	15.374	4.6295	0.18569	0.43195	0.43200				
77	A.1344	7.4494	0.098246	0.22854	0.53000				
47	19.362	3.0299	0.12153	0.29270	9.62903				
52	10.192	3.0690	0.12310	C.28635	0.72700				
· · · · · · · · · · · · · · · · · · ·	10.172	16 06 70	0.12310		0.72700		- <del></del>		<del></del>
NOT TIONS	INL PPESSURE	RATIOS . FEC	OW SPLITTER 1.	. D _•					
AUND	Pi	Pt / PO	PL /PTF	PI /PTP	X/DMAX				•
2	11.665	3.5126	0-14089	U. 32774	0.42200				
57	8.2793	2.4780	0.099393	0.23171	J.67000				
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in Authori	PI	PL/PO	Pt /PTF	PI /PTP	X/DMAX				
7	33.147	9.9911	0.40034	0.93128	0.50800				
?	16.682	5.0232	0.2014R	0.46869	0.58300				
2	3.5749	1.0771	0.043203	0.10050	0.67000				
400 F T 1004	AL PRESSIPE	RATIOS . FJF	FOTOR SHROUD						
D WORE	PL	Pt /PO	PL/PTF	PL /PTP	X/DHĀX		<del></del>		
07	5,6063	1.6PA1	0.067712	0.15751	0.62400				
17	5.1915	1.5632	0.062702	7.145A6	0.83000				
77	4.7916	1.4428	0.057873	0.13462	0.96700				
י,	3.5719	1.0756	0.043142	0.10036	1.0900				
37	4.241P	1.2777	0.051232	0.11918	1.2200				
47	4.1314	1.2447	J. 149904	J. 11679	1.3500				
volt for	AL PAF ; TURE	PATION TOP	LAUDA IMIET						
MUBD	Ρ!	PL /PO	PI /PTF	PL /PTP	X/DMAX				
		1.6881	0.067712	0.15751	-1.0000		•		
	5.6063		0.062702	7.14586	1.0200 -				
	5.6063 5.1915	1 64 23							
12	5.1915	1.5632		0 12442 /	_ 1 0000				
!?	5.19[5 \ 4.7916	1.4420	0.057873	0.13462	-1.0000				
12	5.1915 4.7916 4.5719	1.442n 1.0754	0.057873 0.043142	0.10035	-1.0000		***************************************		
12 27 27	5.1915 4.7916 4.7916 4.2418	1.4428 1.0754 1.2773	0.057873 0.043142 0.051232	0.10036	-1.0000 -1.0000				
12 22 77 77 42	5.1915 4.7916 4.7916 4.8618 4.1314	1. 4429 1. 6754 1. 2773 1. 2442	0.057873 0.043142 0.051237 0.049904	0.10036	-1.0000 -1.0000 -1.0005				
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12 22 27 27 27 42 63	5.1915 4.7916 4.8418 4.1314 3.5319	1.442n 1.07% 1.2773 1.2442 1.0635 1.0635	0.057873 0.043142 0.051232 0.051232 0.049904 0.042658	0.1003 0.14919 0.11609 0.099232	-1.0000 -1.0000 -1.0000 -1.0000				
12 27 77 42 42 67 67	5.1915 4.7916 4.7916 4.8418 4.1314 3.5319 3.5319	1.442n 1.0754 1.2773 1.2447 1.0635 1.0635	0.057873 0.043142 0.051237 0.04904 0.042659 0.042659	0.1003 0.14916 0.11609 0.099232 0.099232	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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			2.1941		0.22853					-
	47	9.0015	7. 7143	0.12741	0.28271	0.42500				
-	•?	. 3+1315 _	2.7534	0.12418	0.28675	3.72703			<del></del>	
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	AVE HEPE	PI	PL / PC	PL/PTF	PL /PTP	X/DMAX				
	67	10.441	3.1483	0.14199	0.37792	0.42200		-		er sakuli i saki i aka ja ji mi maake i ga ka ka ja sa saki
	47	7.3816	2.225	0.17038	0.23163	3.67000				
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	>tnot t tom	AL PRESSURE	PATIOS . FLO	W SPLITTER D	. n.				and solds the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the se	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
	AVE SUPE	PL	PL/PR	PL / PTF	PL/PTP	X/DWAX				
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	>/^^1	AL PRESSURE	PATINS . EJE	CTOP SHPPING						
	AVD WOPD	Pţ	<b>የ</b> ት / የብ	PI /PTF	PL/PTP	Y/DHAY				
	107	4.9559	1,4944	7.067396	0.15565	0.62400				
_	112	4.6107	1.3903	0.062702	0.14481	0.83000				
	122	4.2555	1.2932	0.057871	0.17365	n.96000				
	127	3.5550	1.0720	3.248345	C.11165	1.0930				
	127	3.7952	1.1444	0.051611	0.11919	1.2200				
	147	3.6851	1.1112	0.050114	0.11574	1.3500				
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•			<del></del>	<del>F-F-74-1++-F-</del>						
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	AVITANKO	PL	PL / PG	PL/PTF	PL /PTP	X/DHA:X		•		
	AVIT HORD	PL 4.9559	M / PO 1.4944	PL/PTF 0.067396	0.15565	-1,000		•		
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-	AVI MORO -107 -117 -127	Pt 4.9559 4.4177 4.2555	M / PG 1.4944 1.3903 1.2932	PL/PTF 0.067396 0.062702 0.057871	0.15565 0.14481 0.1336*	-1.0000 -1.0000		•		
-	AVD HORD -107 -117 -127	Pt 4.9559 4.4117 4.2555	M / PO 1.4944 1.3903 1.2932 1.7720	PL/PTF 0.067396 0.06270? 0.057871 0.048345	0.15565 0.14401 0.13365 0.1115	-1.0000 -1.0000 -1.0000 -1.0000		•		
-	AVT MORD -107 -117 -127 -177 -177	Pt 4.9559 4.4177 4.2555 3.5553	M / PO 1.4944 1.3903 1.2932 1.7720 1.1444	PL/PTF 0.06739F 0.06270? 0.057871 0.048345 0.051611	0.15565 0.14401 0.13365 0.11155 0.111719	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
-	AVD MORD -107 -117 -117 -127 -127 -137 -147	Pt 4.9559 4.4177 4.2555 3.4252 3.6351	M / PR 1.4944 1.3903 1.2932 1.7720 1.1444 1.1112	PL/PTF 0.067396 0.06270? 0.057871 0.049345 0.051611 0.050114	0.15565 0.14401 0.13365 0.11151 0.11719 0.11574	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000		•		
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_	AVD MORD -107 -117 -117 -127 -127 -137 -147	Pt 4.9559 4.4177 4.2555 3.4252 3.6351	M / PR 1.4944 1.3903 1.2932 1.7720 1.1444 1.1112	PL/PTF 0.067396 0.06270? 0.057871 0.049345 0.051611 0.050114	0.15565 0.14401 0.13365 0.11151 0.11719 0.11574	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000		•		
_	AVI MORD -107 -117 -127 -127 -177 -147 -167	Pt 4.9559 4.6117 4.2555 3.555 3.4952 3.5750 3.5750	M /PO 1.4944 1.3903 1.2932 1.7720 1.1444 1.1112 1.0629 1.0644	PL/PTF 0.067396 0.06270? 0.057871 0.048345 0.051611 0.050114 0.047937	0.15565 0.14661 0.13365 0.11165 0.11719 0.11574 0.11071 0.11087	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AVI MORD -107 -117 -127 -177 -147 -147 -157 -157 -157	Pt 4.9559 4.4177 4.2555 3.7565 3.4952 3.6654 3.5250 3.5300	M /PO 1.4944 1.3903 1.2932 1.7720 1.1444 1.1112 1.0629 1.0644	PL/PTF 0.067396 0.06270? 0.057871 0.048345 0.051611 0.050114 0.047937 0.048005	0.15565 0.14401 0.13365 0.11157 0.11719 0.11071 0.11087	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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_	AVID MORD -107 -117 -127 -127 -127 -147 -147 -147 -147 -157 -267 -267 -267 -267 -267 -27011104	PL 4.9559 4.4177 4.2555 3.5555 3.5250 3.5250 3.5250 3.5250 3.5250 3.5250 7.5250 7.5250 7.5250 7.5250 7.5250 7.5250 7.5250	M / PO 1.4944 1.3903 1.2932 1.7720 1.1444 1.1112 1.0629 1.0644 PATITI FAR PL/PO 1.0629 1.0644 PATITI - TAR	PL/PTF 0.067396 0.06270? 0.057871 0.047935 0.051611 0.050114 0.047537 0.048005 PL/PTF 0.047937 048005 PEC SHPPHO TI	0.15565 0.14481 0.13365 0.11151 0.11719 0.11071 0.11071 0.11071 0.11067	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
_	AVID MORD -107 -117 -127 -127 -127 -147 -147 -157 -157 -157 -267 -267 -267 -277 -277 -277 -277 -27	PL 4.9559 4.6117 4.2555 3.5255 3.5250 3.5300 AL PRESSUPE PL 3.5250 3.5370 AL PRESSUPE PL 3.5250 3.5370 AL PRESSUPE	PL/PN 1.4944 1.3903 1.2932 1.7720 1.1444 1.1112 1.0629 1.0644  PATITION FAR. PL/PN 1.0629 1.0644  PL/PN 1.0629 1.0649 1.0649	PL/PTF 0.067396 0.06270? 0.057871 0.047935 0.051611 0.050114 0.047937 0.048005 NOTIFICAD PL/PTF 0.047937 0.48005 NEC SHECKO TI PL/PTF 1.047937 1.047937	0.15565 0.14461 0.13365 0.11151 0.11719 0.11574 0.11071 0.11071 0.11071 0.11071 0.11067 PATION	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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_	AVID MORD -107 -117 -127 -127 -127 -147 -147 -157 -157 -157 -267 -267 -267 -277 -277 -277 -277 -27	PL 4.9559 4.6117 4.2555 3.5255 3.5250 3.5300 AL PRESSUPE PL 3.5250 3.5370 AL PRESSUPE PL 3.5250 3.5370 AL PRESSUPE	M / PO 1.4944 1.3903 1.2932 1.7720 1.1444 1.1112 1.0629 1.0644 PATION - FAR PL / PO 1.0629 1.0644 PL / PO PL / PO	PL/PTF 0.067396 0.06270? 0.057871 0.047935 0.051611 0.050114 0.047937 0.048005 NOTIFICAD PL/PTF 0.047937 0.48005 NEC SHECKO TI PL/PTF 1.047937 1.047937	0.15565 0.14461 0.13365 0.11151 0.11719 0.11574 0.11071 0.11071 0.11071 0.11071 0.11067 PATION	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

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STOUTATED	VE bbe22Nbe	BATERS . PP	IMBDA BFIIC		ns (Singletin - American				
tvo anen	PI	ጣ / ቀብ	of /bit	PI /PTP	FIDMAX				
33	12.212	3.6645	0.19739	0.43137	). 4°200				
3.7									
	4.4757	1.0437	O. CP9367	C.22874	1.53000				
4 I	8.01);	2.4936	0.12291	0.74795	0.65400				
52	A.1201	2.4366	0.12460	J. 28687	0.72700				
>ADDITION	AL PRESSURE	FATISS . FLE	W SPLITTER 1.	. 0.					
นจาน กระบ	PL	tal Nation	PL / PTF	ol /btb	X/DMAX				
4.2	0.2944	7. 7960	0.14747	0.32756	0.42200				
17	6.54 16	1.0677	0.10036	0.23124	0.67000				
>And 11 tools	AL PPESSIME	RATIOS . FLO	N SPEETTER O	. 0.					
AVP WERT	Pi	PI / PO	PL / PTF	PL /PTP	X/DMAX				
~~	26.254	7.8781	0.40286	0.92738	0.50900				
P7	13.141	3.9432	0.23164	0.46418	0.58390				
۲۶	3,5955	1.0759	0.055019	9.12665	0.67000				
SAPSIT TON	AL PRESSURE	RATENS . FJF	CYPR SHROUD						
พบ พบคม	PI	ቦL / Pቦ	PI /PTF	PL /PTP	X/DMAX				
107	4 3707								
	4.3707	1.3115	7.067067	0.15439	3.62403				
117	4.0757	1.2230	0.062540	0.14307	0.93000				
122	3.76·16	1.1244	0.057705	0.13294	0.96000				
1 27									
1 * /	3.07 / 32	1.0714	7.0~4744	0.17612	1.3990				
	3.5735 3.3754	1.0714	7.054799 0.051795	0.17612	1.3990 1.2200			`	
137	3.3754 3.2454	1.6129	0.051795	9.11923	1.2200			\	
137	3.3754 3.2454		0.051795 0.050107						
137 142 515577709	3.3754 3.2454 AT BREEZURE	1.6129 0.97985	0.051795 0.050107	0.11923 0.11535	1.2200			\	
137 142 58557777090	3.3754 3.2454 AT DRESSURE	1.6129 0.97985 BIYIOS , FOR PL/PD	0.051795 0.050107 PEACNY INLEY PL/PTF	0.11923 0.11535 PL/PTF	1.2200 1.2500 x/by/n			\	
137 142 5 <u>25577770</u> Vh. HORN	3.3754 3.2454 AT DEECCUBE P1 4.3737	1.6129 0.97585 BITTUE FOR PLYEOS FOR 1.3115	0.051795 0.050107 PERMY INLEY PI/PTF 0.067067	9.11923 0.11535 PL/PTP 0.15439	1.2200 1.2500 x/hy/ri -3/2000			\	
137 142 52557777090 Un unen 107	3.3754 3.2454 AT DEESCURE PI 4.3737 4.0757	1.6129 0.97585 BITTE FOR PLIPO 1.3115 1.2230	0.051795 0.050107 PERFOY TREET PL/PTF 0.067067 0.062540	9.11923 0.11535 PL/PTP 0.15439 0.14397	1.2200 1.2500 x/by/h -1.7000 -1.0000			\	
137 147 SESSYTTING Wh. MORN -107 -112	3.3754 3.2654 AT EXPERSISE PI 4.3737 4.0757 3.7636	1.6129 0.97584 FIVER FOR PLAN 1.3115 1.2230 1.1284	0.051795 0.050107 EARNY INLEY PI /PTF 0.067067 0.0625+0 0.057705	9.11923 0.11535 PL/PTF 0.15439 0.14397 0.13284	1.2200 1.2500 x/hy/ri -3/2000			\	
137 147 51557777090 Vh. uorn -107 -112	3.3754 3.2654 AT EXPERSISE PI 4.3737 4.0757 3.7636	1.6129 0.97584 FIVER FOR PLAN 1.3115 1.2230 1.1284	0.051795 0.050107 PERFOY TREET PL/PTF 0.067067 0.062540	9.11923 0.11535 PL/PTF 0.15439 0.14397 0.13284	1.2200 1.2500 x/bu/fi -1/2000 -1.0000			\	
137 147 525777709 0h unpn 107 112 122	3.3754 3.2656 AT BRESSIDE PI 4.3737 4.0757 3.7636 3.5755	1.6129 0.97585 PIVICE - FOR PL/PO 1.3115 1.2230 1.1244 1.3714	0.051795 0.050107 EACOV TELEY PI /PTF 0.067067 0.062540 0.057705 0.054780	9.11923 0.11535 PL/PTP 0.15439 0.14397 0.13284	1.2200 1.2500 x/ha/ri -1.2000 -1.0000 -1.0000			\	
137 147 5255777709 107 112 127 127	3.3754 3.2656 AT BREESURE PI 4.3737 4.0757 3.7636 5.7755 3.4756	1.6129 0.97584 PLYINE FOR PLYPO 1.3115 1.2230 1.1284 1.3714 1.0129	0.051795 0.050107 PERMY TREEY PI /PTF 0.067067 0.0625-0 0.057705 0.051795	9.11923 0.11535 PL/PTP 0.15439 0.14397 0.13284 0.17647 0.17647	1.2200 1.2500 x/ba/fi -1.7000 -1.0000 -1.0000 -1.0000			\	
137 147 5257777090 1107 1112 127 127 127 127	3.3754 3.2656 AT BRESSURE PI 4.3737 4.0757 3.7636 3.7755 3.156 3.2566	1.6129 0.97585 BIYER FOR PL/PO 1.3115 1.2230 1.1284 1.3714 1.0129 3.97985	0.051795 0.050107 ERECT TRUET PI / PTF 0.067067 0.0625+0 0.057705 0.051765 0.051765	9.11923 0.11535 PL/PTP 0.15439 0.14397 0.1294 0.1792 0.17923 0.17923	1.2200 1.2500 1.2500 x/hh/hi -1.7000 -1.0000 -1.0000 -1.0000 -1.0000			\	
137 147 5255777109 107 117 117 127 127 142 157	3.3754 3.2656 AT BREETURE PI 4.3737 4.0757 3.7636 3.5735 3.1754 3.2656 3.5355	1.6129 0.97585 BIYER FOR PL/PD 1.3115 1.2230 1.1284 1.3714 1.0129 3.97785 1.3609	0.051795 0.050107 PI / PTF 0.067067 0.057705 0.057705 0.051795 0.051795 0.054251	9.11923 0.11535 0.11535 0.15439 0.14397 0.12647 0.17647 0.17647 0.17647 0.11535 0.12480	1.2200 1.2500 1.2500 x/0946 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			\	
137 147 SESSYYTME 107 1117 127 127 127 142 157	3.3754 3.2656 AT BRESSURE PI 4.3737 4.0757 3.7636 3.7755 3.156 3.2566	1.6129 0.97585 BIYER FOR PL/PO 1.3115 1.2230 1.1284 1.3714 1.0129 3.97985	0.051795 0.050107 ERECT TRUET PI / PTF 0.067067 0.0625+0 0.057705 0.051765 0.051765	9.11923 0.11535 PL/PTP 0.15439 0.14397 0.1294 0.1792 0.17923 0.17923	1.2200 1.2500 1.2500 x/hh/hi -1.7000 -1.0000 -1.0000 -1.0000 -1.0000			\	
137 147 3257777799 -1107 -1112 -127 -127 -127 -142 157 -157	3.3754 3.2656 AT BRESSURE PI 4.3737 4.0757 3.7636 3.5735 3.2656 3.5355 3.5635	1.6129 0.97585 BIYINE FOR PL/PO 1.3115 1.2230 1.1284 1.0714 1.0129 1.97985 1.0400 1.0624	0.051795 0.050107 PI / PTF 0.067067 0.057705 0.057705 0.051795 0.051795 0.054251	9.11923 0.11535 0.11535 0.15439 0.14397 0.12647 0.17647 0.17647 0.17647 0.11535 0.12480	1.2200 1.2500 1.2500 x/0946 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			\	
137 147 200 MORN -107 -117 -127 -127 -127 -147 -147 -157 -157	3.3754 3.2656 AT BRESSURE PI 4.3737 4.0757 3.7636 3.5735 3.2656 3.5355 3.5635	1.6129 0.97585 BIYIOS FOR PL/PO 1.3115 1.2230 1.1284 1.0714 1.0129 1.97985 1.0400 1.0624	0.051795 0.050107 PERCOV IRLET 0.067067 0.0625+0 0.057705 0.051795 0.051795 0.054251 0.054333	9.11923 0.11535 0.11535 0.15439 0.14397 0.12647 0.17647 0.17647 0.17647 0.11535 0.12480	1.2200 1.2500 1.2500 x/0946 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			\	
137 147 SENTYTING AVI MORN -107 -112 -127 -127 -142 -157 -157 SADDITING	9.3754 3.2654  ST BRESSIRE  PI 4.3737 4.0757 3.7636 3.5735 3.5735 3.5735 3.5735 3.5735	1.6129 0.97584 BIYERE FOR PL/PR 1.3115 1.2230 1.1284 1.37[4 1.0129 3.97985 1.3600 1.0624 PAYERE FAI	0.051795 0.050107 PI /PTF 0.067067 0.057705 0.057705 0.051795 0.051795 0.054251 0.054251 0.054339	9.11923 0.11535 PL/PTP 0.15439 0.14397 0.13284 0.12647 0.17923 0.17923 0.12506	1.2200 1.2500 x/DMAX -2.7000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
137 147 3.2.3.7.7.7.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	3.3754 3.2656 AT DESCIPE PI 4.3737 4.0757 3.7636 3.2656 3.2656 3.5355 3.5435 AT DESCIPE	1.6129 0.97585 BIYINE FOR PL/PN 1.3115 1.2230 1.1246 1.9714 1.0129 3.97985 1.3609 1.0624 PAYINE FAS	0.051795 0.050107 PH / PTF 0.067067 0.0625-0 0.057705 0.051765 0.051765 0.054251 0.054330 FROM PHAP	9.11923 0.11534 PL/PTP 0.15439 0.14397 0.12647 0.14923 0.14923 0.14923 0.12506 PL/PTP 0.12499	1.2290 1.2590 1.2590 x/hh/h -1.7000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
137 147 2525777709 300 MORD -107 -112 -127 -127 -127 -142 -157 -157 -157 -157	9.3754 3.2654  IT BREESING  PI 4.3737 4.0757 3.7636 5.5736 3.2654 3.5355 3.5435  EI PRESSIME  PI 3.5355 3.5405	1.6129 0.97585 BIVIOE FOR PL/PO 1.3115 1.2230 1.1246 1.0714 1.0129 3.97985 1.3600 1.0624 PATION FAN	0.051795 0.050107 PERCOV TREET 0.067067 0.067067 0.051705 0.051765 0.051765 0.054329 FRETZE FLAP PL/PTF 0.054251 0.054328	9.11923 0.11534 PL/PTP 0.15439 0.14397 0.12647 0.14923 0.14923 0.11535 G.12480 0.12506 PL/PTP 0.12499 0.17506	1.2200 1.2500 x/DMAX -2.7000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			\	
137 147 200 MORD -107 -112 -127 -127 -127 -142 -157 -157 2477171040	3.3754 3.2654  I BRESSIRE  PI 4.3737 4.0757 3.7636 3.2654 3.2654 3.5355 3.5435  II PRESSIRE  PI 3.5355 3.5405  AL ONESSIRE	1.6129 0.97585 BIYINE FOR PL/PN 1.3115 1.2230 1.1284 1.3714 1.0129 1.97985 1.3600 1.0624 PAYINE FAN	0.051795 0.050107 PI /PTF 0.067067 0.0625-0 0.057705 0.051795 0.051107 0.054251 0.054329 FL/PTF 0.054328	9.11923 0.11534 PL/PTP 0.15439 0.14397 0.12507 0.14923 0.11535 0.12480 0.12506 PL/PTP 0.12499 0.12506	1.2290 1.2590 1.2590 x/hh/ki -1.7000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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67	7.3294	2.2940	0.11592	0.23142	0.67000		
	N PRESSIRE	RATINS , FLI	W SPLITTEP C	• n•			
ORTH OVA	PL	PL / PO	P[ /PTF	Pt /PTP	X /DMA X		
77	75.533	9.0056	0.40382	0.0620	Ú.5JA00	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
		4.005F	0.20212	0.40351	0.58300		
92 92	12.790 3.4114	1.0696	0.051952	0.19771	7.67000		
				•••••			
AMOLTIONAC	IL PRESSIPE	PATTOS . FJF	CTOP SHPOIM				
IAU RUBU	PI	PL/PN	PI / PTF	PI /PTP	X/DMAX	The transfer on the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of th	
107	4.2372	1.3285	0.047614	0.13379	0.62400		
112	3.9670	1.2430	3.062739	0.12524	0. f 3000	······································	
122	3.6416	1.1418	0.057594	0.11498	0.96000		
127	3.4063	1.0480	0.053873	0.10755	1.09 %	· · · · · · · · · · · · · · · · · · ·	
137	3.4967	1.1559	0.058306				
147	3. 5265		0.055773	0.11641	1.2200		
		1.1757		0.11175	1.2500		
ZWAT 1 TOW	H BUECCHEE	ALTINE . FOI	ERODY INLET				
DA HLDD	Pt	Pt / Pri	PI /PTF	PI /PTP	X / DM AX	•	
	Pt 4 - 2372	P[ /PO	PL /PTF	PI /PTP	X/DMAX	⊕ r inch i i man inchesiale inchesialis i i ⊕	ade announce agreement and still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the still the
107	4.2372	1.3285	3.067014	0.13379	-1,0000		
107	4.2372 3.9670	1.3285 1.2438	J.067014 0.067739	0.13379 0.12526	1.0000		
-107 -112 -122	4.2372 3.9670 3.4416	1.3295 1.2438 1.1418	J.067014 0.067739 0.057594	0.13379 0.12526 0.11498	-1 0000 1.0005 -1.0000		
107 112 122 127	4.2372 3.9670 3.4416 3.4763	1.3285 1.2438 1.1418 1.0690	J.067014 0.062739 0.057594 0.053873	0.13379 0.12526 0.11498 0.10759	-1 0000 1.0005 -1.0000 -1.0000		
107 112 122 127 137	4.2372 3.9670 3.416 3.4763 3.4967	1.3205 1.7438 1.1418 1.0690 1.1559	J.067014 0.062739 0.057594 0.053873 C.058306	0.13379 0.17526 0.11498 0.10759 0.11641	-1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 137 147	4.2372 3.9670 3.4416 3.4363 3.4367 3.5266	1.3295 1.2438 1.1418 1.0690 1.1559 1.1057	J. 067014 0. 067739 0. 057594 0. 053873 0. 058706 0. 055773	0.13379 0.12526 0.11498 0.10759 0.11641 9.1135	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 137 147 157	4.2372 3.9670 3.6416 3.4763 3.5266 3.3963	1.3285 1.2438 1.1418 1.0680 1.1559 1.1057 1.0649	J.067014 Q.067739 Q.057594 D.053873 C.058306 D.055773 Q.053715	0.13379 0.17526 0.11498 0.10759 0.11641 0.11135 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 122 127 137 142 157	4.2372 3.9670 3.4416 3.4363 3.4367 3.5266	1.3295 1.2438 1.1418 1.0690 1.1559 1.1057	J. 067014 0. 067739 0. 057594 0. 053873 0. 058706 0. 055773	0.13379 0.12526 0.11498 0.10759 0.11641 9.1135	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 122 127 137 142 157	4.2372 3.9670 3.4416 3.4767 3.5266 3.3963 3.3963	1.3285 1.7438 1.1418 1.3680 1.1559 1.1057 1.9649 1.0649	J.067014 Q.067739 Q.057594 D.053873 C.058306 D.055773 Q.053715	0.13379 0.17526 0.11498 0.10759 0.11641 0.11135 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 122 127 137 142 142 165 167 167	4.2372 3.9670 3.4416 3.4767 3.5266 3.3963 3.3963	1.3285 1.2438 1.1418 1.3690 1.1559 1.1057 1.9649 1.9649	J.067014 0.067739 0.057537 0.057537 0.057577 0.055773 0.053715 0.053715	0.13379 0.17576 0.11498 0.10758 0.10758 0.11641 9.11135 0.110724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 137 142 142 157 167	4.2372 3.9670 3.4616 3.4763 3.4767 3.5286 3.3963 3.3963	1.3285 1.2438 1.1418 1.1680 1.1559 1.1057 1.0649 PAYINS FAR	J. 067014 0. C027739 0. C57594 0. 0575973 C. CFR306 0.055773 0.055773 0.052715	0.13379 0.17576 0.11498 0.10777 0.10777 0.1135 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
-107 -112 -127 -137 -147 -157 -157 -157 -158 -158 -159 -159	4.2372 3.9670 3.4416 3.4767 3.4767 3.5206 3.3963 3.3963	1.3285 1.2438 1.1418 1.3690 1.1559 1.1057 1.9649 1.9649	J.067014 0.007739 0.057594 0.057873 C.058705 0.058773 0.058715	0.13379 0.17576 0.11498 0.10758 0.10758 0.11641 9.11135 0.110724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 137 142 157 167 167 167 177 VD WOPD 152 157	4.2372 3.0670 3.4163 3.4763 3.4763 3.3963 3.3963 3.3963 3.3963 3.3963	1.3285 1.2438 1.1418 1.1680 1.1559 1.1057 1.0649 PAYINS FAR	J. 067014 0. C027739 0. C57594 0. 0575973 C. CFR306 2. 055773 0. 053715 0. 053715 0. 053715	0.13379 0.17576 0.1149B 0.10777 0.11641 9.11135 0.10724 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 122 127 147 147 147 147 157 157 5500   T   1048	4.2372 3.9670 3.4763 3.4763 3.4763 3.3963 3.3963 41 PRESSURE	1.3285 1.2438 1.1418 1.1640 1.1559 1.1057 1.0649 1.0649 1.0649 1.0649	J.067014 0.027739 0.057594 0.057673 C.CFR306 7.055773 0.053715 0.053715 WMYJEFLAD	0.13379 0.17526 0.1149P 0.10757 0.1341 9.11135 0.10724 0.10724 PI /PTP 0.10724 C.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 */DMAX -1.0000 -1.0000		
-107 -112 -127 -137 -142 -157 -157 -157 -157 -157 -157 -157 -2601T1698	4.2372 3.9670 3.4416 3.4767 3.5206 3.3963 3.3963 3.3963 91 91 3.3963 3.3963	1.3285 1.2438 1.1418 1.3690 1.1559 1.1057 1.9649 1.3649 PAYINS FAR PLPN 1.3649 1.3649 1.3649	J.067014 0.02739 0.057594 0.057673 0.05773 0.053715 0.053715 0.053715 D.053715	0.13379 0.17526 0.11496 0.10759 0.10754 9.11135 0.10724 0.10724 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 127 137 142 147 147 147 157 167 167 167 167 167	4.2372 3.9670 3.4616 3.4967 3.5286 3.3967 3.3963 3.3963 3.3963 3.3963	1.3285 1.2438 1.1418 1.3690 1.1559 1.1057 1.9649 1.3649 PAYINS, FAR PL/PN 1.3649 PAYINS, 20	J.067014 0.027739 0.057594 D.057873 C. CFR306 D.055773 0.053715 0.053715 D.053715 DEC YHPMIN II	0.13379 0.17576 0.11498 0.10777 0.10777 0.10724 0.10724 PI /PTP 0.10724 PI /PTP 0.10724 PI /PTP 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000		
107 112 127 127 127 137 142 147 147 147 157 167 167 167 167 167	4.2372 3.9670 3.4416 3.4767 3.5206 3.3963 3.3963 3.3963 91 91 3.3963 3.3963	1.3285 1.2438 1.1418 1.3690 1.1559 1.1057 1.9649 1.3649 PAYINS FAR PLPN 1.3649 1.3649 1.3649	J.067014 0.02739 0.057594 0.057673 0.05773 0.053715 0.053715 0.053715 D.053715	0.13379 0.17526 0.11496 0.10759 0.10754 9.11135 0.10724 0.10724 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 122 127 147 147 147 147 157 157 260   T T 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4.2372 3.9670 3.4616 3.4763 3.3967 3.3963 3.3963 3.3963 3.3963 41 pressure	1.3285 1.2438 1.1418 1.3690 1.1559 1.1057 1.3649 1.3649 1.3649 1.3649 1.3649 1.3649 1.3649 1.3649	J.067014 0.027739 0.057594 D.057873 C. CFR306 D.055773 0.053715 0.053715 D.053715 DEC YHPMIN II	0.13379 0.1757 0.1149P 0.10757 0.1141 9.11135 0.10724 0.10724 0.10724 C.10724  PI /PTP 0.10724 C.10724  PI /PTP 0.10724 C.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000		
-107 -112 -127 -127 -137 -142 -142 -142 -142 -142 -142 -142 -142	4.2372 3.9670 3.4616 3.4967 3.5286 3.3967 3.3963 3.3963 3.3963 41 PRESSURE PL 3.3963 3.3963 41 PRESSURE	1.3285 1.2438 1.1418 1.3680 1.1559 1.1057 1.9649 1.3649 PAYINS, FAR PL/PN 1.0649 1.3458 PAYINS, FAR PL/PN 1.0649 1.3649 1.3649 1.3649	J.067014 0.027739 0.057594 0.057597 0.057673 0.057773 0.057715 0.057715 0.057715 DEG CHAPTIN TI 0.057715 0.057715	0.13379 0.17576 0.11498 0.10777 0.11441 9.11135 0.10724 0.10724  PI /PTP 0.10724 0.10724  PI /PTP 0.10724 0.10724  PI /PTP 0.10724 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 147 147 147 157 157 157 157 157 2401 T T 1088 157 2501 T T 1088 157 157 157 177	4.2372 3.9670 3.4163 3.4763 3.4763 3.3963 3.3963 3.3963 3.3963 11 PRECEIRE	1.3285 1.2438 1.1418 1.3680 1.1559 1.1057 1.3649 PAYINS FAF  PL/PN 1.3649 1.3649 1.3649 1.3649 1.3649 1.3649	J.067014 0.027739 0.057594 0.057597 0.055773 0.055773 0.055715 0.053715 DEC CHPCING PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT PLANT	0.13379 0.17576 0.1149P 0.10757 0.1141 9.11135 0.10724 0.10724 0.10724 PI /PTP 0.10724 PI /PTP 0.10724 PI /PTP 0.10724 PI /PTP 0.10724 PI /PTP 0.10724 PI /PTP	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 x/DMAX -1.0000 -1.0000		
ND WOPB 152 157	4.2372 3.9670 3.4616 3.4967 3.5286 3.3967 3.3963 3.3963 3.3963 41 PRESSURE PL 3.3963 3.3963 41 PRESSURE	1.3285 1.2438 1.1418 1.3680 1.1559 1.1057 1.9649 1.3649 PAYINS, FAR PL/PN 1.0649 1.3458 PAYINS, FAR PL/PN 1.0649 1.3649 1.3649 1.3649	J.067014 0.027739 0.057594 0.057597 0.057673 0.057773 0.057715 0.057715 0.057715 DEG CHAPTIN TI 0.057715 0.057715	0.13379 0.17576 0.11498 0.10777 0.11441 9.11135 0.10724 0.10724  PI /PTP 0.10724 0.10724  PI /PTP 0.10724 0.10724  PI /PTP 0.10724 0.10724	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		

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	127	3.4178	1.0555	0.053855	0.13971	1.0906	-		
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	-172 -127 -127 -127 -140 -150 -157	3.6581 3.4178 7.8972 7.9723 3.4178	1.0655 0.97373 0.91104 1.0640	0.152855 0.045652 2.046046 0.052776 0.052698	0.13971 0.1143 0.1145 0.13950	-1.0000 -1.0000 -1.0000 -1.0000			
	-172 -127 -127 -127 -140 -150 -157	3.6581 3.4178 7.8972 7.9723 3.4178	1.0655 9.99323 9.91104 1.0640 1.0624	0.152855 0.045652 2.046046 0.052776 0.052698	0.13971 0.1143 0.1145 0.13950	-1.0000 -1.0000 -1.0000 -1.0000	-		
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	-122 -127 -127 -142 -157 -157 -157 -157 -157 -157	3.65AL 3.617A 2.6972 2.0723 3.612A 3.637A BEFCCIPF PL 3.612B 3.617A	1.0655 9.97373 7.91104 1.0640 1.0624 PATING FAN	0.15=AFE 0.04-657 2.64-6046 0.05-776 0.05-776 0.05-776 0.05-776 0.05-2776 0.05-2776	0.13977 0.1143 0.1145 0.13950 0.13950 PL/PTP 0.13950 C.13930	-1.0000 -1.0000 -1.0000 -1.0000			
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	> 4001 £ [CN3	I PRESSIPE	RATIOS , PRI	MAPY PLUG				
^.	APO HORD	PI	PI /PO	PI / PTF	PL /PTP	x/DMAX		
	12	15.1)3	4.7769	0.21400	9.43147	9.43200	-	
_	37	A.1155	2.5333	7.11391	0.22892	0.5300J		
	47	10.734	3.13?7	7.14784	0.29304	0.62930		
	52	17.164	3.1727	0.14266	0.24671	0.72700	·····	
,	APPR TERPA	L PRESSURE	PATIOS . FLO	W SPLITTEP I	. n.			
	ልሃክ ሣበቶካ	PL	P1 / P13	PL / PT F	PI /PTP	X/DHAX		
	52	11.623	3.6280	0.16314	0.32785	0.42200	Committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the commit	Anni Maria anticidade e a cara de acuacido de fermido de fermido de acuacido d
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	> 40 31 1 1004	PRESSURE	RATIOS . FLO	W SPLITTER P	. D.			
	1VP WORD	PL	PI / PO	PL/PTF	Pi /PTP	X/DMAX		
	77	24.955	9.0344	0.40441	0.81676	0.50900		management and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the
	<b>#</b> 7	14.384	4.4901	C-20199	0.40576	0.58309		
	35	3.4313	1.0711	0.347101	0.096789	0.67000	······································	
	>4PPITIONA	PRESSURE	PATING . EJÉ	ČŤCR SHPANA		M .		
	AAL HUBD	PL	PL /PI	PL/PTF	PL/PTP	X\D4AX		
-	107	4.7965	1.4772	0.067323	0.13530	0.62400		
	117	4.4765	1.3973	0.062832	0.12627	J.#3000		
	177	4.1114	1.2834	0.05770R	0.11597	0.96000	*	to the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the
	127 137	3.4263	1.0695 1.2943	0.04#04! 0.05#149	0.09664A 0.11696	1.0900		
	142	4.1464 1.9614	1.2366	0.044109	0.11174	1.2200 1.3500	· - · · · · · · · · · · · · · · · · · ·	
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	AVITARRI		PL / PÚ	PLINTE	PL /PTP	X/DMAX		
	-10-	P1 4.7965	1.4972	0.067323	0.13530	-1.0000	•	
	-112	4.4745	1.3973	0.067523	0.17627	1.0000		
	-177	4.1114	1.2934	9.057798	0.11597	-1.0000		•
-		4263	1.0495	" ñ. ñ4 Año[ "	T. HOLLER	-1.0000		
	-177	4.1464	1.2747	0.058159	0.13696	-1.0000		3
	-149	3.96	1.2366	0.055602	0.1469A 0.11174	-1.0000		and an experimental and the second and the second and the second and the second and the second and the second
	-152	3.4113	1.0648	9. 64 7891	C.096225	-1.0000		
	-1 57	2.4113	1.0548	9.0478AL	0.096725	-1.0000		
	" SPATITIONAL	bb£22llat	PATITICE FAIL	THITTLE FLEW				
	ለህሙ ዘጣያው	PI	PLIPO	21 / 275	PI /PTP	X/SMAX		
	-152	3.4113	1.0648	0.047PP1	0.096225	-1.0000		
	-1 = 7	3.4113	1.0654	147885	0.094775	-1.0000		· · · · · · · · · · · · · · · · · · ·
	LASSIVIANI	**************************************		NEG SHAPE TH				
				_				
	AVD WCPD	PL	bf\u0	Pt /PTF	SI VOLD	X/DMAX		
	-167	3.4153	1.0664	0.047951	996900	-1.0000		
-	-177	2/111	1.0648	n, n4 7841	6.94552	-1.0000		<i>J</i>
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AND MOED	Pl	PI /PC	PLIPTE	PI /PTP	X/DMAT			
4.7	13.351	4.1020	1. 19/37	0.43309	0.43200			
17	7. )744	7.2212	0.35 6755	0.72790	0.53000			
4.7	4, 7 5 10	7.7502	C. 12227	0.28216	0.62900			+
. 62	# .H 770	2.7863	S. 12787	9.28587	0.72700			
NOTE TOWA	IAI PRESSIME	PATIOS . FL	OW SPEITTER I	. n.				
AVO MOPO					v 4500 6 10			
. •	PL	PI / PC	01/PTF	P1 / P1P	# / DMAX			
f 2	10.163	3.1011	0.14187	0.32740	0.42200			
' 7	7.1644	2.2495	0.10001	G. 230A0	0. 6 7000			
>40011104	IAL PRESSIME	RATIOS . FL	UN ZULLTER E	. 0.				
AVD WE'PD	PL	ጠ / ቀብ	PLIPTE	PL /PTP	K/DMAK			
77	. 3. 104	9.1384	0.40629	0.93757	0.50800	n e e e e e e e e e e e e e e e e e e e		
97	14.450	4.5370	0.70171	0.46549	9.58309			
45	3.4037	1.0697	0.047513	0.10965	3.67000			
>20011100	AL PRESSIBE	PATENS , EJ	ECTOP SHPOID					en designable engage un en en en en en en en en en en en en en
AVD WORD	PI	የር / የብ	Pt /PTF	PL /PTP	X/DMÁX			
107	4.8193	1.5132	0.067274	0.15525	0. 62400			
- 115	4.4372		0.062806	0.14494	0.63000		<del> </del>	<del></del>
127		1.4127	0.057709					
	4.1341	1.2980		0.13316	9.96000			
127	3.3947	1.0671	0.047444	C-10949	1.0900 1.2200			
127	3.6999 3.5888	1.1614	0.051634	0.11916				
147	3.5944	1.1268	0.050097	0.11561	1.3500			
147 	3.5944	1.126A	0.050097	0.11541	1.3500			
147	3.5944	1.1268	0.050097		1.3500 x/DMg/x			
147 <b>- 5450  \$164</b>	3.5988 41 88655486	1.126A	0.050097	0.11541	1.3500			
AND MUND	3,59AA Al BAESCHAE Pl	1.126A AATIOS , FO PL/PO	0. 050097 PF PTF 9. 267274	0.11541 PL /PTP	1.3500 x/DMg/x			
147 -107 -107 -117	3.59AA AL AAESSUAE Pl 4.8193 4.4902	1.1268 847105 , FO Pt/PO 1.5132 1.4127	0.050097 PFAFDY LMCET PI /PTF 9.067274 0.062806	Pt /PTP 0-15525 0-14444	1.3500 */DMA# -1.0100 1.0900			
147	3.5988 M. BRESCHRE Pt 4.8193 4.4902 4.1341	1.1268 #ATTOR FO Pt /PO 1.5132 1.4127 1.2980	0.050097 PERCON INCENT PLANTE 9.067274 0.067270 0.057709	0.11541 Pt /PTP 0.15525 0.14494 0.13310	1.3500 */DM4# -1.0100 -1.0100			
147	3.5988 AL BRESCHRE PL 4.8193 4.4902 4.1341 3.3747	1.1268 ************************************	0.050097 PERCENT INVEST PLANTE 9.567274 0.667274 0.057769 0.047444	PL /PTP 0.15525 0.1444 0.13318 0.1095	1.3500 */DMax -1.0100 -1.0300 -1.0350			
AND WIPP 1-10 -10 -17 -17 -17 -17 -17	3.5988 AI ARESSURE PL 4.8193 4.4902 4.1341 3.3997 734989	1.1268 #1/PO 1.5132 1.4127 1.2980 1.0671 1.1614	0.050097 PERFOY INLEY PLYPTF 0.067274 0.02806 0.051709 0.047444 0.051634	Pt /PTP 0.15525 0.14494 0.13318 0.10944	1.3500 */DMAX -1.0000 1.0000 -1.0000 -1.0000			
AND WORD -10° -117 -12° -12° -12° -12° -13° -14°	3.5988 AI ANESSUPE PL 4.8193 4.4902 4.1341 3.3997 7.5989 3.5988	1.1268 8.47105 FO Pt/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268	0.050097 PERCON INCEN PLANTE 0.067274 0.0677709 0.047444 0.051634 0.050097	Pt /PTP 0.15525 0.14494 0.13318 0.10994 0.11416 9.11561	1.3500 */DMA# -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
147 ANDITION AVQ WOPD -107 -117 -127 -127 -147 -142 -152	3,5988 A1 BRESCHRE PL 4,8193 4,6902 4,1341 3,3947 3,089 3,5848 3,3837	1.1268 PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624	0.050097 PLANTE 9.267274 0.662806 0.057709 0.047444 0.051634 0.050097 0.047234	Pt /PTP 0.15525 0.14494 0.13318 0.10994 0.11561 0.10900	1.3500 */DMA# -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
147 AND MOPD -10° -112 -12° -12° -13° -14° -15° -15° -15°	3,5988 AL BRESCHRE PL 4,8193 4,6902 4,1341 3,3997 1,5848 3,3837 3,3787	1.1268 PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609	0.050097 PLATE 9.767274 0.067776 0.057709 0.047446 0.051634 0.051634 0.05097 0.047234 0.047144	Pt /PTP 0.15525 0.14494 0.13318 0.10994 0.11416 9.11561	1.3500 */DMA# -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
AND WORD -10 -117 -117 -127 -127 -137 -142 -152 -157	3,5988 AL BRESCHRE PL 4,8193 4,6902 4,1341 3,3997 1,5848 3,3837 3,3787	1.1268 PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609	0.050097 PLANTE 9.267274 0.662806 0.057709 0.047444 0.051634 0.050097 0.047234	Pt /PTP 0.15525 0.14494 0.13318 0.10994 0.11561 0.10900	1.3500 */DMA# -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
147  AND MOPD  -10 -117 -117 -127 -127 -142 -152 -157	3,5988 AL BRESCHRE PL 4,8193 4,6902 4,1341 3,3997 1,5848 3,3837 3,3787	1.1268 PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609	0.050097 PLATE 9.767274 0.067776 0.057709 0.047446 0.051634 0.051634 0.05097 0.047234 0.047144	Pt /PTP 0.15525 0.14494 0.13318 0.10994 0.11561 0.10900	1.3500 */DMA# -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
147 ANDITION AND MORD -107 -117 -127 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157	3,5988  At massine  Pt 4,8193 4,4902 4,1341 3,3997 3,5948 3,3787  At parssine	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609	0.050097  PI /PTF	PL /PTP 0.15525 0.14546 0.13318 0.10997 0.11416 9.11561 0.10900 0.1084	1.3500 */DMA# -1.0100 1.0900 -1.0300 -1.0000 -1.0000 -1.0000			
147  AND WIPD  -107  -117  -127  -127  -127  -147  -152  -157  >ADDITION	3,5988  Pt 4,8193 4,4902 4,1341 3,3997 3,5989 3,5989 3,3837 3,3787	1.1268  PL/PG 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609	0.050097 PI /PTF	Pt /PTP 0.15525 0.14444 0.13318 0.10967 0.11414 0.10900 0.10900	1.3500 */DMA# -1.0100 -1.0100 -1.0100 -1.0100 -1.0000 -1.0000			
147  AND WORD -107 -117 -127 -127 -127 -142 -152 -157 -157 -157 -157 -157 -157 -157	3.5988  Pt 4.8193 4.4902 4.1341 3.3997 7.6989 3.3837 3.3787  Pt 3.3837 3.3787	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PATING FAI	0.050097  PI /PTF	Pt /PTP 0.15525 0.14464 0.13318 0.10967 0.11416 0.10900 0.1CRe4  Pt /PTP 0.10900 0.10884	1.3500  **/DMAX* -1.0100 1.0200 -1.0200 -1.0200 -1.0200 -1.0000 -1.0000 **/DMAX* -1.0000			
147  AND WORD  -102  -112  -122  -122  -123  -142  -142  -152  -157  >ADDITION	3.5988  PI 4.8193 4.6902 4.1341 3.3047 3.0089 3.5888 3.3787  AI PRESSIRE 3.3837 3.3787	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PAYING FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIANS FAMILIAN	0.050097 PL /PTF 0.067774 0.062806 0.057709 0.047446 0.051634 0.050997 0.047234 0.047164 PL /PTF 0.047234 0.047164 RFG CHBMIN TI	PL/PTP 0.15525 0.14494 0.13318 0.10956 0.11561 0.10900 0.1CR84	1.3500  */DMA# -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
147  ***********************************	3.5988  Pt 4.8193 4.4902 4.1341 3.3997 3.5988 3.3787  At DRESSIRE Pt 3.3837 3.3787  At DRESSIRE	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PAYING FAI	0.050097 PI /PTF 9.267274 0.062806 0.057709 0.047444 0.051634 9.050097 0.047234 0.047164 N HITTE TEAP PL /PTF 1.047234 DPT C CHRIMIN TEAP	PL/PTP 0.15525 0.14444 0.13318 0.10947 0.11561 0.10900 0.1CR64  PL/PTP 0.10900 0.10884	*/DMAX -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 */DMAX -1-0000 **/DMAX			
147  ***********************************	3.5988  Pt 4.8193 4.4902 4.1341 3.3997 7.4989 1.5988 3.3787  At parssimp	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PAYING FAI	0.050097 PI /PTF 9.967274 0.062806 0.057709 0.047444 0.051634 9.059097 0.047234 0.047164 N NFFFF T.047234 R C47164 PI /PTF 1.047234 PI /PTF 0.047234	Pt /PTP 0.15525 0.14444 0.13318 0.10967 0.11416 9.11561 0.10900 0.1CR64  Pt /PTP 0.10900 3.10884	*/DMAX -1-0100 1-0200 -1-0200 -1-0200 -1-0200 -1-0200 -1-0200 -1-0000 */DMAX -1-0000 */DMAX -1-0000			
147  ***********************************	3.5988  Pt 4.8193 4.4902 4.1341 3.3997 3.5988 3.3787  At DRESSIRE Pt 3.3837 3.3787  At DRESSIRE	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PAYING FAI	0.050097 PI /PTF 9.267274 0.062806 0.057709 0.047444 0.051634 9.050097 0.047234 0.047164 N HITTE TEAP PL /PTF 1.047234 DPT C CHRIMIN TEAP	PL/PTP 0.15525 0.14444 0.13318 0.10947 0.11561 0.10900 0.1CR64  PL/PTP 0.10900 0.10884	*/DMAX -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 -1-0000 */DMAX -1-0000 **/DMAX			
147  ***********************************	3.5988 PL 4.8193 4.6902 4.1341 3.3797 3.989 3.5888 3.3787 AL DRESSIRE PL 3.3837 3.3787 INL DRESSIRE PL 3.3927 3.797	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PAYING FAI	0.050097 PI /PTF 9.967274 0.062806 0.057709 0.047444 0.051634 9.059097 0.047234 0.047164 N NFFFF T.047234 R C47164 PI /PTF 1.047234 PI /PTF 0.047234	Pt /PTP 0.15525 0.14444 0.13318 0.10964 0.13716 0.10900 0.1084  Pt /PTP 0.10900 0.10884  PTAYTON Pt /PTP 0.10900 C.19004	*/DMAX -1-0100 1-0200 -1-0200 -1-0200 -1-0200 -1-0200 -1-0200 -1-0000 */DMAX -1-0000 */DMAX -1-0000			
147  ***********************************	3.5988  Pt 4.8193 4.4902 4.1341 3.3997 7.6989 3.3837 3.3787  At pressire  Pt 3.3837 3.3787  At pressire  Pt 3.3837 3.787	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PAYING FAYING FA	0.050097 PI /PTF 9.967274 0.062806 0.057709 0.047444 0.051634 9.059097 0.047234 0.047164 N NFFFF TLAP PL /PTF 1.047234 0.047164 NPT C CHPMIN 11	Pt /PTP 0.15525 0.14444 0.13318 0.10967 0.11416 0.10900 0.1CR64  Pt /PTP 0.10900 0.10884  PT /PTP 0.10900 C.19984	*/DMAX -1-0100 1-0200 -1-0200 -1-0200 -1-0200 -1-0200 -1-0200 -1-0200 */DMAX -1-0200 -1-0200 */DMAX -1-0200 -1-0200			
147  TATOLITION  AND WIPE  -112 -127 -127 -147 -147 -157 -157  SANOLITION  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  TYD WIPE  T	3.5988  AL BRESCHEE  PL 4.8193 4.4902 4.1341 3.3097 3.5888 3.3787  AL BRESSHEE  PL 3.3787  AL BRESSHEE  PL 3.3797   1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PAYING FAI	0.050097 PERCON INCEP PL /PTF 0.067274 0.062806 0.051709 0.047444 0.051634 0.05037 0.047234 0.047144 PL /PTF 0.047234 PL /PTF 0.047234 PL /PTF 0.047234 PL /PTF 0.047234 PL /PTF 0.047234 PL /PTF 0.047234 PL /PTF 0.047234 PL /PTF	PL /PTP 0.15525 0.14494 0.13318 0.10964 0.13716 0.10900 0.1084  PL /PTP 0.10900 0.10884  PL /PTP 0.10900 C.19884  PL /PTP	1.3500  */DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000  */DMAX -1.0000 -1.0000  */DMAX -1.0000  */DMAX -1.0000  */DMAX -1.0000				
147  ***********************************	3.5988  Pt 4.8193 4.4902 4.1341 3.3997 7.6989 3.3837 3.3787  At pressire  Pt 3.3837 3.3787  At pressire  Pt 3.3837 3.787	1.1268  PI/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609  PAYING FAYING FA	0.050097 PI /PTF 9.967274 0.062806 0.057709 0.047444 0.051634 9.059097 0.047234 0.047164 N NFFFF TLAP PL /PTF 1.047234 0.047164 NPT C CHPMIN 11	Pt /PTP 0.15525 0.14444 0.13318 0.10967 0.11416 0.10900 0.1CR64  Pt /PTP 0.10900 0.10884  PT /PTP 0.10900 C.19984	*/DMAX -1-0100 1-0200 -1-0200 -1-0200 -1-0200 -1-0200 -1-0200 -1-0200 */DMAX -1-0200 -1-0200 */DMAX -1-0200 -1-0200			

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44 C*-1 "H	ts - 1271-141	INTRY TATA	65/11/79	CARRELL	REC 10/13/79 07:31:19.193	FAC BYBYE	PG# F034	RDG 1119
SANOTETO	NAC PRESSURE	BATTOS . PP	INVEA OF FIG		e Mer and a second of			
AND MULE	Pl	Pt /PC	PE / PTF	PI /PIn	X/[IMAX			
4.7	13.351	4.1°20	1. 19/77	0.43109	9.43200			
2.7	7. 3744	2.2213	7.75 6744	0.32790	3.53300			
47	4,7530	7.7502	0.12227	0.28216	0.62900			*
fi ? .	##H 779	2.7863	0.12*R7	0.28587	0.72700			
OND TICONS	NAF PRESSIME	PATIOS . FLO	PW SPEETTER T	.n.				·
AVO HOPO	PL	P[ / P[	OLIPTE	PI /PIP	X/DMAX			
1.7	10.163	3.1011	7.14177	0.32740	0.42200			make the second second second second
7	7-1644	2.2495	0.10301	C+ 230A0	0. 6 7000			
>40011100	NAL PRESSIME	PATIOS . FLO	ON SPEETER C	. 0.			monas a respectivos — success	was a superior of the second decision of the second second decision of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco
AVD WEED	PL	ቢ /ቀበ	PL /PTF	PE /PTP	K/DMAK			
77	73.104	9.1384	0.40629	0.93757	0.50800			man de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de
9.7	14.450	4.5370	0. 79171	0.46549	O. 58300			
45	3.4037	1.0647	0.047513	0.10965	J.67000			
>2001110	ANT BBEZZIIBE	PATIOS , EJI	ECTOP SHPOUR				till restriction of the second section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section s	o sayay <del>san</del> orany so sanage ay of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of t
AVO HORD	PI	<b>թլ / թ</b> ո	Pt/PTF	PL /PTP	K/DMAX	processor for the last of congregation of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of	erigin yakılının üzünün ili yazı erine erini yakının erini yakının erini erini erini erini erini erini erini e	Marin, Japan mengapi sebananganah Menel sejayan bahai mengangga bebasa ya
107	4.8193	1.5132	0.067274	0.15525	0. 62400			
115	4,4392	1.4127	0.362896	0.14494	0.63000		······································	**************************************
122	4.1341	1.29#0	0.057709	0.13318	9,96000			
1						and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th		
127	3.3947	1.0471	0.047646	C.10949	1. 3900			
127	3.6949	1.1614	0.051634	C.10949 C.11916	1. 3900 1. 2200			
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117	3.6949 3.5444	1.1614	9.051634 9.050097	0.11916	1.2200			
117	3.6949 3.5444	1.1614	9.051634 9.050097	0.11916	1.2200			
147 147 AND WIED	3,6999 3,5989 Wai Abesinde	1.1614 1.1268	9.051634 9.050097	0.11916	1.2200 1.3500			
127 147	3.6999 3.5989 W. PARSSHEE Pl	1.1614 1.1268 AATTON FOR	9.051634 9.050097 GATHY INCEY PI /PTF	0.11516 0.11561 Pt /PTP	1.2200 1.3500 */DMA# -1.0000			
127 142 AND WIDED -102 -112 -122	1.6999 3.59## WAI ###55W## PL 4.#193	1.1614 1.1268 AATION FOR PL/PO 1.5132	0.051634 0.050097 IFACDY INCEY PH /PTF 0.067274	0.11516 0.11541 Pt /PTP 0.15525	1.2200 1.3500			
AND WIDER  -10  -112	1.6999 3.5988 WAL PRESCUEE PL 4.8193 4.4902	1.1614 1.1268 AATION FOR PL/PG 1.5132 1.4127	9.051634 9.050097 ICARDY INLEY PLATE 9.067274 0.062806	0.11516 C.11541 Pt /PTP 0.15525 0.14494 0.13318 0.10954	1.2200 1.3500 */DMAX -1.0000			
127 142 AND WIDED -102 -112 -122	3.6999 3.5988  M. PAESCHOE  PL 4.8193 4.6902 4.134	1.1614 1.1268 #ATTOS FOR PL/PG 1.5132 1.4127 1.2980	9.051634 9.050097 644CDV SALEX PLATE 9.067274 0.067709	0.11516 C.11541 Pt /PTP 0.15525 0.14444 0.13318	1.2200 1.3500 */DMAX -1.0000 -1.0000			
117 147 AVQ WIRD -117 -117 -127	7.6999 3.5988 WAL MAESCHAE PL 4.8193 4.6902 4.1341 3.3997 7.6989	1.1614 1.1268 #ATION FOR PL/PO 1.5132 1.4127 1.2980 1.0671	9.051634 9.050097 ICACDY SMLEY PI /PTF 9.967274 0.062806 0.057709 0.047444 0.051634 9.051634	0.11516 0.11541 P1 /PTP 0.15525 0.14444 0.13318 0.10546 0.11561	1.2200 1.3500 */DMA# -1.0000 -1.0300 -1.0300			
AVQ WIPD -107 -117 -127 -127 -127 -127 -142 -152	7.6999 3.5988  WAL PARTYCHOR  PL 4.8193 4.6902 4.1341 3.3967 3.5969 3.5868 3.383	1.1614 1.1268 AATION FOR PL/PD 1.5132 1.4127 1.2980 1.0671 1.1614	9.051634 9.050097 668CDV SMLEX PI /BTF 9.067274 0.062806 0.057709 0.047446 0.051634 9.050397 9.047234	0.11516 C.11541 P1 /PTP 0.15525 0.1444 0.13318 0.10964 0.11561 0.10900	1.2200 1.3500 1.3500 1.3500 -1.0000 -1.0000 -1.0000 -1.0000			
117 147 AVQ WOPD -107 -117 -127 -127 -127 -142	7.6999 3.5988 WAL MAESCHAE PL 4.8193 4.6902 4.1341 3.3997 7.6989	1.1614 1.1768 AATION FOR PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268	9.051634 9.050097 ICACDY SMLEY PI /PTF 9.967274 0.062806 0.057709 0.047444 0.051634 9.051634	0.11516 0.11541 P1 /PTP 0.15525 0.14444 0.13318 0.10546 0.11561	1.2200 1.3500 1.3500 1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
137 147 243011100 AVQ WOPD -107 -117 -127 -127 -142 -152 -157	3.6999 3.5988  WAL MARKSCHAR  PL 4.8193 4.4902 4.1341 2.3297 3.6989 3.5888 7.3831 3.3787	1.1614 1.1768 AATION FOR PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.06.09	9.051634 9.050097 668CDV SMLEX PI /BTF 9.067274 0.062806 0.057709 0.047446 0.051634 9.050397 9.047234	0.11516 0.11541 Pt /PTP 0.15525 0.14494 0.13318 0.10554 0.11561 0.10900 0.10900 0.10904	1.2200 1.3500 */DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
117 147 AND WIPD -107 -117 -127 -127 -137 -149 -159 -157 -157 -157 -157 -157	7.6999 3.5988  IAI PAESCHOE  PL 4.8193 4.6902 4.1341 3.3797 7.6989 7.5888 7.1831 3.3787	1.1614 1.1268 PL/PG 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609	9.051634 9.050097 168CDV IMEE P1.78TF 9.967774 0.662806 0.051709 0.067446 0.051634 9.059097 9.947234 0.047114 0.047114 0.047114	0.11516 C.11541 Pt /PTP 0.15525 0.14444 0.13318 0.10944 0.11561 0.10900 0.10900	1.2200 1.3500 */DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
137 147 247011100 2107 2117 2127 2127 2137 2142 2157 257711107 240 HOPO 2157	3.6999 3.5988  (A) AMESCUME  PL 4.8193 4.4902 4.1341 2.3297 7.6989 7.3831 3.3787  (A) PRESCUME	1.1614 1.1768 AATION FOR PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609 PAYING FAR	9.051634 9.050097 ICACDY INLEY PI /PTF 9.067274 0.062806 0.051709 0.047444 0.051634 9.059097 9.947234 0.047144 FL/PTF 7.047234	0.11516 0.11541 Pt /PTP 0.15525 0.14494 0.13318 0.10561 0.11561 0.10900 0.1084 Pt /PTP 0.10900	1.2200 1.3500 */DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 */DMAX -1.0000			
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177 147 AVQ WIPD -107 -117 -127 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157	7.6999 3.5988  MI PARSCHOR  PI 4.8193 4.6902 4.1341 3.3797 7.5988 7.3837 3.3787	1.1614 1.1268 PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609 PAYING . VAR	9.051634 9.050097 ICACDY INLEY PI /PTF 9.067274 0.062806 0.051709 0.047444 0.051634 9.059097 9.947234 0.047144 FL/PTF 7.047234	0.11516 C.11541 Pt /PTP 0.15525 0.14444 0.13318 0.10966 0.11561 0.10900 0.1CR84 Pt /PTP 0.10900 J.10884	1.2200 1.3500 */DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 */DMAX -1.0000			
177 147 AVQ WIPD -107 -117 -127 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157	7.6999 3.5988  WAL MARSCHAR  PL 4.8193 4.4902 4.1341 7.3997 7.5988 7.3837 3.3787  PL 3.3837 3.3787  VAL BERSSIER	1.1614 1.1268 PL/PO 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609 PAYING . VAR	9.051634 9.050097 168CDV INLEX PI / PTF 9.067774 0.062806 0.057709 0.047444 0.051634 9.059097 9.047234 0.047164	0.11516 C.11541 Pt /PTP 0.15525 0.14444 0.13318 0.10966 0.11561 0.10900 0.1CR84 Pt /PTP 0.10900 J.10884	1.2200 1.3500 */DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 */DMAX -1.0000			
117 147  AVQ WOPD -107 -117 -117 -127 -137 -142 -152 -157 -157 -157 -157 -157 -157 -157 -157	3.6999 3.5988  WAI PARTYCHAE  PL 4.8193 4.4902 4.1341 2.3797 3.3797 3.3797  WAI PARTYCHAE PL 3.3837 3.3797  WAI PARTYCHAE PL 3.3837 3.3797	1.1614 1.1768 #ATION FOR 1.5132 1.4127 1.2980 1.0671 1.1614 1.1268 1.0624 1.0609 #ATTON FAR PL/PD	9.051634 9.050097 ICARDY INLEY PI / PTF 9.267274 0.062806 0.057709 0.047446 9.051634 0.051634 0.050997 9.947234 0.041144 VAPPE THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER APPENDENT TO THE PER	0.11516 0.11541 P1/PTP 0.15525 0.14446 0.13318 0.10960 0.10960 0.10900 0.10864 P1/PTP 0.10900 0.10884	1.2200 1.3500 */DMAX -10000 -1.0300 -1.0300 -1.0000 -1.0000 -1.0000 -1.0000			
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#7 2	14.311	4.4984	0.20167	0.52490	0.58300	
	3.3752	1.0640	0.047977	0.12440	0.67800	
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io	4.7758	1.5022	0.367415	0.17439	0.62400	
112	4.4507	1.4000	0.067976	0.16306	0.83000	
177	4.0856	1.7951	9.057672	2.14970	) <b>.</b> 96000	
127	3.3952	1.06.80	0.047977	0.12440	1.0990	கை அடுகள் உடிகள் இடையுள்ளத் அவறிகள் பாண்டிய இருக்கள் பிடம் படிய வடிய வறிகள் குடிய இருக்கு வறிகள் மறிகள் மறிகள் இருக்கு
137	3.2301	1.0160	0.045597	0.11835	1.2200	
147	3.75 )2	1.0255	9.946929	7.11945	1.3590	en en en en en en en en en en en en en e
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-123	4. 1156	1.2851	0.057672	0.14970	-1.0000	
-127	3952	1. 1440	0. 147527	0.12450	-1.0000	
-127	1. 121	1.0160	0.045557	0.11435	-1.0000	
-147	3.20	1.0255	0.746923	2/1945	-1.0000	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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·?	11.315	3.5292	0.14714	0.28530	0.72700	
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•	16.344	5.0715	0.20150	0.40529	0.56300	
A2		1.0686	0.043051	0.046592	2.67900	
• .	3.4278	1.00.00	0.041011	049-107-12	7.0 . 300	
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	5. 3537	1 5598	0.062842	0.17640	5.63000	
117			0.057817	0.11629	0.96000	
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AVR UPRP -107 -112 -127	Pt. 5.3738 5.0037 4.6335 3.4428	M /PA 1.6752 1.5598 1.4351 1.3735	PI /PTF 0.067491 0.067867 0.057817 0.043240	0.13575 0.17740 0.11629 0.076521	-1,7530 -1,0003 -1,0000 -1,3000	•
AVR UPRP -107 -112 -127 -127 -127	Pt. 5-3739 5-0037 4-6-335 3-4429	P) /PO 1.6752 1.559P 1.4351 1.3735 1.4429	PI /PTF 0.057491 0.057847 9.057817 0.0543247 0.058131	0.13575 0.12740 0.11629 0.046521 0.11492	-1,7530 1,0003 -1,0000 -1,5300 -1,0000	
AVR UNRO -107 -112 -122 -127 -127 -127	Pt. 5.3739 5.0037 4.6335 3.4429 4.6285 4.6285	Pt / Pf 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905	PI /PTF 0.067491 0.062847 0.067817 0.043247 0.068131 0.055618	0.13575 0.12740 0.11629 0.046571 0.11492 0.11497	-1,7330 -1,0003 -1,0000 -1,0000 -1,0000	
AVR UNRE -107 -112 -127 -127 -147 -142 -162	Pt. 5.3739 5.0037 4.6.35 3.4429 4.6.285 4.6.285 4.6.428	Pt/PO 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639	PI / PTF 0. 057491 0. 052847 9. 057817 0. 043247 0. 058131 0. 055618 0. 042867	0.13575 0.12740 0.11629 0.076521 0.1192 0.11197 0.086213	-1,7330 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000	
AVR UNRO -107 -112 -122 -127 -127 -127	Pt. 5.3739 5.0037 4.6335 3.4429 4.6285 4.6285	Pt / Pf 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905	PI /PTF 0.067491 0.062847 0.067817 0.043247 0.068131 0.055618	0.13575 0.12740 0.11629 0.046571 0.11492 0.11497	-1,7330 -1,0003 -1,0000 -1,0000 -1,0000	•
AVR UNRY -107 -112 -127 -127 -127 -147 -167 -167	Pt. 5.3739 5.0037 4.6335 3.4429 4.4295 4.4296 3.4129	Pt/PO 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639	PI /PTF 0.067491 0.067849 0.067817 0.043249 0.068131 0.055618 0.042869 0.042869	0.13575 0.17740 0.11629 0.076571 0.11692 0.11167 0.086213 0.086213	-1,7330 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000	
AVR UNRY -107 -112 -127 -127 -127 -147 -167 -167	Pt. 5.3739 5.0037 4.6335 3.4429 4.4295 4.4296 3.4129	M/PO 1.6752 1.559R 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639	PI / PTF 0.067491 0.062842 9.657817 0.043240 0.058131 0.055618 0.042862 0.042862	0.13575 0.17740 0.11629 0.046521 0.11629 0.1167 0.086213 0.086213	-1,7330 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000	
AVR WARD -107 -117 -127 -127 -149 -149 -167 SADOTT INSI	Pt. 5.3739 5.0037 4.6.335 3.4429 4.429 4.429 3.4129 3.4129	M/Pf 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639 PAYIFF FAR	PI /PTF 0.067491 0.067849 0.067817 0.043249 0.068131 0.055618 0.042869 0.042869	0.13575 0.17740 0.11629 0.076527 0.1197 0.11197 0.086213 0.096213	-1,7330 1.0003 -1.0000 -1.0000 -1.0000 -1.0300 -1.3900	
AVR WORD -107 -117 -127 -127 -127 -147 -167 -167 -167 -167 -167	Pt. 5.3739 5.0037 4.6.335 3.4429 4.4295 4.4295 3.4129 3.4129	M/PO 1.6752 1.559R 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639	PI /PTF 0.067491 0.067849 0.067817 0.043249 0.055618 0.055618 0.042869 0.042869	0.13575 0.17740 0.11629 0.046521 0.11629 0.1167 0.086213 0.086213	-1,7330 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000	
AVR WIRR -107 -117 -127 -127 -127 -147 -149 -169 -169 AVR JORE -169 -169	Pt. 5.3739 5.0037 4.6335 3.4429 4.4295 4.4296 3.4129 Pt. 3.4129	M/Pf 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639 PAYIFF FAR	PI / PTF 0.067491 0.067867 0.057817 0.0543740 0.055618 0.05618 0.042867 0.042867 0.042867 0.042867	0.13575 0.17/40 0.11629 0.046521 0.11/92 0.11/97 0.086213 0.086213	-1,7330 1.0003 -1.0000 -1.0000 -1.0000 -1.0300 -1.3900	
AVR WINRY -107 -117 -127 -127 -127 -147 -147 -167 -167 -167 -167 -167 -167 -167 -16	Pt. 5-3739 5-0037 4-6-335 3-4629 4-6-295 4-6-296 3-4129 3-4129 Pt. 3-4129 2-4129 41 onessible	M/PN 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639 PAYING FAR	PI / PTF 0.067491 0.072847 0.072847 0.073817 0.055618 0.057618 0.042862 0.042862 0.042862 0.042862	0.13575 0.17740 0.11629 0.076527 0.13-92 0.11197 0.086213 0.086213 0.086213	-1,7330 1.0003 -1.0000 -1.0000 -1.0000 -1.03000 -1.03000 -1.0300	
AVR WARN -107 -117 -127 -127 -127 -147 -147 -167 -167 -167 -167 -167 -167 -167 -16	Pt. 5.3739 5.0037 4.6.335 3.4429 4.429 3.4129 3.4129 Pt. 3.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2.4129 2	P/PN 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639 PAYING FAR P/PN 1.7639 1.0639	PI / PTF 0. 067491 0. 072847 9. 057817 0. 054247 0. 055618 0. 055618 0. 042847 0. 042847 0. 042847 0. 042847	0.13575 0.17740 0.11629 0.076521 0.11692 0.11167 0.086213 0.086213 0.086213	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
AVR WINRY -107 -117 -127 -127 -127 -127 -149 -169 -169 -169 -169 -169 -169 -169 -16	Pt 5.3739 5.0037 4.6335 3.4429 4.429 3.4129 3.4129 Pt 3.4129 4129 4129 4129 4129 4129 4129 4129	P/PN 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639 PAYING, FAR PI/PN 1.0634 PAYING, 70 PI/PN 1.0635	PI / PTF 0. 067491 0. 067847 9. 057817 0. 05818 0. 055618 0. 055618 0. 042862 0. 042862 0. 042862 0. 042862 0. 042862 0. 042862	0.13575 0.17/40 0.11629 0.046521 0.11/92 0.11/92 0.11/92 0.086213 0.086213 0.086213	-1,7330 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000	
AVR WINRY -107 -117 -127 -127 -127 -147 -147 -167 -167 -167 -167 -167 -167 -167 -16	Pt. 5.3739 5.0037 4.6.335 3.4429 4.6.245 4.6.246 3.4129 AL PRESSIDE: Pt. 3.4129 AL ORESSIDE: Pt. 3.4129 AL ORESSIDE: Pt. 3.4129 AL ORESSIDE: Pt. 3.4129 AL ORESSIDE: Pt. 3.4129	M/PN 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639 PAYING , FAR M/PN 1.0639 1.0639 1.0639 1.0639	PI / PTF 0.067491 0.072842 9.057817 0.043240 9.055618 9.055618 9.042862 PPOYTE FLAD 0.142862 0.142862 0.142862 0.142862 0.142862 0.142862 0.142862 0.142862	0.13575 0.17440 0.11629 0.076527 0.1197 0.086213 0.086213 0.086213 0.086213 0.086213	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
AVR WINRY -107 -117 -127 -127 -127 -127 -149 -169 -169 -169 -169 -169 -169 -169 -16	Pt. 5.3739 5.0037 4.6.335 3.4429 4.6.245 4.6.246 3.4129 AL PRESSIDE: Pt. 3.4129 AL ORESSIDE: Pt. 3.4129 AL ORESSIDE: Pt. 3.4129 AL ORESSIDE: Pt. 3.4129 AL ORESSIDE: Pt. 3.4129	P/PN 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639 PAYING, FAR PI/PN 1.0634 PAYING, 70 PI/PN 1.0635	PI / PTF 0.067491 0.072842 9.057817 0.043240 9.055618 9.055618 9.042862 PPOYTE FLAD 0.142862 0.142862 0.142862 0.142862 0.142862 0.142862 0.142862 0.142862	0.13575 0.17440 0.11629 0.076527 0.1197 0.086213 0.086213 0.086213 0.086213 0.086213	-1,7330 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000	
AVR WITER -107 -117 -117 -127 -127 -127 -147 -147 -147 -147 -147 -147 -147 -14	Pt. 5.3739 5.0037 4.6335 3.4429 3.4129 3.4129 21 000000000000000000000000000000000000	#/Pf 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 PAYING FAR M/Ph 1.2639 PAYING . 70 PAYING . 70 PAYING . 70 PAYING . 70	PI / PTF 0.067491 0.067491 0.067817 0.054131 0.055618 0.042862 0.042862 0.042862 0.042862 DEC SHECKLO	0.13575 0.17/40 0.11629 0.046571 0.1169 0.1169 0.086213 0.086213 0.086213 0.086213 0.086213	-1,7330 1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000	
AVR WINRY -107 -117 -127 -127 -127 -147 -147 -167 -167 -167 -167 -167 -167 -167 -16	Pt. 5.3739 5.0037 4.6.335 3.4628 4.428 3.4128 3.4128 Pt. 3.4128 2.4128 41 onessibe	P/PN 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 1.3639 1.3639 1.0639 1.0636 PAYING . FAR PI/PN 1.0636 PAYING . FAR PI/PN 1.0655 PAYING . RD	PI / PTF 0.067491 0.067491 0.067491 0.0543240 0.055618 0.055618 0.042862 0.042862 0.042862 DEC SHETTIN T	0.13575 0.17440 0.11629 0.076527 0.1167 0.076213 0.076213 0.076213 0.076213 0.076213 0.076213 0.076213	-1.7330 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	
AVR WITER -107 -117 -117 -127 -127 -127 -147 -147 -147 -147 -147 -147 -147 -14	Pt. 5.3739 5.0037 4.6335 3.4429 3.4129 3.4129 21 000000000000000000000000000000000000	#/Pf 1.6752 1.559P 1.4351 1.3733 1.4429 1.3905 1.0639 PAYING FAR M/Ph 1.2639 PAYING . 70 PAYING . 70 PAYING . 70 PAYING . 70	PI / PTF 0.067491 0.067491 0.067817 0.054131 0.055618 0.042862 0.042862 0.042862 0.042862 DEC SHECKLO	0.13575 0.17/40 0.11629 0.046571 0.1169 0.1169 0.086213 0.086213 0.086213 0.086213 0.086213	-1,7330 1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000	

SS HULD	PL 14.747	M /PO 4.6120	M /PTF 0.18554	Pt /PTP 0.43094	X/MAN 0.43200
37	7. 91 35	2.4476	0. 000270	0.22-24	3.53000
47	4.4405	3.0211	0.12154	0.54558	0.62900
52	9.7951	3.0633	0.12324	0.28623	J. 72 700
					V. 12 100
>ADDIT ION	AL PRESSURE	RATIOS . FLE	W SPLITTER I	. n.	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
AVD WORD	PL	PL /PD	PL/PTF	PI /PTP	X/MAX
67	11.205	3.5041	0.14097	0.32742	0. 42203
67	7.9355	7.4723	0.099465	0.23101	0.47000
>ADDIT ION	AL PRESSURE	PATIOS , FLO	M ZW İTTER C	, n	
AVD WORD	PL.	PL/PO	PL/PTF	PL /PTP	X/OMAX
77	32.254	10.087	0.40587	0.94253	0,50800
82	16. )26	5.0119	0.20164	0.46831	0.58300
97	1.4290	1.0724	0.043143	0.10070	Je67000
>400111004	AL PRESSUPE	PATINS . FJE	CTTR SHAPIN		
AVD HUED	PL	PL/PO	PL /PTF	PL/PTP	X/MAX
197	5.3701	1.6794	0.967565	0.15693	0.62400
115	4.9950	1.5621	0. C62 946	0.14596	0.83000
122	4.5938	1.4354	0.057748	0.13412	9-96900
127	3.4290	1.0724	0.043143	0.10020	1.0900
137	4. 7795	1.2758	0.051327	0.11921	1.2200
	3.9694	1.2414	0.745942	- 1 i # 6 6 **	
14?	-			0. 11599	1,3503
24201110H	AL PRESSIBLE	AA1106 , 600	CAON INCE		
AVE VERD	AL_MESSURE	AATINE . EM	PL /PTF	PI /PTP	×/DNGA
AVI VOPD	PL 5.3701	#41505 - EM #(790 " 1.6794	# /PTF 0.067556	PL /PTP 0-15693	×/0ms/4 -j_x000c
AV UCED -107 -117	PL 5.3701	PL/Ph 1.6794 1.5421	PL/PTF 0.067556 0.062846	Pt /PTP 0.15693 0.14596	×/5mg/ -j. 000c 1. 00ce
AVI UNPD -107 -112 -132	PL 5.3701 4.9950 4.5998	#ATENS ENG #[/Ph 1.6794 1.5421 1.4354	PL/PTF 0.067556 0.062846 0.057748	Pt /PTP 0.15693 0.14596 0.13412	X/DMAX -1.0000 1.0000 -1.0000
AVA UNED -107 -112 -122 -127	PL 5.3701 4.9950 4.5998 3.4270	#43105 500 #1,790 1.6794 1.5421 1.4354 1.0724	MI / PTF 0.067556 0.067546 0.057748 0.043143	Pt /PTP 0.15693 0.14596 0.13412 0.10020	X/DMGA -1.0000 -1.0000 -1.0000
AV WORD -107 -117 -122 -127 -137	PL 5. 3701 4. 9950 4. 5998 3. 4770 4. 795	9(/Ph 1.6794 1.5421 1.4354 1.9724 1.2759	PL/PTF 0.067556 0.067556 0.062846 0.057748 0.043143 0.051327	P1 /PTP 0.15693 0.14596 0.13412 0.10020 0.17521	x/094x -j-000c 1.00c0 -1.0000 -1.0000
AVD 40PD -107 -117 -122 -127 -137 -142	PL 5.3701 4.9950 4.5998 3.42700 4.795 3.9044	#43105 500 #1,790 1.6794 1.5421 1.4354 1.0724	PL/PTF 0.067556 0.062866 0.057748 0.043143 0.051327 0.04942	PI /PTP 0.15693 0.14596 0.13412 0.10030 0.14521 0.11599	x/0max -1.000c -1.000c -1.0000 -1.0000 -1.0000
AV WORD -107 -117 -122 -127 -137	PL 5. 3701 4. 9950 4. 5998 3. 4770 4. 795	PL/Ph 1.6794 1.5621 1.4354 1.7724 1.2759 1.2414	PL/PTF 0.067556 0.067556 0.062846 0.057748 0.043143 0.051327	P1 /PTP 0.15693 0.14596 0.13412 0.10020 0.17521	x/094x -j-000c 1.00c0 -1.0000 -1.0000
AVN 140PD -107 -117 -12 -127 -127 -137 -142 -157	PL 5.3701 4.9950 4.5998 3.4270 4.0795 3.9046 3.4340 3.439	#1705 COM #1700 1.6794 1.5621 1.4354 1.7724 1.2759 1.2414 1.0446 1.01661	MI / PTF 0.067556 0.062866 0.057748 0.057748 0.051327 0.04349492 0.042829	Pt /PTP 0.15493 0.14596 0.13412 0.10036 0.1421 0.11599 0.059472	x/000c -i_000c -i_0000 -i_0000 -i_0000 -i_0000 -i_0000
AVN 140PD -107 -117 -12 -127 -127 -137 -142 -157	PL 5. 3701 4. 9950 4. 9950 4. 5998 3. 4270 4. 7795 3. 4040 3. 4040 3. 4040	#4105 EM #1990 1.6794 1.5521 1.4354 1.0724 1.2759 1.2414 1.0446 1.0661	MI / PTF 0.067556 0.067556 0.067646 0.057748 0.051327 0.042829 0.042829 0.042829 0.042829	Pt /PTP 0.15693 0.14596 0.13412 0.10006 0.14521 0.11599 0.059472 0.099618	X/DMAX -i 0000 -i.0000 -i.0000 -i.0000 -1.0000 -1.0000 -1.0000 -i.0000
AVA UNED  -107 -117 -112 -127 -137 -142 -157 -157 -157 -157 -157 -157 -157	Pt 5.3701 4.9950 4.5998 3.4270 4.7795 3.9044 3.4340 3.4340 3.4340 3.4340 Pt Pt	#1105 E08 #1290 1.6794 1.5421 1.6354 1.0724 1.2759 1.2414 1.0646 1.0661 #ATTIME FAR	MI / PTF 0.067556 0.067556 0.067556 0.077746 0.077747 0.043143 0.051327 0.042929 0.042929 0.042929	Pt /PTP 0.15693 0.14569 0.14512 0.10020 0.14521 0.11559 0.059472 0.099618	X/DMAX -1.000c -1.000c -1.000d -1.000d -1.000d -1.000d -1.000d -1.000d
AND UCPD -107 -117 -127 -137 -142 -167 -167	PL 5. 3701 4. 9950 4. 9950 4. 5998 3. 4270 4. 7795 3. 4040 3. 4040 3. 4040	#4105 EM #1990 1.6794 1.5521 1.4354 1.0724 1.2759 1.2414 1.0446 1.0661	MI / PTF 0.067556 0.067556 0.067646 0.057748 0.051327 0.042829 0.042829 0.042829 0.042829	Pt /PTP 0.15693 0.14596 0.13412 0.10006 0.14521 0.11599 0.059472 0.099618	X/DMAX -i 0000 -i.0000 -i.0000 -i.0000 -1.0000 -1.0000 -1.0000 -i.0000
AVI UNED -107 -117 -122 -177 -142 -157 -157 -157 -157 -157 -157 -157 -157	Pt 5.3701 4.9950 4.9950 4.2700 3.4270 3.4270 3.4270 3.4270 3.4270 4.7705 3.4270 At ORESSIDE	#1105 EM #1290 1.6794 1.5724 1.6356 1.0724 1.2759 1.2414 1.0661 #ATITE FAR #1290 1.0646 1.0661	PL/PTF 0.067556 0.067556 0.067556 0.057748 0.043143 0.051327 0.043143 0.042829 0.042829	Pt /PTP 0.15693 0.14569 0.13412 0.10020 0.14521 0.11529 0.059472 0.099618 Pt /PTF 0.099472 0.069618	X/094X -j.000c 1.000c -1.0200 -1.0000 -1.0000 -1.0000 -1.0000
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<u> 63</u>	15.956 3.4192	4.9860	0.20166	0.52372	0.58300				
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115	4.9741	1.5546	0.062878	0.16330	0.83000				
122	4.5699	1.4280	0.057757	0.15000	0.96000				
127	3.4242	1.0700	0.043277	0.11230	1.0900	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa			
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-122	4.5600	1.4280	0.057757	0.15000	-1.0000				
-127	\$4242	1.0700	0.043277	0.11234	-1.0000				
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-157	3.4042	1.0637	0.043024	0.11173	-1.0000				
-1 57	3.4042	1.0624	0-043074	0.11173	-1.0000		and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t		
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-167	3.3342	1.0622	0.042950	0021157	-1.0000				
-172	3/6347	1.0637	0.047024	0.17473	-1.0000	e nation des	an demo-servaring motive compression breakings	- Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andrews - Andr	
"SANDITIONAC"	- set-24flet	PATTOS . BO	DEC SIMPLE	UCAY SUM					
AVD WED	PL	PL / PO	M/bat	PE /PTP	TOUAX				
-196	2.91 88	0.91296	0.036889	0.095802	-1.0000				

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MASA -I EWI	S PRFL 141	IMARY DATA	06/11/79	CADDE [1	REC 10/13/79 02:08:24,739 FAC 98681 PGM C034 PRIC 1125
>ADDIT 109	AL PPESSUPE	PATIOS PRI	MAPY PLUG		
AVD HOPD	PĮ	PI /PI	PL /PTF	PL/PTP	X/DMAX
2,7	10.747	5. A977	9. 21562	0.43157	2. 43200
37	9.8890	3.1109	9.11374	0.22765	0.53000
47	12.243	7. 9514	0.14081	0.27183	G.62 900
52	12.413	3,0749	0.14276	0.28574	-3.72700
>APP IT INN	AL PRESSURF	PATINS . FLO	W SPLITTER I	. n.	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
AVR MEPR	PL	PL/P7	PL/PTF	PL /PTP	x/DMAX
62	14.262	4.4865	0.16493	0.32830	0.42290
67	10.029	3,1550	0.11535	0.23087	J. 6 7000
>4001110N	AL PRESSIME		W SPLITTER O	.n.	
AVD WOPD	PI	P( /P0	PL/PTF	_ Pt /PTP	X/DRAX
77	35.014	11.015	0.40271	0.AC-03	J-50000
F2	17.534 3.4078	4,515R	0.20164	0.40362	6,58300 3,47000
77.	7.49 [7	1.0721	0.034143	0.078448	0.67000
>ADDITIONA	AT PRESSURE	RATIOS . EJE	CAUS CHEUID		
AVD HOPD	PL	PL/PT	PL/PTF	PL/PTP	X/MAX
107	5.4892	1.8526	0,067733	0.13557	0.62400
112	5.4740	1.7271	9.067958	9.12601	9, 83009
122	5.033R	1.5836	0.057896	0.11588	0.96990
127	3.4229	1.0769	0.639367	0. 078794	1.0900
127	5.0789	1.5977	0.058414		
			ひゅりつれずまや	0.11697	1.4240
147	4.9693	1.5316	0.055997	0.11692 0.11206	1.2200 1.3500
147	4. 7693		0.055997		
147	4.9699 AL DAESSURE	1.5116	0.055997	0.11206	1.3500
147 SCROLLION AND HUBB	4.9693 AL MESSURE PI	1.5316 ************************************	0.055997 F00W-14LFT PL/PTF	0.11206 PL/PTP	1.3500
147 SARRITION AVE HER D -10	4.9693 AL MESSURE PI F.9892	1.5116 ***********************************	2.055997 FACTO LALET  PL/PTF  9.067733	0.11206 PL/PTP 0.13557	1.3500 X/DMAX -1.600
147 	4. 9693 AL PRESSURE PI 5. 9992 5.4749	1.5116 ***********************************	91.055997 PL/PTF 91.067733 01.062958	0.11206 PL/PTP 0.13557 0.12601	1.3500 X/DMAX -1.600 1.0030
147 SZDOLTION AVD MCP D -107 -112 -122	4. 9693 AL MESSURE PI 6. 9892 5.4749 5.0339	1.5116 64140c , con PL/PG 1.8526 1.7221 1.5836	2.055997 PL/PTF 9.067733 0.062958 0.057895	0.11206 P[/PTP 0.13557 0.12601 0.11588	1.3500 X/DMSX -1.4600 -1.0030 -1.0000
147 AVR MCP D -107 -112 -122 -127	4. 9693 AL PRESURE PI 6. 9992 5.4749 5.0339 1.4279	1.5116 ***********************************	0.055997 PL/PTF 9.067733 0.062958 0.057895 0.039367	0.1120f P(/PTP 0.13557 0.12601 0.11566 0.0787/M	1.3500 X/DM3X -1.6000 1.0000 -1.0000
147 AVR MCP D -107 -117 -127 -127 -137	4. 9693 AL AMESSUME PI 6. 9892 5.4740 5.0339 3.4279 5.4789	1.5116 ***********************************	2.055997 PL/PTF 9.067733 0.062958 0.057896 0.039367 0.058414	0.1120f 0.13557 0.13557 0.12601 0.11566 0.11692	1.3500  x/DMLX -1.6000 1.0030 -1.0000 -1.0000 -1.0000
147 320017104 AVR MCP 0 -107 -112 -127 -127 -137 -147	4. 9691 AL ANECCURE PI 6. 9892 5.4740 5.0339 3.4270 5.4779 4.8648	1.5116 PL/PG 1.8526 1.7221 1.5836 1.0768 1.5777 1.5116	2.055997 2.067733 3.062958 0.057895 0.039367 0.058414 0.055997	0.11206 PL/PTP 0.13557 0.12601 0.11588 0.07874 0.11692	1.3500  X/004X -1.6000 -1.0000 -1.0000 -1.0000 -1.0000
147 NAME AND APP 0 -107 -127 -127 -137 -147 -150	4. 9691 AL MESSUME PI 6. 9892 5.4749 5.0339 3.4279 5.0789 4.8688 3.3478	1.5116 A41404 - 600 PL/PG 1.8526 1.7221 1.5836 1.0768 1.5977 1.5116 1.0558	0.055997 PL/PTF 0.067733 0.062958 0.057895 0.057895 0.058414 0.055997 0.039964	0.11206 PL/PTP 0.13557 0.12661 0.11588 0.07674 0.11697 0.11697 0.11208 0.077988	1.3500  X/DMAX -1.600 -1.0030 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
147 SADDITION AVR. MCP.D -107 -117 -127 -127	4. 9691 AL ANECCURE PI 6. 9892 5.4740 5.0339 3.4270 5.4779 4.8648	1.5116 PL/PG 1.8526 1.7221 1.5836 1.0768 1.5777 1.5116	2.055997 2.067733 3.062958 0.057895 0.039367 0.058414 0.055997	0.11206 PL/PTP 0.13557 0.12601 0.11588 0.07874 0.11692	1.3500  X/DMAX -1.6000 -1.0000 -1.0000 -1.0000 -1.0000
147 NAME HOP D -107 -112 -122 -127 -137 -147 -157 -157	4. 9691 AL ANGESUME PI 6. 9892 5.4745 5.0339 3.4270 5.4789 4.8648 3.3978	1.5116 PL/PG 1.8526 1.7221 1.5836 1.0768 1.5777 1.5116 1.0658 1.0658	0.055997 PL/PTF 0.067733 0.062958 0.057895 0.057895 0.058414 0.055997 0.039964 0.038964	0.11206 PL/PTP 0.13557 0.12661 0.11588 0.07674 0.11697 0.11697 0.11208 0.077988	1.3500  X/OMAX -1.600 -1.0030 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
147 NAME OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF T	4. 9691 AL MESSUME PI 6. 9892 5.4749 5.0339 3.4279 5.0789 4.8686 3.3978 3.3978	1.5116 AAIIOR COM PL/PO 1.8526 1.7221 1.5836 1.0768 1.5777 1.5116 1.0558 1.0658 RATIOS FAM	0.055997 PL/PTF 0.067733 0.062958 0.057894 0.057894 0.058414 0.055567 0.038964 0.038964	0.11206 PL/PTP 0.13557 0.12601 0.11588 0.07678 0.11697 0.11697 0.077988 0.077988	1.3500  X/DMAX -1.6000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
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142 SADDITION AVR MORE -107 -122 -127 -137 -142 -152 -157 SADDITION AVD MORE -152	4. 9691 AL MESSUME PI 6. 9892 5.4749 5.0339 3.4279 5.0789 4.8686 3.3978 3.3978	1.5116  PL/PG 1.8526 1.7221 1.5836 1.0768 1.5777 1.5116 1.0658 PAYTON , FAR	0.055997 PL/PTF 0.067733 0.062958 0.057894 0.057894 0.058414 0.055567 0.038964 0.038964	0.11206 PL/PTP 0.13557 0.12601 0.11588 0.07878 0.11692 0.11692 0.11208 0.077988 0.077988	1.3500  X/000  -1.6600  -1.0600  -1.0600  -1.0000  -1.0000  -1.0000  -1.0000
147 NAME TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET TO SET	4. 9690 PI S. 9740 S. 9740 S. 9339 3. 4279 S. 9789 4. 9850 3. 3978 3. 3978	1.5116  A4140x 688  PL/PG 1.8526 1.7221 1.5936 1.0768 1.5777 1.5116 1.0658 1.0658	0.055997  PL/PTF  9.067733  0.062958  0.057896  0.039367  0.056414  0.056414  0.056414  0.058414	0.1120f PL/PTP 0.13557 0.12601 0.11588 0.07878 0.11692 0.11692 0.1208 0.077988	1.3500  X/003X -1.600 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
147  AVR MORD -107 -112 -127 -137 -147 -152 -157  AVD MORD -152 -157	4. 9691 AL MESSURE FI 9892 5.4749 5.0339 3.4279 5.4789 4.8689 3.3978 3.3978 4.2996 4.3978 3.3978 3.3978	1.5116  A4140x	0.055997  PL/PTF 0.067733 0.062958 0.057894 0.058414 0.058964 0.038964 0.038964 0.038964	0.11206 Pt/PTP 0.13557 0.12601 0.11590 0.07790 0.1200 0.077908 0.077908	1.3500  X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
147  AVR MORD -107 -112 -127 -137 -142 -152 -157  AVD MORD -152 -157	4. 9691 AL MESSURE FI 9892 5.4749 5.0339 3.4279 5.4789 4.8689 3.3978 3.3978 4.2996 4.3978 3.3978 3.3978	1.5116  P(/P) 1.8526 1.7221 1.5836 1.0768 1.5777 1.5116 1.0658 1.0658 PAYING FAR	2.055997  PL/PTF 2.067733 3.062958 0.057895 0.057895 0.058414 0.055997 0.059464 0.038964 0.038964	0.11206 Pt/PTP 0.13557 0.12601 0.11590 0.07790 0.1200 0.077908 0.077908	1.3500  X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
147  NOTITION  AVE WERE -107 -112 -127 -137 -147 -157 -157 -157 -157 -157 -157 -157 -15	4.9691 AL MESSUME PI	1.5116  A4140x	0.055997  PL/PTF 0.067733 0.06295P 0.057895 0.057895 0.057896 0.058616 0.055967 0.038966 0.038966 0.038966	0.11206  PL/PTP 0.13557 0.12601 0.11588 0.07818 0.11692 0.11692 0.077988 0.077988 0.077988 PL/PTP 0.077988	1.3500  X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
142  NAME OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF T	4.9691 AL MESSURE PI	1.5116  P(/P) 1.8526 1.7221 1.5836 1.0768 1.5777 1.5116 1.0658 1.0658 PAYING FAR	0.055997  PL/PTF 0.067733 0.062958 0.057894 0.057894 0.058414 0.0555907 0.038964 0.038964 0.038964 0.038966 0.038966	0.11206  PL/PTP 0.13557 0.13567 0.11560 0.07674 0.11697 0.11697 0.077988  PL/PTP 0.077988  PL/PTP 0.077988  PL/PTP 0.077872	1.3500  X/0MAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
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147  AVR MORE -107 -117 -127 -127 -137 -147 -157 -157  AVR MORE -157  AVR MORE AVR MORE -167	4.9691 AL MESSUME PI	1.5116  MI/PG 1.8526 1.7221 1.5836 1.0768 1.5116 1.0558 1.0658 PATINE FAM P/PG 1.0658 RATINE , FAM P/PG 1.0658 RATINE , 20	0.055997  PL/PTF 0.067733 0.062958 0.057894 0.057894 0.058414 0.0555907 0.038964 0.038964 0.038964 0.038966 0.038966	PL/PTP 0.13557 0.12601 0.11588 0.07878 0.13692 0.11208 0.077988 0.077988 0.077988 PL/PTP 0.077988 PL/PTP 0.077988	1.3500  X/0MAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
142  SADDITION  AVE MORE -10 -112 -127 -127 -127 -147 -152 -157  SADDITION  AVE MORE -152 -157  SADDITION  AVE MORE -172 -172 -172	4.9691 AL MESSURE PI	1.5116  A4108 - 600  P(/P) 1.8526 1.7221 1.5836 1.0768 1.5777 1.5716 1.0558 1.0658  RATIOS - FAM  M /PO 1.0658  RATIOS - 20  M /PO 1.0642 1.0642	0.055997  PL/PTF 0.067733 0.062958 0.057895 0.057895 0.058614 0.0355907 0.038964 0.038964 0.038964 0.038964 0.038964 0.038966 0.038966 0.038966 0.038966	0.11206  P[/PTP 0.13557 0.13567 0.11560 0.07674 0.11697 0.11697 0.077988  P[/PTP 0.077988  P[/PTP 0.077988  P[/PTP 0.077988  P[/PTP 0.077978  P[/PTP 0.077978  P[/PTP 0.077972 0.077872	1.3500
147  SECOLITION  AVR MORE -107 -112 -127 -137 -147 -157 -157 -157 -157 -157 -157 -157 -15	4.9691  AL AMESSURE PI 6.9892 5.4745 5.0339 3.4279 5.4779 4.8648 3.3978 AL PRESSURE PL 3.3978 3.3978 AL PRESSURE PL 3.2928 1.24728 PL 3.24728 PL 3.24728	1.5116  PI /PO 1.8526 1.7221 1.5836 1.0768 1.5777 1.5116 1.0658 PATION , FAM PI /PO 1.0658  RATION , ZO PI /PO 1.0642 1.3642 PATION , RO PI /PO	0.055997  PL/PTF 0.067733 0.062958 0.057895 0.057895 0.058414 0.055997 0.058964 0.038964 0.038964 0.038964 0.038964 0.038964 0.038964 0.038964 0.038964 0.038964	0.11206  PL/PTP 0.13557 0.12601 0.11588 0.07878 0.11692 0.11208 0.077988 0.077988  PL/PTP 0.077988  PL/PTP 0.077988  PL/PTP 0.077987  PL/PTP 0.077972 0.077972 0.077972	1.3500
142  AVR MOPD -107 -117 -127 -127 -127 -147 -147 -157 -157  AVD MOPD -152 -157  AVD WOPD -172 -172 -172	4.9691 AL MESSURE PI	1.5116  A4108 - 600  P(/P) 1.8526 1.7221 1.5836 1.0768 1.5777 1.5716 1.0558 1.0658  RATIOS - FAM  M /PO 1.0658  RATIOS - 20  M /PO 1.0642 1.0642	0.055997  PL/PTF 0.067733 0.062958 0.057895 0.057895 0.058614 0.0355907 0.038964 0.038964 0.038964 0.038964 0.038964 0.038966 0.038966 0.038966 0.038966	0.11206  P[/PTP 0.13557 0.13567 0.11560 0.07674 0.11697 0.11697 0.077988  P[/PTP 0.077988  P[/PTP 0.077988  P[/PTP 0.077988  P[/PTP 0.077978  P[/PTP 0.077978  P[/PTP 0.077972 0.077872	1.3500

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>Annitina<	AL PRESSURE	BATTOS . PPI	MAPY PIUG		
Ab hbbu	PL	P1 /P7	PL/PTF	PI /PTP	K/DMAX
32	16.079	5.05%	2,18477	0.43026	7.43200
	M.4654	2.6721	0. 277584	C.22723	2. 53020
47	1-3-479	3.7978	7.12080	0.28129	7.62500
£2	10.639	3.359?	0.127(4	0.28559	0.72760
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40 ALBU	Pİ	PL / PT	PI /PTF	PL /PTP	x/DMAx
12	12.173	3.8424	0.14932	0.32676	0.42200
67	A.5754	7. 79ER	0.094852	0.23019	0.67000
>AND FITTON	AL PPFSSIRF	PATINS . FLO	W SPLITTED O	.n.	Company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the compan
VD WOPE	Pt.	PL/PH	M /PTF	PI /PTP	x/DMAx
77	34.934	11.027	0.40269	0.93771	0.50400
F2	17.497	5.5215	0.20164	0.46954	0.58390
£3	3.1902	1.7701	0.0390#9	0.001002	3.67000
>ennff fnra	al pressupf	RATEOS . FJE	מטאופ שונ	*****	
AD NOW U	PI	PL/PO	PI /PTF	PL /PTP	X/DMAX
107	5.8559	1.8484	0.067593	0.15710	0.62400
117	5,4409	1.7737	D. CA2955	0.14458	0.63000
127	5.0159	1.583?	0.057919	0.13444	0.96900
127	7.3952	1.0717	0. C3 4134	0.091137	1.0990
1 > 7	4.4357	1.4731	0.051132	0.11006	1.2290
14?	4.3156	1.3622	7.044748	6.11584	1.4500
ZIDDIT ION	AL PRECIDE	BATION , FOR	PECENTAL PROPERTY		
חשושייוי	Pl ·	m /en	PL /PTF	Pt 7510	1/000 -1/000 1.6800
102	5.8559	1.8494	0. 667503	0.15719	-1.7000
112	5.4405	1.7237	6.042550	3.1465#	1.0500
127	5.0150	1. 5932	0.657419	G.13464	-1.0000
127	1957	1. 1717	7. 314138	0.091347	-1.9306
137	4. 1357	1.4901	0.051132	0.12604	-1.5000
147	4.31	1.3622	0. 544744	0.14906 0.11584	-1.000
152	3.3652	1.0422	0.934792	0.090331	-1.0998
57	3.3652	1.0522	2. (39792	0.090331	-1.0060
) 176] T [6 <u>9</u>	IL PRESSIDE	RATION, FAR	HETTLE FLAR		
ነው ነጥተው	21	R/M	21 /275	PI /PTP	2/DMAX
167	3.3652	1.96.22	0.734777	0.090331	-1.0000
157	3.3652	1.3322	928797	0.09331	-1.0000
	AL PRESSURF		HEL ZHOUNG ET		
AU MUNU	Pi /	Pt /PD	PJ /PTF	EL 1919	K/OMAY
1/7	3.36.52	1. 1522	7.032797	30063331	-1.0000
172	363452	1.3527	0.039792	0.030331	-1.0000
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VO AFFORD	P1 2.8939	0.91221	7, 933313	0.077573	-1-700

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26301710	IAL PPESSURE	PATINS . PPI	MARY PING							
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:2	14.525	4.5258	0-16575	0.43204	2.43200			*		- Maria
÷ 7	7.6381	3.3964	0.027763	0.22876	0.53000					
4.7	9,4429	2.06 26	9.13850	0.20781	3.62900		* * * *	·	97 - 9 - 47 - 17	
52	9,5778	3.0950	0.1100	0.28686	0.72700					
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f 2	10.967	3.4344	0.12479	0.32787	0.42200					
	7,7331	2.4262	0.098854	0.23160	0.67030					
ant therac	AL PPESSURE	RATIOS , FLO	M SPLITTER O	. D.				· · · · · · · · · · · · · · · · · · ·		e
ልላኮ ብቦጽበ	<b>?</b> 1	Pt /PO	PI /PTF	Pt /PTP	x/DMax					
77	34.989	13.977	0.49203	1.0479	9.50800					-
A2	17.543	5.5038	9.23157	0.52540	0.58300					
97	3.4963	1.0687	0. 039139	0.10202	0.67000			···		
>40171004<	ME PRESSURE	PATENS , FJE	CTOP SHPOON		Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the 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107	5.8777	1.8441	0.047536	0.17604	0.42400					
112	5.4726	1.7177	J. C62841	0.16290	0.83000		<del></del>	<del></del>		
122	5.0774	1.5773	0.057766	0.15957	0.96009					
127	3.4213	1.0734	0.039312	0.19247	1.0900			<del></del>		
137	3.9467	1.2393	0.04=349	0.11870	1.2200					
142	4.2314	1.2555	0.945981	0.11985	1.3500					
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-177	5.9777	1.7441	0.047536	0.17604		and the agency when we seem a superference when				
-112	6.4726	1.7170	0.062891	0.16390	1.0000					
-127	5.7274	1.5773	3.757746	0.15057	-1-0000					
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-137	3.467	1.2383	7.665349	0.11820	-1.0000	ميوديوس بدار دهما ما مدار	ar and the same will determ retired as a second second second second second second second second second second			
-147	4-9334	1.2555	0.245291	11095	-1.0000					
-152	3.3943	1.0456	0.039024	0-10172	-1.0000	. Japan salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah salah sala	- April Marketin - No. 1 miles and a sittle as because			
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-167	3.3963	1.0655	0. (29024	0.10172	-1.0000					
-15"	3.1763	1.35.56	035074	0.10172	-1.0000			and the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the suppli	· parago se · respiri di immediti integrina di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio di imperio	
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	47	11.565	3.6298	0.12175	0.27224	0.62900				and the control of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the same species of the sam
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	AVD WIPS	PL	PI /PO	PL/PTF	PI /PTP	T/(MAX				
	47	13.559	4.2190	0.14151	0.32805	0.47200				
	67	9.5517	2.9721	0.090690	0.23110	0.67000				
	>ADDET HOM	N PEFSSIPF	PATIOS . FLO	N SPLITTER D	. 0.					
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į	AVD WORD	PL	M./P0	PL/PTF	PL/PTP	X/DPAX				
	77 #2	36.115	11.960	0.39786	0.92216	0.50000				
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	107	6.4725	2.9140	0.067552	0.15669	9.62400				
_	112	4. 1275	1.8755	0.042908	0.14483	9.43000		······································		
	172	5.5474	1.7761	0.057899	0.13472	0.56000				
	127	3.4516	1.0749	0.036024	0.083510	1.0900		*		
	127	4.9173	1. 53 63	C. 751530	0.11945	1.2206				
	142	4.7912	1.4927	C. 050068	0.11607	1.3500	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			
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	-122	5.5474	1.7261	0.057858	0.13422	-1.0000				
	-127	4516	1.0745	0.016024	3.073510	-1.0000				
	-1 - 7	4.9373	1.5363	0.051530	0.13465	-1.0000				
	-147	4. 1774	1.4927	0.05006	0./1607	-1.0000	· an in the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the seco			
		3.4166	1.0631	7. 935659	0.072663	-1.0099				
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,	-1=? -1=7		1.0631	ערים ניין פני	リーリカイのヒコ	_T9 0000				
	-157	3.4166	1.0631		U. 111120F3	-1.0000				······································
	-147 "SF55  <b>TI</b> 091	3.4166 FPFTSURF	RATING FAI				<del></del>			
	-157 '3757 <b>17179</b> IVO WORD	3.4166 :	RATION, FAR	- HOVYST FLER M 1985	PI /P1P	X/DMA'X				
	-157 "3757177091 170 WILLIA -152	3.4166 (	MATINA, FAR M/PN 1.0631	1 WAY 1 FE EN M / PTF 0. 075650	PI /PIP 0.092663	X/DMAX -1.3000				
	-157 '3757 <b>17179</b> IVO WORD	3.4166 :	RATION, FAR	- HOVYST FLER M 1985	PI /P1P	X/DMA'X	- · · · · · · · · · · · · · · · · · · ·			
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	-157 "5755111100 140 wilen -152 -157	3.4166 F PPFSSORE PL 3.4166 3.4166	M / PT 1. 7631 1. 0631	0.075640 0.075649	P1 /P1P 0.087663 0.082663	X/DMAX -1.3000				
	-147   3857  171091   190   Willer   162   167   3457  171091	3.4166  PL 3.4166 3.4165  PE 3.4165  3.4165	MAYER PAPER 1. 7631 1. 7631 1. 7631	0.075650 0.075650 0.035659	91 /PTP 0.092663 0.092663	X/DMAX -1-3000 -1-0000				
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	-147 -3757171799 -147 -147 -147 -3457171799 -147 -147 -147 -177 -177	3.4166 PL 3.4166 3.4166 3.4166 3.4166 3.4166 3.4166	M/PH 1- 0631 1- 0631 1- 0631 1- 0647 PAYENS - RO	# / PTF 0- 075650 0- 035650 0- 035650 0- 035650 0- 035711 0FG SHRTING U	91 /919 0.092663 0.092663 PCAYTHN PL /P19 0.392663 0.392786	X/DMAX -1.3000 -1.0000 X/MMAX -1.9000 -1.0000				
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*&51-1 FH J	\ \!\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	EPIARY DATA	06/11/70	CANALI	REG 10/13/79 02:14:02.459 FAC 8X641 PGM C034 PRG 1129	
צחן דוכחעל	IAL_PRESSURE	PATINS PP	INSTAL MIC			
AUND UA	PL	Pt / PO	Pt /PTF	PL /PTP	x/DMAY	
22	15.871	4, 5544	0.16574	0.43069	U.43200	
3 <b>7</b>	P. 3966	2.6211	0.097685	0.22785	0.53009	
ć7	10.346	3.2421	0.10946	0.20103	0.62900	
E 2	10.536	3.2009	0.11992	0.28599	9 <b>.</b> 72700	
>407 TT 104	AL PRESSUPE	RATTOS , FLO	W SPITTER I	. n.		
AU MUND	PL	ምኒ / ምባ	PL /PTF	PI /PTP	X/DMAX	
62	12. 260	3. 7646	0.17594	0.32726	0.42200	
57	8.5766	2, 6554	0.092813	0.23084	0, 67090	
>AN9 11 104	AL PPESSURE	PATIOS . FLE	W SPLITTER O	. D.		
/p 4กคก	PL	PL / PD	PL/PTF	PI /PTP	X/DMAX	
77	38.105	11.495	0.39792	1.0340	U.50808	
*2	19.312	6.0296	0.20168	0.52407	0,58300	
?	3.4259	1.0594	0-035776	0.092966	0.67000	
ADD IT ION	AL PRESSURE	RATIOS . EJF	CTOR SHOOLD			
					er - P - P - N - N - N - N - N - N - N - N	
ያያ ነው። የመጀ	Pt	PL / PO	PI /PTF	PL /PTP	X/DMAX	
07	6.4610	2.0172	0.067490	0.17535	0,62400	
12	6.0314	1.8929	0.062990	0.16368	0.03000	
122	5.5467	1.7315	0.057924	0-15052	0.96000	
27	3.4409	1.0741	0.035933	0.093373	1.0900	
27	4.3514	1.3593	0.245441	0.11800	1.2200	
142	4.4164	1.1786	0.046120	0.11084	1.3500	
*****	ot one stune	pating , fol	FAFFW LORES			
Anen nen		PL /PII	PL/PTF	PI /PTP	X/0M4X	
107	6.4618	7.9172	9.967480	0.17535	-1,4000	
112	6.0318	1. 6929	0. 662 990	0.1636R	1.0300	
22	5.5467	1.7315	0. 057924	0. 15052	-1.0000	
27	3,4409	1.0741	0.034933			
137	4.3614	1.35#3	0.745441	0.093373	-1.0000	
42	4.416	1.3786	0.044120	0/11984	-1.0009	
157	3.4009	1.9616	0.035515	0.792207		
57	3.4359	1. 7632	0.035547	0.092423	-1.0000	
ልካካያ <b>ተ የ</b> ጣዩ	AL PRESSUPE	PATING FM	MOTTLE FLAT			
	••	a (ah	A 1916	PL /PTP	*/MAX	
ID HORD	PL	P( /Pf)	•			
	2 4000	1.0616	0.035515	0.092287		
157	3.4009	1 64 10				
/n wnpn [67 [67	3.4)59	1. 26 33	De035567	0.092473		
E7 E7			DEC SHOWING THE			
(67 (67 6636¶ቸ ሸፍ	3.4)59				x/DMAX	
(5) (67 (67 (67) (67)	3.4)59 Al Pressine	<b>RATURS</b> , 20	DEC SHEMME 11	TEATIPH	x/DMAX	
[67 [67 5656]Ŧ]#% 75 un#n [67	3.4)59 Al Pricsure PI	##11/15 . 70 #1/m1	DEG SHAMBETI PL/PTF	TEATING TO THE	r/DMAR -1.0000	
67   67   67   67   67   67	3.4)59 Al BAFCCIJAF PI 3.4059 3.409	M /PN 1.0632 1.0616	DEG SHAPEN TO PL /PTF 0.035567	0.092423 0.092427	r/DMAR -1.0000	
157 167 565617185 95 WORD 167 177 525517184	3.4359 AI PRESSURE PI 3.4259 3.4259 WERESSURE	#47775 , 20 # /Pn 1.0637 1.0616	DEG SHAMOR TI PL /PTE 0.035567 0.035515 DEG SHAMOR TO	17AT 1198 14 /919 05 092423 0 -0 18297	#/DMAR -1.0000 -1.0000	
E7   E7	3.4)59 Al BAFCCIJAF PI 3.4059 3.409	M /PN 1.0632 1.0616	DEG SHAPPE 11 PL/PTF 0.035567 0.035567	0.092423 0.092427	#/DMAR -1.0000 -1.0000	

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SAL SUBL	PL	PL / PIT	01 / PT F	PL /PTP	x/DMAX				
72	15.723	4. 0755	3.16571	9.43167	0.43200			*	
27	P. 3131	2.6741	J. CP7609	U. 27#73	J. 53J00				
47	10.277	7.2195	0.10831	0.28215	0.62500		•	- marketine and the same	and the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contrac
	19.437	3.26.96	0.11000	0.28655	0.72700				
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AVO WOPD	PL	PL /PO	PL /PTF	PL /PTP	X/DMAX				
~2	11.922	3.7345	0.12564	0.32729	0.42200	• • • • • • • • • • • • • • • • • • • •	The second of the second		The second section of the second section is a second section of the second section of the second section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section secti
67	R.41R0	2.5370	0.089716	0.23111	0.67000				
SAROTT INVA	PRESSURE	RATIOS . FLO	OW SPLITTER C	.D.			er in a composition of the second	ng spoolstations therein signature with a c	on consistings on employ on open or deside pages on collecting pages.
AVD WORD	PL	PL /Pri	PL/PTF	PL/PTP	X/DMAX				
77	37.743	11.623	0.39777	1.0362	0.50000	en de la companya de la companya de la companya de la companya de la companya de la companya de la companya de			-
• ?	19.135	5. 0042	0.20166	0.52533	0.58300				
92	3.4019	1.0657	0.035851	0.093394	0.67000				
>ADDITIONAL	PRESSURE	PATIOS - EJO	CTOR SHAPUD	a an illustra para para p	s settlement of the settlement	The second section is a second section of the second section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section s	- 150 de la constitución de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya del companya de la companya de la companya del companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya		
AVD WOPD	•i	PÉ/PÔ	PL /PTF	PI /PTP	X/DMAX				
107	6.3981	2.0043	0.067428	0.17565	0.62408				
112	5.9730	1.8711	0. 062548	0.16390	G. #3000	<del></del>			
122	5.4929	1.7207	0.057886	0.15080	0.96000				
127	3.4219	1.0719	0. 636962	0.093944	1.0900				
137	4.2924	1.3446	0.045237	0.11784	1,2230				
142	4. 3625	1.3666	0.945975	0.11977	1.3500	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	· · · · · · · · · · · · · · · · · · ·		
-	MESSAE		CARRY PARTY						
NAL MUGD	PL	PL/PO	PL /PTF	PE/PTP	×/mg/k		· ************************************		
-107	6.3941	2. 7043	0.047478	0.17565	-1,0000				
-112	5. 9730	1.A711"	0.062948	0.16396	1.0000	Committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the commit			<del></del>
-172	5.4729	1.7207	0.057899	0.15040	-1.0000				
-127	4219	1.0714	0,036062	0.093944	-1.0000	<del></del>		····	·····
-137	4.2024	1.3446	0.045237	0.11/04	-1.0000				
-147	4.36	1.3664	0. 645975	9/11977	-1.0000	The state of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second			
-1*7	3.3469	1.2617	2.235693	0.392982	-1.0000				
-157	3.3464	1. 3610	0.035693	0.992942	-1.0000				
53007770044	- PPFCSIBE	RATIOS FAR	MOZYLD SLAP						
TAU AUKD	PĹ	M /M	AINE	PL/PTP	X/DMAX		,		
-162	3.3969	0610 /	2.735693	0.092982	-1.0000				
-157	3.3969	1.3612	35035693	0.0-2982	-1.0000	and the second second second second second			
SANOT TONAL	- exteddibe	* ATYPE . 20	DEC SHAMELI	PETTIN					
190 HOPO	PL /	PL /PN	PL/PTF	MATE	X/DHAT				المعارجين المواجب المطلقة بالمرارات فرخه وواز ويتعامل المامورات
-167	3.395	1.0610	0.035653	0.465045	-1.0076				
-177	3.3/159	1.0610	0.035693	0.032645	-1.0000		i i vivini i i i i i i i i i i i i i i i	and an analysis of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of	
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	PL	PL/PT	PI /PTF	PL/PTP "	X/IIIAX	2	· · · · · · · · · · · · · · · · · · ·		
AVO MONT									
AVO 4000 -143	2.9315	0.91931	0. 030894	0.000441	-1.00.				

AU MUBU	PL	PL / PO	PL/PTF	PI /PTP	X /THA X		
32	17.609	5,5989	9.18558	0.43229	0.43200		THE ART IN A COMMAND A COMING OF BUILDING WAR TO BE MANAGED AND
37	9.3080	2.9120	0.098099	6.22851	0.53000		
47	11.516	3.6029	0.12137	0.20272	0.62930		The state of the contract of the contract of the state of the state of the state of the contract of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state
52	11.671	3.6513	0.12300	0.28652	0.72700		
> 400 1 1 100	ML PRESSUPF	RATINS , FLO	W SPITTER 1.	. D.			The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
AU NUED	PI .	PL/PN	PI /PTF	PL /PTP	X/DMAX		
(2	13.399	4.1010	C. 14122	O.32895	3.42200		
6.7	9.4329	2.9511	0.099416	0.23156	0.67000		
>ADDIT FOR	AL PPESSIPE	PATIOS , FLO	W SPLITTER_O	0.			
YD 40PD	Pl	Pt /PO	PL/PTF	PI /PTP	X/DMAX		
77	31.232	11.420	0.39820	0.92756	J. 50000		
	19.156	5.9731	0.20189	0.47029	0.58300		
P? 92	3.4143	1.0692	0.035985	0.083623	9.67000		
_				0411131123	3101000		
>AN1111NN	AL PRESSURE	PATIOS , EJ	CTIP SHPMO			n dender trader i nage i debt in i reger i nage i magazi.	
VN 40PN	PL	PL / PD	M /PTF	PI /PTP	X/DMAX	to the second with the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second	
107	6.4144	2.0068	0.067603	0.15747	0.62400		
112	5,9975	1.8738	0.063125	0.14704	0.83000	<del></del>	
122	5.4996	1.7206	0-057962	0- 13502	0. 96000		
127	3.4343	1.0744	0.036196	U 084314	1.0400		
137	4.8594	1.5203	0.051217	0.11930	1.2200		
142	4.7396	1.4828	0.049952	0.11636	1.3500		
. ~.	44.730	194054	36047477	0844620	863343		
>40017 f04		ALTING , FOR	Ereba Infea			·····	
MUNEU							
ALL MALLE IN	PL	PL/PO	PL /PTF	PL /PTP	x/nyax		<u> </u>
107	PL 6.4144	PL/PN 2.0068	Pt / PTF 0. C67603	PL/PTP 0.15747	×/mux -3.0000		•
	_	2.0068 1.8738		0.15747	×/ngax -1.0000 -1.0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	•
107	6.4144	2.0068 1.8738	0. 67603	0.15747	-1.0000		•
107	6.4144 5.9895 5.4996	2-9968	0. C67603 9. 063125	0.15747 0.14704 0.13502	-1.0000		•
107 112 127	6.4144 5.9895 5.4996	2.9368 1.8738 1.7206 1.0744	0. C67603 9. 063125 9. 057962 0. 036196	0.15747 0.14704 0.13502 0.085314	-1.0000 -1.0000 -1.0000 -1.0000		•
107 112 127 127	6.4144 5.9895 5.4996 2.4343 4.4596	2.0068 1.8738 1.7206 1.0744 1.5203	0. C67603 9. 063125 9. 057962 0. 036146 0. 051217	0.15747 0.14704 0.13502 0.084314 0.11930	-1.0000 -1.0000 -1.0000 -1.0000		
107 112 127	6.4144 5.9895 5.4996 4.4343 4.4596 4.7394	2.0068 1.0738 1.7206 1.0744 1.5203 1.4828	0. C67603 9. 063125 9. 057962 0. 034156 0. 051217	0.15747 0.14704 0.13592 0.095314 0.11636	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 127 127 142	6.4144 5.9895 5.4996 2.4343 4.4596 4.7346 3.4043	2.9368 1.8738 1.7206 1.0744 1.5203 1.4828 1.0651	0. C67603 9. 063125 9. 057962 0. 037136 0. 031217 0. C49952 0. C35879	0.15747 0.14704 0.13592 0.095314 0.1430 0.11636 0.083577	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 127 142 152 157	6.4144 5.9895 6.4996 3.4363 4.4596 4.7394 3.4043 3.4143	2.9368 1.8738 1.7206 1.0744 1.5203 1.4828 1.0651	0. C67603 9. 063125 9. 057962 0. 051217 0. C49952 0. C35879 0. C35879	0.15747 0.14704 0.13592 0.095314 0.11636	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
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107 112 127 127 127 142 152 157	6.4144 5.9895 6.4996 3.4363 4.4596 4.7394 3.4043 3.4143	2.9368 1.8738 1.7206 1.0744 1.5203 1.4828 1.0651	0. C67603 9. 063125 9. 057962 0. 051217 0. C49952 0. C35879 0. C35879	0.15747 0.14704 0.13592 0.095314 0.1430 0.11636 0.083577	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 127 142 152 152 153	6.4144 5.9895 5.4996 4.4343 4.0596 4.7396 3.4043 3.4143	2.9368 1.8736 1.7206 1.0744 1.5203 1.4928 1.0651 1.0651	0. C67603 9. 063125 9. 057962 0. 036136 0. 051217 0. C49957 0. C35879 0. C35879	0.15747 0.14704 0.13502 0.065314 0.1430 0.1630 0.063577	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		•
107 112 127 127 127 142 157 157 542217 [0]	6.4144 5.4996 2.4343 4.4596 4.7344 3.4043 3.4143	2.9368 1.8736 1.7206 1.0744 1.5203 1.4928 1.0651 1.0651	0. C67603 9. 063125 9. 057962 0. 037196 0. 051217 0. C49952 0. C35879 0. C35879	0.15747 c. 14704 0.13592 0.065374 0.1430 0.1636 0.063577 0.063577	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		•
107 112 122 127 127 142 152 153 154 157 157 169 161 161	6.4144 5.4996 2.4343 4.4596 4.7396 4.7396 3.4043 3.4743 2.4743 2.4743	2.9368 1.8738 1.7206 1.0744 1.5203 1.4928 1.0651 1.0651 PATION FAR PL/PD 1.0651	0. C67603 9. 063125 9. 057962 0. 057196 0. 051217 0. C49952 0. C35879 0. C35879 PL/PTF 0. C25879	0.15747 0.14704 0.13502 0.085314 0.083577 0.083577 0.083577 0.083577	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
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107 112 127 127 127 127 142 157 157 240717 [0] VO 40*0 157 157 260717 [0] VO 40*0	6.4144 5.9895 4.4996 4.7346 3.4043 3.4143 2.4143 2.4143 2.4143	2.9368 1.8736 1.7726 1.7744 1.5203 1.4828 1.0651 1.3651 PATION FAMPL PL/PD 1.0651 1.0651	0. C67603 9. 063125 9. 057962 0. 051217 0. C49952 0. C49952 0. C35879 0. C35879 PL/PTF 0. C25879 0. C25879 0. C35879	0.15747 0.14704 0.13592 0.075274 0.21430 0.1636 0.083577 0.083577 0.083577	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
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107 112 127 127 127 142 157 157 157 157 269917100 167 167 172	6.4144 5.9895 4.4996 4.4343 4.4596 4.7344 3.4043 3.4143 2.4343 41 PRESSIME PL 3.4343 1903	2.9368 1.8736 1.77206 1.0744 1.5203 1.4828 1.0651 1.0651 1.0651 1.0651 1.0681 1.0651 1.0651 1.0651 1.0651	0. C67603 9. 063125 9. 057962 0. 037196 0. 051217 0. C49952 0. C35879 0. C35879 0. C25879 0. C25879 0. C35879 0. C35879 0. C35879	0.15747 0.14704 0.13502 0.065274 0.1430 0.1636 0.083577 0.083577 0.083577 0.083577 0.083577 0.083577			
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ANZO-I EMI	c marria	INAPY DATA	06/11/79	CAPOFII	PFC 10/13/	79 07:16:32.294	FAC AXEVI	PC# C#34	Red 16	
>407   T   D %	AL MRESSUPE	RATIOS , PP	IMAPY PLUG							
ሲሁ ላሳትህ	PL	PI /PD	PI /PTF	PL /PTP	X/DMAX				the transfer of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the c	
32	14.501	4.5491	0.16571	0.43121	0.43200					
37	7.6795	7.4192	0. 047754	C.22037	0.53000				and the second designation of the second second second second second second second second second second second	
47	9.4949	2.9794	0.10849	0.28233	3.629 <b>0</b> 0					
57	9,6339	19.7273	n. 11009	0.28649	J. 72700			<del></del>		
>AUDIT IUN	IL PRESSIME	RATIOS . FLO	W SPLITTER I	• O•		*			was are in the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the s	
ስህ ማ <b>ሀ</b> ቴህ	PL	ም_ / ቦባ	PI /PTF	PL/PTP	X/DMAX					
67	11.013	3.4551	0.12586	0.32751	7. 42207				The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	
67	7, 7795	2.4406	0.088901	0.23134	J.67000		<del> </del>			
MINITERIA	L PRESSURE	PATENS . FLO	W SPLITTER O	. D.						
AU MUNU	PL	PL/PG	PL/PTF	PL /PTP	X/DYAX					• • •
77	34.495	10.944	0.39867	1.0374	0. 50700					
82	17.632	5.5316	0.20150	0.52434	0.58300					
77	3.4134	1.0700	3. 03 9037	0.13150	3.67030	···	·			
2701T10W	N PRESSURE	RATIOS . EJF	FÉYCA SHADUD			m comme a	- and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of			
to when		PL /PO		Pi /Pip						
107	PL 5.0)44	1.8523	M /PTF	0.17558	X/DAAX					
			0.067474		0.62400	······································				
112	5.4993 5.0592	1.7252 1.5972	0.052R45	0.16354 0.15045	0.03000					
122 127	3.4234	1.0740	0.057815 0.039121	0.10180	2.96 <b>039</b> 1.0900					
137	3. 7657	1.2451	0.054151	0.1102	1.2730					
142	4.0>34"	1.2623	0.045542	0.11966	1.3500					
	I MESSIE	AATTAL FOR	THE INCH			<u></u>				
				A 4826						
חפרש יוני	PL	M/Mi	M /PTE	PI /PT#	× /5/44		-			
vi umn 107	PL 5.9344	PL/Pri 1.8523	M /PTE 0.067474	0.1755R	-1,0000					
vir umm 107 112	PL 5.9344 5.4343	PL/PH 1.8523 1.7252	m /pts 0.067474 0.062845	0.1755R 0.16384	-1.0000					
vir umn 107 112 122	PL 5.7344 5.4343 5.7572	PL/PH 1.8523 1.7252 1.5872	M /PTF 0.067474 0.062845 0.057815	0.1755R 0.16354 0.15045	-1.0000 -1.0000					
vir umn 107 112 122	FL 5.9344 5.9592 5.9592	ML/PM 1.8523 1.7252 1.5872	74 /pfr 7. 067474 0. 062845 0. 057815	0.1755R 0.16354 0.19045 0.1019	-1.0000 -1.0000 -1.0000					
vi umen 107 112 122 127	PL 5.9364 5.4343 5.0592 4.234 3.4687	M/P1 1. 8523 1. 7252 1.5872 1.0749 1.2451	M /PTE 0.067474 0.062765 0.057815 0.057815 0.0578151 0.045353	0.1755R 0.16354 0.15045 0.1015F 0.13672	-1.0000 -1.0000 -1.0000 -1.0000					
vir uren 107 112 122 127 127	PL 5.9344 5.4343 5.0572 4234 3.4407 4.074	M/P1 1. 8523 1. 7252 1. 5872 1. 0749 1. 2451 1. 2423	M /PTF 0.067474 0.062845 0.057815 0.045353 0.045482	0.17558 0.16354 0.15045 0.1019 0.11672 0.11672	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000					- 40.6
Wir wren 107 112 122 127 137 142	PL 5.9364 5.4743 5.0572 4234 3.4647 4.0744 3.3714	PL/PH 1. #523 1. 7252 1. 5872 1. 0769 1. 2451 1. 2423 1. 2446	M /PTE 0.067474 0.062845 0.057815 0.734121 0.045982 0.045982	0.17558 0.16354 0.15045 0.1019 0.11652 0.1166 0.10091	-1.0006 -1.0006 -1.0006 -1.0006 -1.0006 -1.0006					
With writing 107 112 127 127 127 127 147 147 147 147 147	PL 5. 9364 5. 4743 5. 9592 4234 3. 4687 6.078 3.3916 3.3996	PL/PM 1. #523 1. 7242 1. 5#72 1. 0749 1. 2451 1. 2623 1. 9446 1.9661	M /PTE 0.067474 0.062845 0.057815 3.714171 0.045987 0.045987 0.038878	0.17558 0.16354 0.15045 0.1019 0.11672 0.11672	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000					- 10-2
VI UNP () 107 112 122 127 127 142 142 147	PL 5. 9364 5. 4743 5. 9592 4234 3. 4687 6.078 3.3916 3.3996	PL/PM 1.8523 1.7552 1.5872 1.0769 1.2451 1.2423 1.7446 1.9661	M /PTE 0.067474 0.062845 0.057815 3.334171 0.045363 0.045362 0.038778 0.038836	0.17558 0.16374 0.19045 0.10179 0.11452 0.11452 0.10091 0.10106	-1.0006 -1.0006 -1.0006 -1.0006 -1.0006 -1.0006					
VI WIPD 107 112 122 127 127 142 142 143 147 147	PL 5. 9344 5. 4293 5. 0592 4234 3. 4607 4. 0. 74 3. 3014 3. 3014	PL/PM 1. #523 1. 7252 1. 5872 1. 5872 1. 0749 1. 2451 1. 2423 1. 9446 1. 9661 RAYING, FAR	M /PTE 0.067474 0.062845 0.057815 3.934121 0.045353 0.045982 0.038878 0.038836	0.17558 0.16384 0.14945 0.10198 0.10198 0.11969 0.10091 0.10106	-1.0006 -1.0006 -1.0006 -1.0006 -1.0006 -1.0006					
VI WIPD 112 122 127 127 142 143 143 143 143 144 143 144 147 147	PL 5. 9344 5. 4743 5. 9592 4234 3. 46,074 3. 3014 3. 3044 11 PRESSIBE	PL/PM 1. #523 1. 7242 1. 5872 1. 0749 1. 2451 1. 2453 1. 9446 1. 9661 RAYIN FAR	M /PTE 0.067474 0.062845 0.062845 0.057815 0.045982 0.045982 0.045982 0.038778	0.17554 0.16354 0.19045 0.1019 0.11976 0.10091 0.10106	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
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VI WIPTO 1107 1127 127 127 147 5 EMBITTON 157 147	PL 5.9344 5.4743 5.0592 4.234 3.3914 3.3914 3.3914 3.3914 3.3914 3.3914 3.3914	PL/PM 1.8523 1.7552 1.5872 1.0749 1.2451 1.2423 1.7446 1.9661 RATION FAR PL/PM 1.0646 1.0765	M /PTE 0.067474 0.062845 0.062845 0.057815 0.045982 0.045982 0.045982 0.038778	0.17558 0.16384 0.16345 0.10146 0.10146 0.10091 0.10106 Pl /PTP 0.10091 0.10196	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
VITUTED 112 122 122 127 142 142 142 142 142 142 142 142 142 142	PL 5.9344 5.4743 5.0592 4.234 3.3944 3.3944 3.3944 11 PRESSIBE	PL/PM 1.8523 1.7552 1.5872 1.0749 1.2451 1.2423 1.7446 1.9661 RATION FAR PL/PM 1.0646 1.0765	M /PTE 0.067474 0.062845 0.057815 0.057815 0.045982 0.045982 0.038778 0.038778 0.038778	0.17558 0.16384 0.16345 0.10146 0.10146 0.10091 0.10106 Pl /PTP 0.10091 0.10196	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
VIO WIPD 107 112 122 127 142 147 147 147 5450TT TOMA	PL 5.9344 5.4743 5.0592 4.234 3.3914 3.3914 3.3914 3.3914 3.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914 7.3914	#L/PM 1. #523 1. 7252 1. 5872 1. 0749 1. 2451 1. 2453 1. 3446 1. 7661  #AYING FAR	M /PTE 0.067474 0.062845 0.057815 3.734171 0.045487 0.045487 0.045487 0.038778 0.038778 0.038778	0.17558 0.16384 0.16384 0.10198 0.10198 0.119691 0.10106 PI/PTP 0.10091 0.10126	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
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VI WIPD 107 112 127 127 127 147 147 147 147 147 147 157 157 157 157 157 157	PL 5.9364 5.4743 5.0592 4.236 3.3040 3.3044 3.3044 3.3044 3.3044 3.3044 3.3044 3.3044 3.3044 3.3044 3.3044 3.3044	PL/PM 1.8523 1.7552 1.5872 1.5872 1.0749 1.2451 1.2423 1.9446 1.9661  RATING FAM M /PM 1.0646 1.0753  PL/PM 1.1646 1.0646 1.0646	M /PTE 0.067474 0.067474 0.062845 0.057815 0.057815 0.045982 0.045982 0.038778 0.038778 0.038778 0.038778 0.038778	0.17558 0.16384 0.16345 0.10188 0.10189 0.10001 0.10106 PI /PYP 0.10001 0.10126 PI /PYP 0.10001 0.10126 PI /PYP 0.10001 0.10126	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000					
VI WIPD 107 112 122 127 127 147 147 147 147 147 147 147	PL 5.9344 5.4743 5.0592 4.234 3.3914 3.3914 3.3914 3.3914 3.3914 7.3914 7.3914 7.3914	#L/PM 1. #523 1. 7252 1. 5872 1. 0743 1. 2451 1. 2453 1. 2446 1. 9661  #AYIN FAR  # /PN 1. 1646 1. 0646 1. 0646 1. 0646	M /PTE 0.067474 0.062845 0.057815 0.057815 0.045482 0.045482 0.045482 0.038778 0.038778 0.038778 0.038778	0.17554 0.16354 0.16354 0.1019 0.1019 0.1019 0.1000 0.10106 0.10106 0.10106 0.10106 0.10106	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,7000					

1471-1 FH I	S PPFL14	INSPY DETA	06/11/79	CARRELL	ofC 10/13/79 C2:17:03.230	FAC 8X6X1 PG4 C234 RB6 1133
>400 11 103	AL PRESSUPE	PATIOS . PP	HUDY PLUG			
Au Ausú	PL	P( /PI)	P( /PTF	PI /PTP	X/DMAX	
32	16.146	5.0310	7.18456	0.43164	9.43200	The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th
37	A-5314	2.6549	9.097522	C . 2 2 # G P	3.53000	
47	10.555	3.2097	0-15044	0.29219	0.62500	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
52	10.715	7, 3395	0.12749	0.28647	). 7270 <u>0</u>	
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AU MUBU	-PL	PL/PO	M /PTF	PI /PTP	X/DMAY	
62	12.274	3.8254	0.14031	0.32815	0.42200	
67	P.6463	2,6947	J.098A36	0.23115	0.67000	
>AODIT HON	AL PRESSUPE	PATIOS . FLO	W SPLITTER O	.n.	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	
מפיואי יוע	PL	PL/PO	PI / PTF	PL/PTP	X/DMAX	
77	34.947	10.892	0. 39948	0,93429	0.50800	
2	17.654	5.5620	0.20189	0.47167	0.58300	
92	3.4257	1.0676	0. (39159	0.091583	0.67000	
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yn HARD .	PL	<b>77 / PO</b>	PI /PTF	PL /PTP	X/DMAX	
107	5.9366	1.8408	9-067518	0.15791	0.62400	
112	5.5065	1.7162	0.362545	0.14721	J. 83000	
12?	5.0614	1.5774	0.057857	0.13531	0.96000	
27	3.4357	1.0706	0.035273	0.091850	1.0900	
137	4.4562	1.3896	0.050939	0.11913	1.2290	
142	4.3462	1, 1545	0. (4564)	0.11619	1.3500	
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AU AUAU	PL	PL /PD	PL/PTF	PI /PTP	X /DMg/K	•
107	5.9066	1.0408	0.067518	0.15791	-1.0000	
115	5,5065	1.7162	0.067945	0.14721	1.0000	
127	5-9614	1.5776	0.057957	0.13531	-1.0000	
127	4357	1.0704	0. 130273	0.091950	-1.0000	
137	4. 562	1.3888	0.050939	0.11913	-1.0900	
142	6.3430	1.3545	0.046681	0.11619	-1.3000	
15? 157	3.4107	1-0630	0.038997	C-091182	-1.0000	
- 7	3.4177	1.06 30	" U-03898	0.391162	-1. 9330	
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AU MUED	Pi .	M/Pii	PL 1915	PĹ/PTP	X/DMÄX	
152	3.4137	1.0630	0. 038997	0.091182	-1.0000	
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167	3.43/17	1.0630	0.038987	091102	-1.0000	,
77	36057	1.0414	J* C2463U	0.701048	-1.0000	
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an when	T1	PL/PN	-1 / PIF			
משחוב מע	2 0242	0.01314	0 022282	A A70A77	_1 3000	
VO 2000 147	2.9233 2.9454	7. 91 914 7. 92418	0.0333P2 0.033897	0.07#073	-1.0000 -1.0000	w y we sy ny namen swe we way to see the second committee and the second committee of the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second committee and the second

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	7,9359	3.0840	7.11245	0.72767	2.53000				
3T 47	12.375	1. 41 52	7.13926	0.24195	3.62900		The second section of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco	and the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comments of the second comment	t op de kristingen i de kommen des uit indeel
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67	14. 358	4.4566	9.16750	0.37900	3.42260				
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97	1.4430	1.0677	0.038932	0.078824	0.57600				
SAUDET #	THAL PRESSIME	PATINS , FU	FÖTTR SHROUB	<b></b>		* * * * * * * * * * * * * * * * * * *	atom	electric chief de la constant de la constant de la constant de la constant de la constant de la constant de la	And the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
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107	5,9762	1.8549	0.067636	0.13494	0.42400				
112	4,5761	1.7337	7.042100	0.12777	0.83000				
177	5.1159	1.5479	3.057903	0.11723	0.96000				
127	3.4600	1.0739	0. 639159	0.0792#3	1.0000	1. * 1. * 1. * 1. * 1. * 1. * 1. * 1. *			andricke the specific action and a contract the specific properties the specific and a specific properties the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the specific properties and the spe
177	5.1159	1,5879	0.057900	0.11723	1.2200				
142	4.4)04	1. 5212	0.0 CE 5466	0.11230	1.3500	The second section of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco	, v reprintente antici i responsare, el entre rese de entre el esta de el esta de el esta de el esta de el est		
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-107	5.9762	1,8549	0.967636	0.13694	-1.0000		•		
-112	5.5761	1.7307	0.061134	C.12777	-160300	سرر لينهاموهو المحادات المادرات			and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th
-827	5.1159	1.5479	0.057900	0.11723	1.0010				
-127	4//75	1.0734	7.0144	0.079283	-1.0000				
-127	5. 7450	1.5979	0.057900	0.1132	-1.0000				
-147	4.97	1.5212	9-055465	C-14230	-1.0000	to eather the second contract the second			gyapite destablication (Mighinia dago este alban este este este en en en esta esta en en en en esta en esta en
-157	3.4750	1.0631	0.038762	W.0784F0	-1.0200				
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	72	17. 394	5. 3251	0.21450	0.43113	0.43200		ு பள்ளார். நடிக்கு குறையுள்ள குறிய விகிறி காண்ண பாரார் நடிக்கு குறியத் திறியண்ணும் பாரும் அடிக்கு மி. இ. இ. இ. இ. இ. இ. இ. இ. இ. இ. இ. இ. இ. இ. இ. இ. இ
	37	9,0727	2.9132	0.11332	9.22776	J. 53000		
_	47	11.172	3.4795	0.14016	0.28171	J.62900		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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	10"	5.3922	1.6763	0.067522	0.13572	0.62400		•
	117	5.0121	1.5610	0.062578	0.1263P	J. #3000		
-	122	4.6019	1.4332	0.057732	0.11604	.96000		<b>1</b>
	127	3.4310	1. 7686	0.043043	0.096515	1.0900	***	
	137	4.6318	1.4426	0.058109	0.11679	1.2200		
	147	* . 4267	1.3787	0.055575	0.11162	1.3500		
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<	~ > <del>************************************</del>	f—ast center	PATIOS FOR	<del></del>				3
	JAG HUBE	PI	PI /PI	PL /PTF	PL/PTP	X/D94X		
	-10)	5.3427	1.6763	0.067522	0.13572	-26.3000		
	-117	5.0121	1.5610	0.062879	0.12698	-1.0000		
	-127	4.6318	1. 4332	0.057772	0.11694	-1.0000		•
-	-127	3.431)	1. 16 86	0. 147943	0.086515	-1.0939		
	-137	6318	1.4426	0.058109	0.1670	-1.0000		<b>3</b>
	-147	4.4767	1.3797	0.05535	#.11162	-:.0000		
	-152	2.416)	1.0639	0.042855	0.0%136	-1.0000		
	-157	3.4110	1.7623	0.047792	6.686310	-1.0000		
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	-157	3.4167	1. 75 39	7.042855	0.076136	-1-0300		
-	-147	3.4110	1. 35.25	2.342792	0.096010	-1.0000		•
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	-167	3.441	1.0623	0.042792	8,086010	-1.0000		
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	37	7.8257	?. 4393	0. 038607	0.72956	2.53000	
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_	52	9,000	3.05RR	0.12765	G.PREE1	0.72703	
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	R2	16.003	4.9945	0.20190	0.46799	0.58390	
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	107	5.3547	1.6712	0.067558	0.15659	0.62400	
_	112	4,0045	1.5588	0.063013	C. 14606	0.43000	
	122	4.5742	1.4292	0.057774	0.13391	0. 96900	
	127	3.4332	1.0715	0.043315	0.10040	1.0960	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t
	137	4.0738	1.2714	0.051397	0.11913	1.2200	
	142	3.9547	1.2155	0.049945	0.11577	1.3500	
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	-107	5.3547	1.6712	0.067558	0.15659	-1 (1000	
	-112	4.0945	1.5596	0.043013	0.14656	1.0000	
	-122	4.5792	1.4792	0.057774	0.13791	-1.0000	
_	[5]	4.32	1.0715	0.043315	0.1004	-1.0000	
	-1 ² 7	4.0234	1.2714	0.051397	0.13013	-1-0000	
	-142	3.25MZ	1.2355	0.040045	0/1577	-7.0000	
	-1<2	3.4032	1.0521	0.042936	0.099520	-1,0000	
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	-157	3.4732	1.0621	0. 042936	0.099520	-1.0000	
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47	A.59AO	2.6947	0.10858	0.78217	0,62900
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77	31.401	9. 5669	0.40162	1.0436	0. 40800
92	15.973	5.0052	7.20169	0.52410	0.58300
95	3.41 )7	1.0689	0.043073	0.11193	9.67000
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122	4.5666	1.4312	0.657672	0.14987	0.96000
127	3.4107	1.04 4d	0.043373	0.11193	1.0900
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-112	4.9819	1.5614	0.067917	0.16349	1.0000
122	4.5666	1.4312	2.257672	0.14997/	-1.0000
127	3.41 17	1.0699	0.043073	7.11109	-1.3936
-177	3.6950	1.1270	0.045412	0.14601	-1.0308
142	3.4330	1.1395	0.045917	2.11932	-1.4006
157	1. 1976	1.0627	0.042820	2.11127	-1-0000
.i = 7	3.3906	1.0627	0.942879	3.11127	-1.0000
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32	13.792	4.1684	0.1867R	0.43147	0.43200
÷7	7.0475	2.2191	7. 099033	D. 22877	0,53071
47	9.71.90	2.7339	0.12251	0.28299	0.62500
<b>5</b> 7	8.R330	2.7700	0.12412	0.24677	0.72700
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<b>+2</b>	10.098	3.1667	0.14190	0.37779	0-42200
67	7.1226	2.2336	0.10000	0.23120	0.67000
>ADDITION:	AL PRESSURE	PATINS , FLO	W SPLITTER P	. II.	
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77	29.684	8.9952	0.49307	0.93109	0.5000
97	14.367	4. 5254	0.23188	0.46635	0.58300
?	3.4049	1.0578	0.047847	0.11057	3. 67000
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VO MOPB	PL	PL/PO	ML/PTF	71 /919	1/NAX
107	4.7912	1.5025	9.067327	0.15553	0.42490
112	4.4760	1.4037	0.062897	0.14529	0. 63000
122	4.1 )76	1.2960	0.047623	0.13211	0.96000
127	3, 1999	1-2662	0.047776	0.11036	1.0436
137	3.6652	1.1494	0.051504	0.11997	1.2200
142	3.5601	1.1164	0.050027	0.11556	1.3500
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107	4.7912	1.5025	0. C67327	0.15553	-2. 0430
ii,	4.4760	1.4737	0.062897	0.14526	-1.0036
122	4.1776	1.2960	0.057623	0.13311	-1.0900
27	1979	1.74.62	0.047776	0. 112-6	-1.3530
13.	3.0452	1.1494	0.051504	0,21867	-1.0930
143	3.563	1.1164	0.050027	0.11=56	-1.0900
1=>	3.3949	1.0615	9.247565	0.13980	-1.3000
157	3.3749	1.0615	9. 647548	J.129##	-1.0000
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107	2.3544	J. 92653	0.041516	0.095904	-1.3003

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77	4.1531	7.5407	0.11319	0.22785	a.53000				
4 7	10.193	7.1416	9.13cgf	0.29173	3.6250)				
57	10.245	3,189C	0.14211	C-25+0+	3.72703				
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f ?	11.777	3.6521	9. 16779	0.32751	9.42200				
67	8.2701	2.5750	0.11672	0.23092	0.67303				
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Au Music	٩	Pt /P1	PE /PTF	PL /PTP	X/DMAX				
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P2	14.538	4.5265	0.20166	0.46593	0.58300				
57	3.4333	1.0649	0.047621	0.095851	0.67000				
venngy grind	L PRESSIBE	RATIOS . FJF	CTTP SHPRIM	Fr		<del></del>		- The resistance of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t
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137	4. 3541	1.5114	0.067333	0.13554	0.62400				
ii?	4, 4339	1.4117	7. 667=91	0.12660	0.83000		· · · · · · · · · · · · · · · · · · ·	<del></del>	
122	4.1536	1.2033	9-257617	9.11598	J. 96000				
27	3.4737	1.0584	0.047671	0.055457	1.3936				
137	4.1936	1.3026	0.058033	0.11642	1.2200				
42	3.9785	1.2457	0.055465	0.11165	1.3500	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon			······································
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ALIEN I	PL	PL/P/T	PL/PTF	PE /PT9"	X/tmbx				
137	4.8541	1.5114	9. 067333	0.13554	-1-0000				
112	4.5339	1.4117	0.762491	0.12669	1.6500				
122	4.1536	2.2033	0-057617	0.11598/	-1.0000				
,	4330	1.0589	0.047621	0.095	-1.0000				
37	4.1936	1.3026	0.058033	G-125-82	-1-0000				
142	3.00	1.2450	0.055465	0.12F#2 0.111e5	-1.0000	* * * * * * * * * * * * * * * * * * *			
62	3.4190	1.5542	0.047412	0.095437	-1.9900				
47	3.4193	1.5542	0.047413	0.095437	-1.0000	e en a			
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62	3.4130	1.9642	0.547612	0.055437	-1-0000				
£7	3.4147	1.755	20267412	0.095437	-1-0000				
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167	3.410	1.0527	7.047742	0305-299	-1-0000				
יז!	3,00(3)	1. 76 42	0.547412	0.096637	-1.0009		e contractor of the second of the second	and the second section of the second section is a second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section	an a film in the particular second of the second contract of the
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194	PI 2.9??5	M /PA 1. 93995	0.040539	0.081602	-1.00 <b>00</b>				
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משה שאל	PL	Pt / PO	Pt /PTF	P1 /PTP	x fima x	
22	10.555	3.2922	0.16574	9.43069	2.43203	an an ann an Maragaman ann an ann an an an Albanda an an an an an Albanda an an an an an Albanda an an an an an
~ <del>~</del>	5.6105	1.7500	0.097891	0.72993	0.53000	
47	6.9357	2.1634	0.1)#65	0.24321	).62900	அம் எனும் ஆட்டிய நாட்டிய பட்ட மண்ணுக்கத்தில் கட்டிய மற்று இத்தின் முறிய மற்று மற்று மற்று மற்று மற்றும் மற்றும் மற்று
52	7,0357	2. 1944	2.11022	0.28709	3.12700	
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VD WOPO	Pŧ	PI /PP	PL/PTF	PI /PTP	X/DMAX	
67	A.0436	2.5080	1.12596	9.32899	7.42200	
67	5,6996	1.7719	3.089999	0.23179	0,67000	
POTTEONS	AL PRESSURE	RATIOS . FLO	W SPLITTER IL	.D.	AND THE PROPERTY AND ADDRESS OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O	
מפרצי חצ	PL	PI /PO	PI /PTF	PI /PTP	Y/EMAX	
77	25.650	9.0008	7.40182	1.9466	3,50900	
92	12. 968	4.0138	0.20158	0.52508	J. 5 8 300	
97	7.4196	1.0666	3.053569	0.13953	0.67000	
\400! T ! C~		PATIOS , EJF				
				manage and an exercise		~ ^ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
AL nUbd	PL	PL/PO	PL /PTF	PL /PTP	X/DMAX	
107	4.2701	1.3319	0.066892	0.17424	0.62400	
117	3. 9747	1.7461	0.062592	0.16301	0.63000	
153	7.6547	1. 1431	1.057613	0.14954	0. 96000	
127	3.4146	1.0651	0.053491	0.13933	1.0900	
127	2.4992	0.99432	0.045417	0.11830	1.2200	
142	2.9192	7.91256	2.245731	0.11912	1.3500	
\$400JTJ04	ANT SCIPE	acting , co	COCON INFEE			
חחוניוע	PL	PL/PO	PY /PTF	PL/PTP	x/onex	
107	4.2701	1.3319	0.066892	0.17424	-1.4000	•
1112		1.2461		7.16391	1.0000	
	3,9349		0.062582			
122	3.6647	1.1431	0.057410	0.14954	-1.0000	
127	3,4146	1.0451	0.053491	0.13934	-1.0000	•
137	2.1032	2.92432	0.545417	2.14 30	-1.9000	
147	2.9178	2. 91 056	0.045731	0.11912	-1-0300	
167	3.4946	1.0620	0.053334	0. 13R92	-1.0000	
157	3.4 )46	1. 3627	0.05333	0.13892	-1.0000	
244.144	AL PRESSUPF	RATION	MOTTHE FLAP			
ለ። ተባድብ	PL	PL/PD	PI /PTE	PL/PTP	X/DMAX	
15?	3.4746	1. 2520	0.052334	0.13892	-1.0000	
167	3.4 146	1.9629	3063334	0.13892	-1.0000	
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167	3.4766	1. 3620	0.052334	0.13892	-1.0000	
372	36. 396	1. 16 24	3.053256	0.139.77	-1.0300	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
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Vr anen	PI	Pt / P/I	PL / PTF	PL /PTP	X/IMEX	
5 4 5 0 1 <b>7 1 5 11</b> Vr	P( 2.9)92 2.9633	Pt /P7 7, 99744 4,92617	PL /PYF 0. 045574 0. 346515	0.11871 0.12116	-1.0000	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s

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	34.0111C.v<	1 PPESSIPE	RATIOS . PR	MAPY PLUG						
	AVD WINED	PL	PL/PD	PL/PTE	PL /PTP	X/DMAX				
	??	11.912	3, 7066	0.18678	0.43042	J-43200		-		
	27	6.2691	1.9470	D. C9511*	0.22841	9.53000				
	47	7.7592	2.4344	0.1226A	J.2#271	0.62900				
	52	7.8631	2.4675	0.12434	0.28654	J.7270J				
	APOJ TECNAC	f notestibé	RATIOS 2. FLO	W SPLITTER	1,0,	-	-			
	AVO HOPD	. Ct	PL/PD	PI /PTF	PI /PTP	X/DMAX				
	17	9.9929	7.9221	0.14221	0.32771	J. 42200				
		6.3631	1,9905	0.19030	0.23115	0.67000				
	NOT TECON	1_PRESSUPE	RATINS . FLI	W SPLITTER	r. n.	r can reference in them to the in the september	a compression .			* # # # # # # # # # # # # # # # # # # #
	AVD WORD	PL	PI /PI)	PL /PTF	PI /PTP	Y/DMAY				
	77	25.539	R.0144	0. 47785	0.93965	J. 50800				
	•2	12.731	4.0108	0.20211	0.46575	0.58300				
	97	3.4317	1.0676	0.05:794	0.12397	0.67000				
_	APOT T TODAC	I PRESSURE	PATIOS , FJI	CTER SHPEND	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	er a freed suggested that source and	ere care a so			
8	AVD WOPD	- PL	M /Mi	Pt /PTF	PL/PTP	X/DMAX		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		nan numarak nagumin ningga <del>nagi</del> ngagan ningga s
O.	107	4.2374	1.3297	0.047006	0.15441	0.62400				
	112	3.7673	1.2450	0. 752734	0.14457	0.83000				
	122	3.6379	1.1413	0.057513	0.13254	J. 96000				
	127	3.3969	1.0460	0.052715		1.0900	<del></del>	in a second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of t		- many contract of
	137	3.2619	1.0736	0.051579	0-11886	1.2200				
	147	3.1667	0.09375	0.050075	0.11540	1.3500		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	and the second second second	et a mangathag again get the estage of the anglish of the site of the site of
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	AVI UNEN	PI	PL /PI)	PL /PTF						i kanan ara akindana i karan ana anda akina i karan ana ana ana ana ana ana ana ana ana
	-1,77		1.3297	0.067006	PL/PTP	×/1094%		•		
	-117	4.2374	1.2450	0.062734	0.15441	1.0000				and a special paper of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control o
	-122	3.6370	1.1613	0.057513	0.13754/	-1.0000				
	-127	3,3769	1.0560	0.053715	0.12379	-1.0000		············		
	-137	3.2618	1.0736	0.651579	0.34896	-1.0000				
	-147	3.150	0. 30375	0.950075		-1.0000		a company of a high-management of an o	• • • •	range of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the sec
	-157	3.3969	1.0628	7. 657557	10.12347	-1.0000				
	-157	7.3969	1.0528	0.05355	0.12342	-1.0000		process of the same of the same		
	SAULT LUGAC	L PPFSSIMF	RATION FAR	HOTELE PLAI	<b>,</b>			-		
	AVD WOPD	PL	PLIPO	PL/PTF	PLIPTP	X/DHĀ¥	and the second process			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
	-157	3. 2969	1.0428	0. C53557	0.12342	-1.0000				
	-157	3.3867	1.3626	10023243		-1.0000			· · · -	
	25UULA LUM	I DESCRE	REPTOS . 20	OFF CHANNE	OCATION .	· · · · · · · · · · · · · · · · · · ·				
	C AVD WORD	PI -	PLIM	M /ATF	NE /PTP	X/0MAX	ж.		· · ·	. was compared to a
	-167	7. 7969	1.052	0. 053557	0.42342	-1.0000				
	-172	3 3 369	1.0628	0.053567		-1.0070	-		•	v
	SANTIT INDIA	1 SALZZINE	DA . SULLIA	utic Zimanfin (	DEATION					
•	AVP JAMED	"Pt	PE / P/I	PI /PTF	PL/PTP	x/thex		Jan.		
	-10%	?. 9965	0.23581	0.045644	C.10519	-1.0000	•			
	L /-107	7.9965	1,92466	7.046 594		-1.0000		-		
	SUBTION 5									

MOLTECOAC	AL PRESSURE	RATIOS , PR	MAPY PLUG			
AU MUSU	PL	et /PO	PI /PTF	PL /PTP	x/DMAX	
3?	13.703	4, 3024	0.21540	0.43097	0,43200	e companies e e e e e e e e e e e e e e e e e e
37	7.2549	2.2785	9.11408	0.22824	0.53000	
47	A. 9763	2.8184	0.14110	0.28232	0.62900	<ul> <li>Companies and a property of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of</li></ul>
52	9.1012	2.8576	0.14307	0. 24625	0,72700	
>ADDITION	AL PPESSIME	PATINS , FLO	W SPLITTER I	. O.		
VD WOPD	PL	<b>ም</b> ኒ / <b>ም</b> ብ	PL/PTF	PL /PTP	X/DMAX	
62	10.400	3. 2656	0.16349	0.32711	J.47200	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
67	7.3369	2.3036	0.11533	0.23076	0.67000	
>ADDITION	AL PRESSIME	PATINS , FLO	N SPLITTER O	. n.		
AD HOKD	PL	<b>PE / PO</b>	PL / PTF	PL /PTP	K/DHA K	
77	25.644	8.0516	0.40311	0.80654	0.50A00	MONTH BY MINE AN AREA DAY - CANADA ANTHRONOUS - 19-12 - 1777 - ANDREW CHATTER SCHOOL AND AND CHARGE - 19-14
87	12.929	4. 02 79	0.20166	0.40348	0.58300	
92	3.4764	1.7695	0.053547	0.19714	0.67000	
>ADDIT TON	AL PRESSIME	RATIOS , EJI	CTCP SHROWN			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
VP HOPD	PL	PI /PI	PL/PTF	PL/PTP	X/DMAX	
107	4.2518	1.3350	0.066836	0.13372	0.62400	
115	3.9917	1.2533	0.067748	0.12454	0.83000	
127	3.6515	1.1465	0.057401	0.11495	0.96009	
127	3.3464	1.0564	0.053390	C-104-42	1.0900	to de til to the secondaries - and an appropriate agreement to the tile to the secondaries and appropriate agreement to the secondaries are also to the secondaries and the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to the secondaries are also to th
137	3.7315	1.1622	0.050187	0.11642	1.2200	
147	3.5165	1. 1134	0.055592	0.11123	1.3500	
> 40 × 1 × 10 M	4 4455	AATIAC - FAI	ENOW INCE			
ח אויוא אלי	PL	Pt /P7	PI /PTF	PL /PTP	X/MAK	ORIG
127	4.2518	1.3350	0.066836	0.13372	-1.0000	~ ~ <b>~</b>
115	3.09[7	1.2539	0.062744	0.12554	<b>71.0300</b>	- <del> </del>
122	3.6515	1.1465	0. 057491	0.11485	-1.0000	O 7
127	<b>1.1384</b>	1.7664	0.053397	0.19692	-1.0000	
127	3.2015	1.1627	0.058187	0.12642	-1.0000	<u> </u>
145	3.578	1.1104	0.05559?	9611123	-1.0900	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
·1"?	3.7864	1.0633	0.053233	0.10651	-1.0000	
157	3. 3864	1.0633	7. 053233	0.10651	-1.3000	PAG
SAMPTTONS	AT PRESSUPE	RATTING FAI	T HITTELF FLAF			<u> </u>
VD WORD "	PI	PE /PH	N. 1888	P[ 7F YP	ZMMAT.	
152	3.3864	1.7633	2.057233	0.10651	-1.0900	$\sigma$
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27	14.323	4. 1475	0.21971	0.43431	2.43200
37	7. 7671	2. 3978	0,12963	0.24964	0.53000
47	9.0966	2.5083	0.1417R	0. 241 83	0.62900
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52	10.671	3. 2010	1. 14510	0.32936	0,42260
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AU RUBU	PL	PL /PO	PL /PTF	PL/PTP	X/DMAX
177	5.8174	1.7959	0,999349	0, 10024	9, £ 2499
112	3.6569	1.1289	0.056795	0.11330	J. F 3000
122	2.1759	0. 65631	0.023014	7.065367	
127	3.4419	1.0425	0.053454	0.19663	1.0900
137	3.4769	1.0733	0.053999	0.1077?	1.2200
147	3.5?49	1.0488	0.054775	0.10927	1.3500
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Gary nv	Pi	PI /PI	PL/PTF	PL /P TP	X/final/ -1,4600
107	5.8174	1.7959	0.090349	0-18024	-1.4500
112	3.6569	1.1289	0. 756 795	0. 1 1330	1.0000
122	2.1759	0.65631	0.233014	0.065867/	-1.0000
127	4418	1.0625	0.053454	0.10662	-1.0900
137	3.268	1.0733	0.053599	0. 19772	-1.0000
147	3.576	1.0666	0.054775	9010927	-1.000e
157	3.4519	1.0656	0. C5360°	0.10604	-1.0000
157	3.4518	1.0656	7.057679	0. 1.96.04	-1.0000
>40011104	A PPESSIBE	RATIOS FAI	* H77715 F1 45		
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172	7	1.0641	0.05353?	0.1 Cyse.	-1.0000
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37	A. ARA4	2. 1723	0.17441	0.24083	0.53300									
47	7.9316	7.4772	0.17229	0.27268	0.67500									
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12	9.2115	7. 854R	7.14384	0.3317#	0.42200									
+7	15.60#	4,8373	0.24373	0.56217	0. ( 9200									
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127	3.4197	1.0598	0,053349	0.12317	1.0990									
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	החד דניים ארב	PI	PI /PI	PL / PTF	PL /PTP	X\UMBX .				
	AVD 1997	PÌ	PL /PO 1-0423	PL /PTF 0=0522F3	PL /PTP 0.13555	X/0MAX -1-0000		· · · · · · · · · · · · · · · · ·		
. <b>.</b>	<i>,</i>		PL /PR 1.0423 2.97197	PL/PTF 0.0522P3 0.048712	Pt /PTP 0.13555 0.12629	*/DMA* -1.0000		* w . · · · · ·		

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NAS 1-1 FV I	c ballia	INAPY DATA	06/11/79	CADDELL	RFC 10/17/79 02:	03:42.339	FAC AREXL	PGM C034	PAU 18 PRG 1158
SANST TOPAC	AL PPESSIME	PATTOS . PP	MAPY PLING			········			
AVD HORC	ρį	P1 / P-1	PL /PTF	PI /PTP	X/DMAX				
72	15.753	4. 8552	0.21704	0.43672	0.43200	managadhari i agus jana mir mir mir mir mir mir mir mir mir mir	• "		
37	P.6793	2.4750	0.11956	0.24062	0.53000				
47	10.154	3,1797	0.13991	0.28151	J. 62900	to the same of			* *
52	10. 369	3, 1959	0.14787	0,29747	0.72700			<del></del>	
>4701T [0N	AL PRESSUPE	RATINS , FLO	SPLITTEP I	.n. ·				•	
AVD HORD	Pl	PL / PG	PI /PTF	PL /PTP	×/DMAY				
62	11.004	3.6690	7.16407	3.33902	9.42790				A 4 96
67	15.503	4.7792	0.21360	0.42979	0.69200				
>ADSITION	AL PRESSURE	RATIOS . FEE	W SPLITTEP C	. D.	arge videnav i ga	_			
GROW GVA	PL	PL /PG	PL /PTF	PI /PTP	X/DMAX				
77	28.492	4.7764	0.39242	0.78961	0.56400				•
82	8.8843	2.7392	9.12741	0.24630	0.63500				
~ 3	3,4754	1.0697	0.047921	0. 196222	0.69200			<del></del>	
SATORY TON	AL PRESSUPE	PATINS . EJ	CTO SKEDUD	ه بیدند کیدهد دیده در دوست					
AVD "HIRD"	Pl	PL / Pri	PL/PTF	PLIPTP	X/DMAX				and the second second second second
107	6.4634	1.9921	0.049052	0.17919	0.62400				
112	4.1766	1.2718	0.056855	0.11440	0.83000	<del></del>			
122	2.3945	7.73900	0.032991	0.066382	0.96000				
127	3,4554	1.0651	7.047614	0.045436	1.0900	والتنامس سبيل مهروا ووجاده	and the second of the second of	The second contract of	and the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contrac
13"	3.4963	1.2009	0.053683	0.10692	1.2270				
145	3.9514	1.2174	0.054442	0.10954	1.3500				
-21021110M	I MECCINE	AANAC , FA	FARM TALL						
AM HUBD	er.	P(751	PLIPTE	PL/TP	v žina sa		un i		
-127	6.4634	1.9921	0.04905?	0.17919	x/DM4# -1_0000				
-ji> 🔪	4.12/6	1.2718	7,356455	0.11447	1.3550		* + *** - * ** + - **		man the second to the
-i2'	2.3745	7.73700	0.032991	0.066392	-1.0000		_		
-127	4.4558	1.9651	0.047614	0.04594	-1.0000	<del></del>	<del>)</del>		
-177	3. 106.3	1.2)09	0.053683	0.10002	-1.0000	79.2	Ō.		
-147	3. 05N	1.2178	0.054442	0410954	-1-3050	7 mg 2	<b>5</b>		
-157	3.4504	1.0636	0.047545	0.095447	-1.0000	ರ್ಷ	1		
-157	7.455#	1.0651	0.047614	0.095816	-1.0000		<u> </u>	4	
						OF POOR	-		
/W.1311 ft. At	of bacazime	HATING FAR	FILAP			ော်			
AVP JEPD	PI	PL /PT >	M /PTF	PI /PTF	4/ <b>0</b> MA9	<u> </u>	•		
-157	3.4568	1.0434	0.047545	0.095667	-1.0000	> 2			
-1=7	7.455	1.3651	yr Srakir	0.095806	-1.3000	QUALIT			
SEABLE INC.	il belocibe	REMAY . 20	DER SHRPIM T	PEATING		<del></del>			
AND MIND	PI /	רקו אין	PI / PTF	AL IPTP	X/IMAX	. 03			
-16*	7.45	1.0451	7.047614	0.005804	-1.0000				
-177	3,4554	1.0651	0.047614	0.095,600	-1.0000				
שייין דן מייגל	नकारटाबन क	DR . PRIFAR	तहत डाल्स्यक र	IN: ATTING					
AVE SPEED	PE	oe\ Pl	PL/PTF	PL /PTP	X/DNAX	-			
-150	3.4359	1.0589	0.947339	0.095251	-1.0000				
	9 94 4	<b>ე</b> "ሳባኖለሳ	0.764513	0.08956 T	-1.0000				
A 97	3.73.16	THOUST WIDE		to 17 16. T	100000 /				

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	IZ BOEFIAE	MUDA LITA	06/11/79	CADDEII.	PEC 10/17/79 02:35:04.627	FAC MENT	PGM C034	500 1124 Miles 18
>90511167	AL PRESSURE	PATIOS . PRI	MARY PLUG					
NU AUSD	PL	PL/PO	PL/PTF.	PL/PTP	X/DMAX			
37	13.942	4.2314	7.18896	0.43508	9.43200	mer res q		
37	7.6405	2,3356.	0.10430	0.24070	0.53000			
47	A.9413	2.7332	0.12706	84148.0	0 500	# 17 g - 1 ## 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	• • • •	* **
52	9,1314	2.7913	0.12465	0.28767	9, 72700			
>ADDIT IDDA	IAL PPESSUPE	BATINS . FLM	H, SPI ITTEP I	• D•		**		** ** *
VO WOPD	PL	m /PO	PL/PTF	OL/PTP	X FIMAX			
<del>+2</del>	10.492	3.2772	0.14322	0.33053	0.42700	• •		. •
<u> </u>	15,457	4,7250	0.21107	0,44695	9.69200			
SUDITIONS	IAL PRESSIPE	RATIOS , FLO	K SPLITTER O	. 0.	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	*** ***** ******		
AU MUSE	Pì	PL/PO	PL / PIF	PL/PTP	x/max			
77	21. 740	A. 7855	0. 19233	0.90541	0.56400		**************	The second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the second section of the section of the second section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the secti
#?	8.9713	2.7424	0.12247	U. 28262	0.63500			
n2	3.4861	1.0656	0.047587	0.10982	0.69200			
>ADDIT FOR	IAL PRESSUPE	RATIOS . FJF	CTOP SHPOUR	Programme — hall-there adaptives and colorest de	e e e e e e e e e e e e e e e e e e e	man action only a majority of the		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
אר אראף	Pl	የር / የባ	PI /PIF	PL /PTP	x/DRAX			
107	6.4996	1.9938	0.988598	0.20444	0-62400			
112	4.1420	1.2461	0.056541	0.13049	0.83000			
122	2.4093	0.73650	0. C32589	0.075902	0.96000			
127	3.4710	1.0619	0.0473RZ	0.10935	1.0900	and the same of the same of the same of the same		
137	3.6?63	1.1085	0.049501	0.11474	1.5500			The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa
147	₹.4560	1.0565	0. 047177	0.10888	1-3500			
21001110N	AL PRESSURE	BATIOS . FOR	FROM IMET					
מחחשתע	Pt	PI / PO	PLIPTE	M /PTP	X /DMA X			a man a section of the section of
	6.4796	1.9938	0.088588	0.20444	-1.0400			
1117			0.054541	0.13049	-2.0000			and the same and arranged to the agreement of the case of the
	4.1420	1.7561						
112	4.1420	1.2461		0.075902	<b>/-1.0070</b>			
112		0.73653 1.0610	0.032889 0.047382	0.075902	-1.0079			
117 127 127	2.4093 9.4710 3.7263	0.736=0 1.0610 1.1085	0.032889 0.047382 0.049501	0.10935 0.11544	-1.0000 -1.0000			<del>,</del>
117 127 127 127 127	2.4793 3.4710 3.4763 3.4764	0.736=3 1.0610 1.1085 1.0565	0.032889 0.047382 0.049501 0.047177	0.10935 0.11574 0.10988	-1.00:00 -1.00:00 -1.00:00			
117 127 127 127 127 142 157	2.4993 2.4710 3.1263 3.4569 3.4760	0.736=0 1.0610 1.1085 1.0565 1.0626	0.032889 0.047382 0.049501 0.047177 0.047451	0.10935 0.11544 0.10988	-1.0000 -1.0000 -1.0000 -1.0000			
117 127 127 127 127 142 162 167	2.4993 3.4710 3.1263 3.4760 3.4760	0.736=0 1.0610 1.1085 1.0565 1.0626	0.032889 0.047382 0.049501 0.047177 0.047451 0.047451	0.10935 0.11574 0.10988	-1.00:00 -1.00:00 -1.00:00			
117 127 127 127 127 142 162 167	2.4993 3.4710 3.1263 3.4760 3.4760	0.736=0 1.0610 1.1085 1.0565 1.0626	0.032889 0.047382 0.049501 0.047177 0.047451 0.047451	0.10935 0.11544 0.10988	-1.0000 -1.0000 -1.0000 -1.0000			
112 122 127 127 137 142 152 157 240017 104	2.4993 3.4710 3.7263 3.4760 3.4760 41 PPESSIPE	0.736=0 1.0610 1.1085 1.0565 1.0526 1.0626	0.032889 0.047382 0.049501 0.047177 0.047451 0.047451 W0771F TAP	0.10935 6.1194 0.10961 0.10951	-1.0000 -1.0000 -1.0000 -1.0000			
112 122 127 127 127 142 142 152 167 DAPPIT ION VO. WORD	2.4993 3.4710 3.4263 3.4760 3.4760 41 PPESSIPE	0.73650 1.0610 1.1085 1.0565 1.3626 1.3626 RATION, FAH	0.032889 0.047382 0.049501 0.047177 0.047451 0.047451 W0771F TAP	0.10935 0.1194 0.10988 0.10981 PL/PTP 0.10981	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
112 122 127 127 127 142 142 152 167 DAPPIT ION VO. WORD	2.4993 3.4710 3.7263 3.4760 3.4760 41 PPESSIPE	0.736=0 1.0610 1.1085 1.0565 1.0526 1.0626	0.032889 0.047382 0.049501 0.047177 0.047451 0.047451 W0771F TAP	0.10935 6.1194 0.10961 0.10951	-1.0000 -1.0000 -1.0000 -1.0000			
112 122 127 127 142 152 157 240717 ION VO WORD 152	2.4993 3.4710 3.4263 3.4760 3.4760 41 PPESSIPE	0.73650 1.0610 1.1085 1.1085 1.3626 1.3626 RATION, FAH PL/MG 1.0626	0.032889 0.047382 0.049501 0.047177 0.047451 0.047451 W0771F TAP	0.10935 0.1194 0.10951 0.10951 0.10951 0.10951 0.10951	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
112 127 127 127 127 142 152 157 247717 ION VO MORO 152 157	2,4993 3,4710 3,4760 3,4760 3,4760 MI PPESSIPE ( 3,4760	0.73650 1.0610 1.1085 1.1085 1.3626 1.3626 RATION, FAH PL/MG 1.0626	0.032889 0.047382 0.049501 0.047177 0.047451 0.047451 WM771F TAP 0.047451 0.047451 0.047451	0.10935 0.1194 0.10951 0.10951 0.10951 0.10951 0.10951	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
112 122 127 127 142 152 152 167 VO WORD 152 157 VO WORD 167	2.4993 3.4710 3.4760 3.4760 3.4760 MI PPESSIPE ( 3.4760 MI PPESSIPE ( 3.4760	0.73650 1.0610 1.1065 1.1065 1.0626 1.0626 RATION, FAM PL/MG 1.0626 RATION, 20 (	0.032889 0.047382 0.047501 0.047177 0.047451 0.047451 0.047451 0.047451 0.047451 0.047451	0.10935 0.1194 0.10951 0.10951 0.10951 0.10951 0.10951 0.10951	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
112 127 127 127 127 142 152 157 VO WORD 152 157 VO WORD 167 167	2.4993 3.4710 3.4760 3.4760 3.4760 41 PPESSIPE 1 3.4760 41 PPESSIPE 1 3.4760 41 PPESSIPE 1 3.4760	0.736=0 1.0610 1.1085 1.1085 1.0565 1.0626 RATITY FAM PL/MG 1.0626 RATITY 20 1	0.032889 0.047382 0.049501 0.047177 0.047451 0.047451 0.047451 0.047451 0.047451 0.047451 0.047451 0.047451	0.10935 0.11945 0.10951 0.10951 0.10951 0.10951 0.10951 0.10951 0.10951	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
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የለሁ ብርፁሁ	PL	ቦ! / ቦባ	PL/PTF	PL /PTP	x/DMAX			
37	17.477	7,7597	0.16861	0.43614	0.43200			
77	6.8615	2.0823	0.093138	0.24094	J.53000			
47	8.0391	2.4393	0.17911	0.29225	0.62900			
57	P.1993	2,4979	9-11129	0.2P788	<u>0.72790</u>			
SAUDITIONAL	PRESSIPE	MATINS . FLE	UM ZEFTALE T	·n•				
LVD HUSD	PL	ML/PA	PL/PTT	PL /PTP	X/DMAX			
67	9.4707	2. 85 86	0.12796	0.33076	U-42209			
6.7	15.405	4. 4744	0.20908	0.54987	<u> ጉ. € 9200</u>			
>ADDITIONAL	PRESSIME	PATERS . FU	OM SPLITTEP O	. De.				
NO MOPO	PL	<b>94 / P</b> ()	PL /PTF	PL /PTP	X/D#AX			
77	24.932	n. 7788	0.39766	1.0158	0.56400	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		
<b>P</b> 7	9.0303	2.7401	0.12756	0.31705	0,63500			
οZ	3.5167	1.9571	0.047728	0.12347	0.69200			
וארחן דומראכ	PRESSIRE	RATINS . FJ	CTOP SHPOUD		The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th		· / · · · ·	
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113	4.1680	1.2647	0.056567	0.14634	0.43000			
127	2.4301	0.74016	0.737106	0.085642	0.96000			
127	3.4966	T. 06 ID	0. (47458	0.12274	1.0900			
127	3.4966	1.0610	0.047456	0.12276	1.2200			
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WA WIRE	PI	PL /PN	PL/PTF	PL /PTP	X/OMAX		5€	
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-115	4. [675	1. 2647	0.056557	C.14634	-56000		26	
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-137	396398	1.0610	U. 047456	0.12276	-1.0000		<b></b>	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t
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157	3.5066	1.0540	0.047592	12312	-1.0000			-
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	ř1 /	M 707	PL/PTF	M 1010	X/DMAX	•	• • • •	Minds on said
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	CAUP OAL	PL	PL /PI	M/b4k	PI /PTP	X/DMAX		
	32	17-845	5.3977	9.21789	0.43713	0.43200	ala :	
	27	5.9137	2. 96.84	0.11977	0.24039	0.53000		*·* **
	47	11.449	3.4749	0.14021	0.28142	2.62900		* * * * * * * * * * * * * * * * * * * *
	52	11.743	3,5520	0.14333	0.20766	0.72700		
	>+ODITIONA	L PRESSURE	PATITS . FIT	W SPLITTER L	. De			
	AVP WIRD	. PL	PL/PD	M/PTF	PI /PTP	x/DMAY		se de la companya de la companya de la companya de la companya de la companya de la companya de la companya de
	F.3	17.503	4.0847	0.16480	0.33076	9-42700		
		15.352	4.6435	0.18737	0.37605	0.69200		
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	AVP WEED	PL	PL / PO	PI / PTF	PL/PTP	x/OMAT	_	
	77	31.935	9.4592	0.38975	0.70225	0.56400		
_	82	10,019	3,0334	2.12279	0.24541	0,63500		
	97	3.5359	1.0695	0.043154	0.086613	J.6920J		
	>ADDITIONA	L PRESSIPF	PATINS . FJF	CTOP SHOPED			<b></b>	gradient de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la
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	197	7,1483	2.1622	9.0R7244	0.17510	0. 62400		
	117	4.6769	1.4146	0.057021	0.11456	U.#3000		
	12?	2.6959	0.81664	0.032952	0.066136	0.96000		
	127	2.5159	1.0634	0.047713	0.06122	1.0900		
	177	4.4117	1.3344	0.053844	0.10007	1.2200	in alconomic with a second of the second	e comme to a series experience of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of th
	142	4.4717	1.3526	0.054477	0. 10954	1.3500		
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	URUS. MAN	PI	PI /PO	PL / PTF	PL /P TP	X/DMAX	• · · · · · · · · · · · · · · · · · · ·	who was the state of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
	-107	7.1483	2.1622	0.097244	0.17510	-1.9200		
	-112	4.6769	1.4145	0. (57(9)	0.11456	-1.0nee	The second of the second of the second of	AND THE REAL PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE P
	-172	7.6999	0.21664	0.032952	0.066136	1.0000		
	-177	3.5159	1.0634	0.047910	0.0M123	-1.0000		
	-127	456113	1.3344	0.053844	0.1 CP#1	-1.0000		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
	-142	4.477	1.3526	0.054577	0.10954	-1-0000		
	-15?	3.5159	1.0634	0. 347910	D.086125	-1.0000		The same of the case of the same same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of t
	-! 57	3.5158	1.0634	0. 242910	0.006155	-1.0000		
_	APPITTIPAL	I PPF SSIJOE	RATING FAR	POTTE FLAT	· · · · · · · · · · · · · · · · · · ·			
	מעט אניפט	PI	mi / inn	PEINT "	PL/PTP	×/PHÁX	The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th	
	-15?	7.5158	1.0634	C.047913	0.0%122	-1.0000		and a section compared by the company of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the c
	-1=7	3.5159	1.0634	0.647910	0.046122	-1.6076		
	>27717101M	1 PPFSSIPF	PATION . 70	DEC CHANGE	OCATION			
	AVD 4PPD	PL	PI PPO	" PR/PTF"	Q /PTP	X/DMAX		
		2.5159	1.0634	0.642910	C-Q#6127	~1.000C	_	•
	-167	3.51 PA	1.0634	0.642910	0.000155	-1.0000		
-	-167 -177			REC SUFFIRM T	DETAILM >			
		नवारशक्त	PATTICE - 40	,, 51, 1				
-	-177	नवा <i>ग्रह</i> नको ११	**************************************	in /oth	PL /PTP	HAMMAH		
_	-17: 5467   7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7				Pt /PTP 0.089432	X/MAX -1.0000		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s

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29	15.407	4.6532	0.18771	0.43533	J. 43200
37	8.4962	7.5460	0.17373	0.24006	0. 53000
47	5.9519	3.0356	J. 12002	0.24119	0.62900
52	19.152	3.3660	0.12335	0.28684	1. 72703
Milet Elecak	I PRESSURE	RATIOS . FLO	W SPLITTER I	n. , ,	
AVD HEED	Pt	PL/PN	PL /PTF	PL /PTP	x/DMAX
62	11.647	3. 51 76	0.14152	0.32909	0-42200
67	15.327	4.6790	0.18624	0.43307	0.69200
SAUDITIONA	L PRESSIRE	RATIOS , FLO	W SPLITTER (	. 0.	in the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of
AVD WORD	PI	PL / PO	PE / PTF	PL /PTP	X/DMAX
77	37.062	9.6431	0.38957	0.90590	0.50400
92	10.077	3.0434	0.12744	0.28472	0.63500
97	2,5213	1.0635	0.042786	0.099493	0.69200
>APPLY TOUA	I PPFSSURF	RATIOS . FJF	CTOP SHROW		
LYD WOPD	PL	PI / P(1	PI / PTF	PL/PTP	Y/CMAX
107	7.1803	2.1686	0.087245	0.20288	0.62400
117	4.7070	1.4216	U.C57203	0.13302	U. A 3 1000
127	2.7100	0. 81 846	0.032928	0.076571	
127	3.5063	1.0580	0. 647603	0. 09406	
137	4.0871	1.2344	0.049660	0.11548	1.7200
142	3. 8568	1.1648	0.046762	C. 10847	1.3500
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NA MENERAL	P1	PL /PO	PL/PTF	PL/PTP	X/TMAX
-197	7.1803	7.1686	7.087245	0.20788	-1,4000
					The first transformation of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the cont
-117	4.7079	1.471	0. C57203	0.13302	<b>71.3000</b>
-122	2.7100	0.81946	0.032978	0.13302 0.076571	1.2000
-127 -127	2.7100	0.81846 1.0589	0.032928 0.042603	0.076571	
-127 -127 -137	2.7100 5063 4.0471	0.81846 1.0589 1.2344	0.03252R 0.042603 0.049660	0.076571 0.099048 0.11448	-1.0000 -1.0000 -1.0000
-127 -127 -137 -142	2.7100 3.5063 4.0471 3.4564	0. 81 946 1. 05 89 1. 23 44 1. 16 48	0.032578 0.042603 0.049660 0.646662	0.076571 0.009014 0.1144 0.16497	-1.0000 -1.0000 -1.0000 -1.0000
-127 -137 -137 -142 -152	2.7100 3.5063 4.0471 3.8563	0. 81 946 1. 05 89 1. 23 44 1. 16 48 1. 05 89	0.032578 0.042603 0.049660 0.64662 0.042603	0.076571 0.009018 0.1148 0.099068	-1.0000 -1.0000 -1.0000 -1.0000
-122 -137 -137 -142 -152	2.7100 3.5063 4.0471 3.4564	0. 81 946 1. 05 89 1. 23 44 1. 16 48	0.032578 0.042603 0.049660 0.646662	0.076571 0.009014 0.1144 0.16497	-1.0000 -1.0000 -1.0000 -1.0000
-122 -127 -137 -142 -152 -157	2.7100 9.5063 4.0471 3.4523 3.5063 7.5113	0.81846 1.0589 1.2344 1.1648 1.0589 1.0605	0.032578 0.042603 0.049660 0.64662 0.042603	0.076571 0.009018 0.1148 0.099068	-1.0000 -1.0000 -1.0000 -1.0000
-127 -137 -137 -142 -157 -157 -25751717444	2.7100 5063 4.0471 3.6763 2.5063 2.5113	0. 81 946 1.05 89 1.2344 1.16 48 1.05 89 1.06 05 RAYINS FAR	0.03257R 0.042603 0.049660 0.64660 0.042603 0.042603 0.042655 NC77LL FLAP	0.076571 0.0090JA 0.114A 0.1049 0.0099069 0.0099069	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-127 -137 -137 -142 -152 -157 -2575177648 AVO MOPO -152	2.7100 5063 4.0471 3.4571 3.5063 7.5113 1 PPESSIPE Pt 3.5063	0. 81 946 1. 05 89 1. 23 44 1. 16 48 1. 05 89 1. 06 05 RAYINS FAR M / Ph 1. 05 89	0.03297R 0.047607 0.047607 0.04760 0.042607 0.042607 0.042607 0.042603	0.076571 0.089378 0.1146 0.16897 0.099068 0.099210	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-127 -137 -142 -167 -167 -167 -2001777046	2.7100 5063 4.0471 3.6763 2.5063 2.5113	0. 81 946 1.05 89 1.2344 1.16 48 1.05 89 1.06 05 RAYINS FAR	0.03257R 0.042603 0.049660 0.64660 0.042603 0.042603 0.042655 NC77LL FLAP	0.076571 0.0090JA 0.114A 0.1049 0.0099069 0.0099069	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-127 -137 -142 -142 -157 -275171744A	2.7100 4.5063 4.0471 3.5063 2.5113 1 PPESSIPE PL 3.5063 3.5113	0. 81 946 1.0589 1.2344 1.1648 1.0589 1.0685 RAYINS FAR 9 /80 1.0589	0.03297R 0.047607 0.047607 0.04760 0.042607 0.042607 0.042607 0.042603	0.076571 0.09904 0.1148 0.1689 0.099068 0.099068 0.099068 0.599210	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-127 -137 -142 -142 -157 -157 -157 -157 -157 -157 -157 -157	2.7100 \$ 5063 4.0471 3.652 3.5063 3.5113 II PRESSIRE PL 3.5063 3.5113	0. 81 846 1.0589 1.2344 1.1648 1.0589 1.7605 RATIOS FAR M /Ph 1.0589 1.7605 WATER 20	0.03247R 0.042603 0.044660 0.042603 0.042603 0.042603 0.042603 0.042603 0.042603	0.076571 0.09904 0.1144 0.16497 0.099068 0.099068 0.099068 0.099068	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
-127 -137 -142 -142 -157 -157 -2470177744 AVO MORP -152 -2770177744 AVO MORP -167	2.7100 5063 4.0471 3.452 3.5063 3.5113 H PPESSUPE PL 3.5063 3.5113 H PPESSUPE PL 3.5063 3.5113	0. 81 946 1.05 89 1.2344 1.1648 1.05 89 1.06 05 RAYINS FAR PLOS PAR 1.05 99 1.76 05 PLOS PAR 1.04 05	0.03247R 0.042603 0.049660 0.042603 0.042603 0.042603 0.042603 0.042603 0.042603	0.076571 0.0090/A 0.114A 0.16897 0.099068 0.099068 0.099068 0.599210	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
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-127 -137 -142 -142 -157 -157 -277 -277 -277 -277 -277 -277 -277 -2	2.7100 \$5063 4.0471 3.4572 3.5063 3.5113 11 MPFCSUPE Pl 3.5063 3.5113 11 MPFCSUPE Pl 3.5113	0. 81 846 1.0589 1.2344 1.1648 1.0589 1.0605 RAYINS FAN 1.0589 1.7609 FAYINS 70 PL/PR 1.0405 1.0574	0.03247R 0.042603 0.049660 0.042603 0.042603 0.042603 0.042603 0.042603 0.042664 0.042644 0.042644	0.076571 0.009048 0.1148 0.16897 0.099068 0.099068 0.099068 0.399210	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
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NOT 40PO PL 17.70 PL/PT PL/PTP X/DMAX 29 9,9919 3,0393 0,1222 0,11707 0,55500 30.11113 1,0ARO 0,02POS 0,111142 0,69200 30.11113 1,0ARO 0,02POS 0,111142 0,69200 30.11113 1,0ARO 0,02POS 0,111142 0,69200 30.11113 1,0ARO 0,02POS 0,111142 0,69200 30.11114 1,0ARO 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02POS 0,02	SAPOTT TON	AL PRESSURE	RATIOS . FLO	W SPLITTER P	, n,	
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92 3,913 1.0440 0.047923 0.11142 0.69200  >ANDITIONAL PRESSURE RATIOS , FJECTUR SHRIGHT  NOT YORRO PL 107 7,1503 2.1749 0.007474 PL/PTP X/DRAX 112 4.7329 1.4336 0.07511 0.15015 0.96200  112 4.7329 1.4336 0.07511 0.15016 0.96000  122 3,4912 1.0619 0.08714 0.085360 0.96000  123 3,4912 1.0519 0.08714 0.1079 1.2000  124 3,4912 1.0519 0.08714 0.1237 1.2200  125 3,4912 1.0519 0.08714 0.1237 1.2200  126 3,4912 1.0519 0.08714 0.1237 1.2200  127 3,4914 0.1762 0.977415 0.1237 1.2200  128 3,4912 1.0519 0.082190 0.1842  NAMONITIONAL BREESCHEE RATIOS SOCIEMON IMLEX  NOT THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF THE PLANT OF		21.422				
3, \$113						
DARDITIONAL PRESSURE RATIOS , FUFCTOR SURGUD  VON YORD PL 107  7,1503  2,1749  0,0874.09  0,225.00  0,62400  117  4,7129  1,6396  0,675.01  0,15019  4,63029  127  2,6000  0,81822  0,032914  0,085360  0,96003  127  3,4912  1,0019  0,06718  3,11079  1,0500  127  3,4914  1,1792  0,947435  0,12297  1,2200  142  3,4812  1,0019  0,06295  0,11047  1,3500  ADDITIONAL ABESSURE RATIOS , EDERATOR IMET  VON HOPE PL 107  7,1503  2,1749  0,07460  0,22690  1,0000  112  4,7379  1,4396  0,079910  0,15019  2,0000  112  4,7379  1,4396  0,074910  0,15019  2,0000  112  4,7379  1,4396  0,074910  0,15019  2,0000  112  4,6902  1,0019  0,462714  0,11079  1,0000  112  1,4692  1,0619  0,462714  0,11079  1,0000  117  4,4912  1,0619  0,462714  0,11079  1,0000  147  3,4603  1,0038  0,042455  0,26007  1,0000  147  3,4603  1,0038  0,042455  0,26007  1,0000  147  3,4603  1,0038  0,04275  0,26007  1,0000  147  3,4603  1,0038  0,04275  0,11094  1,0000  147  3,4603  1,0038  0,04277  0,11094  1,0000  147  3,4603  1,0038  0,04277  0,11094  1,0000  147  3,4603  1,0038  0,04277  0,11094  1,0000  147  3,4603  1,0038  0,04277  0,11094  1,0000  147  3,4603  1,0038  0,04277  0,11094  1,0000  147  3,4603  1,0038  0,04277  0,11094  1,0000  147  3,4603  1,0038  0,04277  0,11094  1,0000  147  3,5013  1,0650  0,042040  0,11110  -1,0000  2200110044  PRESSURE RATION  20 PRE SURFOR INFANTION  VON HARD PL 107  1,0550  0,042040  0,11110  -1,0000  VON HARD PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20 PRESSURE RATION  20						
NON WORD PL MI/PO MI/PTF PL/PTP X/DMAX  107 7-1503 2-1749 0.0874-09 0.226-90 0.624-00  112 4.7129 1.439-0 0.675191 0.15019 4.8307/0  127 2.6900 0.81822 0.0327-16 0.085360 0.96003  127 3.4912 1.0619 0.042710 3.11079 1.0500  127 3.4912 1.0569 0.0427-9 0.11047 1.3500  AMOUSTIONAL RESCUES BATIOS COMERCON LIMES  NON HOPP PL MI/PP MI/PTF PL/PTP X/DMAX  107 7-1503 2-1749 0.087360 0.226-90 -1-99900  112 4.7329 1.4394 0.07913 0.15019 -1.0000  127 2.6900 0.81822 0.032914 0.085369 1.00000  127 4.912 1.0619 0.042719 0.10791 -1.0000  127 4.912 1.0619 0.042719 0.10791 -1.00000  127 3.468 1.1792 0.0474-35 0.12392 -1.00000  144 3.4681 1.0549 0.042755 0.7104 -1.00000  145 3.4681 1.0549 0.042755 0.7104 -1.00000  147 3.4683 1.0649 0.042755 0.7104 -1.00000  147 3.4683 1.0649 0.042755 0.7104 -1.00000  147 3.4683 1.0649 0.042755 0.7104 -1.00000  147 3.4683 1.0649 0.042755 0.7104 -1.00000  147 3.5013 1.0659 0.042775 0.11094 -1.00000  147 3.5013 1.0659 0.042775 0.11094 -1.00000  147 3.5013 1.0659 0.042775 0.11094 -1.00000  147 3.5013 1.0659 0.042775 0.11094 -1.00000  147 3.5013 1.0659 0.042779 0.11094 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000  147 3.5013 1.0659 0.042780 0.11110 -1.00000	SADOTÝ ŘÓM	A ADECC: ME	BA7105 E 16	c Ton Cumpum		
107 7.1503 2.1749 0.0874889 0.22690 0.622400 117 4.7329 1.4349 0.067591 0.15019 4.83079 127 2.4900 9.81822 0.032914 0.085360 0.96003 127 3.4912 1.0569 0.042795 0.11079 1.0500 127 3.4912 1.0569 0.042595 0.11047 1.3500  ***MANDITIONAL RESSURE ANTOS COSERDOY LAGE**  WINDOWN PI PI PI/PN 9/PTF PI/PTF			KATENS + MUC	CALL SHARING		
117						
127						0.62400
127 3.4912 1.0619 0.02718 3.11079 1.2000 127 3.4747 1.1722 0.247435 0.12307 1.2200 142 3.4712 1.0669 0.042795 0.11047 1.3500  ADDITIONAL BRESSURE RATIOS FOREADON IMEN  WHIPPY PI PI PY PI PI PI PI PI PI PI PI PI PI PI PI PI						
127 3.4876 1.1792 0.487435 0.12392 1.2200 142 3.4812 1.0569 0.042595 0.11047 1.3500  MONOTIONAL BRESSURE RATIOS FOREMON IMET  WINDOWN PL M/PM M/PM M/PM 0.22690 -1.0600 112 4.7379 1.43396 0.087913 0.15019 -2.0000 112 4.7379 1.43396 0.087913 0.15019 -2.0000 112 4.9320 0.81822 0.032914 0.085394 -1.0000 127 4.912 1.0619 0.767718 0.11079 -1.0000 127 4.912 1.0619 0.767718 0.11079 -1.0000 147 3.406 1.1792 0.047435 0.12392 -1.0000 147 3.406 1.1090 0.047435 0.12392 -1.0000 147 3.406 1.1090 0.042755 0.1004 -1.0000 147 3.406 1.1059 0.042755 0.11004 -1.0000 147 3.406 1.0635 0.042740 0.11110 -1.0000  DEDITIONAL PRESSURE PATION FAM MOVILE FLAP  WIN MYSH PL M/PM M/PM PATION 0.11094 -1.0000 157 3.5013 1.0650 0.042740 0.11110 -1.0000  DANDITIONAL PRESSURE BATION 2.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 1.0659 0.042740 0.11110 -1.0000  DANDITIONAL PRESSURE BATION 2.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 2.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 2.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 2.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN MAPP PL M/PM PATION 3.00 DEG SURPON (MCATION)  WIN M/PM PATION 3.00 DEG SURPON (MCATION)  WIN M/PM PATION 3.00 DEG SURPON (MCATION)  WIN M/PM PATION 3.00 DEG SURPON (MCATION)  WI						0.96003
14-7 3.4812 1.0589 0.042595 0.11047 1.3500  AADDITIONAL BRESSURE RATIOS FOREADON INLEY  WOLLDON PL 107 7.1503 2.1749 9.07480 0.22690 -1.9000 112 4.7379 1.4596 0.057910 0.15019 -2.0000 112 2.6900 0.81822 0.032914 0.085349 -1.0000 127 4.4912 1.0019 0.767714 0.11079 -1.0000 127 3.408 1.1792 0.047435 0.12392 -1.0000 147 3.408 1.0589 0.04255 0.27027 -1.0000 149 3.4083 1.0635 0.042779 0.11094 -1.0000 157 3.4093 1.0635 0.042779 0.11094 -1.0000 157 3.5013 1.0650 0.042779 0.11094 -1.0000  AADDITIONAL PRESSURE PATION, FAN WORTLE IAP  WOUNDED PL 4043 1.0635 0.042779 0.11094 -1.0000  ADDITIONAL PRESSURE BATION 2.006 SWRTON INTATION  WOUNDED PL MIPPO PLYPT V/ONAX  AND WITHOUT PRESSURE BATION 2.006 SWRTON INTATION  WOUNDED PL MIPPO PLYPT V/ONAX  177 3.5013 1.0650 0.042840 0.11110 -1.0000  AND WITHOUT PRESSURE BATION 2.0062840 0.11110 -1.0000  AND WITHOUT PRESSURE BATION 3.0062840 0.11110 -1.00000				0.04271R		
ADDITIONAL ARESSURE RATIOS FOREROW IMES  VICULOPO PL PL/PO PL/PTP PL/PTP X/DMAX  107 7-1503 2-1749 0,071910 0.15019 1.0000  112 4.7379 1.4396 0.071910 0.15019 1.0000  112 2.6900 0.81822 0.032914 0.00534-0 1.0000  127 1.9012 1.0610 0.767714 0.11079 1.0000  127 1.912 1.0610 0.767714 0.11079 1.0000  127 3.450 1.1792 0.047435 0.12372 1.0000  147 3.4611 1.0589 0.042555 0.1047 1.0000  147 3.4611 1.0589 0.042779 0.11094 1.0000  147 3.4613 1.0650 0.042779 0.11094 1.0000  22011Y[ONAL PRESSURE PATION, FAN WOYZEFLAP  WOUNDED PL PL/PO PL/PTP N/DMAX  157 3.4963 1.0635 0.942779 0.11094 -1.0000  2ADDITIONAL PRESSURE FATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PO PL/PTP Y/DMAX  147 3.5013 1.0650 0.042840 0.1110 -1.0000  2ADDITIONAL PRESSURE FATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PO PL/PTP Y/DMAX  147 3.5012 1.0650 0.042840 0.1110 -1.0000  2ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PO PL/PTP Y/DMAX  147 3.5012 1.0650 0.042840 0.1110 -1.0000  2ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  147 3.5012 1.0650 0.042840 0.1110 -1.0000  2ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  2ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  2ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  2ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  2ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  2ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  ADDITIONAL PRESSURE PATION, 70 DEG SURCON (TRATION  WOUNDED PL PL/PTP Y/DMAX  ADDITIONAL PRESSURE PATION (TRATION  PL/PTP Y/DMAX  ADDITIONAL PRESSURE PATION (TRATION  PL/PTP Y/DMAX  ADDITIONAL PRESSURE PATION (TRATION  PL/PTP Y/DMAX  ADDITIONAL PRESSURE PATION (TRATION  PL/PTP Y/DMAX  ADDITIONAL PRESSURE PATION (TRATION  PL/PTP Y/DMAX  ADDITIONAL PRESSURE PATION (TRATION  PL/PTP Y/DMAX  ADDITIONAL	127	3.8768	1.1792	0.047435	0.12392	1,2200
Minuson PI MI/PO MI/OTE PI/PTP Y/DMAY 107 7.1503 2.1749 0.007460 0.22690 -1.0000 112 4.7379 1.4596 0.057910 0.15019 -2.0000 112 2.6900 0.41822 0.032914 0.003340 1.0000 127 4.912 1.0619 0.767714 0.11079 -1.0000 127 3.4076 1.1792 0.647435 0.12372 -1.0000 142 3.4678 1.0599 0.042455 0.10647 -1.0000 145 3.4678 1.0599 0.042779 0.11094 -1.0000 147 3.5013 1.0635 0.042779 0.11094 -1.0000 147 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042779 0.11094 -1.0000 157 3.5013 1.0655 0.042790 0.1110 -1.0000 157 3.5013 1.0655 0.042790 0.1110 -1.0000 167 3.5013 1.0655 0.042790 0.1110 -1.0000 167 3.5012 1.0655 0.042790 0.1110 -1.0000	147	3.4812	1.0569	0.042595	0.11047	1,3500
107 7.1503 2.1749 9.087890 -1.0800 112 4.7379 1.4396 0.087910 0.15019 -2.0000 112 2.6900 0.81822 0.032914 0.085369 1.0000 1127 4.4912 1.0619 0.96.7718 0.11079 -1.0000 1127 3.4912 1.0619 0.96.7718 0.11079 -1.0000 1147 3.4612 1.0589 0.042755 0.2007 -1.0000 1149 3.4612 1.0589 0.042779 0.11094 -1.0000 1152 3.4943 1.0635 0.042779 0.11094 -1.0000 1157 3.5013 1.0635 0.042779 0.11094 -1.0000 128011 [INNAL PRESSURE PATION FAN NOTITE FLAP 1157 3.5013 1.0635 0.962779 0.11094 -1.0000 1157 3.5013 1.0635 0.962779 0.11094 -1.0000 1157 3.5013 1.0635 0.962779 0.11094 -1.0000 1157 3.5013 1.0635 0.962779 0.11094 -1.0000 1157 3.5013 1.0650 0.962779 0.11094 -1.0000 1157 3.5013 1.0650 0.962840 0.11110 -1.0000 1157 3.5013 1.0650 0.962840 0.11110 -1.0000	PAUDIT TON	20122300 14	BATIOS . FOR	EARDY INLEY		
107   7,1503   2,1744   7,08748   0,087910   0,15019   1,0606     112   4,7379   1,4536   0,087910   0,15019   1,0006     112   2,6900   0,81822   0,032914   0,085369   1,0000     112   2,6901   1,0619   0,767718   0,11079   -1,0000     112   3,4912   1,0619   0,047435   0,12392   -1,0000     1147   3,4872   1,0589   0,042755   0,21057   -1,0000     1157   3,4993   1,0635   0,042779   0,11094   -1,0000     1157   3,5013   1,0635   0,042740   0,11110   -1,0000     1252   3,4943   1,0635   0,962779   0,11094   -1,0000     1252   3,4943   1,0635   0,962779   0,11094   -1,0000     1253   3,4943   1,0635   0,962779   0,11094   -1,0000     1254   3,4943   1,0635   0,962779   0,11094   -1,0000     1257   3,5013   1,0635   0,962840   0,11110   -1,0000     127   3,5013   1,0635   0,962840   0,11110   -1,0000     127   3,5012   1,0650   0,962840   0,11110   -1,0000     127   3,5012   1,0650   0,962840   0,11110   -1,0000     127   3,5012   1,0650   0,962840   0,11110   -1,0000     128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   128   12						
112 4.7379 1.4396 0.057910 0.15019 -X0000 122 2.6902 0.41822 0.0332914 0.085364 1.00000 127 1.4912 1.0619 0.967718 0.11079 -1.9000 127 3.496 1.1792 0.047435 0.12372 -1.0000 127 3.496 1.1792 0.047435 0.12372 -1.0000 142 3.4612 1.0589 0.042755 0.34047 -1.0000 145 3.4963 1.0635 0.042779 0.11094 -1.0000 147 3.5013 1.0650 0.042840 0.11110 -1.0000  >20011 (ONAL PRESSURE PATION, FAN HOPPLE FLAP  WOUNDED PL PLAPS 0.042779 0.11094 -1.0000  >20017 (ONAL PRESSURE PATION, FAN HOPPLE FLAP  WOUNDED PL PLAPS 0.042779 0.11094 -1.0000  >20017 (ONAL PRESSURE PATION, 20 DEC SHROW OFFATION  NOT WORD PL PLAPS 0.042840 0.11110 -1.0000  >20017 (ONAL PRESSURE PATION, 20 DEC SHROW OFFATION  NOT WORD PL PLAPS 0.042840 0.11110 -1.0000  >20017 (ONAL PRESSURE PATION, 80 DEC SHROW OFFATION)  NOT WORD PL PLAPS 0.042840 0.11110 -1.0000  >20017 (ONAL PRESSURE PATION, 80 DEC SHROW OFFATION)  NOT WORD PL PLAPS 0.042840 0.11110 -1.0000						17(max
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37	0,2410	7,8257	0.10316	0.24021	0.53000			
47	1).043	7.3219	3.125AP	0.28139	J. 626-90			
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107	7,7954	2.3663	0.086109	0.20045	0.62400			
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127	3.5044	1.063A	0.036709	0.090111	1.0900			
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(N 446U	PI 3.5094 3.5144	1.0653	Q. 03#764	0.090240 0.090368	-1.0000			
/N WYPN  57  57  407      101	P1 3.5094 3.5144 AI PRESSURE	1.0653 1.3668 AAYJAS . 20	DEG SHROUN II	0.090240 0.090368 TCATION	-1.0000			
/N WYPN   57   67   6409   7   10     70 WYPN   167	PL 3.5094 3.5144 AL PRESSUME PL 3.5094	1.0653 1.3668 AAYIMS . 20 PL/PIP 1.0653	DEG SHROUP II	0.090240 0.090368 TATION PL/PTP 0.090240	-1.0000 -1.0000			
/(D HYPP()   57   40つすず   口見  (D HYPP()   167	P1 3.5094 3.5144 AI PRESSURE	1.0653 1.3668 AAYJAS . 20	DEG SHROUN II	0.090240 0.090368 TCATION	-1.0000 -1.0000			
/N WYPN  57  67  ANYTHINN  N WYPN  67  72	Pt. 3.5094 3.5144 AI. PRESSUME Pt. 3.5094 3.5044	1.0653 1.3668 RATIAS . 20 PL/PIN 1.0653 1.0638	DEG SHROUP II	0.090240 0.090368 TEATION TO PTP 0.090240 0.090240	-1.0000 -1.0000 X/00AX -1.0000			
/N WYPN   627   57   57   62741   1011   167   172   6674   144	PL 3.5094 3.5144 AI PRESSUME PL 3.5094 3.5044 W PRESSUME	1.0653 1.3668 AAYIAS . 20 PQ / PRO 1.0653 1.0638	0. 038764 0. 038825 DEG SHRCUM (1) PI / PYF 0. 038764 9. 038700	0.090240 0.090368 TEATION PL/PTP 0.190240 0.090111	-1.0000 -1.0000 X/NPAX -1.0000 -1.0000			
VN 49PN 157	Pt. 3.5094 3.5144 AI. PRESSUME Pt. 3.5094 3.5044	1.0653 1.3668 RATIAS . 20 PL/PIN 1.0653 1.0638	0. 038764 0. 038825 DEG SHREUM I PI / PYF 0. 038764 0. 038769	0.090240 0.090368 TEATION TO PTP 0.090240 0.090240	-1.0000 -1.0000 X/00AX -1.0000			

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	C	INARY DATA	06/11/79	CADDELL	PEC 10/17/79 02:13:34.631	FAC ANAX1	PGP C034	ROW 18
VASA-I FUI		•		· krast 1	+40 TALTILLA 05:13:14*221	FRI. #49A.E	F9F 1.039	RDG 1166
2600111114	AL PRESSIRE	PATINS . PRI	MARY PLUI.					
TAU MUEU	PI	PL /PO	PI /PTF	PI /PTP	X/DMAX			
32	15.344	4.6290	0.1677	0.43414	9.43209			
3*	<b>4,4</b> 55)	7.5512	7.697456	0.24033	J.57000			
47	5.9102	7,9903	9.10837	0.28149	0 <b>.</b> 62900			
57	10.100	3.0477	0.11045	0.28709	0,72700			
NOT TECOM	at batssibt	RATIOS . FLE	W SPLITYER I	, O	#			
מפחו ייע	PL	PI /PD	PL/PTF_	PL/PTP	x/OHA*			
62	11.600	1,5003	0.12685	0.32973	0.42200			
£ 7	15.149	4.5711	0.16566	0.43050	0.69200			
>AUDITION	AL PRESSIRE	RATIOS . FLO	W SPLITTER D	. 0.			w.·	
VO WORD	PI	PI /PO	PL/PTF	PL/PTP	X/DMAX_			
77	35.290	10.646	0.39479	1.0028	0.56400	and the second of the second of the second	* * **	
92	11.185	3.3751	9.12231	0.31793	0.63500			
<u>a</u> 5	3.5417	1.0647	0.038729	0.10067	0.69200			***************************************
> ADÓT T TON	AL PPESSIRE	RATINS . FJF	CTOR SHPPUP			na de Alba (n. ) (giag anos) a tropas distribitos anos se e		MASS regar on
עה שחתם	PL	Pt /Pn	PI /PTF	PI /PTP	X/DMAX	alay na matanan da sanan da da ayan ay nagaran na matanan ay na manan na ma		
107	7.8398	2.3656	0.085729	0.22284	0.62400			
112	5,1963	1.5686	7.056844	0.14776	J.83000		· · · · · · · · · · · · · · · · · · ·	
122	3.0211	0.91160	0. 033036	0.085874	0.96000			
27	5.5217	1.0427	3.034513	3.10013	1.0900			
137	4.3376	1.3988	0.047432	0.12329	1.2200			
142	3.0921	1. 1744	0.042561	0.11063	1.3500	· · · · · · · · · · · · · · · · · · ·		
-44414144	L MF 17 P.	AA4105 - FRA						
VA WINED		ማ / ሶስ	P. / PTF	PI /PTP	X/DMAY			
107	7.8398	2,3656	0.045729	0.22284	-1,9000	•		
iis	4,1983	1.5686	0.056844	0.14776	2,0000			
	3.0211	9.91160	0.033036	0.085874	-1.0000			
122		1.0627	2.028513	0.10010	-1.0000			
	5217							
127	4.3376			0.12229	-1,0030			
127 137	4.3276	1,3088	0.04743?	0.12229 0.41063	-1.0020 -1.0020	ungar – Ar Ambi Andria in de la Attra v <b>allati materiologic</b> ammidi		
127 137 142		1.1744	0.04743?		-1.0000		tid alata Provident de la Probabilité e e	
127 137 142 157	- 4.3376 1.8075	1,3088	0.04743?			erus - M. Belle II. dala si di un distribuitation apparate de servicia.	and about the	
127 137 142 157	4.3376 1.6071 2.5317 3.5317	1.1744 1.0657	0.04743? 0.1424A\$ 0.038620 0.038627	0.1063	-1.0000 -1.0000			
127 137 142 157 157 53753337111	4. 3376 1. 6077 2. 5317 3. 5317 EL PPESSIBE	1.1746 1.9657 1.9657	0.04743? 0.1425AI 0.039620 0.039627	0.1063 0.10039 0.10039	-1.0000 -1.0000 -1.6000			
127 137 142 152 152 2491717194 VN WOPD	4.3276 3.8025 2.5317 3.5317	1,3086 1,1744 1,2657 1,2657 FAYING, FAR	0.04743? 0.14244 0.034620 0.034627 MIDTIE FLAP	0.1063 0.10039 0.10035	X/MAXX			
127 137 142 152 152 247317171 Vh. wash 152	4. 3376 1. 6077 2. 5317 3. 5317 EL PPESSIBE	1.1746 1.9657 1.9657	0.04743? 0.1425AI 0.039620 0.039627	0.1063 0.10039 0.10039	-1.0000 -1.0000 -1.6000			
127 137 142 152 152 157 249) Y TOU 152 157	4.3476 3.6021 3.5317 3.5317 2.5317 41 PPESSIBE 91 3.5317 3.5317	1.3986 1.1744 1.9657 1.9657 FAYING FAR M/HI 1.0657	0.04743? 0.1424XI 0.034620 0.034627 WITTTE TEAP V.037620 0.037620	0,1063 0.10039 0.10039 0.10039 0.10039	-1.0006 -1.0000 -1.0006 -1.0000			
127 137 142 152 157 157 249717191 152 157	4.376 3.802 2.5317 3.5317 3.5317 3.5317	1,3086 1,1744 1,9657 1,9657 FAYING FAR M /HN 1,0657 1,0657	0.04743? 0.1428A 0.038620 0.038627 NOVIE FLAP 0.038620 0.038620 0.038520	0 1063 0.10039 0.10039 0.10039 0.10039	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 142 157 157 5279317104 157 5279377104	4.3476 3.8074 2.5317 3.5317 3.5317 3.5317 4.5317	1,3086 1,1744 1,9657 1,3657 FAYINS, FAR MI /HN 1,0657 1,0657 1,0657	0.04743? 0.1426AE 0.038620 0.038627 NOVE TAP 0.038620 0.038620 0EG SHRINGE TO	0.10039 5.10039 0.10039 0.10039 0.10039	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 142 152 152 157 157 157 157 257717174	4.376 3.802 2.5317 3.5317 3.5317 3.5317	1,3086 1,1744 1,9657 1,9657 FAYING FAR M /HN 1,0657 1,0657	0.04743? 0.1428A 0.038620 0.038627 NOVIE FLAP 0.038620 0.038620 0.038520	0 1063 0.10039 0.10039 0.10039 0.10039	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 137 142 157 157 25751717171 157 257517717171 167 177	4.3476 1.8021 2.5317 3.5317 3.5317 3.5317 40 PPT CORPE PL 2.5317 3.5317	1,3986 1,1744 1,2657 1,2657 1,2657 1,0657 1,0657 1,0657	0.04743? 0.1428X; 0.038627 0.038627 NIDTE FLAP 0.038620 0.038520 0.038520 0.038620 0.038620	0.1063 0.10039 0.10039 0.10039 0.10039 0.10039 0.10039	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
157 -157 -257 -257 -257 -267 -267 -267 -277 -277	4.376 1.802 1.802 3.5317 3.5317 3.5317 4. PPESSIBE PL 1.5317 3.5317 4. SPESSIBE PL 1.5317 1.5317	1,3086 1,744 1,0657 1,0657 1,0657 1,0657 1,0657 1,0657 1,0657 1,0657	0.04743? 0.1424X 0.038623 0.038623 0.038629 0.038620 0.038620 0.038620 0.038620	0 / 1063 0.10039 0.10039 0.10039 0.10039 0.10039 0.10039	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 -137 -142 -152 -152 -157 -157 -157 -157 -157 -157 -157 -177 -17	4.3476 1.8071 2.5317 3.5317 2.7317 2.7317 2.7317 2.7317 2.7317 2.7317 2.7317 2.7317 2.7317 2.7317 2.7317	1.3086 1.1744 1.9657 1.9657 PAYINS FAR M/HN 1.0657 1.0657 1.9657 1.9657 1.0657	0.04743? 0.1424\$ 0.038627 0.038627 0.038620 0.038620 0.038620 0.038620 0.038620 0.038620	0 / 1063 0.10039 0.10039 0.10039 0.10039 0.10039 0.10039	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 142 152 157 249717104 VN WIPD 152 157 249717104 VN WIRD 167 177	4.376 1.802 1.802 3.5317 3.5317 3.5317 4. PPESSIBE PL 1.5317 3.5317 4. SPESSIBE PL 1.5317 1.5317	1,3086 1,744 1,0657 1,0657 1,0657 1,0657 1,0657 1,0657 1,0657 1,0657	0.04743? 0.1424X 0.038623 0.038623 0.038629 0.038620 0.038620 0.038620 0.038620	0 / 1063 0.10039 0.10039 0.10039 0.10039 0.10039 0.10039	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

>ADDITION	AL PRESSUPE	PATIOS . PP	MAPY PLUG					
IAU NUUD	PI	PL/PO	M /PTF	PL/PTP	x/DMAX			
37	18.677	5.6531	0.146e1	0.43604	0.43200 0.53000			
37 47	19.257 12.035	3.110A 3.6434	J. 12179	0,29103	0.62900	•		
52	12.265	3.7223	0.12443	0.27711	U- 72 700			
>4.011.11mm	vF hus 22ms.		IW. SPLITTER. I			•		e i
LAU MUSU"		PL/PC	PL /PTE	PL/PTP	XZDMAX			
62	14.139	4.2912	0.14344	0.33009	0.42200			
67	15,079	4,5763	0.1529P	0, 15299	U_69200			
>voult lun	AL PRESSIME	PATINS , FLI	W_SPLITTEP_C	, n	and a second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control o			
AD MUSE	PL	PI / PP	PI /PTF	PL /PTP	X/DHAX			
77	37.653	11.427	0.39700	0.88144	0.56400			
45	12.060	3.6601	0.12235	0,28231	0.63500			
97	3.5165	1.0672	0.035675	0.082319	7.69200			
SAND IT IN	AL PPESSUPE	PATIOS - 545	CTOS SUSOIS			and a second second second second second second second second second second second second second second second		
						Marketter state control of the state case. Market stress and and case	Marie - Campania de Carrero - Campania de Carrero - Campania de Carrero - Campania de Carrero - Campania de Ca	سلاموريني يوسنا مغد وفاقطت بيومور يوشون المغددين
NO HOPE	PL	PL/PO	PL/PTF	PL/PTP	X\UWVX			
107	0.3798	2.5432	0.095014	0.19617	0,62400	<del></del>		
112	5.6285	1.7082	0.057102	0.13176	0.83000			
127 127	3.2512	0.99671	0.032984	0.076108	0.96000			
127	3.5165 4.9329	1.0672 1.4971	0.035675 0.050945	0.082319 0.11548	1.0900 1.2200			
142	4,6727	1.4181	0. 047405	0.10936	1.3500	er i central de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania del compania del compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania del la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania de la compania della compania de la compania de la compania de la compania de la compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compania della compa		
AND AUD U	AL PRESSUP?-	PATING , FRI PI /PN	M /PTF	PL/PTP	×70#AX			
197	8.3798	2.5432	0.085014	0.19617	-1_0000	•		
1117	5.6285	1.7042	0. 957192	0.13176	/1.0000			
12?	3.2512	9. 98671	0.032984	0.075108	-1.9090			
-127	5165	1.0672	9.035675	0.082345	-1.0000			
-127	4.3629	1.4971	3.050045	0.13/49	-1.0000			
-14?	4.672	1.4141	9. 34749K	Q41093P	-1.0000			
-15?	3.5065	1.0642	0.035574	0.082085	-1.0000 -1.0000			
-1 = 7	3.5065	1.1647	0.035575	0.002085	-1.0000			
SANSITION	AL PRESSUPE	PATTOS PAR	4 NC77 LE EL ST					
IVP YËRD	PL	PL/P0	MI JOSE	PI /PTP	KZDHAR			w washings in a second interest of
-1=2	3.5065	1.9547	0.035574	0.092085	-1.0000			
-157	3.5365	1.0657	0.035574	0.077045	-1.0000			
>4001710W	AL PRESCUPE	RATHIS . 20	DEC SHADON	OCATION				
IAU ALBL	PI	PI /PI	M /PTF	N. 1818	Y/DMAX	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		
-16.7	1.504	1.0642	0.035574	0.002005	-1.0000			
172	3,8565	1.0642	0.035574	0.000005	-1.0000	Caracteristic Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control		n a war is a
SANTITION		DR . 701734	nec Stenor T	TEATTING -				
	PI					w		
190 POON		Pi /Pri	Pt /Ptf	PL /PTP	XAMMAX			
	4.0971 2.1970	1.2789	7.041414 7.040=53	0.095560	-1.0000			•
A 67	- · · · · · · · · · · · · · · · · · · ·	1.2131	**************************************	0.093568	-1.0000			
APT TOU 5	. MERSUPEN	TUBILLY MARAN	CTED C					

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NOT TICON	AL PRESSUPE	PATIOS . PP	MAFY PLUG					
VD HORD	PL	PI / PO	PI /PTF	PI /PTP	x/DMAX			
32	16.591	5.0294	7.16763	0.43545	1.43200			
7	9.1396	2.7703	0.092333	0.24013	0-53000			
47	10.699	3.7437	7. 10,000	0.28112	3.62903			· alley · . Mr ··
52	10.928	3.3129	0.11042	0.24716	0.72700			
>kuattini	At PRESSIPE	RATIOS , FLO	W SPLITTER L	. n	grade - refer again	· •		
VO MURD	Pt.	PL /PD	PL /PTF	PL /PTP	x/DMAX			
67	12.488	7,7957	0.12617	0.32814	0.42200			
67	15. 36/	4.5674	0.15223	0.39590	0.69200			
>vout t tow	AL PRESSURE	PATIOS . FLO	W SPI ITTER O	.0.	er der de desemble i de desemble i de de de de de de de de de de de de de		4.40.5	
YN WAPA	PL	PL/PD	PL/PTF	PL /PTP	Y/DMAX			
77	37.669	11.419	0.38060	0.98980	0.56400		<b>-</b>	
R2	12.073	3.6594	0.12198	0.31724	0.63500			
	3,5147	1.0657	0.035521	U. 092378	0,69200			
Ann (Ting	AL PRESSUPE	PATINS , EJF	CTCP SHPNUN					er en <del>et e</del> n
VD WORD	PE	M/M	PL/PTF	PL /P TP	X/DMAX	manufacture and a support of the second	بالبوم ويوريون بالمالي	
107	8.4135	2. 5505	0.985007	0.22107	0.62400			
13	5.5624	1.7165	0.057211	0.14879	0.83000			
2?	3.2694	0.98836	0.032942	0.085470	0.96000			
127	3.5706	1. 9612	0.035360	0.001003	1.0900			Andrews Committee of the State of the
1.27	4.7019	1.4253	0.047505	0.12354	1.2200			
42	4.2163	1.2781	0.042603	0.11079	1.3500			
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107	6.4135	2.5505	0.085007	0.22107	-1.0000			
115.	₹.6624	1.7165	7.057211	0.14679	-2.0000			
122	3.2694	0. 98836	0.032942	0.085670	-1.0090			
27	3.5006	1.0612	0. 035369	0.091432	-1.0000	<del></del>		
127	4.701B	1.4253	0.047505	0.123/54	-1.0000			
47	4.2163		0.042699	0,21079	-1.0000		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
157	3.5006	1.0612	0.235369	A.091983	-1.0000			
57	7.5356	1:3454	0.035420	0.092115	-1-0000	THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE P	tione i anno 1911 e sistematica de la mandra de	- Anglia do de Mestro - Mestro Mestro - M
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545017104 112 112 127 127 127 127 147 147 147 167 167 167 167 167 177 177 17	PI 9.3902 5.7160 3.2605 3.7376 4.9210 4.6510 3.4956 3.4956 3.4956 11 PPECCIPE PI 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.5000 2.50	PI / Ph 2.5495 1.7369 0.92075 1.0652 1.4953 1.4148 1.3622 1.7622 1.7622 1.0622 1.0632 1.0637 1.0622	0.067707  PLATE 0.085061 0.0857649 0.032055 0.035630 0.035430 0.035430 0.035430 0.035430 0.035430 0.035430	0.10941  Pi /PYP 0.19735 0.19735 0.076490 0.087257 0.11875 0.17875 0.082270 0.082270 Pi /PYP 0.082220  ATTOM	1.3500  X/NMAY -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
545017104 112 112 127 127 127 127 147 147 147 167 167 167 167 167 177 177 17	PI 9.3902 5.7160 3.2605 3.2605 3.4050 3.4050 3.4056 3.4056 1 PPFSSIRE N	# /Fn 7.5495 1.7369 1.7369 1.0652 1.4953 1.6148 1.3622 1.7622 1.7622 1.7622 1.7622 1.7632	0. 067709  PLAPTE  0.085061  0.0879649  0.032055  0.0378527  0.645800  0.035430  0.035430  0.035430  0.035430  PLAPTE  0.035630  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630  PLAPTE  0.035630	0.10941  PI /PTP 0.19735  G.1345 0.076690 0.087257 0.11875 0.092270 0.082270  PI /PTP 0.082220  ATTIM	1.3500  X/NNAY -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
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4427-FEAL	e mellal	NAPY DETA	DE/11/79	CADOFII	PEC 10/17/79 32:10:2	7.066 FAC	exect .	PG# C934	Row 18 Ping 1171
34221110W	AL DEESSUPE	RATIOS	IMARY MUS.		was the second	er sitte med in in in	was commenced to the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced with the commenced w		t 196 - en afte dagrammente
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3.7	10.405	F. 8544	0.21299	0.43734	0-43200				
37	10.670	3.2191	2.11717	0.24947	3.53003				
47	12.512	3, 7746	0.13733	0.29198	J-62900				
_52	12.772	3.8531	7.14025	0.29784	1.72700	W dida contributo man as wellands. Whitehali	months of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second se	re-or - productive instruction	~
2001110M	N, PRESSIRE	PATIOS, # .FIG	W SPLITTEP I	n.					
AVP WORT	_PL	PJ / PO	PI /PTF	PI /PTP	X PRIMA X				
£2	14. 703	4.435R	9.16145	0.33136	3.42200				
47	14,978	4,5198	0.16449	0.33757	3,69299				
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77	34. 909	13.502	0. 38224	0.78449	0.56400	* .* *.	*** * *** ***		#in-
82	11.151	3,3640	0.12244	0.25130	0.63509				
9?	3.5345	1.0463	0.038812	0.079654	0.69203				
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107	7.8018	2.3537	0.085671	0.17583	0, 62400				
112	5.1927	1.5666	0.057021	0.11703	0.83003				
122	3.0033	0. 90505	0.032979	0.067685	0-96000				
127	3.5294	1.064#	0.030757	0.079543	1. 3970			a company of the second pages to	M
137	4.4070	1.4502	0.052745	0.10834	1.2200				
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107 0.041747 0.041747 -1.0600	<i>-</i>							

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77	15.171	4.6009	1.16743	0.43606	0.43200				
37	0.3771	2.5430	0.092390	0.2404	0.531100				
47	0.7823	2.9713	1,11794	0.27118	9.62900				
52	9, 4023	3.0351	-11026	0.78721	3.72703				
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62	11.482	3.4876	0.12672	0.33074	9.47200				
67	14.981	4,5200	0.16420	0.42773	0.69200				
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AVD WOLD	PL	M /PN	PI /PTF	PI /PTP	X/DMAX	₩ v sw			
77	34.540	10.491	0.39113	0.99281	0.56403				
<u> 87</u>	11.067	3,3616	0.12212	0.31611	0.63500			<del></del>	
	3.5141	1.0674	0, 038776	0.10101	0.69200				
>ADDITIONA	E PRESSIPE	PATINS , FUE	CTOP SHROWN						
AVD HOPD	PL	PL /PI)	PI /PTF	PI /PTP	X/OHAY	roma a das amostos			** * * * * * * * * * * * * * * * * * * *
107	7.7670	2,3592	0.085703	0.22325	0.62400				
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127	2.9985 3.4991	1.0424	0.038610	0.10058	0.96000 0.96000			•	Andrew Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the Comment of the
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147	3.9495	1.1693	0.042476	0.11065	1.3500			1 M M W W W W W W W W W W W W W W W W W	
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-115	5-1656	1.5590	0.056599	0.14848	1.9000				
-155	2.9985	3, 90775	0.032976	0.085901	-1.0000				
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-127	4.8949	1.3046	0.047391	0.12545	-1.0000		and the second second		<del></del>
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-152	3.5041	1.0644	0.038665	0.10072	-1.0000				
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-152	3.5041	1.0644	0. 038665	0.10072	-1.0000				
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- 22	3,5262	1.9647	0. 042575	0.11077	3.69200		· · · · · · · · · · · · · · · · · · ·		<del></del>
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AVD WORD	PL 7.2457	PL/PN	M/MF	PI /PTP	X/DMA X				
107	7.2457	2.1877	0.087484	0.22680	0.62400				
1133	4.7079	1.4215	0.022820	0.14736	0.83000				
122	7.7100	3.42123	0.032839	0.085135	0.96000				
127	3.5312	1.0571	5.142272	J. 10950	1.0900				
127	3.9168	1.1826	0.047291	0.12260	1.2200			and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	
142	3. 41 62	1.0617	0.042454	0.11006	1.3500				
	IN NECETIBE	A41)35 . FOR	ENTON IMES				<del></del>		
<del>/</del>									
AVO VORD	PÎ	PL/PÖ	M /PTF	PL /PTP	XZDMAX				
AVO VORD	PI 7.2457	2.1877	0. 687484	0.22680	-1-2000	- · <u>-</u> ·	anger and refer to the activities and the		
AVO VORD	PI 7,2457 4,7079	2.1877 1.4215	0.057484 0.057843	0.14736	-1-0000 -1-0000				· · · · · · · · · · · · · · · · · · ·
AV7 UNRN -107 -117 -127	PI 7.2457 4.7079 2.7199	2.1977 1.4215 2.92123	0.056843 0.056843	0.22680 0.14736 0.085135	-1.0000 -1.0000 -1.0000				
AV7 VARA -107 -112 -122 -127	PI 7.2457 4.7079 2.7199	2.1977 1.4215 2.92123 1.9571	0.056843 0.056843 0.032839 0.042277	0.22680 0.14736 0.085135 0.10959	-1.0000 -1.0000 -1.000		•		
AV7 VORD -107 -117 -127 -127 -127	PI 7.2457 4.7079 2.7199 5012 3.0468	2.1877 1.4215 2.92123 1.0571 1.1826	0.056843 0.056843 0.032839 0.047291	0.22680 0.14736 0.085135 0.10959 0.12260	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000		•		
AV7 VARA -107 -112 -127 -127 -127 -127 -127	PI 7,2457 4,7079 2,7199 5012 3,068 3,516	2.1877 1.4215 2.92123 1.0571 1.1826 1.3617	0.07484 0.056843 0.032839 0.042277 0.047291 0.242454	0.22680 0.14736 0.085135 0.10959 0.12260 0.11006	-1.0000 -1.0000 -1.000				
AV7 VARA -107 -117 -127 -127 -127 -127 -142 -152	Pi 7.2457 4.7079 2.7199 5012 3.168 3.5168	2.1877 1.4215 2.92123 1.0571 1.1826 1.3617 1.9602	0.087484 0.056843 0.032839 0.047277 0.047291 0.047291 0.042363	0.22680 0.14746 0.085125 0.10959 0.12260 0.11006 0.10990	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AV7 VARA -107 -112 -127 -127 -127 -127 -127	PI 7,2457 4,7079 2,7199 5012 3,068 3,516	2.1877 1.4215 2.92123 1.0571 1.1826 1.3617	0.07484 0.056843 0.032839 0.042277 0.047291 0.242454	0.22680 0.14736 0.085135 0.10959 0.12260 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AV7 VARA -107 -117 -127 -127 -127 -142 -157	PI 7.2457 4.7079 2.7199 3.5169 3.5169 1.5112 3.5162	2.1877 1.4215 2.92123 1.0571 1.1826 1.3617 1.9602	0.087484 0.056843 0.032839 0.042277 0.047291 0.342454 0.042303 0.042454	0.22680 0.14746 0.085125 0.10959 0.12260 0.11006 0.10990	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AV7 VARA -107 -117 -127 -127 -127 -142 -157	PI 7.2457 4.7079 2.7199 3.5169 3.5169 1.5112 3.5162	7.1877 1.4215 2.92123 1.0571 1.1826 1.3617 1.9602 1.0617	0.087484 0.056843 0.032839 0.042277 0.047291 0.342454 0.042303 0.042454	0.22680 0.14746 0.085125 0.10959 0.12260 0.11006 0.10990	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AV7 VARA -107 -117 -127 -127 -127 -127 -142 -157 -157	PI 7.2457 4.7079 2.7199 5012 3.5163 3.5163 3.5163	2.1877 1.4215 2.82123 1.0571 1.1826 1.3617 1.0602 1.06417 PAYING FAN	0.087484 0.052839 0.032839 0.042277 0.047291 0.042454 0.042454	0.1474 0.045135 0.095135 0.10959 0.12240 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AV7 VARA -107 -117 -127 -127 -127 -142 -157 -157 -157	PI 7.2457 7.7199 2.7199 5012 3.5163 3.5163 3.5162 3.5152	2.1877 1.4215 2.92123 1.0571 1.1826 1.3617 1.0602 1.0617	0.087484 0.052839 0.032839 0.042277 0.047291 0.242454 0.0423454 NP7711 FLAP	0.12240 0.14714 0.045175 0.10959 0.12240 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AV7 VARA -107 -117 -127 -127 -127 -142 -157 -157 -157 -157 -157	PI 7.2457 7.2457 4.7079 2.7199 5012 3.5163 3.5163 3.5163 3.5163 3.5162	2.1877 1.4215 0.92123 1.0571 1.1826 1.3617 1.0602 1.0617	0.087484 0.052839 0.032839 0.042277 0.047291 0.242454 0.042454 NP771 FLAP 0.042439 0.042439 0.042434	0.22680 0.1474 0.085135 0.1095 0.12260 0.11006 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVN WARN -107 -117 -117 -127 -127 -127 -142 -157 -157 -157 -157 -157 -157 -157 -157	PI 7.2457 4.7079 2.7199 3.5163 3.5163 3.5163 3.5162  PPESSUPE CL 3.5112 3.5162  WAL PRESSUPE	7.1877 1.4215 9.92123 1.0571 1.1826 1.3617 1.0602 1.0617 PAYING FAR 91/80 1.0602 1.0613	0. CR 7484 0. OS2839 0. CS2839 0. O62277 0. O62277 0. O62277 0. O62265 0. O62265 0. O62454 0. O62393 0. O62454	0.14746 0.045125 0.10955 0.12260 0.11006 0.11006 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVD VORD -107 -117 -127 -127 -127 -127 -127 -157 -157 -157 -157 -157 -157 -157 -15	PI 7.2457 4.7079 2.7199 5012 3.5163 1.5112 3.5152 VAI PPECCUPE	2.1877 1.4215 2.92123 1.9571 1.1826 1.3617 1.9602 1.0617 PAYING FAR 91/80 1.3602 1.3612 1.3612	0.087484 0.052839 0.032839 0.042277 0.047291 0.242454 7.042303 0.042454 MP7711 FLAP 0.042393 0.042454 DEC SHPOINT TO	0.1240 0.14746 0.085175 0.1220 0.1220 0.1220 0.11006 0.11006 0.11006	-1.9000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVO VORO -107 -117 -127 -127 -127 -127 -127 -127 -157 -157 -157 -157 -157 -157 -157 -15	PI 7.2457 4.7079 2.7199 3.5163 3.5163 3.5162 VAI PPECCUPE  2.5162 VAI PPECCUPE  2.5162 VAI PPECCUPE	2.1877 1.4215 1.92123 1.9571 1.1826 1.3617 1.9602 1.0617 PAYINS FAN 91/80 1.3602 1.3613 PAYINS . 20	0.087484 0.052839 0.032839 0.042277 0.047291 0.242454 0.042363 0.042454 MP771FFLAP 0.042393 0.042454 DEG SHROUNT II	0.22680 0.1474 0.085135 0.10950 0.12260 0.11006 0.11006 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVN WIRN -107 -117 -127 -127 -127 -127 -127 -157 -157 -157 -157 -157 -157 -157 -15	PI 7.2457 7.2457 7.2457 7.7199 2.7199 3.5163 3.5163 1.5112 3.5152 VAI PPFCSUPF PI 3.5112 3.5162 VAI PPFCSUPF PI 2.5162	7.1877 1.4215 9.92123 1.0571 1.1826 1.3617 1.0602 1.0617 PAYIN FAR 91/80 1.36.02 1.36.13 PAYIN 20 PL/PO 1.06.32	0. CR 7484 0. CR 7484 0. CR 7484 0. CR 747291 0. CR 7291 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 747454 0. CR 7292 0. CR 747454 0. CR 7292 0. CR 7293	0.14746 0.045125 0.10955 0.12260 0.11006 0.11006 0.11006 0.11006 0.11006	-1.9000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVO VORD -107 -117 -127 -127 -127 -127 -127 -127 -157 -157 -157 -157 -157 -157 -157 -15	PI 7.2457 7.2457 7.2457 7.7199 2.7199 3.5163 3.5163 1.5112 3.5152 VAI PPFCSUPF PI 3.5112 3.5162 VAI PPFCSUPF PI 2.5162	2.1877 1.4215 1.92123 1.9571 1.1826 1.3617 1.9602 1.0617 PAYINS FAN 91/80 1.3602 1.3613 PAYINS . 20	0. CR 7484 0. CR 7484 0. CR 7484 0. CR 747291 0. CR 7291 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 747454 0. CR 7292 0. CR 747454 0. CR 7292 0. CR 7293	0.14746 0.045125 0.10955 0.12260 0.11006 0.11006 0.11006 0.11006 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVO VORD	PI 7.2457 7.2457 7.7199 2.7199 3.5162 3.5162 VAI PPECCUPE PI 2.5162 PI 2.5162 PI 2.5162 PI PPECCUPE PI 2.5162 PI PPECCUPE PI 2.5162	2.1877 1.4215 1.92123 1.0571 1.1826 1.3617 1.0602 1.0617 1.0602 1.3617 PAYINS FAN PLAYINS FAN 1.0602 1.0617 1.0632 PAYINS RO	0.087484 0.052839 0.032839 0.042277 0.047291 0.242454 0.042363 0.042454 MP771FFLAP 0.042393 0.042454 DFG SHPOINT 11	0.22680 0.14746 0.085176 0.10953 0.12260 0.11006 0.11006 0.11006 0.11006 0.11006 0.11006 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
AVN WIRN -107 -117 -127 -127 -127 -127 -127 -157 -157 -157 -157 -157 -157 -157 -15	PI 7.2457 7.2457 7.2457 7.7199 2.7199 3.5163 3.5163 1.5112 3.5152 VAI PPFCSUPF PI 3.5112 3.5162 VAI PPFCSUPF PI 2.5162	7.1877 1.4215 9.92123 1.0571 1.1826 1.3617 1.0602 1.0617 PAYIN FAR 91/80 1.36.02 1.36.13 PAYIN 20 PL/PO 1.06.32	0. CR 7484 0. CR 7484 0. CR 7484 0. CR 747291 0. CR 7291 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 7292 0. CR 747454 0. CR 7292 0. CR 747454 0. CR 7292 0. CR 7293	0.14746 0.045125 0.10955 0.12260 0.11006 0.11006 0.11006 0.11006 0.11006	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

NASK-LEFI	S P#FL141	NAPY PATA	06/11/79	CADDE11	FEC 10/17/79 C	2:26:04.413	FAC SX6X1	PG4 C034	//WW /8 PDG 1177	
		PATIOS . PRI								
ZB1144								···		
AU NUKD	FL	PL/Pn	PL/PTF	PL/PTP	X/DMAX					
3.5	16.201	4.2960	2.21692	0.43718	0.43200					
37	A. 9220	2.6908	2.11946	0.24076	0.53000					
47	10.442	7.1492	0.13571	0.28178	0.62900					
52	12.657	3,2141	0.14269	0.28759	0.72700					
>4901 T ION	AL PRESSURE	ATINS . FLO	W SPLITTER, I	• D•						
AU MULU	Pt	PL/PO	Pt / PTF	PL /PTP	X/FMAX		_			
62	12.267	3.6996	0.16425	0.33103	0 <b>.42700</b>					
<u> </u>	14,776	4,4443	0.19731	0.35764	0,69200					
>403 T [0N	AL PRESSIRE	RATIOS . FLO	W SPLETTER O	.n.						
VA WAPA	PL	PL/PO	PI / PTF	PI /PTP	X/DMAX					
77	28.776	A. 6784	0.38578	0.77452	0.56400					
R2	9.1220	2,7511	9.1221	0.24616_	0.63500					
92	7.5433	1.0686	0.047441	0.095615	0.69200					-
ADD Í T ÍÐÁ	AL PRESSURE	RATIOS . EJF	CTOR SHROUD				profession and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco			-
VO WORD		Pt /Pfi	Pt/PTF	PI /PTP	X/DMAX		The second section of the second section is a second section of the second section section is a second section of the second section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section s			
107	6,6169	1.9953	0.098583	0-17053	0-62400					
12	4.2441	1.2800	0.056825	0.11453	0.03000					
22	2.4618	0.74746	0.032962	0.066433	0.96000					
27	3.5293	1.2641	0.047240	0.095210	1.0900			··· - · · · · · · · · · · · · · · · · ·		
27	3.99RB	1.2760	0.053561	0.10791	1.2700					
47	4.0489	1.2711	0.054211	0.10926	1.3500	•				*
		807 - SOITAR								
AU ALLEU	Pt	የዚ/ የብ	PL/PTF	PL /PTP	X /DHAX		•			
107	6.6167	1.9953	0.088593	0.17853	-1-0000					
112	4.2441	1.2400	0. 054 925	0.11453	1.0000					
122	2.4FIR	J. 74246	0.032562	0.066433	-1.0000					
177	5293	1.0641	0.047740	0.095240	-1.0000					
	a.pqea	1.2060	0.053541	0.30191	-1.0000					-
									The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th	
147	4.74	1.2211	0.054211	0.10926	-1.0000					
137 147 153	3.5283	1.0641	0. 547240	0.095210	-1.0000	•			ngan ang ang ang ang ang ang ang ang ang	-
147 152	4.74							The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	en en en en en en en en en en en en en e	
14? 15? 15?	4.94P 3.5283 3.5283	1.0641	0. 047240	0.095210	-1.0000	• ·				
147 157 5 <u>40917 (AM</u> VD HORD	4.04P 3.5283 3.5283 41 PRESSIPE	1.0641 1.0641 PATIOS FAN	0. 547240 0. 047242 MN77 JE FEAR	0.095210 0.095210	-1.0000 -1.0000	• ·				
147 167 157 >APTITION VD HORD 152	4.04P 3.5283 3.5283 AL PRESSIPE PL 3.5283	1.0641 1.0641 PATIOS FAN PI/PO 1.0641	0. 547240 0. 047242 HN7714 FEAR M / PTF 0. 047242	0.095210 0.095210 PL/PTP 0.095210	-1.0000 -1.000J X/DMAX -1.0000	<u>.</u> .				-,
147 157 5 <u>807   TIAN</u> VD. HORD 152	4.04P 3.5283 3.5283 41 PRESSIPE	1.0641 1.0641 PATIOS FAN	0. 547240 0. 047242 MN77 JE FEAR	0.095210 0.095210	-1.0000 -1.0000					
142 162 157 5 <u>APTITION</u> VD HORD 152	4.04P 3.5283 3.5293 AL PRESSIME PL 3.5293 3.5293	1.0641 1.0641 PATIOS FAN PI/PO 1.0641	0. 547240 0. 647247 H07774 FLAP PI /PTF 0. 047240 10.047240	0.095210 0.095210 Pt /PTP 0.095210 0.095210	-1.0000 -1.000J X/DMAX -1.0000					
147 157 57 VN HORD 157 157	4.04P 3.5283 3.5293 AL PRESSIME PL 3.5293 3.5293	1.0641 1.0641 PATIOS FAN 1.0641 1.0641	0. 547240 0. 647247 H07774 FLAP PI /PTF 0. 047240 10.047240	0.095210 0.095210 Pt /PTP 0.095210 0.095210	-1.0000 -1.000J X/DMAX -1.0000					
167 157 ADDITION VO HORD 157 167 ADDITION	4.04P 3.5283 3.5283 41 PRESSIME PI 3.5283 41 PRESSIME PI 3.5283	1.0641 PATION FAN M/PO 1.0641 1.0641 PATION 20	0. 047249 HD77 JE FLAP M / PTF 0. 047249 M (1047249 D (1047249)	0.095210 0.095210 0.095210 0.095210 0.095210	-1.0000 -1.0000 X/DMAX -1.0000 -1.0000					-
147 167 157 DADTITION VO HORD 157 157	4.04P 3.5283 3.5283 AL PRESSIPE PL 3.5283 3.5283 AL PRESSIPE	1.0641 1.0641 PATION FAN M / PO 1.0641 1.0541 PATION 20 M / PO	0. 547240 0. 647249 H077 JF FLAP PI / PTF 0. 047249 M5.047240 NFC SHPCOR LI	0.095210 0.095210 0.095210 0.095210 0.095210 0.095210	1.0000 -1.0000 -1.0000 -1.0000					
167 167 167 167 167 170 167 167 167 167 167	4.947 3.5283 3.5283 AL PRESSIPE PL 3.5283 AL PRESSIPE PL 3.5283 AL PRESSIPE	1.0641 PATION FAN M / PO 1.0641 PATION . 20 M / PO 1.0641	0. 547240 0. 647249 H077 JE FLAP M / PTF 0. 047249 M / PTF 0. 047240 M / PTF 0. 047249 0. 647240	0.095210 0.095210 0.095210 0.095210 0.095210 0.095210 0.095210 0.05210	1.0000 -1.0000 x/DMAX -1.0000 -1.0000					-
167 167 167 167 167 167 167 167 167 177 17	4.04P 3.5283 3.5283 3.5283 41 PRESSIPE PL 3.5283 41 PRESSIPE PL 3.5283 3.5283 41 PRESSIPE	1.0641 1.0641 PATION FAN M / PO 1.0641 1.0541 PATION 20 M / PO 1.0641 1.0641 1.0641	0. 547240 0. 647240 HD77 JF FLAP 19 / PTF 0. 047240 DFC SHPTON L PLAP OF CHAPTON L 0. 647240 0. 647240	0.095210 0.095210 0.095210 0.095210 0.095210 0.095210 0.095210 0.095210	-1.0000 -1.0000 x/DMAX -1.0000 -1.0000 -1.0000 -1.0000					
167 LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE LET TONE	4.947 3.5283 3.5283 AL PRESSIPE PL 3.5283 AL PRESSIPE PL 3.5283 AL PRESSIPE PL 1.793	1.0641 1.0641 PATION FAN M/PO 1.0641 1.0541 PATION AC PATION AC	0. 547240 0. 647240 HD77 F FLAP PI /PTF 0. 047240 DFC SHPORD LI PI /PTF 0. 647240 DFG SHPORD LI PI /PTF	0.095210 0.095210 0.095210 0.095210 0.095210 0.095210 0.095210 0.095210	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
147 157 157 VN HORD 157 157 157 VN HORD 167	4.04P 3.5283 3.5283 3.5283 41 PRESSIPE PL 3.5283 41 PRESSIPE PL 3.5283 3.5283 41 PRESSIPE	1.0641 1.0641 PATION FAN M / PO 1.0641 1.0541 PATION 20 M / PO 1.0641 1.0641 1.0641	0. 547240 0. 647240 HD77 JF FLAP 19 / PTF 0. 047240 DFC SHPTON L PLAP OF CHAPTON L 0. 647240 0. 647240	0.095210 0.095210 0.095210 0.095210 0.095210 0.095210 0.095210 0.095210	-1.0000 -1.0000 x/DMAX -1.0000 -1.0000 -1.0000 -1.0000					

4427-1 EM 1	< PPFL141	IMARY PATA	06/11/79	CADDETT	REC 10/17/79	07:26:47.375	FAC RYGXI	PG4 C034	flun /8 RFG 1178
>47017Inv	AL PRESSURT	PATING , PR	MARY PLUC				man on a company of a		
AND MUND	C1	P[ /P7	M /PTF	PI /PTP	X/DMAY				
3.2	14.119	4.2430	7. 19991	7.43617	0.43200				
37	7.7956	7.347#	0.10430	0.24983	0.53000				
47	9.1767	2.742R	0.17211	0.24195	6,62900				
52	9.3014	2.7954	0.12446	0.28736	0.72700				
>APOIT FORM	AL PRESSUPE	RATIOS , FLO	W SPLITTER 1	. n.					
IVD WEED	PL	P( /PI)	PL / PTF	PI /PTP	x/DMAX				•
6.2	10.708	3.2179	0.14327	0.33079	0.42200				•
67	14.694	4,4129	9.19647	0,45363	0.69200				
NOT TICCA	AT PRESSUPE	RATINS . FLI	N SPLITTER O	. D.	<del></del>				
VP HORD	Pl.	PL/PG	PL/PTF	PL /PTP	X/DMAX				
77	24. 905	9. 686P	0.38475	0.89298	0.56400		· · · · · · · · · · · · · · · · · · ·		
R2	9.1567	2.7518	0.12252	0.28288	0.63500				_
57	3.5401	1.0630	J. 047367	0.10937	0.69200				
>10011 (194)	AL PRESSURE	PATINS . EJI	CTOR SHPOIN					V	
vn unpn	PL	PL/PI)	PI /PTF	PI /PTP	YAMAY	The second second			ب السواد الم
107	6.5944	1.9918	0.098272	0.20372	J. 62400				
11.5	4.2563	1.2791	0.056649	0.13149	0.43000		······································	<del></del>	······································
127	2.4692	0.74175	0.033074	0.076250	3.96000				
157	3.5251	1.0594	~ 7.047145	0.10090	1.0900				
137	3.7204	1.1191	0.049779	0.11494	1.2200				
147	3.5301	1.0609	0.047242	0,10906	1.3500	· · · · ·			
****	-	******	FACINE TALES		<del></del>				
	Pl.	PL /PN	PL/PTF	PL /PTP	X/0442	mg. • • • ··			· · · · · · · · · · · · · · · · · · ·
		*1 / ***	0.09823?	0.20372	-1,0000		•		
		3.0818							
107	6.5344	1.9818		""" A. 1 5122	<b>4</b> 1 0000				the same a propagation of a company of the
107	6,5744	1.2791	0.056949	0.13145	1.0000				the same a proportion of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the st
107 112 122	6.5944 4.2563 2.4682	1.7791	0.056949 0.033024	0.076250	-1.0000				
107 119 129	6.5944 4.2563 2.4682	1.2791	0.056949 2.033924 3.347165	0.076250	-1.0000 -1.0000	***************************************			
107 112 127 127	6.5944 4.2563 2.4682 5.551 3.1204	1.7791 1.74175 1.3594 1.1181	0.056949 2.033024 0.047165 0.549779	0.076250 0.10898 0.11494	-1.0000 -1.0000 -1.0000				
107 115 127 127 137 142	6.5944 4.2563 2.4682	1.7791	0.056949 2.033024 0.347165 0.549779 0.047232	0.076250	-1.0000 -1.0000 -1.0000 -1.0000			.,	
107 115 127 127 137 142	6.5944 4.2563 2.4682 3.5751 3.7204 3.5338	1.7791 7.74175 1.3594 1.1181 1.0609	0.056949 2.033024 0.047165 0.549779	0.076250 0.10498 0.11494 0.10406	-1.0000 -1.0000 -1.0000				
107 112 122 127 127 127 142 162 163	6.5744 4.2563 2.4682 3.751 3.7206 3.5331 3.5331	1.7791 7.74175 1.3594 1.1181 1.0609 1.0609	0. 056949 2. 033024 3. 047165 0. 549779 0. 047232 0. 047232	0.076250 0.10498 0.11494 0.10406 0.10406	-1.0000 -1.0000 -1.0000 -1.0000				
107 112 122 127 137 142 152 152 157	6,5744 4,2563 2,4682 5,751 3,7204 3,53,31 3,5401	1.2791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639	0. 056949 2. 033024 0. 047165 0. 04719 0. 047232 0. 047232 0. 047327	0.076250 0.10898 0.11996 0.10906 0.10906 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 137 142 162 167 Sannytinm	6.5744 4.2563 2.4682 3.5751 3.57331 3.5401	1.7791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639	0. 056949 2.033024 0. 347165 0. 24779 0. 047232 0. 047232 0. 047323 WITTIE FLAN	0.076250 0.10898 0.11494 0.10406 0.10406 0.10437	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 137 142 157 5570111000	6,5744 4,2563 2,4682 5,751 3,7204 3,53,31 3,5401	1.2791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639	0. 056949 2.033024 0. 047165 0. 04719 0. 047232 0. 047232 0. 047327	0.076250 0.10898 0.11996 0.10906 0.10906 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 119 129 127 127 149 149 149 149 147 547 147 147	6.5744 4.2563 2.4682 3.571 3.571 3.5601 11 PPFSSUPF PL 3.5731 3.5601	1.7791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639 PAYIO FAR EL/PN 1.0509 1.0639	0. 056949 9. 033024 9. 047165 0. 049779 0. 047232 0. 047387 WICTTUE FLAP FLAPTE 0. 047232	0.076250 0.10898 0.10906 0.10906 0.10937 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 1127 127 127 142 167 5877	6.5744 4.2563 2.4682 3.571 3.571 3.5601 11 PPFSSUPF PL 3.5731 3.5601	1.7791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639 PAYIO FAR EL/PN 1.0509 1.0639	0. 656949 2.033024 0. 47165 0. 249779 0. 047237 0. 047327 0. 047327 WITTIE FLAP PL/PTE C. 047232 0. 047327	0.076250 0.10898 0.10906 0.10906 0.10937 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 1127 127 127 127 127 127 127 127 127 1	6.5744 4.2563 2.4682 3.5751 3.5704 3.5731 3.5401 H PPFSSUPF PL 3.5731 3.5401 H ORESSUPF PL 3.5731 3.5401	1.2791 2.74175 1.3594 1.1181 1.0609 1.0609 1.0639 PAYITO FAR PL/PT 1.0509 1.0639	0. 056949 9. 033024 9. 047165 0. 049779 0. 047232 0. 047367 WITTTLE FLAP 0. 047387	0.076250 0.10898 0.11494 0.10906 0.10906 0.10937 Pt /PTP 0.10937 PTATTINI	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
VN ₩00N 1=7	6.5744 4.2563 2.4682 3.5751 3.5704 3.5331 3.5401 11 PPFSSUPF PL 3.5331 3.5401 11 PRFSSUPF PL 3.5301 3.5401	1.2791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639 PAYITH, FAR PL/PN 1.0509 1.0639 1.0639	0. 056949 9. 033024 9. 047165 0. 047237 0. 047232 0. 047387  WICTOL FLAP 0. 047387  PL/PTF 0. 047387	0.076250 0.10896 0.10906 0.10906 0.10937 0.10936 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 117 127 127 142 157 5277117711 5277117711 5277117711 70 HOPD 167	6.5744 4.2563 2.4682 3.5751 3.7204 3.5331 3.5401 11 PPFSSUPF PL 3.5331 3.5401 11 78FSSUPF PL 3.5331 3.701	1.2791 2.74175 1.3594 1.1181 1.0609 1.0609 1.0639 PAYITO FAR PL/PN 1.0509 1.0639 PAYITO FAR PL/PN 1.0624 1.0609	0. 056949 9. 033024 9. 047165 0. 047179 0. 047232 0. 047232 0. 047232 0. 047232 0. 047387  DEG SIMPRO (0 91/PTE 9. 047307	0.076250 0.10898 0.11494 0.10906 0.10906 0.10937 0.10937 0.10937 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 117 127 127 127 142 157 5555111000 157 5555111000 167 177	6.5744 4.2563 2.4682 3.5751 3.5701 3.5701 11 PPFSSUPF PL 3.5701 3.5801 11 PRFSSUPF PL 3.5701 1 PRFSSUPF PL 3.5701 1 PRFSSUPF PL 3.5701	1.7791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639 1.0639 1.0639 1.0639 1.0639 PAYIOS . 20 PL/PRI 1.0624 1.0609 PAYIOS . 80	0. 656 949 2.033024 3.347165 0. 549779 0.047232 0.647367 WITTTLE FLAP 0.047232 0.47387  DEG SEPTEND 11 0.047303 0.047322	0.076250 0.10898 0.10896 0.10906 0.10937 0.10937 0.10937 0.10937 0.10937 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 117 127 127 127 142 157 5555111000 157 5555111000 167 177	6.5744 4.2563 2.46A2 3.5311 3.5311 3.5401 II PPFSSUPF PL 3.5311 3.5401 II PRFSSUPF PL 3.5301 3.701 PRFSSUPF PL 3.701 PRFSSUPF	1.7791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639 1.0639 1.0639 1.0639 1.0639 PAYINS . 20 PL/PM 1.0624 1.0609 PAYINS . RO	0. 656 949 2.033024 2.033024 3.047165 0.047232 0.047232 0.047232 0.047232 0.047232 0.047327 0.047327 0.047327 0.047327 0.047327 0.047327	0.076250 0.10896 0.10906 0.10906 0.10937 0.10937 0.10937 0.10937 0.10937 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 117 127 127 137 147 167 5500111000 167 5600111000	6.5744 4.2563 2.4682 3.5751 3.5701 3.5701 11 PPFSSUPF PL 3.5701 3.5801 11 PRFSSUPF PL 3.5701 1 PRFSSUPF PL 3.5701 1 PRFSSUPF PL 3.5701	1.7791 7.74175 1.3594 1.1181 1.0609 1.0609 1.0639 1.0639 1.0639 1.0639 1.0639 PAYIOS . 20 PL/PRI 1.0624 1.0609 PAYIOS . 80	0. 656 949 2.033024 3.347165 0. 549779 0.047232 0.647367 WITTTLE FLAP 0.047232 0.47387  DEG SEPTEND 11 0.047303 0.047322	0.076250 0.10898 0.10896 0.10906 0.10937 0.10937 0.10937 0.10937 0.10937 0.10937	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

	MASS-LEHES	bit la	NAPY PATA	06/11/7°	CADDELL	PEC 10/17/7	9 02:27:16.962	far areas	PGP (Q34	PRG 1170
,	>*************************************	L PRESSUPE	#ATIOS . PRI	MARY PLUG						
~	evn inte	rı	PJ /PI)	PL / PTF	PI /PT#	x/OMAX				The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th
	15	12.572	3,7490	0.16822	0.43525	3.43209				
	37	6.3467	7,0936	0.092949	0.24049	2.53000				
٠-	47	A. 1423	2.4539	0.13895	6.791##	0.62900				
	E 2	P=3923	2.5121	9.11199	Q. 20742	v. 72790				
_	APPRI TERRAC		PATINS . FLO							
						X / PWAX				
	TAU MUNIC	9.5226	PI / PG	M /PTF	PL /PTP					
	6.7 4.7	14.612	7. 9699 4.4036	0.12741	0.12966 0.50585	0.42200 0.692 <b>00</b>				
-		174716	3,71129	176 19 3 3 1	0.30283	V*???¥¥		**- *** <del>******************************</del>	~ <del>~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ </del>	
_	>400 LT 10MA	PPESSUPE_	RATIOS . FIG	H SPLITTEP O	. 0		a company and a	-		4 .
	AND HORD	PL	<b>PL/</b> Pባ	M /PTF	PI /PTP	X/DMAX			***	
•	77	24.911	9. 71 30	0.3Pf 94	1.0009	0.56400				
	<u> </u>	9.1575	2.75 GR	0.12253	0.31703	0.63500				
_	97	3.5434	1.7646	0.047417	0.12268	J. 69200				
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_	11?	4.2544	1.7972	0.04692#	0.14729	0.83000				
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്ടുമോഷ്യിലെ ക്രാ<del>സ്ക്രൂം. പ്രത്യം ത്രൂത്ത്</del>യ ത്രൂര്യ്യ് ആരുക്കുന്ന അവുക്ക് എന്നു എന്നു വരുന്ന വേശന അവരുന്നു. വിവരം വരു വരുന്നു വരുന്നു വരുന്നു.

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>40017 104	AL PRESSIME	RATIOS , PPI	MAPY PLUG		
VO WOPO		PL/PN	P1 / PTF	PI /PTP	X/DMAX
32	PI 11.344	3.3508	0. 16797	0.435=7	0.43200
27	6.1389	1.8535	0.18797	0.24094	1. 53030
47	7.1503	2.1694	7.10875	0.28201	0.62900
F. 7	7.3005	2.2150	0.11104	0.28743	0.72700
SADDET FON	AL PRESSUPE	RATIOS , FLO	W SPLITTEP I	.n.	
ላቦ ሐባቀበ	PL	PL /PO	PI /PTF	PL /PTP	X/DMAX
62	8.4368	2.5597	0.1203?	0.33274	0.42200
67	14. 526	4.4971	0.22093	0.572#9	0.69200
************************	AL PRESSURE	PATIOS . FLO	W SPLITTER C	.D.	
מפחש חצי	PL	PL /PO	PL /PTF	PL/PTP	X/DMAX
77	25.678	7,7900	0.29045	1.0129	0.56400
A2	8.0563	2.4443	0.12253	0.31774	0.63500
97	3,5196	1.0679	0.053531	0.13891	J-69200
>ADDÍTÍÐN	AL PRESSIPE	PATINS . FJF	CTCP SHPOUD		
vo woed "	PĹ	PL/PN	M /PTF	PI /PTP	X //MAX
107	5.9237	1.7977	0.090095	0.23363	0.62400
112	1,7350	1.1332	0.056808	0.14731	0.43000
122	2.1719	0.65894	0.033032	0.085657	0.56000
127	3,4446	1.0572	0.05299A	0.13743	1.0966
137	3.1098	0.94322	7.647283	9.12761	1.7200
14?	2.7932	1,84745	0.042482	0.11016	1.3500
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vi unën "	PL	PL /PR	PL /PTF	PL /PTP	VOMAN
107	5.9237	1.797?	0. 090095	0.23363	1/5000 -1 0000
i 17	7.7350	1.1332	0.056800	0.14731	1.0000
122	2.1718	0. 65 294	0.033032	0.045657	-1.0900
127	4.446	1.0572	0.0525.4	0.13755	-1.0000
137	3.3098	0.94322	0.047283	0.12761	-1.0000
142	2.73	0. 84745	0. 642442	0611016	-1.0000
152	3.5746	1.0633	0.652303	C.13822	-1.0000
157	3.5046	1.0633	0.0533037	0.13777	-1.0000
SANTITION	AL PURSSUPE	PETTOS FAR	HOTELE FLAD		
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162	3.5946	1.0633	0.053303	0.13022	-1.0000
157	3.5746	1.0633	0.053304	0.13R22	-1.0000
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1 / 7	3.5096	1.7648	7.752379	3,13842	-1,000
	2,0046	1.0433	0.053303	0.1422	-1.0000
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33	12.442	2,7747	3.14926	0.43647	0.43200		
?7	6.8702	2.0843	0.104=0	0.24101	J. 53000		
47	A. 0459	2.4410	0.12239	0.29225	0.62900		
52	9.2359	7,4096	7.12462	0.20707	0.72740		
NULTICOR	AL PHESSIPE	PATINS . FIR	W SPLITTER I	. n.			
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67 67	9.4564 14.462	7 <b>.</b> 9699 4 <b>.</b> 3874	0.14385 0.21598	0.33174 0.50732	0.42200		
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77	25.673	7, 7888	7.39052	0.90062	0.56400	- · · · · · · · · · · · · · · · · · · ·	1,000 - 00 - 0
72	B,0509	2,4425	0.12247	0. 2P243	ψ _e € 35 <b>0</b> 0		
c 2	3.5218	1.0685	0.053571	0.12355	0.69290		
NOT TECOM	AL PRESSIME	PATINS . FJE	CTOR SHROUN		en en en en en en en en en en en en en e	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th
VD WIPD	PL	PL /PO	M /PTF	PI /PTP	X/DHAX	n cale o compression and compression of the second	ساند و المحافظة المحافظة المراسية المرس والمحافظة المحافظة
107	5.9144	1.7944	0. CR9967	0.2074F	2.62400		
113	3.7321	1.1323	3.056779	0.13097	0.83000		
122	2.1749	9. 65980	0.033081	0.076297	0.96000		
27	3.4967	1.0400	0.053150	0.12267	1.0900		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
137	3.2614	0.98947	9.049611	0.11441	1.2200		
147	3.1062	0.94739	0.047250	0.10497	1.3500	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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137	5,9144	1.7944	0.CR9967	0.2074#	-1.0000	•	
117	3.7321	1. 1323	0. 056773	0.13092	-1.0000		a special to the second of the contract of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of t
177	2.1749	0.65980	0.033061	0.076293	-1.0000		
12-	3.4967	1.0609	2.053190	0.12261	-1.0000		
137	3.2614	0. 25947	0. 049611	0.1/641	-1.0000		
42	3.1062	.)•°423A	0.047250	0.17441	-1.0000		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
152	3.5010	1.0f 24	0.053267	0.12284	-1.0000		
157	3.5110	1.0554	0.051419	0.12319	-1.0000		
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152	3.5019	1.0624	0.053267	0.12274	-1.0000		. , ,
[57	3.5114	1.0654	253410	0.17319	-1.0000		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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YO WUPD	Pl /	PI /PI	PF/PYF	VP1 /PTF	x/DMAX	. = .	
147	3.5349	1.0639	0.053343	12302	-1.0000		
172	3,7119	1.0654	9.053419	0.12310	-1.0000		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
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77 10720	2.79	17073	7.71 0.041	0.207 0.	959 0.98	1.015	0.7773	<b>4,770</b> 7	1.0177	7.7100	1.7170			
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NASA-LFWI	S PRELIMI	MARY DATA	06/28/79	CADNETT	REC 10/18/79 00:47:05.889	FAC SKEX1	PGM C034	MOR 1502
>ACDITION	AL PRESSURE	RATIOS . PRI	MARY PLUG					
IVD WORD	PL	PL / PO	PL /PTF	PL/PTP	X/DMAX			
32	14.540	4.3561	7.21954	U.43746	0.43200			
37	A.02A7	2.40-3	0.12123	0.24156	0.53000			
47	9.3984	2.8157	0.14141	0.28276	0.62900			* v. v.
52	9, 5783	2.8696	0.14463	3.29818	0.72700			
>ADD ET TON	AL PRESSURE	RATIOS . FLO	W SPLITTER I	• 0•				THE RESIDENCE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF T
VD WORD	PL	PL/PO	M/PTF	PL/PTP	X/DMAX			
95	11.093	3.3232	0.16749	0.33374				
67	13.091	3.9220	0-19767	0.39387	0.69200			
>ADDIT ION	AL PRESSURE	RATIOS . FLO	M SPLITTER O	. D.		and the graph page of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco		minimization and problem distinguishing the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control
VD HORD	PL	PL/PO	PL/PTF	PL /PTP	X/DMAX			
77	26,223	7, 8963	0.39596	0.78697	0.38400			
82	R.1937	2.4548	0.12372	0.24452	0.63500			·····
92	3.5027	1.0674	0.053795	0.10719	0,89200			
>ADDIT TON	At PRESSURE	9 <del>13 , 20</del> 1748	CTOR SHROUD			na anggang ng nakata sa ja dibinang naka na ang at	make make a second control of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
AD MOND		PL/PO	PLIPTE	PI. /PIP	X7DWAX			
107	8.0737	2.4188	0.12191	0.24291	0.62400			
112	3,9279	1.1708	0.039309	0:t1818	0:63000	~ <del></del>		
155	2.3516	0.70456	0.035510	0.070756	0.96000			
127	3.5477	t.0629	0.053568	0.10674	1.0900			
137	3.7328 	1.1103 1.0498	0.056363 0-059230	0.11231 	1.2200 			
>4001 <b>730</b> 4	AL-02233972:	241101 . POP	24007 EMET					
VO MORO	- <del>N</del>	PL/PD		PL /PTP	TONAT	en la companya de la companya de la companya de la companya de la companya de la companya de la companya de la		
107	6.0737	2.41 88	0.12191	0-24291	-1,0000	•		
-115	<del> 3.9279</del>		···· 0.059309~		<b>71.0000</b>	·		
	2.3510	0.70456	0.035510	0.070756	-1.0000			
·12? `	<b></b>	1.0629	<del>0.033988</del>	0.10079	-1.0000			
127					7 7 7 2 2 2 2			
127 137	3.7328	1.1183	0.056363	0.11231	-1.0000			
127 137 142	3.7328	1.1183	0.055230	0 × 1005	-1.0000	ndyn dy'n de yn deithiol de yr yn gymrygy, yndd i'r rinn o ryger, y	- Paragraphy and gradients of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of the paragraphy of	de capación discollination, secrega, in or disconación (par el 1800) el sena
-127 -127 -137 -142 -152	3.1328 3.6578 3.5527	1.1183 1.0998 1.0644	0.055230	0.10689	-1.0000 -1.0000			ng gyanga Marikatang sarangga A - A Milatan Antilipp A Milatan Antil
127 137 142 152	3. 7324 3. 6574 3. 5527 3. 5527	1.1183 1.0998 1.0644 1.0644	0.055230 0.053644 0.053644	0 × 1005	-1.0000		. The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second sec	
127 137 142 152 157 >aont104	3. 7324 3. 6574 3. 5527 3. 5527	1.1183 1.0998 1.0644	0.055230 0.053644 0.053844 WOZZIS FLAP	0.10689	-1.0000 -1.0000			
127 137 142 152 157 >ADD 17 104	3.7328 3.6578 3.6577 3.5527 3.9527 ML PRESSURE	1.1183 1.0958 1.0644 1.0644 RATIOS PAN	0.055230 0.053644 0.053644 HOZZIS FLAP	0.1005 0.10689 0.10689	-1.0000 -1.0000 -1.0000			
-127 -137 -142 -152 -157 	3.5527 3.5527 3.5527 3.5527 3.5527	1.1183 1.0958 1.0644 1.0644 RATIOS PAN	0.055230 0.053644 0.053644 HOZZID FLAP 0.053644	9.1005 0.10689 0.10689 91.7979 0.10689	-1.0000 -1.0000 -1.0000			
127 137 142 152 157 >ADDITION	3.7328 3.6578 3.6577 3.5527 3.9527 ML PRESSURE	1.1183 1.0958 1.0644 1.0644 RATIOS PAN	0.055230 0.053644 0.053644 HOZZIS FLAP	0.1005 0.10689 0.10689	-1.0000 -1.0000 -1.0000			
127 137 142 152 157 >ADDITION VO MORD 152	3.5320 3.6570 3.6577 3.5527 3.9527 ML PRESSURE PL 3.5527 3.5527	1.1183 1.0958 1.0644 1.0644 RATIOS PAN	0.053230 0.053644 0.053844 WOZZIS PLAP 0.053644 0.053644	0.10689 0.10689 0.10689 0.10689	-1.0000 -1.0000 -1.0000			
127 137 142 152 157 >ADDITION	3.5320 3.6570 3.6577 3.5527 3.9527 ML PRESSURE PL 3.5527 3.5527	1.1183 1.0958 1.0644 1.0644 RATIOS PAN PL/PO 1.0644	0.053230 0.053644 0.053844 WOZZIS PLAP 0.053644 0.053644	0.10689 0.10689 0.10689 0.10689	-1.0000 -1.0000 -1.0000			
127 137 142 152 157 >ADDITION IND MORD 152 >ADDITION IND MORD IND MORD 140 IND MORD	3.5527 3.5527 3.5527 3.5527 3.5527 ML PRESSURE PL 3.5527 ML PRESSURE PL 3.5527	1.1183 1.0958 1.0644 1.0644 1.0644 1.0644 1.0644 1.0644	0.059230 0.053644 0.053644 NOZZIS PLAP 0.053644 0.053644 DEG SIRPORT	9 1005 0.10689 0.10689 0.10689 0.10689	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 142 152 157 >ADD IT ION 150 157 >ADD IT ION 157 >ADD IT ION 140 HORD 167	3.5327 3.6578 3.6578 3.5527 3.9527 ML PRESSURE PL 3.5527 3.5527 ML PRESSURE	1.1183 1.0998 1.0644 1.0644 RATIOS PAN PL/PO 1.0644 1:0644	0.053230 0.053644 0.053644 NOZZID PLAP 0.053644 0.053644 0.053644	9.1005 0.10689 0.10689 0.10689 0.10689	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 142 152 157 >ADD IT ION 150 157 >ADD IT ION 157 >ADD IT ION 140 HORD 167	2477 3.1320 9.0578 3.5527 3.5527 3.5527 3.5527 ML PRESSURE PL 3.5527 3.5527 3.5527	1.1183 1.0958 1.0644 1.0644 1.0644 1.0644 1.0644 1.0644	0.053644 0.053644 0.053644 0.053644 0.053644 0.053644 0.053644	0.10689 0.10689 0.10689 0.10689 0.10689 0.10689 0.10689	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 -137 -142 -152 -157 -20017104 -152 -157 -20017104 -167 -172 -20017104	3.5527 3.5527 3.5527 3.5527 3.5527 ML PRESSURE PL 3.5527 ML PRESSURE PL 3.5527 3.5527	1.1183 1.0958 1.0644 1.0644 1.0644 1.0644 1.0644 1.0644 1.0644 1.0644	0.059230 0.053644 0.053644 NOCELD PLAP 0.053644 0.053644 DEB SHRIVELL 0.053644 0.053644	0.1005 0.10689 0.10689 0.10689 0.10689 0.10689 0.10689	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 -137 -142 -152 -157	3.5527 3.5527 3.5527 3.5527 3.5527 ML PRESSURE PL 3.5527 ML PRESSURE PL 3.5527 3.5527	1.1183 1.0998 1.0644 1.0644 RATIOS PAN P/PO 1.0644 1.0644 1.0644	0.059230 0.053644 0.053644 NOCELD PLAP 0.053644 0.053644 DEB SHRIVELL 0.053644 0.053644	0.1005 0.10689 0.10689 0.10689 0.10689 0.10689 0.10689	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

NASA-LEWI	IS PRFLIM	INARY DATA	06/28/79	CADDETT	REC 10/18/79 00:48:38.921	FAC REGEL	PG# C034	17UN 17
>ADDITION	VAL PRESSURE	RATIOS . PRI	MARY PLUG		•			
AVD WORD	PL	Pt./P0	PL/PTF	PL/PTP	X/DMAX			
32	12.505	3.7774	0. 19117	D. 43869	0.43200			
37	6.9107	2.0876	0.10565	0.24244	0.53000			
47	5.0508	2.4411	0.12354	0.28349	0.62900			
52	1.2458	2.4909	0-12606	0.28928	0.72700			
>ADD IT IOR	ML PRESSURE	RATIOS , FLO	W SPLETTER E	.0.		in the Marketine	n a santa i de la compania	r <del>an</del> gere
AVD WORD	PL	PL/PO	PL / PTF	PL/PTP	X/DMAX			
62	7.6407	2. 9123	0.14730	0.33872	0.42200			
67	12.974	3.9193	0. 19835	0.45517	0.69200			
>400 IT ION	ML PRESSURE	RATIOS . FLO	W SPLITTER O	.D.				
AVD WORD	PL	PL/PO	PL/PTF	PL /PTP	x/DMAX			
77	25. 944	7.8373	0.39663	0.41018	0.56400			
82	9-1058	2.4486	0. 12392	0.28437	0.43500			
92	3.5440	1.0706	0.054180	0-12433	0. 59200			
>ADDITION	ML PRESSURE	RATIOS , EJF	CTOR SHROOD					
AVD WIND.	Pt	PL7P0	PE/PTF	PLIPTP	XYUMAX			
107	7.9708	2.4079	0. 121 06	0.27964	0.62400			
115	3-11792	1.1719	0.059305	0.13604	0.83000			
122	2-3228	0. 70167	0.035510	0.001400	0.96000			
127	3.5190	1.0630	0.053797	0.12349	1.0900			
137	3.2637	0.98592	0.049895	0.11450	1.2200			
142	3.1686	0.95719	0: 04842	0.11116	1.3900			
X1:0011101	al berious	*******	**************************************					
AVID WINED	Pt.	PL/PO	PL /PTF	PLIPTP	KICHAR			
-107	7.9708	2.4079	0.12186	0.27964	-1.0000			
-117	3-8792	1.1719	0.059305	0.13609	-2:0000			
-122	2.3220	0.70167	0. C35510	0.081488	-1.0000			
-127	SE 21 40	1.0630	0.053797	0-12343	-1.0000			
-137	3.8637	0. 98592	0.049895	0.11550	-1.0000			
-142	3.168	0.95719	0.048442	- 0,21116	-1.0000			
-152	3-5290	1.0660	0.053950	0.12380	-1.0000			
-157	3. 9290	1-0000	0. 053950	0.12380	-1.0000			
> <u>*D71710</u> 1	Mt PRESSURE	RATIOS C PAN	HOZZLO FLAP					
AVD WORD	PL	PE 190	Kim	PLIPTP	T/ORAT			
	3.5290	1.0660	X0.053950	0.12300	-1.0000			
-152	3.9290	1.0699	prosseso-	0:12380	-1.0000			
-157 -157								
-197		מס ו פויזעייי	DES 31M CONT.	DUAT TUM				
-197 -> <del>************************************</del>	ME PRESSURE	/		<b>\</b>				
-197 >ADDITION AVD WORD	Pl/	91.790	PL/PTF	ME YELF	X/OMAX			
-157	3.5290	1.0660	0.053950	g>£5380	-1.00 <b>00</b>			
-197 >ADDITION AVD WORD	Pl/							
-197 	3.5290 3.8290	1.0660	0.053950 0.053990	0.15380	-1.00 <b>00</b>			
-197	3.5290 3.8290	1.0660 1.0660 PATIOS , 80	0.053950 0.053990	0312380 0.12380 ncat ton	-1.00 <b>00</b>			
-197 	PL 3.5298 3,8290 pt <del>pressure</del>	1.0660 1.0660 PATIOS , 80	0.053950 0.053990 DEG SHROUD L	0312380 0.12380 ncat ton	-1.0000			

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	S PRELIMI	NAPY DATA	96/28/79	CADDETT	REC 10/19/79 00:50:12.050	FAC SYGXL	PGM (034	### 79 RNG 1207
>ADD T T COM	N PRESSIME	RATIOS . PRI	MARY PIUG	•				
AVD WORD	PL	PL /PD	PL/PIF	PL/PTP	X/DMAX			
32	11-139	3, 3616	0.16834	0.43702	0.43200			_
37	6.1656	1.8613	0.093235	0.24197	0. 53000			
47	7.2058	2.1753	- 0.10897	0.28280	0.62900			
52	7.3799	2.2251	0-11146	0.28928	0.72700			
	<del></del>				0.72700			
>ANDITION	AL PRESSURE	RATIOS . FLO	M SPLITTER I	. D	e spice from the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the cont	**		
TAU MUMD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX			
62	8.6379	2.6070	0.13059	0.33893	0.42200		· production and the second second second	
67	12.904	3. 6956	0.19514	0.50645	0.69200			
>40017100	AL PRESSURE	RATIOS . FLO	W SPLITTER O	.D.				
WD WARD	PL	PL /PD	PL/PTF	PL/PTP	X/DMAX		The same of the same of the same	
	20:159	7.8755	0.39990	1.0264	0.98400			
82	8.1609	2.4636	0.12341	0.32020	0.63500			
45	3.7390	1.000	0.093918	0.13887	0-89200			<del></del>
>40017 1mm	t- PRESSURE-	RATIOS EJE	CTCP SHADIO	_ <b>_</b>	en com se communication and production and communication and commu	- M on the r on the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of 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the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of th	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second 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second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	the consequently represent the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second 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VO WORD		PL790	PL/PTP		R/DMST			
107	0.0759	2.4300	0.12212	0.31695	0.62400			
112	3.9293	1.1847	0. 059343	0.19401	0.83000			
122	2.3428	0.70726	0.035428	0.091947	0. 96000		-	
127	3.5140		0.053138	0:13791	1.0700	· +		
137	2.9435	0. 68858	0.044511	0.11552	1.2200			
142	2.8734	0.86743		0.11277	1.3900			
				00000				
24021 <b>7.10</b> 11	H- 20013W00	RATIOS - DO	8000Y-14L87		7	<del></del>		<del></del>
AD RUSS	-Pt	72/90	PL/PTF	91-7919	Trongs			
107	0.0759	2.4300	0. 12212	0.31695	-1.0000	•		
		1.1847	0.059343		1.0000			
-112	3:4763		0.035428	0.091947	-1.0000			
	3 <del>.9243</del> 2.3428	0. 70726						
122	2. 3428	0. 70726						
127	2.3428	1.0000	0.055150	0-13791	-1.0000 -1.0000			
-127 -127 -137	2.3428 9.9140 2.9435	1.0000 0.88858	0.099190 0.044511	0.32552	-1.0000			
122 127 137 147	2.3428 2.9140 2.9435 2.8136	1.0000 0.88858 0.86743	0.099198 0.044511 0.049491	0.14552 9c11277	-1.0000 -1.0000	of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of		
127 127 137 147	2.3428 2.5140 2.4435 2.8736 3.5240	0.88858 0.86743 1.0638	0.055150 0.046511 0.045451 0.053289	0.12552 0.11277 0.13030	-1.0000 -1.0000 -1.0000			
127 127 137 147	2.3428 2.9140 2.9435 2.8136	1.0000 0.88858 0.86743	0.099198 0.044511 0.049491	0.14552 9c11277	-1.0000 -1.0000			
122 127 137 147 152	2.3428 2.5140 2.4435 2.8736 3.5240	0.88858 0.86743 1.0638	0.059190 0.044511 0.043951 0.053289 0.053289	0.12552 0.11277 0.13030	-1.0000 -1.0000 -1.0000			
127 127 137 149 152 157	2. 3428 3. 7140 2. 9435 2. 9734 3. 5240 3. 5240	1.0000 0.8858 0.96749 1.0630 1.0630	0.055150 0.04511 0.045451 0.053289 0.053289	0.14552 0.11277 0.13030 0.13030	-1.0000 -1.0000 -1.0000			
127 127 137 147 149 152 157 20017 10%	2, 3428 9, 9140 2, 9140 2, 9435 2, 8736 3, 5240 3, 5240 11. PRESSURE	1.0000 0.8856 0.86743 1.0638 1.0638	0.059190 0.04511 0.04991 0.053289 0.053289	0.14552 0.11277 0.13030 0.19030	-1.0000 -1.0000 -1.0000 -1.0000			
-112 -122 -137 -147 -152 -157 -20017 104 LVO WORD -152 -157	2. 3428 3. 7140 2. 9435 2. 9734 3. 5240 3. 5240	1.0000 0.8858 0.96749 1.0630 1.0630	0.099190 0.04511 0.04991 0.053289 0.053289 WOFZIE PLAP	0.14552 0.11277 0.13030 0.13030	-1.0000 -1.0000 -1.0000			
127 127 137 137 147 152 157 280017 10% VO WORD 152 157	2, 3428 9, 9140 2, 9143 2, 8736 3, 5240 3, 5240 PL 3, 5240 9, 5240	1.0000 0.48456 0.80749 1.0638 1.0638 RATIOS PAN PL/PIT 1.0638	0.099190 0.04511 0.04991 0.053289 0.053289 WOFZIE PLAP	0.18552 0.11277 0.13030 0.19030 0.19030 0.13030	-1.0000 -1.0000 -1.0000 -1.0000 R/OWAX -1.0000			
122 127 137 149 152 157 20017 10%	2.3428 9.7140 2.9435 2.8734 3.5240 3.5240 9.5240 9.5240	1.0600 0.88556 0.86745 1.0630 1.0630 1.0630 1.0630 1.0630	0.099190 0.044511 0.04991 0.053289 0.053289 WOFZIE PLAP PL/PTP 0.053289 0.053289	0.1852 0.11277 0.13030 0.19830 0.19830 0.13830 0.13830	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 127 137 149 152 157 2001710W	2. 3428 9.7140 2. 9435 2. 8736 3. 5240 3. 5240 3. 5240 3. 5240 3. 5240 4. PRESSURE	1.0000 0.48456 0.80749 1.0630 1.0630 RATION PAN PL/PD 1.0630 1.0630 PL/PD	0.099190 0.046511 0.0494951 0.053289 0.053289 0.053289 0.053289 0.053289	0.1852 0.13030 0.13030 0.13030 0.13030 0.13030 0.13030	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
-127 -127 -137 -147 -152 -157 -240017 10% -152 -157 -240017 10%	2.3428 9.7140 2.9435 2.8734 3.5240 3.5240 9.5240 9.5240	1.0600 0.88556 0.86745 1.0630 1.0630 1.0630 1.0630 1.0630	0.099190 0.044511 0.04991 0.053289 0.053289 WOFZIE PLAP PL/PTP 0.053289 0.053289	0.1852 0.11277 0.13030 0.19830 0.19830 0.13830 0.13830	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 127 137 147 152 157 20017 10W 152 157 20017 10W 167 167	2.3428 9.7140 2.9435 2.8734 3.5240 3.5240 9.5240 9.5240 9.5240 9.5240 9.5240 9.5240	1.0600 0.8858 0.86745 1.0638 1.0638 1.0638 1.0638 1.0638 1.0638 1.0655 1.0655	0.099190 0.046511 0.049991 0.053289 0.053289 0.053289 0.053289 0.053289	0.1852 0.11277 0.13030 0.19830 0.19830 0.13830 0.13830 0.13830 0.13850 0.13850	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 127 137 147 152 157 20017 10% 152 157 20017 10% 140 WOPD 167 167 172	2, 3428 3, 9140 2, 9140 2, 9174 3, 5240 3, 5240 HL PRESSURE PL 3, 5240 HL PRESSURE PL 3, 5270 3, 5270 3, 5270 ML PRESSURE	1.0000 0.88558 0.86749 1.0638 1.0638 1.0638 1.0638 1.0638 RATIOS 20 PL/PR 1.0653 1.0653	0.099190 0.044511 0.049991 0.053289 0.053289 0.053289 0.053289 0.053289 0.053365 0.053365	0.18552 0.11277 0.13030 0.19030 0.13030 0.13030 0.13030 0.13050 0.13050	#/OMAR -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
122 127 137 139 139 152 157 20017 104 140 4080 167 167 167 167 167	2. 3428 9. 9140 2. 9435 2. 8734 3. 5240 3. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240 9. 5240	1.0000 0.8858 0.86743 1.0638 1.0638 1.0638 1.0638 1.0638 1.0638 1.0653 1.0653	0.099190 0.044511 0.043991 0.053289 0.053289 0.053289 0.053289 0.053289 0.053365 0.053365	0.1852 0.11277 0.13030 0.13030 0.13030 0.13030 0.13030 0.13030 0.13050 0.13050	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
-122 -127 -137 -137 -152 -157 -20017104 -150 MORD -152 -157	2, 3428 3, 9140 2, 9140 2, 9174 3, 5240 3, 5240 HL PRESSURE PL 3, 5240 HL PRESSURE PL 3, 5270 3, 5270 3, 5270 ML PRESSURE	1.0000 0.88556 0.80749 1.0630 1.0630 1.0630 1.0630 1.0630 1.0633 1.0653 1.0653 1.0659	0.099190 0.046511 0.093991 0.053289 0.053289 0.053289 0.053289 0.053289 0.053385 0.053365 0.053365	0.1852 0.11277 0.13030 0.13030 0.13030 0.13030 0.13030 0.13050 0.13050 0.13050	#/OMAR -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

NASA-LEWI	2 Luchia	MARY DATA	06/28/79	CADDETI	REC 10/18/79 00:51:53.159 FAC 8X6X1 PGM C034 RDG 1208
>ADDITION	AL PRESSURE	PATIOS . PRI	MARY PLUG		
VN WORD	PL	PL/PO	PL / PTF	PL /PTP	X/DMAX
32	16.217	4.8829	0.21859	0.43778	0.43200
37	8.9335	2.6898	0. 12041	0.24116	0.53000
47	10.459	3.1490	0.14097	0.28234	0.62900
52	10.684	3. 21 68	0.14400	0.28841	0.72780
>40011100	····		W SPLITTER I		
-					A SAMAN
VD WORD -	PL 12.243	PL / PO	PL /PYF	PL/PTP	X/ONAX
67	12.933	3.6864 3.8640	0.16503 0.17298	0.33052 0.34644	0.422 <del>00</del> 0.69200
			W SPLITTER O		
			· <del></del>		
VD WORD 77	PL	PL/PO	PL/PTF	PL/PTP	X/ONAX
	27.306	8.8239	0.39502	0.79113	0.56400
82 <del>92</del>	9.1786	2.7636	0.12372	0.24778	0.63500
76	3,5451	1.0674	0.047785	0.095703	0.69200
>ADDITION	ME PRESSURE	RATIOS . EJE	CTOR SHPTION		
VD WORD.	- M	WL 7PO	PLYPTE	PEPPP	X/MAX
107	9.0735	2.7320	0.12230	0.24494	0.62498
112	4.4010	1.3251	0.059322	0.11881	0.83008
122	2.6290	0.79158	0.035436	0.070971	0. 96000
127	3.9351	1.0644	0.047650	0.095432	1,0700
137	4.1758	1.2573	0.056286	0.11273	1.2200
142	4.0807	1.2287	0.055004	0.11016	1,396
3) X (W.) X ( 2 ) ( 10	1 1 4 min 2 4 3 1 1 1 2 min	241105 PO			7
AB MUKU	PL	PL7P0	PLYPTF	PL/PTP	
107	9.0735	2. 7320	0 <b>.</b> 122 <b>30</b>	0.24494	-1,0000
112	4.4010	1.3251	0.059322	0.11881	1.0000
122	2.6290	0.79158	0.035436	0.070971	<b>∕</b> -1.0000
127	<b>Q.3331</b>	1.0644	0.047650	0.045582	-1-0909
137	4.1758	1.2573	0.056286	0.12273	-1.0000
145	4.0967	1.2287	0.055004	- 94(1016 -	-1.0000
152	3.5351	1.0644	0.047650	0.095432	-1.03 <b>00</b>
157	3.54013	1.0659	0:047717	0.095567	-1.0000
>ADDIT TON	AL PRESSURE	RATTOS . PAR	HOTELE PLAP		
VD WORD	. pt		MITTE		
152	3.5351	1.0644	< 0.047650	PL/PTP 0.095432	-1.0000
	3.5401	1.0659		0.095567	
	J. 740E		-	VeU72201	- 99 AAAA
PADOTT TON	ME PRESSURE	RAZETIS . 20	DEC SHEUMD FO	RCATTON	
AU AUED	Pt	PL/PO	PLIPTE	PLIPTP	T/OHAX
167	3.5401	1.0659	0.047717	0.095567	-1.0000
172	3,5401		0.047717		-1.0000
>400 <b>11-10</b> 9	MESSURE	RATIOS . 80	DEG SIMOUD L	OCATION -	
AD AULD.			PL/PTP		X760AX
102	3.3449	1.0071 0.98000	0.045086	0.090297	-1.0000 -1.0000
187					

MASA-LEWI	S PRFE 191	NARY DATA	06/28/79	CADDELL	REC 10/18/79 00:52:38.836 FAC 8X681 PGM C036 RNG 1209
		RATIOS , PRI			
AVD WORD		PL/PG	·		of Africa
32	PL 14.195***	4.2527	PL / PTF	PL/PTP 7-43745	V.43200
37	7.8314	2.3463	9.10439	0.24135	0.53000
47	9.1704	2.7474	0.12224	0.28262	0.62900
52	9, 3602	2.8043	0.12477	0.28847	0.72700
>ADDIT MN	AL PRESSURE	RATIOS , FLO	W SPLITTER I.	. D.	
AD MUND	PL	PL/P0	PL/PTF	PL/PTP	X/DMAX
	10.689	3. 2024	0.14248	0.32942	0.42200
67	12.756	3.8218	0-17003	0.39314	0,69200
>ADDIT TON	AL PRESSURE	RATIOS , FLO	W SPLITTER B.	. 0.	
VO HORD	PL	PL/PO	PL/PTF	PL/PTP	X/DRAX
77	29, 602	8,9690	0.39457	0.91229	0.98400
62	9.2803	2.7804	0-12370	0.28601	0.63500
92	3.5677	1.0689	0.047555	0-10995	9.89200
>And1 <b>110</b> N	AL PRESSURE	RAT103 . EJE	CTOR SHPOUD		
AD AUKD	- <del>M</del>		PLIPTE	PLIPTP	X/OHAX
107	9.1604	2.7445	0.12210	0.20231	0.42400
112	+.4458	1.3310	0.039219	0-13692	0.83000
122	2.6625	0.79770	0.035490	0.082056	0.96990
127	3.5477	1.0629	0.047289	0:10934 -	1:0900
137	3.7127	1.1123	0.049488	0-11442	1.2290
142	3.6077	1.0807	0.048089	0.11119	1,3500
3400 12:20 W	41-406-55100	2.41264 201	PRINT 114 27		
VIT WORD	9.1604	PL/PN 2.7445	0.12210	PL/PTP 0-29231	-1.9 <b>40</b> 0
115			0. C59219	0.27231	
-122	2.6625	0.79770	0.035490	0-082056	-1.0000
127	3-9477	1:0429	0.047289	0.10934	-1.0000
-137	3. W27	1.1123	0.049488	0.11542	-1.0000
-142	3.60 Pt	1.0809	0.048089	0. M119	-1.0000
-152	3.5577	1.0659	0.047422	0.10964	-1.0000
-157	3.5577	1.0659	0.047422	0.10964	1-0000 mentioned and the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of
-> <del>&gt;&gt;011110</del> 4	AL PRESSURE	*******	- WORTE FLAT		
LYD WORD	Pt	PL/PD-	Rime	PL/P1P	TO THE RESIDENCE COMMON CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRA
-152	3.5577	1.0659	X0.047422	0.10964	-1.0000
-157	3.5577	1.0659		0. t0964	1.0000 The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the secon
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-167 -172	3.5577	1.0659 1.0659	0.047422 0.047422	0.18964	-1.0000
<del>/101 7 1 () () A&lt;-</del>	AT TRESSUPE	## <del>***********************************</del>	DEB SIRCUD LI	DEATION -	
AVO MOSE	Pt	- PL/PO	- PL-/PTF	PL /PTP	
/	3.3527	1.0045	0.044689	0-10333	-1.00gg
-192 -191					

NASA-LFWI		NARY DATA	06/28/79	CADDELL	REC 10/18/79 00:53:33,972 FAC 8X6X1 PGM C034 ROG 1210
MOI TIONS	AL PRESSURE	RATIOS . PRI	MARY PLUG		
VD WOPD	PL	PL/PO	PL/PTF	PL/PTP	x/DMAX
32	17.613	3.7776	0.16928	0.43816	0.43200
37	6.9674	2.0865	0.093505	0.24203	0.53000
47	R. 1469	2.4398	0.10933	0.28300	0.62900
52	8.3168	2.4907	0.11162	19895.0	0. 72700
>AND IT 10%	AL PRESSURE	RATIOS , FLO	M SPLITTER I	. D.	
VD WORD	PL	FL/PG	PL/PTF	PL /PTP	K/DMAX
57	9. 5061	7. 8468	0.12758	0.33022	0.42200
67	12.703	3.8043	0.17048	0.44128	0.49200
ADD IT ION	IL PRESSURE	RATIOS , FLO	W SPLITTER C	. D.	
YD WORD	PL	PL/P0	PL/PTF	PL /PTP	X/DMAX
77	29.368	11.7949	0.39613	1.0202	CUSSESS.
12	9.2013	2. 7555	0.12349	0.31963	0.43500
72	3.4673	1.0683	0.047875	0.12392	0.69200
ADDIT TON	L PRESSURE	RATIOS , EJE	CTUR SHRIND		
n wat		P[7P0	PLYPIF	PLIPIP	770AX
07	9-0514	2.7107	0.12147	0.31442	0.42400
112	9.4778	1.3407	0.060091	0.15554	0.83000
22	2.6369	0. 78969	0.035389	0-091600	0.96000
27		1.0606	0.097540	0.12305	7. 78000 
37	3.3222	0.99492	0.044586	0.11541	1.2200
147	3:2572	0.77772	0.04371	0:11319	1-2200
		241305 - 201			
					<del></del>
DANIMO	P(	PL/P0	PLIPTE	PLIPIP	TORAL
107	9.0514	2.7107	0.12147	0.31442	-1.9600
112	4.4776	1.3409	0.060091	7.19994	-2.0000
55	2.6369	0.78969	0.035389	0.091600	<b>/-1.0000</b>
27	262653	1.0606	0.047540	0.12305	-1.0000
37	3.3222	0.99492	0.044576	0.11541	~1.0000
42	3.5336	0.97545	O. C43713	0,21315	-1: 0060
52	3.5523	1.0638	0.047674	0-12340	-1.0000
157	3.5523	1.0638	0.047674	0.12340	-1.0000
TT TOTAL	L PRESSURE	PATERIA PAR	HUEZES FLAR		
n word	Pt.	PL/P0	KIPIF	PE/PTP	¥/664X
52	3.5523	1.0638	×0.047674	0.12340	-1.00 <b>0</b> 0
197	3, 9923	1.0639		0.12340	-1:0000
FARDIT YOU	NI PRESSURE		DEC SHROOD L		
		/			
ID WORD	Pt	PL/PD	PL/PTF	AL APTR	TOTAL COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COLUMN COL
167	3.5573	1.0653	0.047741	0.12357	-1.0000
172	3.3813	1.0693	0.047741	- 0.12251	-1.0000
ADDIT IN	PRESTURE	*#T105 ; 80	DEG SIROUD LI	OCATION -	
י מיפניי פי	Pt	91 /90			N/MAX
192	3.3573	1.0054	0.045056	0.11662	-1.0000
77		0.97845			

NASA-LEWIS	PRELIM	MARY DATA	06/28/79	CADDFIL	REC 10/10/79 00:55:20.501 FAC BX6X1 PGM C034 RRG 1211
ABO IT IONAL	PRESSURE	RATIOS . PRI	MARY PLUG		
VD WORD	PL	PL /PD	PL /PTF	PL /PTP	X/DMAX
32	18.090	5.4564 -	0.21975	0.43781	0.43200
37	9.9432	2.9992	0.12079	0.24065	0.53400
47	11.647	3.5131	0.14148	0.281 RR	0.62900
52	11.912	3.5930	0.14470	0.28829	0.72700
>ADD   T   1044	PRESSURE	RATIOS . FLO	W SPLITTER I	.0.	
	PL	PL/PN	PL/PT+	PL /PTP	X/OMAX
62	13.635	4.1128	0.16563	0.33000	0.42290
67	12.454	3.8175	0.15374	0.30630	0.69200
ANDI TIDRA	PRESSURE	RATIOS , FLO	W SPLITTER O	.D.	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
VD WORD	PL	PL/PO	PL/PTF	PL/PTP	x/gmax
77	32-189	<del>9.7022</del>	0.39098	0.77896	0.78490
82	10.143	3.0595	0.12322	0.24549	0.63500
92	3.5393	1.0676	0.042443	0.085639	0.89200
ANDITIONAL	PRESSURE	RATTOS , EJE	CTOR SHROUD		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
VD WORD	Pt	FE / PO	PL/PTF	PLIPTP	TARAK COMPONENCIA CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONT
107	10.003	3.0173	0.12152	0.24210	0.62400
112	4.9097	1. 4609	0.039642	0.11003	0-83000
122	2-9090	0.87745	0.035338	0.070404	o. 96000
127		1.0646	0.042873	0.085417	1.0900
[37 [48	4.6546	1.4040	0.056544	0.11265	1.2200
	4:5496	1:3453	0.055268	0.11011	1.3900
×*************************************		247103 + FOR	PROV. 120.07		7
AU AUBO	Pt	PL/PO	PLIPTP	PL/PTP	
107	10.003	3.0173	0. 12152	0-24210	-).00 <b>00</b>
112	4.9997	1.4009	******************	0.11nn9	1.0000
122	2.9090	0.97745	0.035338	0.070404	-1.6600
127 137	4.0546	1.4949	0.042873 0.056544	0.009417	-1.0000
142	4.549	1.3723	0.057268	0.1265 9:11011	-1.0000 -1.0000
152	3.5243	1.0631	0.042812	0.085296	-1.0000 -1.0000
57	3.5249	1.0631	0.042813		-1.0000
**************************************	PRESSURE	RATIOS PAN	HOZZYZ PLAP		
n wasp	Pt	PL/PD	him		THE RESIDENCE OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY
152	3.5243	1.9631	0.042812	0.085796	-1.0000
	3.5243	1.0631		0.085296	-1.0000
<del> AND T ONA</del>	PRESSURE	<del>2413/15 v 20</del>	DEO SIRINGE LI	DCATION -	
YD WORD .	PL >	n/100 -	-MIME	CE PPTP-	TO THE TOTAL THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR AND THE SECOND STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACTOR STREET CONTRACT
167	3.5293	1.0646	0.042873	0.085417	-1.9000
17?	3.5243 -		0.942873		-1.0900
>ADD17-1049	PRESSIME	<del>RATIOS + 90</del>	nes simous t	ncation -	
VO WORK	<b>Pt</b>		PL/PF-		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
102	3.3442	1.0047	0-040625	Pt /PTP	1.00g0
4 T- 65-	Jo J776		A* A4A44 C2	U • U = U = D = D	-10 A A A A

NASA-L EWIS	PRELIM	INARY DATA	06/28/79	CADDEII	REC 10/18/79 00:56:59.941 FAC BM6X1 PGM C034 RBG 1212
SADDIT TONAL	. PRESSURE	RATIOS . PRI	MARY PLUG		
VD WORD	PL	PI./PO	PL/PTF	PL/PTP	W JOHA V
37 W(M)	15.558	4.691	0:18642	0.43762	x/9max 0.43260
37	A.5A35	2.5885	0-10397	0.24155	0.53000
47 52	10.034 10.249	3.0258	0.12154 0.12414	0.28236 0.20041	0.62900 0.72700
	<del></del>		OW SPLITTER I		
AD MUND	PL	PL / PO	PL/PTF	PL/PTP	X/DMAX
62 WIND	11.719	3.5340	0.14195	0.32978	0.42200
67	12.599	3.7994	0. 15261	0.35454	0.69200
>ADDITIONAL	PRESSURE	RATIOS , FLO	DW SPLITTER O	. D.	
<b>*</b>					nga manggapan pendadhan menjadi sanggah sanggah sanggah sanggah sanggah sanggah sanggan pendadhan menjadi sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sanggah sang
AD MUND	<b>인</b>	PL/P0	PL/PTF	PL/PTP	TOWAX
77 82	32.370	7.7556 3.0726	0.39185 0.12341	0.91036	0.58400 0.63500
92	10.189	1.0589	0.042933	0.099744	0.69200
••	303445	100007	0001033	000	<b>4.07.3.0</b>
>40ºITIONA	L'PRESSURE	RATIOS . EJI	ECTOR SHIPOUD		general and the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second
VD WORT	PT	- N/MT	PLIPTE	PLIPTP	TOTAL
107	10.054	3.0319	0.12178	0.28292	0.62400
112	4.9611	1.4981	0.060092	0.13961	Q. 83806
122	2.91 06	0.88015	0.035353	0.002133	0.96000
127	3.5345	1.0699	0.042812-	0.099482	
137	4.0551	1.2229	0.049118	0.11411	1.2200
142	3.9500	1-1-15	0.047849	0.11116	1,3900 - Commence - Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence o
340017 1014	- 110233102		LEBOOY INCET		
	-				
	PE OFA	7 (7)	PE /PTF	PT/PTP	7/003
107	10-054	3.0319	0.12178	0.28292	-1,4600
115	4.9611	1.4961	0.060092	0.13961	1.0000
122	2.9186	0. 88015	0.035353	0.042133	/ -1.0 <del>000</del>
127	3,5345	1.0659	0.752812	0.077552	-1.000
137	4.0651	1.2229	0.049118	0.13411	-1.0000
142	3.9500	1.1912	0.047845	0,71116	-1.0000
152	3.5345	1.0659	0.042812	0.099462	-1.0 <del>00</del>
157	3.5299	1.0644	0.042751	0.099322	-1,0000
> ROOTT TONK	PRESSUPE	RATTOS C PAI	N HOZZED PLAP		
VD WORD	Pt	PL 190	A1978-	PL/PTP	TOWAR CO. CO. CO. CO. CO. CO. CO. CO. CO. CO.
152	3.5345	1-0659	X0.042812	0.099462	
197	3.9295	1.0049		0.049322	
YADDIT 10NA					
			THE SHRIBER L		
AD MOND	Pt	70/10	····PL/PTF······	MISSE	*/OMAX
167	3.5345	1.0659	0.042812	0>099462	
	3.5845	1.0659	0.042812	0.090462	-t.0000
172					
	PRESSURE	AN1602 4 MA	DEG SIMILOU (	01,21,21,11	
172 > <del>20017 1014</del> VO. 40 <b>2</b> 0				_	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
	P1 3.3492	PL/PO	PL/PTF	_	1/548T

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	S PRELIMI	INARY DATA	06/28/79	CADDETT	REC 10/18/79 00:57:52.451 FAC BYEKE PGM CB34 PNG 1213
MULTIOUP	L PRESSURE	RATIOS . PRI	IMARY PLUG		
VD WORD	PL	PL/PO	PL / PTF	PL /PTP	X/DMAX
37	13.924	4.1961	0.16911	0.43770	0.43200
37	7.6932	2.3153	0. 093309	0.24152	0.53000
47	R.9978	2.7115	0.10927	0.28284	0.62900
52	9.1627	2.7612	0.11129	0.28802	0.72700
>ADDITION	IL PRESSURE	MAYINS , PEC	DW SPLITTER 1.	. D.	مهري مسه على المنافقين المنافق المنافق المنافق المنافق المنافق المنافق المنافق المنافق المنافق المنافق المنافق
VD WORD	PL	PL/P0	PL/PTF	PI /PTP	K/DMAK
62	10.532	3.1732	0.12791	0.33107	0.52200 *** *** *** *** *** *** *** *** ***
67	12.531	3.7761	0.15218	0.39389	0.49200
>ADDIT LONA	AL PRESSURE	RATIOS . FLO	DW SPLITTER O.	. D.	
	a mare min or he	PL/PO			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
AD MUND	PL		PL/PTF	PL/PTP	K/DMAK
	- 32:323	7.7404	0.39299	1.0160	0-96400 Telephone and the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of
82	10.157	3.0609	0.12336	0.31929	0.63500
95	3.5325	1-0649	0.042901	0.11104	9:89200
Anni Tiom	IL PRESSURE	RATTOS , FJE	PCTCP SHROUD		
40 MUBD	- Pt	PL 7PG	PL/PTF	PLIPTP	TANKS
107	10.027	3.0217	0.12178	0.31520	0.42400
112	4.9991	1.9002	0.060700	0.19711	G. 8 300G
172	2.9021	0.87453	0.035245	0.091225	
127	- 3.5129-	1.0585	0.042656	0.11041 ·	The street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of th
137	3-6726	1.1067	0.044602	0.11544	1.2200
142	3.7927	1:0926	0.043630		
		<del>-</del>		0.11293	\$3500 · · · · · · · · · · · · · · · · · ·
>4903 <b>7 30</b> 11		211101 . 100	12000Y 21127		
ANJANUED	Pt	PL/PD	PL/PTP	Pt-/PTP	TOWAY
107	10.027	3.0217	0.12170	0.31520	
115		1.5062	0.060700	0.15711	-1.00fs
122	2.9021	0.87453	0.035245	0.091225	
		1.0707			71.000
127	2,5129		0.042890	0.11041	1.0000
137	3.6726	1.1067	0.044602	0.115	-1.0000
142	9.5925	1.0020	0.043630	פרצאע.ס	-1:0000 management of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest of the rest
152	3.5225	1.0615	0.042779	A. 11073	-1.0999
157	3.5225	1.0015	0.042779	<b>0.11073</b>	-1.0000
	IL PRESSURE	-	1 HOFELE #140		
>400 17 10W					
VO WORD	Pt	161.0	X 0 062770	PL/PTP	
VN WNRO	3.5225	1.0615	X0.042779	0.11073	-1.000
VN WNRO 152 157	3.5225 3.5225	1.0615	0.042779	0.11073 0.11073	
VN WNRO 152 157	3.5225 3.5225	1.0615	X0.042779	0.11073 0.11073	-1.000
VD WORD 152 157	3.5225 3.5225 H. PRESSURE	1.0615 1.0615 RATIOS V 20	0.042779 042779 070 SHRITER LE	0.11073 0.11073 9C4710W	-1.0000 -1.0000
VO MORD 152 157 > <del>ADDIT-ION</del> M VO WORD 167	3.5225 3.5225 HE PRESSURE PL 3.5225	1.0615 1.0615 ******* 20	0.042779 002779 002779 000 SHRRING LE PL/97F 0.042779	0.11073 0.11073 0.11073	-1.0000 -1.0000
VO MORD 152 157 > <del>ADDIT-ION</del> M VO WORD 167	3.5225 3.5225 H. PRESSURE	1.0615 1.0615 RATIOS V 20	0.042779 042779 070 SHRITER LE	0.11073 0.11073 9C4710W	-1.0000 -1.0000
VD MORD 152 157 >ADDIT TOMA VD MORD 167 172	3.5225 3.5225 M. PRESSURE PL 3.5225 3.5225	1.0615 1.0615 RATIOS , 20 PL/PO 1.0615 1.0015	0.042779 9 042779 BEG SIMPLE CO PL/PIF 0.042779 0.042779	0.11073 0.11079 0.11079 0.11073 0.11073	-1.0000 -1.0000
VD WORD 152 157 >ADDIT TOWN VD WORD 167 172 >ADDIT TOWN	3.5225 3.5225 HE PRESSURE PL 3.5225 3.5225 W PRESSURE	1.0615 1.0615 RATIOS , 20 PL/PD 1.0615 1.0015	0.042779 002779 002779 0042779 0.042779 0.042779 0.042779	0.11073 0.11079 0.11079 0.11073 0.11073	-1.0000 -1.0000 -1.0000
VN WORD 152 157 ***********************************	3.5225 3.5225 M. PRESSURE PL 3.5225 3.5225 M. PRESSURE PL	1.0615 1.0615 RATIOS : 20 PL/PO 1.0615 1.0615 PATIOS : 80	0.042779 042779 060 SIMPLE CO PL/PTF 0.042779 0.042779 0.042779 0.042779	0.11073 0.11073 0.11073 0.11073 0.11073 0.11073	-1.0000 -t.0000 -1.0000 -1.0000
VN WORD 152 157 ***********************************	3.5225 3.5225 M. FRESSURE PL 3.5225 M. FRESSURE PL 3.3224	1.0615 1.0615 PL/PO 1.0615 1.0615 PATIOS . 00 PL/PO 1.0012	0.042779 0.042779 0.042779 0.042779 0.042779 0.042779 0.042779 0.042779	0.11075 0.11079 0.11079 0.11073 0.11073 0.11079 0.11079	-1.0000 -1.0000 -1.0000 -1.0000
VD MORD 152 157 >ADDIT TOMA VD MORD 167 172	3.5225 3.5225 M. PRESSURE PL 3.5225 3.5225 M. PRESSURE PL	1.0615 1.0615 20 2.0615 1.0615 1.0615 2.0615	0.042779 042779 060 SIMPLE CO PL/PTF 0.042779 0.042779 0.042779 0.042779	0.11075 0.11079 0.11079 0.11073 0.11073 0.11079 0.11079	-1.0000 -t.0000 -1.0000 -1.0000

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37	9.4510	2.8463	0.10392	0.24119	0.53000	
47	11.090 ~ ~	3.3280	0.12150	0.28201	*	na kalaman ka mana kalaman ka ka ka ka ka mana ya mana mana ka ka ka ka ka ka ka ka ka ka ka ka ka
52	11.290	3.4002	0.12414	0.20013	0.72700	
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67	12.415	3.7306	0.13650	0.31662	0.49200	
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77	37.471	10,683	0. 39001	0.90523	** 0.56400***********************************	erana kan geograpina nementra in virus prominin labori. Man mer ada manaril ni kinapi sapagaman
42	11-215	3.3776	0.12331	0-50655	0.43500	
92	3.9449	1.0676	0.038977	0.090457	0.69209	
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107	11.035	3.3235	0.12134	0.28163	0.62400	
112-	7.7010	1.6746	0.061144	0.14192	0:83000	
122	3.2196	0.96965	0. 035401	0.082167	0.96000	
127	3.5349	t.0646	0.038867	0.090212	1.0900	The form the contract of the second of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the con
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152	3. 5349	1.0646	0.038867	0.090212	-1.0000	
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167	3.5355	1.0646	0.039867	02040515	-1.3000	
172	3,9299	1.0631	0.030012	0.010064	-1.0000	
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<del>&gt;49917199</del> NO MARD 182 187	PL 3.3697	1.0088	0.036831 0.035951	0.085487	-1.0000	age and a contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the cont

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37	10.386	3.1091	0.47507 0.2597t	0.73007	0.53000				
47	12.167	3.6431	0.30432	0.28179	6.62906				
52	12.427	3. 7209	0. 31082	0.28781	0.72700				
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62	14.280	4.2757	0.35717	0.33073	0.42200			the by a contract the	r drock in a
67	12.312	3.6865	0. 38 794	0.28515	9.69200				
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77	34.603	11:559	0.96992	0.89404	8.56400				and the second of the second
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112	-0.0007	1.7967	0.17009	0.13896	6. 83000	<del></del>			
122	3.5353	1.0585	0.088422	0.081877	0.74000				
127 -	3.5653	1.0675	0.009179	0.002572	1.0900		The section appears from the sec-	was access as a control of the control of	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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-122 -127 -137 -142 -152 -157 ->ADDITIONAL -157 ->ADDITIONAL 	3.5353 3.5053 4.0756 4.0756 4.0200 3.5453 9.5553 1.75553 1.75553 1.75553	1.0595 1.0675 1.4599 1.4599 1.4615 1.0645 RATIOS TM PL/PO 1.0615 1.0645	0.08%22 0.08%173 0.12195 0.12057 0.098672 0.088922 1 HORPLS FLAP 0.088672 0.088672 0.088922	0.061677 0.062926 0.1276 0.47165 0.062108 0.062340 Pt/PTP 0.082108 0.062340	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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122 127 137 142 152 157 >ABDIT INW WIN WIRD 152 157 >ABDIT INW WO MIRD 167	3.5353 3.0053 4.0756 4.0756 4.0750 3.5453 9.5553 PRESSURE PL 3.5553 1.5753	1.0595 1.0675 1.4599 1.4599 1.4615 1.0645 1.0615 1.0645 1.0645 1.0645	0.088422 0.009173 0.12195 0.12057 0.088672 0.088672 0.088672 0.088672 0.088922 0.088922 0.088922	0.061877 0.062972 0.11252 0.41165 0.062108 0.062340 0.062340 0.062340 0.062340 0.062340 0.062340	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
-122 -127 -137 -142 -152 -157 -240017 1044 -157 -240017 1044 -167 -167 -172	3, 5353 4, 8754 4, 8754 4, 8750 3, 5453 3, 5553 1, PRESSURE PL 3, 5553 1, 5753 1, 5753 PRESSURE	1.0595 1.0675 1.4599 1.4599 1.4639 1.0615 1.0645 1.0645 1.0645 1.0645 1.0645	0.08%22 0.08%173 0.12195 0.12097 0.08672 0.086922 1.402715 FLAP 0.088672 0.088922 0.08922 0.088922 0.088922	0.061677 0.062972 0.11272 0.1145 0.062108 0.062340 Pt./PTP 0.062340 Pt./PTP 0.062340 0.062340 0.062340	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
122 127 137 142 152 157 20017 1044 152 157 200 UNRD 167 167 172 200 UNRD	3.5353 3.0053 4.0256 4.0206 3.5453 9.7559  **PRESSURE** PL 3.5553 1.5753 PRESSURE** PL	1.0595 1.0479 1.4599 1.4599 1.4615 1.0645 1.0645 1.0645 1.0645 1.0645 1.0645	0.08%22 0.009173 0.12195 0.12037 0.08672 0.08672 1.00215 PLAP 0.086672 0.086672 0.086922 0.088922 0.088922	0.061877 0.062972 0.1149 0.41149 0.062108 0.062340 PE/PTP 0.062340 PEATION PE/PTP	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
-122 -127 -137 -142 -152 -157 	3.5353 3.0053 4.0756 4.0206 3.5453 9.5553 1.5653 1.5753 1.76550RE PL 3.5550 PRESSURE	1.0595 1.0675 1.4599 1.4599 1.4639 1.0615 1.0645 1.0645 1.0645 1.0645 1.0645	0.088422 0.089173 0.12195 0.12097 0.088672 0.088672 0.088672 0.088672 0.088922 0.088922 0.088922 0.088922	0.061677 0.062972 0.11272 0.1145 0.062108 0.062340 Pt./PTP 0.062340 Pt./PTP 0.062340 0.062340 0.062340	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

NASA-LEWI!	S PRELIMI	NARY DATA	06/28/79	CADDELL	REC 10/18/79	01:06:39.521	FAC BROKE	PGM CO34	PRG 1218
>ADDITION	AL PRESSURE	RATIOS . PRI	MARY PLUG						
AD MUND	PL	Pt /P0	PL /PTF	PL /PTP	X/DHAX				
32	16.846	5.0423	0.55878	0.43793	0.43200		* · · · · · · · · · · · · · · · · · · ·		
37	9.2687	2.7743	0. 30745	0.24095	0.53000				
47	10.834	3.2427	0.35935	0.28163	0.42900			+ 4	
52	11.070	3.3160	0.36748	0.28800	0.72700				
NOT TEGGA	AL PRESSURE	RATIOS . FLO	W SPLITTER I	.0.					
VD MORD	PL	PL/PO	PL/PTF	PL/PTP	K/DMAK				_
67	17.638	3.7020	0.41921	0.32854	0.42200				
67	12.283	3.6766	0.40744	0.31932	J-69200				
>ADDIT TON	LL PRESSURE	RATIOS , FLO	W SPLITTER II	. D.					
VD WORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX	•••			The comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the comment of the co
77 TOTAL	39.725	11.591	1.2845	1.0057	0.56400				The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
82	12-333	3.6916	0.40910	0.32062	0.43500				
92	3.5759	1.0703	0.11961	0.092959	0.69200				
>4091 <b>11</b> 04	IL PRESSURE	RATIOS , EJE	CTOR SHADON				A so appropriate that is	generalistic of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of	a national and an experience of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract o
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107	12.073	3.6138	0.40048	0.31386	0.62400				
112	6.0678	1.8162	0.20127	0.15774	0.83000				
122	3.5508	1-0628	0.11778	0.092309	0.94900				
27	3.5609	1.0658	0.11012	0.092569	1.0900				
137	4.3866	1.3130	0.14551	0.11404	1.2200				
42	4.3916	1.3145	0.14557	0.11417	1.3508		والمساسو راجدات المستند		
>+00 <b>11100</b>	IZ	247108 POR	2=00x=1×12x=						
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107	12.073	3. 61 38	0.40048	0.31366	-1.0000				
112	6.0678	1.0167	0.20127	0.15774	1.0000		management of the college of the college of		- management of the second of the second
122	3.5508	1.0628	0.11778	0.092309	-1.0000				
27	3,5609	1.0658	0.11712	0.092369	-1.0500				
37	4.3466	1.3130	0.14551	0.12404	-1.0000				
42	4.3916	1.3145	0.14567	Del 1417	-1.0000				magain at the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the second section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the se
152	3.5659	1.0673	0.11828	0.092699	-1.0000				
57	3.5709	1.0688	0.11849	0.092829				The second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of	compared to the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of th
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ID WORD	Pt.			PL/PTP	···· • ********		en jako na wanansa i ionga ma pin	A #0.5 (M. )	ger nig i nagagagasana sersa sersa sejaga sersa sersa diberia
	-		PL/PTF 0.11828		X/DMAX				
152 157	3.5659 3.5709	1.0673	0.11828	0.092699	-1.0000 -1.0000				and the second second section of the second section is a second section of the second section of the second section is a second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the second section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of t
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NO MUNO	71	PL/PI	PL/PTP	M PPTP	T/OMAX				
167	3.5654	1.0673	0.11828	0.092699	-1.0000				
172	3,8704	1.0688	0.11845	0-038859	-1.0000	19 49			
AND IT INY	PRESSIME	RATIOS . FO	<del>DEG SHROUD L</del>	DEATION				· · · · · · · · · · · · · · · · · · ·	,
ראפעו חו	PL	PL/PD	PL/PTF -	PL/PTP-	XIDROX				
197	3.3857	1.0134	0. 11 230	0.008015	-1-0000				
A7	3.3128	0.99093	0.10981	9.0860e3	-1.0000				
		THRUST PAPAM		~~ ~~~~					

NASA-LEWIS	PRFLIM	NARY DATA	06/78/79	CARDELL	REC 10/18/79 01:08:42.692 FAC 8X6X1 PGM C034 RDG 1219
>40017 <b>10</b> 04	L PRESSURE	RATIOS , PRI		± · · · · · · · · · · · · · · · · · · ·	
VD WORD	PL	PL/P0	PL/PTF	PL/PTP	X/DMAX
32 · · ·	19.418	5.5923	0-18941	0.43839	
37	10.112	3.0484	0.10399	0-24064	0.53000
67	11.842	3. 56 <b>98</b>	0.12176	0.27186	0.523000 To the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the contr
52	12.131	3.6482	0.12445	0.28805	0.72700
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	N 40 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	and the second control of		. Igeran busines of the same	and the same state and the same of the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state and the same state a
VD WORD	PL	PL/PN	PL/PTF	PL/PTP	K/DRAK
65	13.911	4.1936	0.14306	0.33111	0.42200
67	12.216	3.6829	0.12563	0.29078	0.69200
APOI T ICCA<	L PRESSURE	RATIOS . FLO	W SPLITTER C	. O.	
VD WORD	PL	PL/PO	PL/PTF	PL/PTP	X/SMAX
	37.833	11-392	0.38729	0.89630	0.36400
32	11.982	3-6120	0-12322	0.28519	0.63500
92	3.7397	1.0671	0.038402	0.084254	0.69200
ADDITIONA	L. PRESSURE	RATIOS , EJI	CTOR-SHROUN-		the Problem of Block - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State - State -
ND W/RD	Pt	PC/PO	PI /PTF	PLIPTP	X/OREX
107	11.737	3.5382	0.12070	0.27936	0.62400
112	7. 9404	1.7926	0:001193	0.14194	0.83000
122	3.4396	1.0369	0.035373	0.001571	0.96000
27	3.5947	1:0656	0.036351	0.084135	1,0900
137	4.7557	1.4337	0.048908	0.11320	1.2206
142	4.TOOT	1.4171	0.048342	0.11107	1.3900
>=001710M	C-99533198	241101 20	28007 19L2T		7
ONDED	Pt	- Pt /PD		Pt /PTP	T/ONEX
107	11.737	3.5382	0. 12070	0.27936	-140000
115	5. 9464	<del>1. 7926</del>	7.061159	0: 141 54	1:000
122	3.4396	1.0369	0.035373	0.081871	-1.0000
127	->59997	1.0656	0.036371	0.094155	1,900
137	4,7557	1.4337	0.048908	0.12520	-1.000
42	4. 7007	1.4171	0.048342	0411189	1.0000
152	3.5297	1.0641	0.036299	0.084014	-1.000
57	3.5347	1.0656	0:036351	0.084135	
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ro worn	Pt		_ <u> </u>		
152	3.5297	1.0641		PE/PTP	
157	3.5347	1.065	0.036299	0.084616 0.084135	
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<del>201110</del>	t-PRESSURE	<del>RATJØS 1 20</del>	OFO SHRINGE L	DCATEON-	
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167	3.5297	1.0641	0.036299	₫ <b>&gt;Q</b> ₹4016	-1.0000
177	3,5267	1:0656	··· 0. 03624 <del>6</del>	c~0 <b>926</b> 20	To \$000 - Annual management against the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the first through the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of
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182/	3.3445	1.0083	0.034395	0.079608	-1.0000
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NASA-L FWIS	PRELIM	INARY DATA	06/28/79	CADDETT	REC 10/18/79 01:09:49.14	T FAC RYSKL	PG# (034 #86	
SACRIT IRNA	L PRESSURE	MATINS . PPI	MARY PLUG					
ING HUBB	PL	PL/PO	PL/PTF	PL/PTP	1/DMAX			
32	16.399	4.9315	0.16870	0.43596	5.43200			
37	9.0072	2.7103	0.092715	0.24125	0.53000			
47	10.532	3.1691	0.10441	0.24209	0.62900			
52	10.762	3.2383	0.11078	0.28824	9- 72709			
SADDIT INNA	L PRESSURE	RATIOS , FLO	w SPLITTER I.	. D.				
ORNW GV	PL	PI / PO	PL/PTF	PL/PTP	X/DMAX			A APPROXIMATION APPROXIMATION
67	12.326	3.7090	0.126WB	0.33015	0.42200	and the second of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		
67	12.187	3.6469	0.12544	9-32640	0.69200			
>ADDITIONA	L PRESSURE	PATIOS . FLO	w SPLITTER O.	. D.				
VD WORD	PL	PL/PD	PL /PTF	PL /PTP	K/DMAX	The transfer conserve the conserve against the conserve		
77	37.595	11-315	0.38698	1769	0.56400			
82	11-967	3.6007	0.12319	0.32051	0.63500			
92	3,5398	1.0551	U-036437	0.32031	0.69200			
_				444 74 510				
MOTTI GOAC	E. MEZZINE.	WATEDS , FIE	CTINE SHROUD		entalecca communicate the extra account of	The first of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second		entrate de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la company
AD RUBIL	<b>P</b> [	PC / PO	KIPIF		KYTHAY	the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	planty approximate to the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco	patricipage and a second participage and a sec
107	11.727	3.5285	0. 12071	0.31400	0.62490			
115	5.6315	1.7-47	9.080026	0.13619	0.83000			
122	3.4297		0.035304	0.091861	0.96000			
127	3.5296	1.6.1	0.038334	0.094542	1.0900	THE R. M. LEWIS CO., LANSING MICHIGAN PROPERTY AND ADDRESS.	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t	
137	4.2605	1.2820	0.043855	0.11411	1.2200			
142	4.2679	1.2920	0. 043855	0.11611	1.3500	tan and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same o	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	· · · · · · · · · · · · · · · · · · ·
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AD AURD	Pt	PC/PG	PL/PTF	PE /PTP	TIONNE		\$ <u>\$</u>	
107	11-727	3.5285	0.12071	0.31408	-140000	•	RIGINAL POOR	
1112	- 5.8315	1.7947	0.060026	0.15619	1.0000	e e la la casa de la desagración de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la companión de la compani		
122	3.42 <b>97</b>	1.0320	0.035304	0.19614	-1.0000		83	
127				0.094342				
	3 52 98	1.0621	0.036334	0.050	-1.0000		25	
127	4.2405	1.2820 1.2820	0.043855	0.11411	-1-0000		<b></b>	
		164723		0-094408	-1.0000		Č 70	
147	6.2603		U U31383					
142 152	3.5248	1.0606	0.036282		-1.0000			
142 152			0.036282	0.094542	-1.0000		PAG QUAL	
142 152 157	3.5248	1.0606	0. 035339				<del></del>	
162 152 157 <del>287917 TONK</del>	3,5248 3,5298 L PRESSUPE	1.0606 1.0621 PATTOS PAT	0. 035339 WIZZYZ FLAF	0.094542	-1.0000		<del></del>	
142 152 157 <del>28791770W</del> VD WORD	3.5248 3.5298 L PRESSUPE	1.0606 1.0621 PATTITS PAN	0.035339 MIZZYZ PLAP VL/PTP	0.094942 Pt /PTP	-1.0000 *********************************		100	
162 152 157 <del>&gt;877177048</del> VD W78D 152	3.5248 3.5298 L PRESSUPE PL 3.5248	1.0606 1.0621 PATTITS PAN PL PPO 1.0606	0. 036339 WIZZYE FLAP PL/PHF Q.036282	0.094542 Pt /PTP 0.094408	-1.0000 7/0MAR -1.0000		<del></del>	
162 152 157 > <del>200171008</del> VD WYRD 152 157	3.5248 3.5298 L PRESSUPE PL 3.5248 3.5298	1.0606 1.0621 PATTOS PAR 1.0606 1.0621	0.036339 WIZZY PLAP PL /PTF 0.036282 0:036394	Pt /PTP 0.094408 0.094542	-1.0000 *********************************		<del></del>	
142 152 157 2 <del>079  T  (100</del> VD WYRD 152 157	3.5248 3.5298 L PRESSUPE PL 3.5248 3.5298	1.0606 1.0621 PATTITS PAN PL PPO 1.0606	0.036339 WIZZY PLAP PL /PTF 0.036282 0:036394	Pt /PTP 0.094408 0.094542	-1.0000 7/0MAR -1.0000		<del></del>	
142 152 157 <del>2879171048</del> VD WYRD 152 157 2890171048	3.5248 3.5298 L PRESSUPE PL 3.5248 3.5298	1.0606 1.0621 PATTI S PAN PATTI S PAN 1.0606 1.0621 PATTI S 20	0.036339 WIZZY PLAP PL /PTF 0.036282 0:036394	Pt /PTP 0.094408 0.094542	-1.0000 7/0MAR -1.0000		<del></del>	
142 152 157 >ADDITIONAL VD WORD 152 157 >ADDITIONAL VD WORD	3.5248 3.5298 L PRESSUPE PL 3.5248 3.5299 L PRESSUPE	1.0606 1.0621 PATITIS PAR PL/PTI 1.0606 1.0622 PATETS . 20	0.036339 MIZZLE PLAN MIZZLE PLAN MIZZLE PLAN 0.036282 0:036334 DEG SHATUR LI	Pt /PTP 0.094408 0.094542	770MAR -1.0000 -1.0000		<del></del>	
162 152 157 >ADDITIONAL VD WORD 152 157 >ADDITIONAL VD WORD 167	3.5248 3.5248 PL PRESSUPE PL 3.5248 3.5298 L PRESSUPE	1.0606 1.0621 PATTI S PAN PATTI S PAN 1.0606 1.0621 PATTI S 20	0. 035339 WIZZY PLAP PL /PTP 0.036339 0:036319 DEG SHATUR LI	0.094542 Pt /PTP 0.094408 0.094542 PCATION	-1.0000 7/DMAH -1.0000 -1.0000		<del></del>	
162 152 157 2879171048 VD WYRD 152 157 2890171048 VD WYRD 167 172	3.5248 3.5248 1. PRESSUPE PL 3.5248 3.5298 1. PRESSUPE PL 3.5358 3.5298	1.0606 1.0621 PATTI S PAN PATTI S PAN 1.0606 1.0624 PATTI S 20 PATTI S 20 PATTI S 20	0.036339 M12212 PLAP 1.07628? 0.03628? 0.036334 DEG SHRTUD L1 PL/PTP 0.036385 0.036334	Pt /PTP 0.094408 0.094542 PCRTION PC /PTP 0.894676 0.099542	-1.0000 Y70MAR -1.0000 -1.0000 T/DMAY -1.0600		<del></del>	
VD WINED 152 157 28301777000 VD WINED 167 172 2833177000	3.5248 3.5248 1 PRESSUPE PL 3.5248 3.5248 1 PRESSUPE PL 3.5358 3.5298 PRESSUPE	1.0606 1.0621 PATINS PAN 1.0606 1.0621 PATINS . 20 PL/PN 1.0636 1.0621 PATINS . 80	0.036339 WIZZY PLAP PL/PYP 0.036287 9.036387 PL/PYP 0.036385 0.036385 0.036334	Pt /PTP	-1.0000 770MAH -1.0000 -1.0000 T/DMAH -1.0000 +1.0000		<del></del>	
142 152 157 2879171048 VD WORD 152 157 2870171048 VD WORD 167 172 2879171048	3.5248 3.5248 1.5248 3.5248 3.5298 1.78250PE Pt. 3.5358 3.5358 7.7298	1.0606 1.0621 PATITIS PAN PL/PD 1.0606 1.0621 PATITIS . 20 PL/PD 1.0636 1.0621 PATITIS . 80	0.036339  WIZZJE PLAP  PL/PTF  0.036385  0.036334  DEG SIMPUD 10  PL/PTF	Pt /PTP D.094408 0.094542 Pt /PTP D.294676 D.099542 Pt /PTP	-1.0000 Y/DMAR -1.0000 -1.0000 T/DMAR -1.0000 *********************************		<del></del>	
142 152 28791710NB VD WUND 152 157 289017710NB VD WUND 167 172	3.5248 3.5248 1 PRESSUPE PL 3.5248 3.5248 1 PRESSUPE PL 3.5358 3.5298 PRESSUPE	1.0606 1.0621 PATINS PAN 1.0606 1.0621 PATINS . 20 PL/PN 1.0636 1.0621 PATINS . 80	0.036339 WIZZY PLAP PL/PYP 0.036287 9.036387 PL/PYP 0.036385 0.036385 0.036334	Pt /PTP	-1.0000 770MAH -1.0000 -1.0000 T/DMAH -1.0000 +1.0000		<del></del>	

	S PRELIMI	MARY DATA	06/28/79	CADDELL	REC 10/10/79 01:10:27.685	FAC BROKE	PGM C034	// // /4 PNG 1221
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VD WORD	PL	PL/PD	PL/PTF	PL /PTP	X/OPAX	and the second section of the second section of the second section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section sec	United and the State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State of State	
32	16.448	4: 9510	n. 16901	0.43829	0.43200			
37	9.7564	2.7300	0.093005	0.24119	0.53000			
47	10.391	3.1976	9.10276	0.78206	0.62900		•	
52	10.821	1. 2619	0.11113	0.20810	0.72706			
>4001110M	IL PRESSURE	PATINS . FLE	M SPLITTER I	.0.				
VO WORD	PL	PL/PO	PL/PTF	PL /PTP	K/DMAX			
62	12.270	3.5988	0.12601	0.32678	0.42200	and a common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of the common of	e i i magazini magazini se	Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of the Complete of th
67	12-155	3.6641	0.12483	0.32372	0.69200			
>ADDITIONA	L PRESSURE	RATIOS , FLO	M SPLITTER D	. D.				
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62	11.986	3.6129	0.12308	0.31920	0.63500			
72	3.5446	1.0689	0.030401	0.094399	0.69200			
APPET FORM	L-PRESSURE	PATIOS , TUE	CTOR SHROUD		the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th		the secondary regarded before the total of the secondary of
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107	11.761	3.5451	0.12078	0.31321	0.62430			
112	7.0910	1.7728	0.000393	0.19662	0-831 00			
122	3,4395	1.0368	0.035322	0.091600	0.96:/00			
27	<del>9.9290</del> -	1.0640	0.036247	0.093999	1.0900			- Inches and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second
137	4.2752	1.2987	0.043904	0.11386	1-2200			
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107~					1.0000	e gaj personante e cuidan e debe e pero estámica mediente a la masca.		
		t.7728	0.060395				Annual Control of the Principle of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of t	
115	5.8810	1.7728	0.060395	0.19662			A STATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PAR	gerengger voormaan vermaagen verschin voorwelde van hij voorme. Die vier een 'n 18
112	5.8810 3.4395	1.0368	0.035322	0.091600	-1.0000			
112	5.8810 3.4395 2.5296		0.035322 0.036247	0.091600	-1.0000 -1.0000			
112 122 127 137	5.8810 3.4395	1.0368	0.035322	0.091600 0.093979 0.11366	-1,0000 -1,0000 -1,0000			
112 122 127 137 142	5.8810 3.4395 3.7290 4.2752 4.2742	1.0368 1.0640 1.2887	0.035322 0.036247 0.043904 0.044004	0.091600 0.093979 0.14386 0.11412	-1,0000 -1,0000 -1,0000 -1,0000			
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112 122 127 137 142 152	5.8810 3.4395 5.7296 4.2752 4.2752 3.5346 3.5296	1.0368 1.0640 1.2887 1.2917 1.0655	0.035322 0.036247 0.043904 0.044004 0.036298 0.036243	0.091600 0.093979 0.12186 0.11412 0.094133	-1,0000 -1,0000 -1,0000 -1,0000			
112 122 127 137 142 152 157	5.8810 3.4395 2.9296 4.2752 4.2752 3.5346 3.5296	1.0368 1.0640 1.2887 1.2917 1.0655 1.0640	0.03532? 0.035247 0.043904 0.044004 0.036298 0.036243	0.091600 0.093999 0.12386 0.11412 0.094133	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
112 122 127 137 142 152 157 • ADDITION	5.8810 3.4395 3.9296 4.2752 4.2942 3.5346 3.5296	1.0368 1.0690 1.2887 1.2917 1.0655 1.0640	0.035322 0.030247 0.043904 0.044904 0.036298 0.036263	0.091600 0.093999 0.12386 0.11412 0.094133 0.093999	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
112 122 127 137 142 157 157 160 WIPD	9.0010 3.4395 9.9290 4.2752 4.2952 3.5346 3.5290 11. PRESSURE- PL 3.5346	1.0368 1.0690 1.2887 1.2917 1.0455 1.0640 PATEOS 1 FAM	0.035322 0.030247 0.043904 0.044004 0.036298 0.036247 MOZZLA FLAN PL FFFF 0.036298	0.091600 0.093999 0.12386 0.11412 0.094133 0.093999	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
112 72 127 137 142 152 157 0 MIP D 152 157	9.0010 3.4395 2.9290 4.2752 4.2752 3.5346 3.5296 PL 3.5346 3.5346	1.0368 1.0640 1.2887 1.2917 1.0655 1.0640 PATEOS : FAM PL/PO 1.0655 1.0640	0.035322 0.030247 0.043904 0.044004 0.036298 0.036243 MOZZIA FLAN PL/PTF 0.036248 0.036247	0.091600 0.093999 0.12366 0.11412 0.094133 0.093999 Pt/PTP 0.094133 0.093999	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
112 122 127 137 142 152 157 0 MIP D 152 157	9.0010 3.4395 2.9290 4.2752 4.2752 3.5346 3.5296 PL 3.5346 3.5346	1.0368 1.0640 1.2887 1.2917 1.0655 1.0640 PATEOS : FAM PL/PO 1.0655 1.0640	0.035322 0.030247 0.043904 0.044004 0.036298 0.036247 MOZZLA FLAN PL FFFF 0.036298	0.091600 0.093979 0.11418 0.094133 0.093999 Pt/PTP 0.094133 0.093999	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
VD WAPD 152 157 <del>&gt;40017-104</del> 4 VD WARD	9.0010 3.4395 4.2752 4.2752 4.2752 4.2752 3.5346 3.5296 14. PRESSURE PL. 3.5346 3.5296	1.0368 1.0640 1.2897 1.2917 1.0655 1.0640 PATEOS : FAM PL/PN 1.0655 1.0640 PATEOS : FAM PL/PN 1.0655 1.0640	0.035322 0.036247 0.043904 0.044004 0.036298 0.036247 NO2214 FLAN PL /PTF 0.036247 DEG SHATTUG 1	0.091600 0.093999 0.11416 0.094133 0.093999 Pt/PTP 0.094133 0.093999	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
112 122 127 137 142 152 157 PARRITIONA VD WIRD 157 PARRITIONA VD WIRD	9.8810 3.4395 9.9296 4.2752 4.2952 3.5346 3.5296 1. PRESSURE PL 3.5346 3.5296	1.0368 1.0640 1.2887 1.2917 1.0655 1.0640 PATEGS FAM PL/PT 1.0655 1.0640 PATEGS FAM PL/PT 1.0655	0.035322 0.036247 0.043904 0.044004 0.036298 0.036243 NOZZLA FLAN PL /PTF 0.036247 REG SHATING LI	0.091600 0.093999 0.12366 0.11412 0.094133 0.093999 Pt/PTP 0.094133 0.093999	-1,0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000			
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112 122 127 137 142 152 157 >4001710M VD WIPD 152 157 >4001710M VD WIRD 167	9.0010 3.4395 9.7270 4.2752 4.2752 4.2752 3.5346 3.5276 11. PRESSURE PL 3.5346 3.5276 11. PRESSURE PL 3.5346 3.5346 3.5346	1.0368 1.0640 1.2887 1.2817 1.0655 1.0640 PATEOS : FAM PL/PN 1.0655 1.0640 PATEOS : 20- PATEOS :	0.035322 0.036247 0.043904 0.044004 0.036298 0.036243 NOZZLA FLAN PL /PTF 0.036247 REG SHATING LI	0.091600 0.093979 0.11418 0.094133 0.093999 Pt/PTP 0.094133 0.093999 9CAT109 0.094133 0.094133	-1,0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000			
112 127 127 137 142 152 157 >ADDITIONS VD WIRD 167 172 >ADDITIONS VD WIRD	9.0010 3.4395 9.7270 4.2752 4.2752 4.2752 3.5346 3.5276 11. PRESSURE PL 3.5346 3.5276 11. PRESSURE PL 3.5346 3.5346 3.5346	1.0368 1.0640 1.2887 1.2817 1.0655 1.0640 PATEOS : FAM PL/PN 1.0655 1.0640 PATEOS : 20- PATEOS :	0.035322 0.036247 0.043904 0.044004 0.036298 0.036243 NO2714 FLA- PL/PTF 0.036248 0.036247 PL/PTF 0.036249 0.036299	0.091600 0.093979 0.11418 0.094133 0.093999 Pt/PTP 0.094133 0.093999 9CAT109 0.094133 0.094133	-1,0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000			
112 122 127 137 142 152 157 >************************************	9.0010 3.4395 9.7270 4.2752 4.2752 4.2752 3.5346 3.5270 11. PRESSURE PL 3.5346 3.5276 11. PRESSURE PL 3.5346 3.7340	1.0368 1.0640 1.2807 1.2817 1.0655 1.0640 PATEOS FAM PL/PT 1.0655 1.0655 1.0655 1.0655	0.035322 0.036247 0.043904 0.044004 0.036298 0.036243 NOZZIA FLAN PL /PTF 0.036247 REG SIMPLO 10 0.036298 0.036298 0.036299	0.091600 0.093979 0.11412 0.094133 0.093999 Pt/PTP 0.094133 0.093999 0.094133 0.093999	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
112 122 127 137 142 152 157 20 WIPD 152 157 2001*10WI	9.0010 3.4395 9.9290 4.2752 4.2952 3.5346 3.5296 11. PRESSURE PL 3.5346 3.5296 11. PRESSURE PL 3.5346 3.7346	1.0368 1.0640 1.2887 1.2917 1.0655 1.0640 PATEOS . FAM PL/PO 1.0655 1.0640 PATEOS . 20 PATEOS . 20	0.035322 0.036247 0.043904 0.044004 0.036298 0.036243 NO2714 FLAN PL/PTF 0.036248 0.036247 PL/PTF 0.036298 0.036299 0.036299	0.091600 0.093999 0.12366 0.11412 0.094133 0.093999 0.094133 0.093999 0.094133 0.094133 0.094133	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			

NASA-LEWI	S PRELIMI	INARY DATA	06/28/79	CADDELL	REC 10/18/79 01:12:15.214	FAC RYSKI	PGF C034	PNG 1222
>ADDITION	AL PRESSUPE	RATIOS . PR	TMARY PLUG					
LYO WORD	PL	PL /PD	PL/PTF	PL/PTP	X/DMAX			
32	17.606	5. 5769	0.18999	0.43877	0.43200			
37	10.216	3.0620	0.10431	0-24091	0.53000			
47	11.969	3.5876	0.12222	0.28226	0.42900	and the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contra		
52	12.204	3.6580	0.12462	0.28779	0.72700			
>4001710M	A. BRECCIME		OW SPLITTER I	<del></del>				
	4E PRE330RE	N. S. III. IN CO. SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC. OF SEC.			a compared to the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the con			The second second section of the second section section section sections section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section secti
AD MOND	PL.	PL/PO	PL/PTF	PL/PTP	I/DMAX			
62	. 4 . 045	4.2239	0.14389	0.33737	0.47200			
67	11:-124	3.6340	0.12380	0.28591	0.69200			
>ADD!~!ON	AL PRESSURE	RATIOS . FLO	IN SPLITTER I	.D.				
VO WORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX			
77	37.998	11.362	0.38708	0.89394	0.56400			
62	12.069	3.4176	0.12324	0.28461	0.43500			
92	3.5675	1.0693	0.036428	0.084129	0.89200			
>ADDITION	AL PRESSURE	RATIOS , EJI	FCTOR SHROUN				THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF TH	e con il vienta quantità delle con e con e quantità delle con este delle con este delle con este delle con est
VU WORD	Pt	PL/PO	PC/PTF	PLIPTP	K/OMAX	and tradering to be independently conditions on a passe in		-
107	11.854	3, 5532	0.12104	0.27955	0.62400			
112	5.8528	1.7543	0.059763	0.13802	0.03000			
122	3.4675	1.0393	0.035407	0.081770	0.96000			
127	- 3.5575	1.0663	0.036326	0.083894	1.0900			
137	4.8028	1.4396	0.049041	0.11326	1.2200			
142	4.7373	1.4701	0:048378	0.11173	1.3900	and the supplier to the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the supplier of the suppli		
>2001110H	AL PRESSURE	RATIOS PO	SERODY INCES					
AD MUKU	Pt	PL/PN-	PL/PTF	PLIPTP	ж/онаж			
107	11.854	3.5532	0.12104	0.27955	9000 مر1-			
115	5.8528	1.7943	0.059763	0.13802	1.0000			
122	3.4675	1.0393	0.035407	0.091770	<b>∕-1.0000</b>			
127	3,5575	1.0663	0.036326	0.083896	-1.0000			
137	4.3028	1.4396	0.049041	0.13326	-1.0000			
142	~~ \$.73 <b>78</b> ~ ~	1.4201	0.048378	- 0/1173	-1.0000			
152	3.5525	1.0648	0.036275	0.083776	-1.0000			
157	3.5575	1:0883	0.036326	C.083994	-1.0000			
ZADDIT ION	L PRESSURE	PATION PAR	<del>- 1112213 - 1127</del>					
AD MUMB	<b>PL</b>	PLIPO	him	PL/PTP	X/DMRX			
152	3.5525	1.0648	× 0.036275	0.083776	-1.0000			
197	3.5975	1.0663	0,036326					
			1					
	AL PRESSURE		DEC SIMPLE					
VIT WITED	Pt /	PL/PD	PL/PTF	~ PE / PTP	X7DMAX -	Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communication of the Communica		
167	3.5578	1.0663	0.036326	8-083894	-1.0000			
172	3.9529	1.0648	0.036275	0.043776	-1.0000			
PARTICULA	PRESSURE	******* * ***	DEG SIMOUN L	OCATION -				
VI WOPT	PL	PL/PN	PL/PTP	PL /PTP	X7DHAX			
192	3.3575	1.0063	0.034283	0.079175	-1.0000			
167	3.2724	0.98086	0.033415	0.077170	-1.0000	erge er i sager annær ge		

	PRELIMI	NARY DATA	06/28/79	CADDETT	REC 10/10/79 0	1:13:17.689	FAC SW641	PG# 1734	RNG 1223
MODITICON	L PPFSSUPE	RATIOS . PPI	MAPY PLUG	any decorate and the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract	al hites also the complete hites of the complete his complete his con-				
VD WORD	PL	PL / PO	PL/PTF	PL /PTP	X/DMAX				
32	15.447	4.6148	0.16861	0.43803	0.43200				
17	0.5032	2.5403	0.092#12	0-24112	0.53000				
47	9.9485	2.9721	9-10859	0.28210	0.62706				
52	10.163	3.0363	0.11093	0.28820	0.72700				
AGDITION	L PRESSURE	RATIOS . FLO	W SPLITTER I	.0.					
IN WORD	PL	PL /PO	PL /PTF	PL/PTP	X/DMAX				
52	11.693	3.4814	0.12720	0.33045	0.42200				
67	12.098	3.6144	0.13205	0.34307	0.69200				
ADDET 10M	IL PRESSURE	RATIOS . FLO	W SPLITTER D	.D.					
O WORD	PL	PL / PO	PL/PTF	PL/PTP	X/DMAX				
77	35 <del>. 575</del>	10.628	7.38830	1.0088	0.58400			Age is access.	and the second contract the contract to
92	11.283	3.3709	0.12316	0.31996	0.63500				
2	3.5548	1.0620	0. 038801	0.10080	0.69200			<del></del>	
ADDITION	L PRESSURE	RATIOS , FJI	CTOR SHROUD						
O WORD		- PL /PO		PLIPTP	- X/DH&X				
197	11.083	3-3112	0.12098	0.31429	0.62400				
112	5.5017	1.6436	0.000051	0.19601	0.83000		<del></del>		
122	3.2394	0.96777	0.035358	0.091 858	0. 96000				
		-1:0420	0.030001	0-10050					and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
137	4.0053	1-1966	0.043718	0-1135R	1.2200				
142		1.1996	0.043827		1.3500	and the second second			
40017 10M		041181 ₁ 461	:6A60#_14t_6f_						
	<b>#t</b>	Pt /PO		Pt /PTP	x/ongs				
M HORD			0.12098	0.31429	-1.0000		•		
		3. 311 <i>2</i>							
107	11.003	3.3112 1.6436	0.060051	0.12001	71.0000				
107	11.003	1.6436 0.96777	0.060051 0.035358	0.091858	-1-0000				
107 112 122	11.093 5.5017	1.6436							
107 112 122 127	11.083 5.5017 3.2394	1.6436 0.96777	0.035358	0.091858	-1-n000				
107 112 122 127	11.083 5.5017 3.2394 3.9548	1.6436 0.96777 1.0820	0.035358 0.036801	0.091858	-1-0000				
107 112 122 127 137	11.003 5.5017 3.2394 3.2396 4.0053	1.6436 0.96777 1.0620 1.1966	0.035358 0.036802 0.043718 0.043827	0.091858 0.10090 0.11358	-1-0000 				
107 112 122 127 137 142	11.003 5.5017 3.2394 9.5598 4.0053 4.0198	1.6436 0.96777 1.0820 1.1966 1.1996	0.035358 0.038801 0.043718	0.091858 0.10090 0.11358 0.11386	-1-0000 -1-0000				
107 112 122 127 137 142 152	11.083 5.5017 3.2394 9.9948 4.0053 4.0153 3.5548	1.6436 0.96777 1.0620 1.1966 1.1990 1.0620	0.035358 0.036801 0.043718 0.043827 0.038801	0.091858 0.10090 0.11358 0.11386 0.10000	-1-0000 				
107 112 122 127 137 142 152 157	11.083 5.5017 3.2394 9.9948 4.0053 4.0153 3.5548	1.6436 0.96777 1.0620 1.1966 1.1990 1.0620	0.035358 0.058801 0.043718 0.043827 0.038801	0.091858 0.10090 0.11358 0.11386 0.10000	-1-000 -1-000 -1-0000 -1-0000				
107 112 122 127 137 142 152 157 >anottinu	11.083 5.5017 3.2394 4.97948 4.0153 4.0149 3.5548 9:5548	1.6436 0.96777 1.0620 1.1966 1.1996 1.0620 1.0620 RATTINS , FAN	0.035358 0.036802 0.043718 0.043827 0.038801 0.038801 HN72212 FLAP	0.091858 0.10090 0.1258 0.11588 0.10090 0.10090	-1-0000 -1-0000 -1-0000				
107 112 122 127 137 142 152 157 980017 1010	11.083 5.5017 3.2394 4.0253 4.0143 3.5548 3.5548 Pt. 3.5548	1.64% 0.96777 1.0020 1.1966 1.1996 1.0620 RATTINE , FAN PL/PO 1.0620	0.035358 0.043601 0.043718 0.043801 0.038801 0.038801 0.038801	0.091858 0.10097 0.12358 0.1358 0.10090 0.10090	-1-000 -1-000 -1-000 -1-000 -1-000				
107 112 122 227 137 142 152 157 240017 1014 70 WIPD 152 157	11.083 5.5017 3.2394 4.0253 4.0193 3.5548 3.5548 Pt. 3.5548 3.5548	1.6436 0.96777 1.0020 1.1966 1.1996 1.0620 1.0620 Pt/PO 1.0620 1.0620	0.035358 0.036801 0.043718 0.043821 0.038801 0.038801 0.038801 0.038801	0.091858 0.10090 0.1258 0.11368 0.10090 0.10080 PL/PYP 0.10080	-1-0000 -1-0000 -1-0000				
107 112 122 127 137 142 152 157 980017 1010 10 WIND 152 157	11.083 5.5017 3.2394 4.0253 4.0143 3.5548 3.5548 1 PRESSURE PL 3.5548 3.5548	1.6436 0.96777 1.0020 1.1966 1.1990 1.0620 1.0620 1.0620 1.0620 1.0620	0.035358 0.036801 0.043718 0.043827 0.038801 0.038801 0.038801 0.038801 0.038801	0.091858 0.10090 0.11458 0.11986 0.10090 0.10080 0.10080	-1-000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
VD WOPD 152 157 > <del>ADDITION</del> VD WORD	11.083 5.5017 3.2394 42053 4.0153 3.5548 3.5548 7.5548 3.5548 3.5548	1.6436 0.96777 1.0020 1.1966 1.1996 1.0420 1.0020 0.47102 , FAN PL/PO 1.0620 1.0620 1.0620	0.035358 0.036801 0.043718 0.043827 0.038801 0.038801 0.038801 0.038801 0.038801	0.091858 0.10090 0.11358 0.11368 0.10090 0.10090 0.10080 0.10080	-1-000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 122 127 137 142 152 157 2400 (7 1014) 152 157 2400 (7 1014) 100 400 (7 1014)	11.083 5.5017 3.2394 4.0253 4.0143 3.5548 3.5548 4. PRESSURE Pt. 3.5548 3.5548 4. PRESSURE	1.6436 0.96777 1.0020 1.1966 1.1996 1.0620 2.0620 2.0620 2.0620 1.0620 2.0620 2.0620 1.0620 2.0620 1.0620	0.035358 0.043601 0.043616 0.043627 0.038801 0.038801 0.038801 0.038801 0.038801	0.091858 0.10090 0.1358 0.11368 0.10090 0.10080 PL/PTP 0.10080 0.10080	-1-0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 122 27 137 142 152 157 200 WIPD 152 157 200 WIPD 157 200 WIPD	11.083 5.5017 3.2394 42053 4.0153 3.5548 3.5548 7.5548 3.5548 3.5548	1.6436 0.96777 1.0020 1.1966 1.1996 1.0420 1.0020 0.47102 , FAN PL/PO 1.0620 1.0620 1.0620	0.035358 0.036801 0.043718 0.043827 0.038801 0.038801 0.038801 0.038801 0.038801	0.091858 0.10090 0.11358 0.11368 0.10090 0.10090 0.10080 0.10080	-1-000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 122 127 137 142 152 157 0 40017 1010 157 0 40017 1010 107 107 107 107 107	11.083 5.5017 3.2394 4.0253 4.0143 3.5548 3.5548 7.7548 3.5548 3.5549 7.76550PE	1.6436 0.96777 1.0020 1.1966 1.1990 1.0620 1.0620 1.0620 1.0620 1.0620 PL/PN 1.0620 1.0620	0.035358 0.043601 0.043616 0.043627 0.038801 0.038801 0.038801 0.038801 0.038801	0.091858 0.10090 0.11358 0.11368 0.10090 0.10080 0.10080 0.10080 0.10080 0.10080 0.10080	-1-0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 122 127 137 142 152 157 >=nno(7-1nw) 152 157 >=nno(7-1nw) 157 157 >=nno(7-1nw) 167 172	11.083 5.5017 3.2394 4.0253 4.0143 3.5548 3.5548 3.5548 3.5548 3.5549 4 PRESSURE PL 3.5548 3.5548	1.6436 0.96777 1.0920 1.1966 1.1996 1.0620 0.0620 0.0620 0.0620 0.0620 0.0620 0.0620 0.0620 0.0620 0.0620	0.035358 0.043601 0.043627 0.039801 0.038801 1 WHIZLE FLAP 0.038801 0.038801 0.038801 0.038801 0.038801 0.038801	0.091858 0.10090 0.1358 0.11368 0.10090 0.10080 0.10080 0.10080 0.10080 0.10080 0.10080	-1-0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 122 127 137 142 152 155  •••••••••••••••••••••••••••••	11.083 5.5017 3.2394 4.0253 4.0143 3.5548 3.5548 3.5548 3.5549 4. PRESSURE PL 3.5548 3.5549 4. PRESSURE PL 3.5558 4. PRESSURE PL 4. PRESSURE PL	1.6436 0.96777 1.0920 1.1966 1.1990 1.0620 0.0620 0.0620 0.0620 1.0620 0.0620 0.0620 0.0620 0.0620 0.0620 0.0605	0.035358 0.036801 0.043718 0.043827 0.038801 0.038801 0.038801 0.038801 0.038801 0.038801 0.038801 0.038801 0.038746	0.091858 0.10090 0.11358 0.11368 0.10090 0.10090 0.10090 0.10090 0.10090 0.10090 0.10090 0.10090	-1-000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 122 127 137 142 152 157 >=nno(7-1nw) 152 157 >=nno(7-1nw) 157 157 >=nno(7-1nw) 167 172	11.083 5.5017 3.2394 4.0253 4.0143 3.5548 3.5548 3.5548 3.5548 3.5549 4 PRESSURE PL 3.5548 3.5548	1.6436 0.96777 1.0020 1.1966 1.1990 1.0620 1.0620 1.0620 1.0620 1.0620 1.0605 RATIOS v 00 91/P0 1.0052	0.035358 0.036801 0.043718 0.043827 0.038801 0.038801 0.038801 0.038801 0.038801 0.038801 0.038746	0.091858 0.10090 0.1358 0.11368 0.10090 0.10080 0.10080 0.10080 0.10080 0.10080 0.10080	-1-0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

NASA-I FWI	S PRELIMI	INAFY DATA	06/28/79	CADDETI	REC 10/10/79 01:13:52.855	FAC BY6KL	PGM C034	PW 19 RDG 1224	
		PATIOS . PRI				THE BADAS	- G CU34		
VD HORD	PL	PL/PO	PL / PTF	PL/PTP	X/DMAX				
32	17.238	5.1852	0.18726	0.43791	0.43200				
37	9.4844	2.852R	0.1035R	0.24094	0.53000				
. 7	11.104	3.3399	0.12126	0.28207	0.62900				
52	11.333	3.4090	0.12377	0.28791	0.72700				
>ADDIT ION	AL PRESSURE	RATIOS . FLO	W SPLITTER I	.D	and a second of the second of the second of the second of the second of the second of the second of the second			reares eres	
VD WORD	Pt	PL/PO	PL/PTF	PL /PTP	x/DMAX				
62	13.047	3.9245	0. 14249	0.33144	0.42200	* - · *· · · · · ·			
<u> </u>	12.098	3.6390	0.13212	0.30733	0.69200				
>ADDITION	PRESSURE	RATIOS , FLO	W SPLITTER O	. D.		· · · · · · · · · · · · · · · · · · ·	<del></del>	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
VO WORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX				
77	35.547	10.692	0.38821	0.90302	0.56400				
92 92	11.293	3.3970	0.12334	0.28689	0.63500				
	3.5539	1.0590	0.038817	0.090280	0.69200				
		RATIOS , EJE			The Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Co				
/N WORD ~		P[/PI	PL/PTF	P[/P[P	X/MAX				
.07	11.099	3.33R4 1.6573	0.12121 0.060172	0.28194	0.62400 0.83000				
22	3.2387	0.97416	0.035369	0.082273	0.96000				
27	3.5469	1.0879	0.038797	0:040153	1.0900			<del></del>	
37	4.4594	1.3413	0.048700	0-11328	1.2200				
	4,4143	1.3278	0.048209	0.11214	1.3500				
************	AL - 882 SSIME	247101 200	ERCOV INCET						
ADMINED	- Pt	PL/PO							
107	11.099	3.3384	0.12121	0.28194	*/DMAY -1-9000	•			
12	<del>5.5097</del>	1.8973	0.060172	0.13997	-1.0000 -31.0000	. <del></del>			
22	3.2387	0.97416	0.035369	0.082273	-1.0000				
27	\$ 5489	1.0675	0.03875?	0.090135	-1.0000			<del></del>	
37	4.4694	1.3413	0.048700	0. 1 1228	-1.0000				
42	4.4149	1.3278	0.048209	0./1214	-1:0000				
52	3.5439	1.0660	0-038702	0.090026	-1.0000				
.57	3.5389	1.0645	0.038648	0.089899	-1.0000				
#1011100#	AL PRESSURE	HATTING PAN	HOPELS FERR						
D WORD	Pt -	- PL/PO	MIPTE -		X/DWAX				
.52	3.5439	1.0660 /	0.038702	0.090026	-1.0000				
157	3.5389	1.0093	Dr. 03 8648	0.089899	-1-0000				
/4001T10W	AL PRESSURE	<del>RATIONS , 20</del>	<del>DEG SHRODA L</del>	OCATION				<del></del>	
O WORD	Pt	91.790	PL-/PTP	M. SELE	X/DRAX				
67	3.5397	1.0645	0.038648	0>089899	-1-0000				
	3,8439	1.0660	0.038702	0.0300Se.	-1.0000				
172	AL PRESSURE	RATIOS . RO	DEG SHROUD L	OCATION				······	
					_				
172 <del>&gt;ADDITIN</del> Y VD YMKD	<b>91</b>	PL/Ph	- PL:/PTF	PL /PTP	X/DMAX				
940917109	PL	1.0103	PL/PTF	PL /PTP 0.085323	1.000Q	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	The second section of the second section is a second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the	and the second of the second	

	S PPFLIMI	MARY DATA	06/28/79	CADDELL	REC 10/18/79 01:14:46.056 FAC 84641 PGM C834 MNG 1225
>ADDIT ION	IAL PRESSURE	PATIOS , PRI	MARY PLUG		
ND MUMD	PL	PL/PO	PL/PTF	PL /PTP	X/DMAX
32	19.329	5.8190	0.21239	0.43906	0.43200
37	19.597	3-1901	0.11644	0.24070	0.53000
47	12.406	3.7346	0.13631	0.28179	0.62900
52	12.675	3.8159	0. 1392 A	0.28791	0.72700
>ADDITION	ML PRESSUMF	PATIOS . FLO	M SAFIALEM I	• D•	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
VO WORD	PL	PL/PO	PL /PTF	PL/PTP	x/DMAx
62	14.634	4.4054	0.16080	0.33240	0.42200
67	12.086	3.6384	0.13260	0.27452	0.69200
>ADDET ION	AL PRESSURE	RATIOS , FLO	N SPLITTER O	.0.	
VD WORD	PL	PL / PO	PL/PTF	PL /PTP	X/DMAX
77	35.391	10.642	0.38844	0.80298	0.58400
62	11.226	3.3796	0.12335	0.25500	0.63500
92	3.9912	1.0691	0.039021	0.080664	0.89200
>ADDIT TON	ML PRESSURE	********	CTOR SHROUD		
VD WORD	- <b>PL</b>	- R7P3	PL/PTF	PE /PTP	TINAT
107	11-021	3,3:19	0-15110	0.25035	0.62400
112	9.4722	1.0414	0.060128	0.12430	0.83000
122	3.2310	0.97267	0.035502	0.073390	0.96000
127	- 3.5462 -	1.0676	0.038966	- 0.080550	1.0900
137	4.9620	1.4938	0.054522	0.11271	1. 2200
142	4. 8920	1:4697	0:053643	0.11089	1.3900
• ••	10 0 320		56655645	000.00	200000
>4001 <b>110</b> #	MI PRESSURE	RATIOS FOR	\$800V=1MLST		
AUMURD	<b></b>				
	Pt	- PL/PO			X/OMAX
107	11.021	3.3179	0-12110	0.25035	-1 م
112	-5.4722	1.6474	0.060129	0.12490	1.0000
122	3.2310	0.97267	0.035502	0.073390	<b>∕</b> -1.0000
127	35 3405	1-0676	0.038966	0.000550	-1.0000
137	4.94.20	1.4938	0.054522	0.11271	-1.0000
142	4.9820	1.4697	0.053643	9211089	-1.0000
152	3.5362	1-0646	0.038856	0.080323	-1.0000
157	3.5362	1.0646	0.098856	0.000923	-1.0000
<del>&gt;4001710</del> 9	AL PRESSURE	RATIOS FAR	HOLLY PLAP	<del></del>	
AD MUSD	PL -	PL/P0	M1998	PL /PTP	T/DMAX
152	3.5362	1.0646	0.038856	0.080323	-1.0000
157	3. 5362	1.0696	0.039056	0.080323	1.0000
>499 <del>1710</del> N	ML PRESSURE	****** . 20	nea swanda t	ncat ton	
VO WORD	P1 /	PL/P0	PL/PYF	RI /PTP	X/OMAX
	3.5412	1.0661	0-038911	05080437	-1.0000
167	3.5562	1.0646	0.038856	0.070373	-1.0000
167 172					
172			<del>DEO SIMBUD 1</del> 1	ਹ <b>ਦ≥₹ 1ਹੀੀ</b> `~	
172	PRESSURE	*#*103 <b>†</b> 50			
17? <del>&gt;4981718</del> 9 VN WOKN	Pt	PL/PO	PL/PTF	PL/PTP	KIDNAK
172	•			PL/PTP 0.076345 -0.074413	x/buax

	PRELIMI	NARY DATA	06/28/79	CADDELL	NEC 10/18/79 01:15:58.631 FAC 8X6X1 PG" C834 PRG 1226
>ADDIT IONA	IL PRESSIME	RATIOS , PRI	MARY PLUG		
ORGH OVA	PL	PL/PO	PL/PTF	PL/PTP	x/DMAX
32	13.894	4.1904	0.1690Y	0.43733	0.43286
31	7.6724	2.3140	0.093332	0-24151	0.53000
47	8.4721	7.7060	0.10914	0.24241	0.62900
52	9.1520	2. 7603	0.11133	0.28808	0.72700
>ADDITIONA	L PRESSURE	RATIOS . FLO	M SPLITTER I	.D.	
AVO MORO	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX
62	10.736	3.2381	0.13060	0.33794	0.42208
67	12.015	3.6239	0.14616	C.37621	0.69200
>ADDITION	AL PRESSURE	RATIOS . FLO	W SPLITTER D	.0.	
AVD WORD	PL	PL / PO	PL/PTF	PL/PTP	x/DMAx
77	32.147	Y. 6958	0.39106	1.0119	0.56490
A2	10.162	3.0648	0.12361	0.31985	0.63500
92	3,7467	1.0697	0.043144	0.11164	0.69200
>ADDITION	T PRESSURE	RATIOS , EJE	CTOR SHROUD		
AND MINKE	- PL	PLYPO	<del></del>	PC /PTP	X/OHAY
107	9.9616	3.0045	0.12118	0.31356	0.62400
1112	4.9523	1.4936	0.060243	0.15558	0. #3000
122	2.9113	0.87806	0.035414	0.091638	0.96000
127	3.5267	1.0637	0.042901	0.11161	1.0900
137	3.6217	1.0923	0.044057	0.11400	1.2200
142	3.6217	1.0923	0.044057	0.11400	1.3500
~~~~	N=PRECURS	*****	######################################		
					
	- Pt	PC/P0	PEPPF	PLIPTP	X70MAR
-107	9.9616	3. 0045	0.12118	0.31356	-10000
-115 J	4.9523	1.4936	0:060243	0.19988	1.0000
-172	2.9113	0.87806	0.035414	0.091639	~1.0000
-127	4-2501	1.0637	0.042901	0.11191	-1.0000
-137	3,4217	1-0923	0.044057	0.11400	-1.0000
-142	3.627	1.0923	0. 04405T	9211400	-1.0000
-152	3.5317	1.0652	0.042961	0.11117	-1-0000
-157	3.9267	1.0637	0.042901	0.11101	-1.0000
SADDIT TON	IL PRESSURE	HATEDS - PAN	HOTELE FLAP		
VO WORD	Pt	··· PL/PD·····	MITTE -	PLIPTP	T/OMEX
-152	3.5317	1.0652	0.042961	0.11117	-1.0000
-157 ~	3.5267	1.0637	0.045901	0.11101	=1.0000
->xDDTT IDN	IL PRESSURE	RETOOS , 20	DEC SHADOO E	OCATION	
LVD WORD	Pt ···	PL 190	- PLIPTE	CLIPTP	X/DMAX: The second of the seco
-167	3.53	1.0652	0.042961	2011117	-1.0000
-172	3.5867 ~	1:0637	0.042901	-0.1H01	-1-0000
->#100 TT 1014	PRESSURE	R#T105 , 80	DEG SHROUD 1	OCATEON -	
	Pt	PI /PN	- PLIPTP	- Pt /PTP	X/DEAX
tau nuere					
evn woen -182	3.3366	1.0063	0.040568	0.10503	-1.0000

SANDITION	AL PRESSIME	RATIOS . PR	IMARY PLUG		
AD MUND	PL	PL/PO	PL/PTF	PL /PTP	K / DMA K
32	15.497	4.6481	0.16831	0.43879	30.43200 mmm - 111 mm
37	9.5197	2.5620	0.10379	0.24186	9_53000
47	7.7695	2.9980	0.12146	0.28302	0.52906
52	10.174	3, 05 96	0-12396	0.28884	0.72700
> ADD ET TON	AL PRESSURE	RATIOS . FLI	DW SPLITTER I	-0-	
VD WORD	PL	PL/PO	PL/PTF	PI /PTP	X/OMAX
62	11.779	3.5421	0.14390		0.42200 mm
67	11.764	3,5977	0.14576	0.33964	0.69200
>ADDIT IDN	AL PRESSURE	RATIOS . FLI	OW SPLITTER O	. O.	
-	and the second		a and who is not a	er manage a supplier to the contract of	نوريز در در است می در در است و در در در میشود. در در در است است است و در در در است میشود. در است در در در است در در است در است در است است است است است است است
AD MOND	PL	PL/PII	PL/PTF	PL/PTP	X/DMAX
77	35.102	7.6716	0.341#3	0.91303	The state of the s
65	10.160	3.0551	0.12377	0.28841	0-63500
92	3.9477	1.0865	0.043221	0.10071	8.89200
>ADDITION	AL-PRESSURE	RATIOS , EJI	ECTOR SHIROUR		Est formation and the second of the second o
VD WORD	Pt	PL/PD	PLIPTE	PL/PTP	X/OREY
107	9.9346	2.9875	0.12103	0.20203	0.62400
112		1.4912	0.060412	0.14077	0,83800
122	2.9071	0.87420	0.035417	0.082527	Q. 96000
27	3.5327	1.0629 -	0-043038	0.10029	1,090
137	3.9930	1.2008	0.048647	0.11336	1-2200
142	3.9480	1.1972	0.010098	0.1129R	The STATE CONTROL OF THE CONTROL OF
				~~~~~	
24001710M	M - PRESSINE	******	******		
PE WORD -	Pt	PL793 -			
107			PL / PT P	PL/PTP	1.4000
	7.9146	2.9875	0.12103	0.28203	
115	4.9967	1.4912	0.060412		1.0000 year or and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second
122	2.9071	0.87420	0.035417	0.082527	/ -1.0000
127	A-3351	1.0023	0.047038	0.10029	-1.9000
137	356530	1.2008	0.048647	0.11836	-1.6000
1-12	3.1100	1.1072	0.048098	0/1208	TO BE AND THE THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE
57	3.5427	1.0653	0.043160	0.10057	-1-0000
157	3.5577	-1-06-98	0:043099	0.19043	- 1.0000 - The second - 1. C. C. C. C. C. C. C. C. C. C. C. C. C.
MOI-TEOCRA	N <del>L PRESSIME</del>	RATERS - PAI	N HOTELE FLAS		
YO MORD	PL	PL/PD	him		THE RESERVE AND ADDRESS OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE
152	3.5427	1.0653	× 0.043160	0.10057	-1.0000
57	3.5377			0-100+3	
> <del>4071110</del> 1	AL PRESSURF	RATEOS - 20	DES SINCUE L	ncatton	
VO WORD	PI	PL 190	PLIPTE		
167	3.5324	1.0638	0.043099	0×10043	#/DMAX: NO CONTROL OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROP
107 172		1.0653			-1.0000
412	3,8527	1.0023	0.043160	- 0.10057	
>ADDITION	PRESSURE	RATIOS y 90	DEG SHROUD L	OCATION	
un	. Pt	· -PC/PD	PL/PY#	Pt /PTP	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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VD WHEN 188	3.3375	1.0036	0.040660	0.094746	~1.000@

MASA-LFW1	S PRELITI	HARY DATA	06/29/79	CADDELL	REC 10/18/79 01:17:57.533 FAC 9X6X1 PGR C034 90G 1228
NOTT FOOL	AL PRESSURE	RATIOS . PR	MARY PLUG		
VD WORD	PL	Pt /PO	PL/PTF	PL/PTP	X/DMAX
32	18.177	4.4439	0.21914	0.43916	0.43208
37	9.9857	2.9907	0.12039	0.24126	0.53080
47	11.665	3.4938	0.14064	0.78184	0.62900
52	11.935	3.5746	0.14389	0.28836	0.72700
NOET 100A	AL PRESSURE	RATIOS . FLO	W SPLITTER I	.0.	
va wa <b>a</b> a		PL/P0	PL/PTF	PL/PTP	x/DMAX
VO WORD	PL 13.796	4,1314	0. 16631	0.33328	0.42200
62 67	11.985	3.5896	0.14449	0.28957	0.47200
					AS A 1500
MOTTEGOR	AL PRESSIME	RATERS , FLO	W SPLITTER O	.D.	ார். இது அண்ணும் அன்று அரசு நார் நார் நார் நார் நார் நார் நார் நார்
VO WORD	PL	PL/PG	PL/PTF	PL /PTP	X/OMAX
77	37.300	7, 5777	0. 39038	0.78234	G. 56400
#2	10.221	3.0611	0.12322	0.24694	0.63500
45	3.5732	1.0702	0.043078	0.086330	0.69200
>ADD [11004	AL PRESSURE	RATIOS , FJI	CTOR SHROOT	reference on an additional description of the second	THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O
AD MUMO.	· •	PETPIT	PLIPTE	-9(7010	TORRES OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL
107	10.046	3.0787	0.12111	0.24271	0.42400
112	4.7743	1.4758	0.060212	0.12067	0.83000
122	2.9325	0.87829	0.035354	0.070#51	0-74000
127	3.5581	1.0697	0.042897	0.085967	
137	4.6491	1.3924	0.056050	0.11233	1.2200
142	4.5991	1.3774	0.055447	0.11112	восского — 1. 3500 жини от типе по постояння по то по по постанования по на постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по постанования по по постанования по постанования по постанования по по постанования по по по по по по по по по по по по по
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112		1, 4958	0.060212		
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122 1 <del>27</del>	2.9325	0.87826	0.035354	0.070851	/ -1.0000
137	3.5581	1.0657	0.042897	0.005987	-1.0900
	656491	1. 3924	0.056050	0.13233	-1.0000
142 · · · · · · · · · · · · · · · · · · ·	4.590	1.0657	0.055447	9/11112	=1.0060
172 157	3.5581	1.0542	**************************************	0.085967	
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152	3.5591	1.0657	× 0.042897	0.085967	
157	3.5531	1.0092	8-042837	0.005847	
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167	3.5581	1.0657	0.042897	0.085967	
177	1.3861	1.0457	0.042897	0-yazəe1	-1.0000
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	3.3760	1.0117	0.040725	0.081414	
182	3.3760 3.2979	1.0117	0.040725 0.039760	0.081614	

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> ADDITERM	ME SEESONE	PATIOS . PRI	THAPY PLUG		
VO WORD	PL	7L/PN	PL /PTF	PL/PTP	X/DMAX
32	12.657	***************************************	0.16859	0.43725	<b>5.43200</b> Third Control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the contr
37	6.9911	2.0908	0.093119	0.24152	0.53000
47	8.1816	- Z. 4468	0.10898	0.28265	0.52900
52	8.3416	2.4947	0.11111	0.20017	0.72700
>400 IT EOM	AL PRESSURE	RATEOS . FLI	W SPLITTER I	. D.	
VD WORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX
	7.6220	2.8776	0.12916	0.33240	0.42200
67	11.952	3.5744	0-15920	0.41290	0.49200
>ADDITION	AL PRESSURE	RATIOS . FLO	W SPLITTER O	.0.	
VO WORD	PL	PL/P0	PL/PTF	PL /PTP	X/DMAX
77	29.521	8, 8285	0.39321	1.0198	0:55400
92	9.2769	2.7744	0.12357	0.32048	0.43500
92	3.9631	1.0656	0.047460	0.12309	0.89200
>ANDIT TOW	NE PRESSURE	RATIOS , FJE	CTOR SHROUD		
VD WORD		PE7P0	PL/PTF	PL/PTP	X/ONAX
107	9.0969	2.7205	0.12117	0.31426	0.62400
112	4.7091	1,3989	0.080061	0.19977	0.83008
172	2.6569	0.79458	0.035389	0.091787	
127	3.5431	1.0596	0.047199	0. 12240	1.0900
137	3.2928	0.98474	0.043859	0.11375	1-2200
142	5.2070	0 <u>-90324</u>	0:043792	····· 0: 11998	1.3508
146	20.00				
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24001730W	AL - PRESSURE	RATIOS	18800Y 1HL8T	PL/P1P	
24001710W	Pt 9.0969	PL /PO 2.7205	PL/PTP 0.12117	PL/PTP 0.31426	1.0000
NO WORD 112	Pt 9.0969	PL /PO 2.7205 1.3485	PL/PTP 0.12117 0.060061	PL/PTP 0.31426 0.19977	x/09/afr -1/0900
NO WORD 107 1122 127 137	PL 9.0969 4.5091 2.6569 3.2928	PL /PO 2.7205 1.3465 0.79458	PL/PTP 0.12117 0.080061 0.035389	0.31426 0.15577 0.091787 0.12290 0.12375	1.0000 -1.0000 -1.0000
240017 5000 100 WORD 112 112 127 137	Pt 9.0969 9.0969 9.5091 2.6569 9.3491 3.2928 9.2846	PL/PD 2.7205 1.3485 0.79458 1.0996 0.98474 0.98324	PL/PTP 0.12117 0.000001 0.035389 0.047193 0.043859 0.043792	0.31426 0.15577 0.091787 0.12290 0.11575 9411358	X/00/26 -),0000 -1.0000 -1.0000 -1.0000 -1.0000
NO WORD 107 112 122 127 137 147	Pt 9,0969 9,0969 9,5091 2,6569 9,5931 3,2928 9,2848 3,5581	PL/PD 2-7205 1-3485 0.79458 1.0396 0.98474 0.98924 1.0641	PL/PTP 0.12117 0.000001 0.035389 0.047193 0.043859 0.043792 0.04793	PL/PTP 0.31426 0.15577 0.091787 0.12290 0.12775 0.11358 0.12292	*/00/af
MO WORD 112 107 112 122 127 137 147	Pt 9.0969 9.0969 9.5091 2.6569 9.3491 3.2928 9.2846	PL/PD 2.7205 1.3485 0.79458 1.0996 0.98474 0.98324	PL/PTP 0.12117 0.000001 0.035389 0.047193 0.043859 0.043792	0.31426 0.15577 0.091787 0.12290 0.11575 9411358	X/00/26 -),0000 -1.0000 -1.0000 -1.0000 -1.0000
PQ WORD 107 112 122 127 137 147 157 157	Pt 9.0969 4.5091 2.6569 3.59431 3.2928 3.5581 3.5581	PL/PD 2.7205 1:3485 0.79458 1:0596 0.98474 0.98329 1:0641 1:0841	PL/PTP 0.12117 0.000061 0.035389 0.047193 0.043859 0.047393 0.047393	PL/PTP 0.31426 0.15577 0.091787 0.12290 0.12775 0.11358 0.12292	*/00/af
PO WORD 107 112 122 127 137 149 1552 157 1000	Pt 9.0969 9.0969 9.5091 2.6569 3.5931 3.2928 9.2948 3.5581 9.5581	#1706 ; #00 2.7205 1.3485 0.79458 1.0996 0.98474 0.98924 1.0641 1.0641	PL/PTP 0.12117 0.000001 0.035389 0.047193 0.043859 0.047393 0.047393	0.31426 0.15577 0.091787 0.12250 0.1275 0.1358 0.12292 0.12292	*/69.06 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
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NO WORD 107 112 122 127 137 147 152 157 >ADDITION VD WORD 152 157	Pt 9.0969 9.0969 9.5091 2.6569 9.59431 3.2928 9.2346 3.5581 9.9581	#1706 ; 200 2.7205 1.3465 0.79458 1.0996 0.98474 0.98924 1.0641 1.0641 **RATIOS ; PAR	PL/PTP 0.12117 0.060061 0.035389 0.047193 0.043859 0.047393 0.047393	0.31426 0.15577 0.091787 0.12290 0.1275 0.1358 0.12292 0.12292 0.12292	T/0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
VQ WORD 107 112 122 127 137 142 152 157 >AD91T10W VD WORD 152 157 >AD91T10W VD WORD	Pt 9.0969 9.0969 9.5091 2.6569 3.5581 9.5581 9.5581 9.5581 9.5581	#1706 ; #00 2.7205 1:3465 0.79458 1:0996 0.98474 0.98924 1:0641 1:0641 RATIOS ; PAR #1/PO 1:0641	PL/PTP 0.12117 0.000001 0.035389 0.047193 0.043859 0.047393 0.047393 0.047393 0.047393 0.047393	PL/PTP 0.31426 0.19977 0.091787 0.12290 0.1275 0.12292 0.12292 0.12292 0.12292 0.12292	#/894# -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
VANDET INW 107 112 127 137 142 152 157 24091710W VD WORD 152 157 24091710W VD WORD 167	Pt 9.0969 9:5091 2.6569 9:9431 3.5581 3.5581 3.5581 At PRESSURE Pt 3.5581 7.5581 41 PRESSURE Pt 3.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.5581 7.55	#1708 ; 200  PL/PO 2.7205 1.3485 0.79458 1.0996 0.98474 0.98924 1.0641 1.0641 1.0641 1.0641 1.0641	PL/PTP 0.12117 0.060061 0.035389 0.047193 0.043859 0.047393 0.047393 0.047393 0.047393 0.047393 0.047393 0.047393	0.31426 0.15977 0.091787 0.12290 0.12575 0.12292 0.12292 0.12292 0.12292 0.12292 0.12292	X/00/2X -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
VANDET INW 107 112 127 137 147 157 24091710W VD WORD 152 157 24091710W VD WORD 167	Pt 9.0969 9.0969 9.5091 2.6569 3.5581 9.5581 9.5581 9.5581 9.5581	#1706 ; #00 2.7205 1:3465 0.79458 1:0996 0.98474 0.98924 1:0641 1:0641 RATIOS ; PAR #1/PO 1:0641	PL/PTP 0.12117 0.000001 0.035389 0.047193 0.043859 0.047393 0.047393 0.047393 0.047393 0.047393	PL/PTP 0.31426 0.19977 0.091787 0.12290 0.1275 0.12292 0.12292 0.12292 0.12292 0.12292	#/894# -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
NADDITION 107 112 122 127 137 147 157 NADDITION 152 157 NADDITION VD WORD 152 157 NADDITION VD WORD 167 177	Pt 9.0969 9:5091 2.6569 9:2931 3.2928 9:2348 3.5581 3.5581 3.5581 3.5581 3.5581 3.5581 3.5581 3.5581 3.5581	PL/PD 2.7205 1.3485 0.79458 1.0595 0.98474 0.98329 1.0641 1.0641 1.0641 1.0641 1.0641 1.0641 1.0641	PL/PTP 0.12117 0.060061 0.035389 0.047193 0.043859 0.047393 0.047393 0.047393 0.047393 0.047393 0.047393 0.047393	PL/PTP 0.31426 0.19977 0.091787 0.12775 0.12792 0.12292 0.12292 0.12292 0.12292 0.12292 0.12292 0.12275 0.12275	X/00/2X -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
VANDITION  107 112 127 137 147 157 24091710W  VD WORD 152 157 24091710W  VD WORD 167 177	Pt 9.0969 9:5091 2.6569 9:2931 3.2928 9:2348 3.5581 3.5581 3.5581 3.5581 3.5581 3.5581 3.5581 3.5581 3.5581	#1708 ; 200  PL /PO 2.7205 1.3485 0.79458 1.0996 0.98474 0.98924 1.0641 1.0641 1.0641 1.0641 1.0641 1.0641 1.0641 1.0641 1.0641	PL/PTP 0.12117 0.000001 0.035389 0.047193 0.043859 0.047393 0.047393 0.047393 0.047393 0.047393 0.047393 0.047393 0.047393	PL/PTP 0.31426 0.19977 0.091787 0.12290 0.12575 0.12292 0.12292 0.12292 0.12292 0.12292 0.12292 0.12275 0.12275	X/00/2X -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
VQ WORD 107 112 122 127 137 147 152 157 24D9TT10W VD WORD 152 157	Pt 9.0969 9.5091 2.6569 9.2948 3.5581 9.5581 9.5591 Mt. PRESSURE Pt 3.5581 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE Pt 3.5591 Mt. PRESSURE PT 3.5591 Mt. PRESSURE PT 3.5591 Mt. PRESSURE PT 3.5591 Mt. PRESSURE PT 3.5591 Mt. PRESSURE PT 3.5591 Mt. PRESSURE PT 3.5591 Mt. PRESSURE PT 3.5591 Mt. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESSURE PT 3.5591 MT. PRESS	PL/PD 2.7205 1.3485 0.79458 1.0595 0.98474 0.98329 1.0641 1.0641 1.0641 1.0641 1.0641 1.0641 1.0641	PL/PTP 0-12117 0-000001 0-035389 0-047199 0-043859 0-047393 0-047393 0-047393 0-047393 0-047393 0-047393 0-047393	PL/PTP 0.31426 0.19977 0.091787 0.12775 0.12792 0.12292 0.12292 0.12292 0.12292 0.12292 0.12292 0.12275 0.12275	X/00/2X -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000

37 7. 47 9. 47 9. 52 9. >ADDITIONAL PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O	4.174 .8202 .1554 .3494 RESSURE R 0.750 1.915 RESSURE R 9.435 .2454 .5678	PL/PN 4.2417 2.3400 2.7395 2.7949 tatios . Ft n PL/PO 3.2167 3.5652 tatios . Ft n PL/PO 8.8076 2.7464 1.0676	PL/PTF 0.18954 0.10458 0.12243 0.12243 0.12491 W SPLITTER I. PL/PTF 0.14376 0.15933 W SPLITTER II. PL/PTF 0.39563 0.12364 0.067711	Pt/PTP 0-33180 0-34775 0.34775 0.91/PTP 0-40F51 0-29536 0-11012 Pt/PTP 0-27949 0-13854 0-081692	X/DMAX 0.43200 0.53000 0.62900 0.72700  X/DMAX 0.42206 0.69200  X/DMAX 0.53600 0.63500 0.69200  X/OMAX 0.62600 0.69200
32 14 37 7, 37 7, 47 9, 52 9, >ADDITIONAL PI VD WORD PL 77 21 82 9, 92 33 >ADDITIONAL PI VD WORD PL 17 9, 112 4, 122 2, 127 3, 142 3,  ***SERBUTTONAL MI VD WORD PL ************************************	4.174 .8202 .1554 .3494 RESSURE R 0.750 1.915 RESSURE R 9.435 .2454 .5678 RESSURE R	4.2612 2.3400 2.7395 2.77949  RATIOS - FLO PL/PO 3.2187 3.5652  RATIOS - FLO PL/PO 8.9076 2.7644 1.0876  RATIOS - EJE PL/PO 2.7046 1.3931 0.79197 1.0031	0.18954 0.10458 0.12243 0.12491 0.12491 0.16491 0.16376 0.15933 0.15933 0.15933 0.12364 0.067711 0.12110 0.060025 0.035394	0.43748 0.24137 0.78258 0.28829 .D. Pt/PTP 0.33180 0.34775 .D. Pt/PTP 0.29536 0.11012 Pt/PTP 0.27949 0.13856 0.081692	0.43200 0.53000 0.62400 0.72700 X/DMAX 0.42205 0.69200 X/DMAX 0.535400 0.63500 0.63500 0.63500 0.62406 0.83000
77 7. 47 9. 47 9. 52 9. >ADDITIONAL PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O	.8202 .1554 .3494 RESSURE R 0.750 1.915 RESSURE R V.435 .2454 .5678 RESSURE R	2.3400 2.7395 2.7949 RATIOS . FLO PL/PO 3.2187 3.5652 RATIOS . FLO PL/PO 8.8076 2.7464 1.0876 RATIOS . EJE PL/PO 2.7096 1.3831 0.79197 1.0831	0.10456 0.17243 0.12491 DM SPLITTER I. PL/PTF 0.14376 0.15933 DM SPLITTER II. PL/PTF 0.39363 0.12364 0.067711 CTOR SHIPOD PL/PTF 0.12110 0.060025 0.035394	0.24137 0.78258 0.28829 .0. Pt/PTP 0.33180 0.36775 .0. Pt/PTP 0.29536 0.11012 Pt/PTP 0.27949 0.27949 0.13856 0.081692	0.53000 0.62900 0.72700 X/DMAR 0.42205 0.69200 X/DMAR 0.43500 0.63500 0.63500 0.63500 0.62400 0.62400
47 9. 52 9. >ADDIVIONAL PI AVD WORD PL 62 17 67 11  >ADDITHONAL PI AVD WORD PL 77 29 62 9. 92 3.  >ADDITHONAL PI 107 9. 112 6. 122 2. 127 3. 142 3.  ***********************************	.1556 .3494 RESSURE R 0.750 1.915 RESSURE R 9.435 .2454 .5678 RESSURE R	2.7395 2.7949 RATIOS . FLO PL/PO 3.2167 3.5652 RATIOS . FLO PL/PO 8.8076 2.7664 1.0676 RATIOS . EJE PL/PO 2.7096 1.3931 0.79197 1.0031	0.12243 0.12491 0.12491 0.12491 0.12491 0.14376 0.15933 0.15933 0.12344 0.047711 0.12140 0.12110 0.060025 0.035394	0.78258 0.28829 .0. PI/PIP 0.33180 0.36775 .0. PI/PIP 0.40751 0.29536 0.11012 PI/PIP 0.27949 0.13856 0.081692	0.62400 0.72700 X/DMAX 0.42206 0.69200 X/DMAX 0.58400 0.63500 0.63500 0.69200
52 9.  >ADDIT IONAL PI  AVO WORD PL  77 24  62 9.  AVD WORD PL  77 27  62 9.  >ADDIT IONAL PI  AVD WORD PL  17 24  12 2.  127 3.  142 3.  AVD WORD PL  34001710001 PL  34001710001 PL	.3404  RESSURE R 0.750 1.915  RESSURE R 9.435 .2454 .5678  RESSURE R .0554 .6468 .5528	2.7949  RATIOS . FLO  PL/PO	0.12491 M SPLITTER I. PL/PTF G.14376 0.15933 M SPLITTER II. PL/PTF G.39363 0.12364 G.007711 CTIR SHROUD PL/PTF O.12110 G.060025 0.035394	0.28829 .0. P1/PTP 0.33180 0.36775 .0. P1/PTP 0.40751 0.29536 0.11012  P1/PTP 0.27949 0.13854 0.081692	0.72700  X/0MAX 0.42205 0.69200  X/0MAX 0.58400 0.63500 0.63500  X/0MAX 0.62406 0.83000
>ADDIT IONAL PI 62 IG 67 II >ADDIT HONAL PI AVD WORD PL 77 29 62 96 92 36  >ADDIT HONAL PI 107 96 112 66 122 26 127 36 137 36 142 36	RESSURE R 0.750 1.915 RESSURE R 9.435 .2454 .5678 RESSURE R	PL/PO 3.2167 3.5652 1ATIOS - FLO 9L/PO 8.8076 2.7464 1.0876 1ATIOS - EJE PL/PO 2.7096 1.3831 0.79197 1.0831	PL/PTF 0.14376 0.15933 W SPLITTER 0. PL/PTF 0.39363 0.12364 0.007711 CTOR SHIPOUD PL/PTF 0.12110 0.060025 0.035394	PL/PTP 0.33180 0.36775 0.0. PL/PTP 0.40751 0.29536 0.11012 PL/PTP 0.27949 0.13656 0.081692	X/DMAX 0.42205 0.69200 X/DMAX 0.58400 0.63500 0.63500 0.89200
AVD WORD PL  52 IT  57 IT  57 IT  58 IT  ADDIT HUMAL PI  AVD WORD PL  77 29  62 9.  92 3.  >ADDIT HUMAL PI  107 9.  112 4.  122 2.  127 3.  142 3.  AVD WORD PL  AVD WORD PL  34001710001 PL	0.750 1.915 RESSURE R 9.435 .2454 .5678 RESSURE R .0554 .6488 .5528	PL/PO 3.2167 3.5652 IATIOS . FLO PL/PO 8.8076 2.7464 1.0676 (ATIOS . EJE PL/PO 2.7096 1.3831 0.79197 1.0631	PL/PTF 0.14376 0.15933 W SPLITTER 0. PL/PTF 0.39363 0.12364 0.007711 CTOR SMMOUD PL/PTF 0.12110 0.060025 0.035394	Pt/PTP 0-33180 0-34775 0.34775 0.91/PTP 0-40F51 0-29536 0-11012 Pt/PTP 0-27949 0-13854 0-081692	0.42266 0.69200 X/DMAX 0.554.00 0.63500 0.63500 0.63500 0.62406 0.83000
62   16 67   11  >ADDIT HONAL PI  AVD WORD PL 77   29 62   9 62   9 72   36  >ADDIT HONAL PI  AVD WORD PL 107   9 117   6 122   2 127   3 137   3 142   3 142   3  AVD HORD PL	0.750 1.915 RESSURE A 4.435 .2454 .5678 RESSURE T .0554 .6468 .5528	3. 2167 3. 5652 IATIOS , FLO PL/PO 8. 8076 2. 7464 1. 0876 IATIOS , EJE PL/PO 2. 7096 1. 3831 0. 79197 1.0631	0.14376 0.15933 M SPLITTER O. PL/PTF 0.39363 0.12364 0.047711 CTOR SHIPOD PL/PTF 0.12110 0.060025 0.035394	0.33180 0.36775 .0. PL/PTP 0.40751 0.29536 0.11012 PL/PTP 0.27949 0.13656 0.081692	0.42266 0.69200 X/DMAX 0.554.00 0.63500 0.63500 0.63500 0.62406 0.83000
62   16 67   11  >ADDIT HONAL PI  AVD WORD PL 77   29 62   9 62   9 72   36  >ADDIT HONAL PI  AVD WORD PL 107   9 117   6 122   2 127   3 137   3 142   3 142   3  AVD HORD PL	0.750 1.915 RESSURE A 4.435 .2454 .5678 RESSURE T .0554 .6468 .5528	3. 2167 3. 5652 IATIOS , FLO PL/PO 8. 8076 2. 7464 1. 0876 IATIOS , EJE PL/PO 2. 7096 1. 3831 0. 79197 1.0631	0.14376 0.15933 M SPLITTER O. PL/PTF 0.39363 0.12364 0.047711 CTOR SHIPOD PL/PTF 0.12110 0.060025 0.035394	0.33180 0.36775 .0. PL/PTP 0.40751 0.29536 0.11012 PL/PTP 0.27949 0.13656 0.081692	0.42266 0.69200 X/DMAX 0.554.00 0.63500 0.63500 0.63500 0.62406 0.83000
**************************************	1.915 RESSURE R 9.435 .2454 .5678 RESSURE R .0554 .6488 .5528	3.5652 PL/PO 8.8076 2.7464 1.0676 RAYIOS . EJE PL/PO 2.7096 1.3831 0.79197 1.0631	0.15933 NV SPLITTER C. PL/PTF 0.39363 0.12364 0.067711 CTOR SHWOUD PL/PTF 0.12110 0.060025 0.035394	0.36775 0.0. PL/PIP 0.40751 0.29536 0.11012 PL/PIP 0.27949 0.13856 0.081692	X/DMAX V.554.00 0.63500 V.59200 X/DMAX 0.62408 V.83000
>ADDIT HONAL PI AVD WORD PL 77 29 62 9. 92 3.  >ADDIT HONAL PI 107 9. 112 4. 122 2. 127 3. 142 3.  >ADDIT HONAL PI  AVD WORD PE 107 9. 117 4. 120 2. 127 3. 140 3.	RESSURE R 9.435 .2454 .5678 RESSURE R .0554 .486 .6488 .5528	PL/PO 8.8076 2.7464 1.0676 (AYIOS . EJE PL/PO 2.7096 1.3431 0.79197 1.0631	PL/PTF 0.39363 0.12364 0.007711 CTOR SWOOD PL/PTF 0.12110 0.060025 0.035394	PL/PTP 0.40751 0.29536 0.11012  PL/PTP 0.27969 0.13856 0.081692	X/OMAR U.58400 0.63500 U.69200 X/9MAX 0.62406 U.83000
AVD WORD PL 77 29 62 9. 92 3.  >ADDITIONAL PI 107 9. 112 4: 122 2. 127 3. 137 3. 142 3:  >ADDITIONAL MADDITIONAL MADITIONAL MADITIONAL MAD	7.435 .2454 .5678 RESSURE 11 .0554 .7866 .6468 .9528	PL/PO 8.8076 2.7664 1.0676 (AYIOS , EJE PL/PO 2.7096 1.3931 0.79197 1.0631	PL/PTF 0.39563 0.12364 0.057711 CTOR SHIPOUD PL/PTF 0.12110 0.060025 0.035394	PL/PTP 0.40F51 0.29536 0.11012  PL/PTP 0.27949 0.13854 0.081692	U.58400 0.63500 U.69200 X/8MAX 0.62406 U.83000
77 29 62 9, 92 3, 92 3, >ABDITIONAL PI 107 9, 112 4; 122 2, 127 3, 137 3, 142 3;	7.435 .2454 .5678 RESSURE 18 .0554 .7896 .6468 .5928	8. 8076 2. 7664 1.0676 (AYIOS - EJE PL/PO 2. 7096 1. 3431 0. 79197 1.0631	0. 39363 0. 12364 0. 047711 CTOR SWOUD PLYPTF 0. 12110 0.060025 0. 035394	0.40751 0.29536 0.11012 PLYPTP 0.27949 0.13854 0.081692	U.58400 0.63500 U.69200 X/8MAX 0.62406 U.83000
82 9. 92 3. 92 3. 92 3. 93 3. 94 3. 95 3. 96 3. 97 3. 97 3. 97 3. 97 3. 97 3. 97 3. 97 3. 97 3. 97 3. 97 3. 97 3.	.2454 .5678 RESSURE N .0554 .7886 .6468 .5528	2.7664 1.0676 (AVIOS , EJE PL/PO 2.7096 1.3431 0.79197 1.0631	0.12364 0.047711 CTIR SHOUD PLAPTE 0.12110 0.060025 0.035394	0.29536 0.11012 PL/PTP 0.27949 0.13854 0.081692	0.63500 0.57200 X/BMAX 0.62406 0.83000
82 9. 92 3. >ADDITIONAL PI AVD WORD PL 107 9. 112 4: 122 2. 127 3. 137 3. 142 3:  >ADDITIONAL M	.2454 .5678 RESSURE N .0554 .7886 .6468 .5528	2.7664 1.0676 (AVIOS , EJE PL/PO 2.7096 1.3431 0.79197 1.0631	0.12364 0.047711 CTIR SHOUD PLAPTE 0.12110 0.060025 0.035394	0.29536 0.11012 PL/PTP 0.27949 0.13854 0.081692	0.63500 0.57200 X/BMAX 0.62406 0.83000
>ADDITIONAL PI 107 9. 112 4. 122 2. 127 3. 137 3. 142 3.	.0554 .7886 .6448 .5928	M.7PO 2.7096 1.3431 0.79197	PL/PTF 0.12110 0.060025 0.035394	0.11012 P[7PTP 0.27949 0.13854 0.081692	V/8MAX Q.62400 U.83000
AVD WORD PE 107 9. 117 4. 122 2. 127 3. 137 3. 142 3. 34003710001 M	.0554 .7886 .6468 .5528	7L/PO 2.7096 1.3431 0.79197 1.0631	PL/PTF 0.12110 0.060025 0.035396	0.27949 0.13854 0.081692	9.42400 9.83000
107 9. 112 6. 112 2. 127 3. 137 3. 142 3. 24001710001 91	.0554 .488 .6448 .5528	2.7096 1.3431 0.79197 1.0631	0.12110 0.060025 0.035394	0.27949 0.13854 0.081692	9.42400 9.83000
107 9. 112 6. 112 2. 127 3. 137 3. 142 3. 24001710001 91	.0554 .488 .6448 .5528	2.7096 1.3431 0.79197 1.0631	0.12110 0.060025 0.035394	0.27949 0.13854 0.081692	9.42400 9.83000
117 122 2. 127 3. 137 3. 142 3.	. 6468 . 5528 . 6629	1.3431 0.79197 1.0631	0.060025 0.035394	0.13854 0.081692	6-83006
122 2. 127 3. 137 3. 142 3. 142 3.	.6468 .5528 .6629	0.79197 1.0631	0.035394	0.081692	
127 3. 137 3. 142 3. 34001710001 PE	.5528 .6629	1.0631			
137 3. 142 3. 34001710ML M	. 6629		U_U_ (310)	0.10966	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
142 3:			0.048983	0.11305	1.2200
AND HUND ME		1.0025	0.048390	0.11166	
NO HUND ME.					
	NESSUNE-1	######################################	EDCOR-THEFT		
	-	PL/PO	PLYPTF	PT 7PTP	
	. 0554	2-7096	0-12110	0-27949	-1/1000
-112	4586	1.3431	0.060025	0.13854	
	.4468	0.79197	0.035354	0.081692	
	. 5528	1.0631	0.047510	0.10966	-1.7660
	6629	1.0960	0.048983	0-14505	-1.0000
	. 61 M	1.0825	0.048380	0211166	1,000
	. 5528	1.0631	0.047510	0.10966	-1.0000
	. 5578	1.0646	0.047577	0.10981	T. 1000 with the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the secon
SADDITERNAL PA	RESSURE P	ATTITS - PAN		·	
AVD WORD PL		PL / PA	A PTF	PLIPTO	ANALY ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND ALL AND
	.5528	1.0631	0.047510	0.10966	-1.0000
-157	.5578	1.055	0.041211	0:10981 ··	1.0000
SAPOTTTOMAL PR	RESSURE A	A ZOGS . 20	DEG SIMPLE EL	DEST TON	
		/		\	
		PL/P0	PL /PTP	OF SPAR	TOMAT
-167 3. -172 3.	.5578	1.0646	0.047577	0.10981	-1.00g
""	<b>*</b>	4. Un 70	U- (19 19 11	0.10401	_ 1º AAAA
- 24001111004 PR	<del>RESSURE R</del>	ATTITS . 80	DEG SHROUD LI	DESTION -	
AVD WORD PL		PL/P0	PE / PTP	- Pt /PTP	A STATE OF THE PROPERTY OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE
	.3526	1.0332	0.044833	0-10348	-1.0000
	.2675		0.043699		- 1.0000

	S PRELIMI	MARY DATA	06/28/79	CADDETT	REC 10/18/79 01:20:38.654 FAC 98681 PGM C034 PDG 1231
>ADDIT ION	AL PRESSURE	RATIOS . PR	MARY PLUG		
VD WORD	PL	PL/PO	PL/PTF	PL /PTP	Y/DMAX
32	16.21#	4.88BZ	0.21811	0.43690	** 0.43200 *** *** *** *** *** *** *** *** ***
37	8.9265	2.6905	0.12005	0.24048	9.53000
47	10.449	3, 1495" "	0.14053	0.28149	0.62900
52	10.674	3.2172	0. 14355	0.28755	0.72700
>ADDITION	NL PRESSURF	RATIOS . FLO	W SPLITTER I	. D.	
VD WORD	PL	PL / PO	PL /PTF	PL /PTP	K/DMAX
	12.271		0.16503	0.33057	7-10-14-2200 Minimum 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
62 67		3.6986 3.5752	0.15953	0.33057	
	11.862	3.7176	0.15753	0.31977	0.69200
>4001 T 1004	L PRESSURE	PATIOS . FLO	W SPLITTER O	. D.	n n tro wantan ga a wantan a a a cara ya na sana a sana a sana a sana a sana a sana a sana a sana a sana a san
UN WORD	PL	PL/PO	PL/PTF	PL /PTP	X/DMAX
??	29.200	8.8210	0.39359	0.78840	0.56400
12	9.1811	2.7673	0.12348	0.24733	0. 43500
2	5-2470	1.0691	0.047703	0.095553	
>AD717 <b>(</b> D10)	L PRESSURE	RATIOS ; FJI	CTOR SHROUD		· The street of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the c
יי פאלאו חו	Pt	PL/P0	PLIPTE	PETPTP	TATOMAN
107	8.7764	2.7116	0.12099	0.24236	0.62400
112	4.4614		0.080001	0.27235	0.83000
122	2.6373	0. 79492			0.96000
			0.035469	0.071048	
127	3.5370	1.0661	0:047568	0.095284	1.0900
137 142	4.1666 4.1200	1.2559 1.2458	0.056036 <del>0.05</del> 54 <del>99</del>	0-11225 	1-2200 
/8001330W	1-91-33107	211111 201	2260x 17127		
AUND	Pt-	PL/PG	PL /PTP	PL /PTP	
107	8.7764	2.7116	0.12099	0.24236	-)x 6000
iis —	4:4614	1.9647	0.060001	0.12019	1.0000 · · · · · · · · · · · · · · · · ·
155	2.6373	0.79492	0.035469	0.071048	-1.0 <del>000</del>
127	3,7370	1.0001	0.047968	0.093269	1.6000
137	4. 7666	1.2559	0.056036	0.11225	~1.0000
	4.126	1.2438	7.055499	2.11117	-1.000
147	3.5320	1.0646	0.047501	0.095149	-1.0000
					*****
152	3.5370	1.0661	0. 04 7568	0.095284	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
152 157	3.5370		0. 04 7569	0.095284	-10000
52   57 <del>  ADRITION</del>	3.5370	RATIOS FAI	<del>, nuezat el</del> ab		
152 157 <del>•ADD 1710W</del> VD WORD	3.5370 IL PRESSURE	##1105 FAI	<del>  111221E 11</del> 40   <b> </b>   11276	PL /PTP	T/OHAY
152 157 > <del>ADD ET FON</del> FD NORD 152	3.5370 NL PRESSURE PL 3.5320	#41103 FAI #4 /PR	PL /PTF Q.047501	Pt /PTP 0.095149	-1.0000
152 157 > <del>ADD 1710W</del> VD WORD 152	3.5370 IL PRESSURE	##1105 FAI	<del>  111221E 11</del> 40   <b> </b>   11276	Pt /PTP 0.095149	T/OHAY
152 157 <del>28001770</del> 4 10 41480 152 157	3.5370 ht. PRESSURE- Pt. 3.5320 3.5370	RATIOS - FAI PL /PR 1.0546 1.0541	PL /PTF Q.047501	Pt /PTP 0.095149 0.095284	-1.0000
152 157 >ABDITTOW 15 WITE 157 >ABDITTOW VD WITE	3.5370 AL PRESSURE PL 3.5320 3.5370 AL PRESSURE PL	# /PO	PL /PTF	Pt /PTP 0.095149 0.095284	7/0HAX -1.0000 →1.0000
152 157 >ADRITION VD WIRD 157 >ADRITION VD WIRD 167	3.5370 NL PRESSURE PL 3.5320 3.5370 NL PRESSURE PL 3.5320	RATIOS - FAI R. /PN 2.0646 1.0661 RATIOS - 20	PL PPTP 0.04 7501 0.04 7569 076 SHPROD 1	Pt /PTP 0.095149 0.095284	-1.0000 -1.0000
152 157 20011110W 152 157 20011110W 40 4080	3.5370 AL PRESSURE PL 3.5320 3.5370 AL PRESSURE PL	# /PO	PL /PTF	PL /PTP 0.095149 0.095284 Cartion	7/0MAX -1.0000 →1.0000
152 157 >ADDITION 152 157 >ADDITION VD WIRD 167	3.5370 ht PRESSURE Pt 3.5320 3.5370 ht PRESSURE Pt 3.5320 345370	RATIOS - FAI PL /PO 1.0646 1.0646 1.0646 1.0661	PL/PTF 0.047501 0.047501 0.047509 0.047509 PI/PTF 0.047501	PL /PTP 0.095149 0.095284 CCATION PL /PTP 0.095149 0.095284	7/0MAX -1.0000 -1.0000
VD WORD 152 157 >ADDITION VD WORD 167 172 >ADDITION	3.5370 AL PRESSURE PL 3.5320 3.5370 AL PRESSURE PL 3.5320 3.5370 AL PRESSURE	#47105 FAF # /PT 1.0646 1.0941 #47105 + 20 PL/PO 1.0646 1.0661	PL/PTF 0.047501 0.047501 0.047509 0PG SHERRID 1 0.047501 0.047501 0.047501	Pt /PTP 0.045149 0.095244 0.095244 0.045149 0.045284	T/DHAX -1.0000 -1.0000 -1.0000 -1.0000
152 157 20011110W 152 157 20011110W VD HIRD 167 172 20011110W	3.5370 HL PRESSURE PL 3.5320 3.5370 HL PRESSURE PL 3.5320 3.63370 HL PRESSURE PL	#47105 FAF 1.0646 1.0646 1.0661 #47105 FAF #47105 FAF	PL/PTF 0.047501 0.047501 0.047509 0F6 SHRNID 1 0.047501 0.047501 0.047501	PL /PTP 0.095149 0.095284 0.095284 0.095284 0.095284 0.095284	-1.0000 -1.0000 -1.0000 -1.0000
152 157 >ADDITTION VD WORD 152 157 >ADDITTION 167 172 >ADDITTION	3.5370  AL PRESSURE  PL 3.5320 3.5370  AL PRESSURE  PL 3.5320 3.5370  AL PRESSURE  PL 3.3421	#47105 PAP # /PT 1.0646 1.0941 #47105 20 PL/PO 1.0646 1.0661	PL/PTF 0.047501 0.047501 0.047509 0PG SHERRID 1 0.047501 0.047501 0.047501	Pt /PTP 0.095149 0.095284 OCATION Pt /PTP 0.095284 OCATION Pt /PTP 0.090033	-1.9000 -1.9000 -1.9000 -1.9000 -1.0000

NASA-LEWIS	PRELIM	NARY DATA	06/28/79	CADDELL	REC 10/10/79 01:21:46,718	FAC REGEL	FGH C034 RDG 12	
>ADDITIONA	L PRESSURE	PATENS . PRI	MAPY PLUG					
LVD WORD	PŁ	PL/PO	PL/PTF	PL/PTP	X/DMAX			
32	11.131	3. 3462	0.16849	0.43792	0.43200			
37	6.1525	1.8507	0.093137	0.24207	0.53000			
47	7.1935	2.1639	0.10889	0.28302	0-62900			
52	7.3536	2.2120	0.11132	0.28932	0.72700			
>ADDITIONA	L PRESSURE	RATIOS , FLO	W SPLITTER I	.D.	on a second way of the second			
AVD HOPD	PL	PL/PO	PL/PTF	PL /PTP	X/DRAX			
67	8.4894	2.5537	0.12051	0.33401	0.42200			
67	11.821	3.5558	0.17894	0.46508	0-69200			
>ADDITIONA	L PRESSURE	RATIOS . FLO	W SPLITTER O	.D.			والمهورون المالية والمساوية والمالية	
LAD MUMD	PL	PL/PO	PL/PTF	PL /PTP	X/BMAX			
77	26.439	7.9732	0.40024	1.0402	0,54400	e need an include the entropy	were a summer of the second of the second of	no the a second
82	8.1492	2.4574	0.12367	0.32141	0.63500			
92	3.5493	1.0677	0.053729	0.13964	0. 69200	<del></del>		
>ATT IT ITM	L PRESSURE	NATIOS , EJE	CTOK SHEOUS		restance the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of the contribution of 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VO WORD	<b>P</b> I	PL7PO	VC/PTF	PLIPTE	XZONAX		Living Company of the Company of the Company	and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th
107	7.9991	2.4062	0.12109	0.31472	0_62400			
112	3.9659	1.1927	0.060021	0.15600	0.83006			
122	2.3473	0.70609	0.035534	0.092354	0. 96000			
127	3.5192	1.0596	0.053274	-0.13846	1.0900	والمراجعات المحويط المداني المالويين ووج	والمعوروس والمراجع المراجع d makes they are a companion of their	
137	2.8983	0.87182	G-043874	0.11403	1.2200			
142	2.8932	0.87032	0.043798	0.11383	1:3500			
~######		******************************	CONTRACT					
		247105 - 200						
CHEN MAN	PL	PL/PO	PLIPTE		X/ORS			
WR WIRD	PL 7.9991	PL/P0 2.4062	PL/PTF 0-12109	0.31472	600هـرا-			
107 112	7.9991 3.9849	PL/P0 2.4062 1.1927	PL/PTF 0.12109 0.060021	0.31472 0.15600	-1,6000 1.0000			
107 107 112	7.9991 3.9649 2.3473	PL/P0 2.4062 1.1927 G.70609	Pt / PTF 0. 12109 0.060021 0. 035534	0.31472 0.15600 0.092354	-1.0000 -1.0000 -1.0000			
107 -107 -112 -127	PL 7.9991 3.9649 2.3473 3.5192	PL/PD 2.4062 1.1927 C. 70609 1.0586	PL / PTF 0.12109 0.060021 0.035534 0.053274	0.31472 0.15600 0.092354 0.13858	-1.0000 -1.0000 -1.0000 -1.0000			
107 -107 -112 -127 -127	PL 7.9991 3.9649 2.3473 3.5192 2.4983	7L/P0 2.4062 1.1927 G.70609 1.0586 0.87182	PL/PTF 0.12109 0.060021 0.035534 0.053274 0.043874	0.31472 0.19600 0.092354 0.13850 0.11403	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
107 -107 -112 -127 -127 -137	PL 7.9991 3.9849 2.3473 2.5192 2.8983 2.8982	7L/PD 2.4062 1.1927 G. 70609 1.0586 0.87182 0.87032	PL/PTF 0-12109 0-060021 0-035534 0-053274 0-043874 0-043798	0.31472 0.15600 0.092354 0.13858 0.11403	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
VB W/R7 -107 -112 -127 -137 -147 -152	PL 7.9991 3.9649 2.3473 3.5192 2.4983	7L/P0 2.4062 1.1927 G.70609 1.0586 0.87182	PL/PTF 0.12109 0.060021 0.035534 0.053274 0.043874	0.31472 0.19600 0.092354 0.13850 0.11403	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
VR WIRT 107 112 127 127 127 147 152	7.9991 3.7649 2.3473 3.5192 2.4983 2.8932 3.5343 3.5393	R/P0 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0646	0.12109 0.060021 0.035534 0.053274 0.043874 0.043798 0.053502 0.053578	0.31472 0.19600 0.092354 0.13838 0.11403 0.11383 0.13905	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
VIN WINTO 1107 1112 127 127 127 127 127 127 147 152 157 >ADDITTIONS	PL 7.9991 3.9649 2.3473 3.5192 2.893 2.8932 3.5343 3.5393 L PRESSURE	7./F0 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646	PL/PTF 0.12109 0.060021 0.035534 0.053274 0.043774 0.043798 0.053502 0.053578	0.31472 0.15600 0.092354 0.13831 0.11403 0.13831 0.13835 0.13905	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
VIR WIRTS 1107 1112 127 127 127 127 127 127 127 157 7800TT 1378	PL 7.9991 3.9649 2.3473 3.5192 2.0983 2.0982 3.5343 3.5393 L PRESSURE	PL/PD 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 RATIOS . FAR	PL/PTF 0.12109 0.060021 0.035534 0.053274 0.043874 0.043797 0.053502 0.053578	0.31472 0.19600 0.092354 0.13851 0.1383 0.1383 0.13905 0.13925	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
VIN WORD -107 -112 -127 -127 -147 -152 -157 -> MOUTT TONE -152	PL 7.9991 3.9649 2.3473 3.9192 2.8932 3.5343 3.5393 L PRESSURE PL 3.5343	R/PD 2.4062 1.1927 G.70609 1.0386 0.87182 0.87032 1.0631 1.0646 RATIOS . FAN	PL/PTF 0.12109 0.060021 0.035534 0.053274 0.043874 0.043798 0.053502 0.053578	0.31472 0.19600 0.092354 0.1383 0.1103 0.1383 0.13905 0.13925	-1,6000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
VB WORD 107 112 127 127 147 147 152 157 >BOOTT WAR	PL 7.9991 3.9649 2.3473 3.5192 2.0983 2.0982 3.5343 3.5393 L PRESSURE	PL/PD 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 RATIOS . FAR	PL/PTF 0.12109 0.060021 0.035534 0.053274 0.043874 0.043797 0.053502 0.053578	0.31472 0.19600 0.092354 0.13851 0.1383 0.1383 0.13905 0.13925	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
Vin Winty 1107 1112 127 127 127 147 147 152 157 VADOTT TONA VID WINTY 152 157	PL 7.9991 3.9649 2.3473 3.5192 2.8932 3.5343 3.5343 3.5393 L PRESSURE PL 3.5343 3.4393	7L/F0 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 RATIOS . FAN	PL/PTF 0.12109 0.060021 0.035534 0.053274 0.043874 0.043798 0.053502 0.053578	0.31472 0.15600 0.092354 0.13831 0.11403 0.13905 0.13925 PL/PTP 0.13905 0.13929	-1,6000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
WIN WORD -107 -112 -127 -137 -147 -152 -157 -2001T 1010	PL 7.9991 3.9849 2.3473 3.5192 2.8932 3.5343 3.5393 1. PRESSURE PL 3.5343 PL PRESSURE PL	7L/PO 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 RATIOS . FAR PL/PO 1.0631 1.0646	PL/PTF 0.053502 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578	0.31472 0.19600 0.092354 0.1383 0.1383 0.13905 0.13925 0.13925 0.13925 0.13925	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
VA WIND	PL 7.9991 3.9649 2.3473 3.5192 2.0932 3.5343 3.5393 L PRESSURE PL 3.5343 3.1993 L PRESSURE PL 3.5343	PL/PD 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 PATIOS . FAR PL/PD 1.0631 1.0694 PL/PD 1.0631	PL/PTF 0.12109 0.060021 0.035534 0.053574 0.043798 0.053502 0.053578 I NOZZLZ PLAP PL/PTF 0.053502 0.053502 0.053502 0.053502 0.053502	0.31472 0.15600 0.092354 0.13831 0.13935 0.13905 0.13925 PL/PTP 0.13905 0.13929	-1.6000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
VB WORD -117 -112 -127 -137 -147 -152 -157 -2800171048	PL 7.9991 3.9849 2.3473 3.5192 2.8932 3.5343 3.5393 1. PRESSURE PL 3.5343 PL PRESSURE PL	7L/PO 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 RATIOS . FAR PL/PO 1.0631 1.0646	PL/PTF 0.053502 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578 0.053578	0.31472 0.19600 0.092354 0.1383 0.1383 0.13905 0.13925 0.13925 0.13925 0.13925	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000			
VIR WIRD	PL 7.9991 3.9849 2.3473 3.5192 2.8932 3.5343 3.5393 L PRESSURE PL 3.5343 3.1993 L PRESSURE PL 3.5345 3.9393	PL/PD 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 RRTIUS . FAN PL/PD 1.0631 1.0631 1.0645	PL/PTF 0.12109 0.060021 0.035534 0.053574 0.043798 0.053502 0.053578 I NOZZLZ PLAP PL/PTF 0.053502 0.053502 0.053502 0.053502 0.053502	0.31472 0.19600 0.092354 0.1383 0.1103 0.13905 0.13925 0.13925 0.13925 0.13925 0.13925	-1.6000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
VIR WIRD	PL 7.9991 3.9849 2.3473 3.5192 2.8932 3.5343 3.5393 L PRESSURE PL 3.5343 3.4393 L PRESSURE PL 3.5345 3.7393 L PRESSURE	PL/PD 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 RRTIUS . FAN PL/PD 1.0631 1.0631 1.0645	PL/PTF 0.053502 0.053502 0.053502 0.053502 0.053502 0.053502 0.053502 0.053502 0.053502 0.053502 0.053502 0.053502	0.31472 0.19600 0.092354 0.1383 0.1103 0.13905 0.13925 0.13925 0.13925 0.13925 0.13925	-1.6000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
VA WIND	PL 7.9991 3.9649 2.3473 3.5192 2.9693 2.9692 3.5343 3.5393 L PRESSURE PL 3.5345 3.9393 L PRESSURE PL 3.5345 3.9393 L PRESSURE PL 3.5345	PL/PO 2.4062 1.1927 G.70609 1.0586 0.87182 0.87032 1.0631 1.0646 PATIOS . FAN PL/PO 1.0631 1.0645 PATIOS . 80	PL/PTF 0.12109 0.060021 0.035534 0.053574 0.043798 0.053502 0.053578 PL/PTF 0.053502 0.053578 PL/PTF 0.053502 0.053578 PL/PTF 0.053502 0.053578	0.31472 0.19600 0.092354 0.13850 0.13850 0.13850 0.13905 0.13905 0.13905 0.13905 0.13905	-1.6000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

NASA-LEWI	PRELIMI	MARY DATA	06/28/79	CADRETT	REC 10/18/79 01:22:21.681	FAC RYSKI	PG# C034	RW 17 RDG 1233
NOTE COA	L PRESSURE	PATIOS . PPI	MARY PLUG					
VD WOPT	PL	PL/PO	PL/PTF	PL /PTP	#/DMAX			
32	12.600	3.8012	0.19046	0.43798	0.43200			
37	6.9564	2.0986	0.10515	0.24190	0.53000			
47	8.1465	2.4576	0.12314	0.28317	0.62900	•		
52	8.3065	2.5059	0.12556	0.28873	0.72700			
>ADDIT ENN	L PRESSURE	RATIOS , FLO	M SPLITTEP I	.n.				
VD WORP	PL	PL / PD	- 40TE	DI 4878	K/DHAX	-		
			PL/PTF	PL/PTP				
62	9.6763	2.9192	0.14626	0.33635	0.42200			
67	11.781	3.5540	0.17807	0.40949	0.69200			
>ADDIT TON	IL PRESSURE	RATIOS . FLO	W SPLITTER P	.D.	The two transferances is the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance to the same transferance transferance to the same transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance transferance tr			
AD MUND	PC	PL/PD	PL / PTF	PL/PTP	x/DMAX			
77	26.494	7.9808	J. 39987	0.91955	0.56400			
62	8.1715	2.4652	0.12352	0.28404	0.63500			
97	3.5346	1.0863	0.053427	0-12286	0-69200			
>ADDITIONA	IL PRESSURE	RATIOS , FJE	CTTR SHROUD	to a contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration of the contration 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second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
YD WORD	Pt	- PL / PO	PL/PTF	PE /PTP	X/OHEX			
107	8.0065	2.4154	0.12102	0.27830	0.62400			
112	3.9700	1.1977	0.060009	0.13799	0.83000			
122	2-3484	0.70849	0.035498	0.081631	0.96000			
	3.5146 ·	1.0605	0.055124	··· 0:12217	1.0900			
137	3.2443	0, 97876	0.049040	0.11277	1.2200			
142	5.2143	0.96970-	0.048586	0.11173	1.3500			
AL AURU	PL	#41803 + POR PL/PO		PL/PTP	X/OHAX	in a second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco		entragency with the research of the second of
	· •		0.12102	0.27930	-1-6000	•		
107	8.0065	2.4154			Z 0000			
107			0.06000A	0.13799	71-0000°			
107	8.0065 9.9750 2.3484	1.1977	0.05000A	0.13799	-1.0000			de la <u>la persona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona de la companiona del l</u>
	3.9750	1.1977						
107 112 122	9.9750	1.1977	0.035498	0.081631	<b>/-1.0000</b>			
107 112 122 127	9.9750 2.3484 3.7146	1.1977 0.70848 1.0603	0.035498 0.053124	0.081631 0.12217 0.13277	-1.0000 -1.0000 -1.0000			
107 112 122 127 117	9.9750 2.3484 3.7146 3.2443	1.1977 0.70848 1.0609 0.97876	0.035498 0.035124 0.049040	0.081631	-1.0000 -1.0000 -1.0000			
107 112 122 127 137 147	9.9750 2.3484 3.7146 3.2443 5.2143	1.1977 0.70848 1.0603 0.97876 0.96970	0.035498 0.033124 0.049040 0.048586	0.081631 0.12217 0.13277 0.11173	-1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 147 152	9.9750 2.3484 3.7148 3.2643 9.2149 3.5296 3.7246	1.1977 0.70848 1.0603 0.97876 0.96970 1.0648	0.035498 0.053124 0.049040 0.048586 0.053351	0.081631 0.12217 0.13277 0.1173 0.12269	-1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 152 157	9.9750 2.3484 3.7146 3.2443 3.2143 3.5296 3.5296 3.5246	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0699	0.035498 0.093124 0.049040 0.048586 0.053351 0.053276	0.081631 0.12217 0.1277 0.1173 0.12269 0.12251	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 152 157 >annit Inni	9.9750 2.3484 3.9146 3.2443 3.2149 3.5296 3.5246 L. PRESTURE	1.1977 0.70848 1.0603 0.97876 0.96970 1.0648 1.0633	0.035498 0.093124 0.049040 0.048586 0.053351 0.053276 WN2218 PLAP	0.081631 0-12217 0-12277 0.12269 0-12251 Pt/PTP	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 147 152	9.9750 2.3484 3.7146 3.2443 3.2143 3.5296 3.5296 3.5246	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0699	0.035498 0.093124 0.049040 0.048586 0.053351 0.053276	0.081631 0.12217 0.1277 0.1173 0.12269 0.12251	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 155 157 PARTY T TOWN VD WORD 152 157	9.9750 2.3484 3.7148 3.2443 3.2149 3.5296 3.5296 3.5246 Pt. 3.5296 3.5246	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0693 RATIOS FAN	0.035498 0.093124 0.049040 0.048586 0.053351 0.053276 mmzzip Flap FL/PTF 0.053351 0.053276	0.081631 0.12217 0.12277 0.12179 0.12269 0.12251 Pt/PTP 0.12269 0.12251	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 152 157 240917 INMED 152 157	9.9750 2.3484 3.7140 3.2443 9.2149 3.5296 3.7246 L PRESSURE PL 3.5296 3.5246	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0699 PL/PO 1.0648 1.0633	0.035498 0.093124 0.049040 0.048586 0.053351 0.053276 WWZZIR PLAP 0.053351 0.053276	0.061631 0-12217 0-13277 0-11173 0-12269 0-12251 Pt/PTP 0-12269 0-12251	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 142 152 157 >ADDIT INNI VD WORD 152 157 >ADDIT INNI	9.9750 2.3484 3.7196 3.2443 5.2149 3.5296 3.5246 1. PRESSURE PL	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0639 RATIOS FAN PL/PO	0.035498 0.053124 0.049040 0.048586 0.053351 0.053276 WM2219 PLAP PL/PTP 0.053351 0.053276	0.081631 0-12217 0.12277 0.1173 0.12269 0-12251 Pt/PTP 0.12269 0.12251	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 152 157 >ADD TT INNA VD WORD 152 157 >ADD TT INNA VD WORD 152 157 >ADD TT INNA VD WORD 166 167	9.9750 2.3484 3.9146 3.2443 3.2245 3.5246 3.5246 1. PRESSURE PL 3.5296 3.5246	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0693 RATIOS FAN PL/PO 1.0648 1.0633	0.035498 0.053124 0.049040 0.048586 0.053351 0.053276 MIZZIS PLAP 0.053351 0.053276 DPG SHRITOS II	0.081631 0-12217 0-12277 0.12179 0.12269 0-12251 Pt/PTP 0.12269 0-12251 BCATION	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 142 152 157 >ADDIT INNI VD WORD 152 157 >ADDIT INNI	9.9750 2.3484 3.7196 3.2443 5.2149 3.5296 3.5246 1. PRESSURE PL	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0639 RATIOS FAN PL/PO	0.035498 0.053124 0.049040 0.048586 0.053351 0.053276 WM2219 PLAP PL/PTP 0.053351 0.053276	0.081631 0-12217 0.12277 0.1173 0.12269 0-12251 Pt/PTP 0.12269 0.12251	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 142 152 157 VD WORD 152 157 VARD11 AN	9.9750 2.3484 3.7146 3.2463 9.2149 3.5296 3.5246 1. PRESSURE PL 3.5256 1. PRESSURE PL 3.5256 3.5256	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0693 RATIOS FAN PL/PO 1.0648 1.0633	0.035498 0.093124 0.049040 0.048586 0.053351 0.053276 WWZZIR PLAP VL/PTP 0.053351 - 0.053276 PL/PTP 0.053276	0.061631 0-12217 0-13277 0-13277 0-1173 0-12269 0-12251 Pt/PTP 0-12251 0-12251 0-12251 0-12251	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 152 157 240717 JAN 167 167	9.9750 2.3484 3.9146 3.2443 3.2245 3.5246 3.5246 1. PRESSURE Pt. 3.5256 3.5256 3.5256 3.5256 3.5256	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0693 RATIOS FAN PL/PO 1.0648 1.0633 1.0633	0.035498 0.093124 0.049040 0.048586 0.053351 0.053276 0.053351 0.053276 0.053276 0.053276 0.053276	0.081631 0-12217 0.12277 0.12179 0.12269 0-12251 Pt/PTP 0.12269 0.12251 DCATION	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 157 157  ADDITIONS 152 157  ADDITIONS 167 172  ADDITIONS VO MOF	9.9750 2.3484 3.5146 3.2443 5.2149 3.5296 3.5246 1. PRESSURE PL 3.5256 3.5256 1. PRESSURE PL 3.5256 3.5246	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0699 PL/PO 1.0648 1.0633 PL/PO 1.0633 1.0633	0.035498 0.093124 0.049040 0.049586 0.053351 0.053276 MM2218 PLAP ML/PYP 0.053351 - 9.053276 DPG SHRMUR 11 PL/PYF 0.053276 DPG SHRMUR 11	0.061631 0-12217 0-13277 0.12173 0.12269 0-12251 Pt/PTP 0.12269 0-12251 BCATION Pt/PTP	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
107 112 122 127 137 147 152 157 240717 JAN 167 167	9.9750 2.3484 3.9146 3.2443 3.2245 3.5246 3.5246 1. PRESSURE Pt. 3.5256 3.5256 3.5256 3.5256 3.5256	1.1977 0.70848 1.0609 0.97876 0.96970 1.0648 1.0699 PL/PO 1.0648 1.0633 1.0633 1.0633 Whites + 80	0.035498 0.093124 0.049040 0.048586 0.053351 0.053276 0.053351 0.053276 0.053276 0.053276 0.053276	0.081631 0-12217 0.12277 0.12179 0.12269 0-12251 Pt/PTP 0.12269 0.12251 DCATION	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

VASA-LEWI	S PRFLIM	INARY DATA	06/28/79	CADDETT	REC 10/18/79 01:23	: 10-191 (	FAC BY6X1	PGM CO34	NOG 1234	
>ADD IT ION	AL PRESSURE	RATIOS , PR	IMARY PLUG							
UN WORD	PL	PL / PO	PL /PTF	PL /PTP	X/DMAX					
37	14.507	4.3736	0.21882	0.43755	0.43200	- · · · · · · · ·			•	
37	8.3015	2.4124	9.12070	0.24134	0.53000					
47	9.3609	2.5222	0.14120	0.28234	0.62900	•		* *		
52	9.5508	2.8795	0.14407	0.29807	0.72700					
AUU TIUUV	AL PRESSURE	RATIOS . FLO	DW SPLITTER E	. D.						
VD WIRD	PL	PL/PN	PL/PTF	PL/PTP	X/DMAX					
62	10.940	7.2983	0. 16502	0.32997	0.42200					
67	11.764	J. 5468	0-17746	0.35483	0-69200					
>ADDIT ION	AL PRESSURE		OW SPLITTER O							
										-
VD WORD	PL	PL/PN	PL/PTF	PL/PTP	X/DMAX					-
77	25.458	7.9857	0.39955	0.79891	0.56400				· · ·	
82 <del>92</del>	8.1915 3.5413	2.4666	0.12341 0.053419	0.24677 0.10681	0.63500 0.69200					
-		_		0-100-1	900 76 <b>00</b>					
		WATTOS . EJI		the thirty country and an employed belongs and the thirty country and the second		To addition the title colors to appear to a			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	•
VI) 41780 "	PL	PC/PU	PC/PTF	PLABAR	KYOMAX			35		
107	8.0265	2-4199	0.12107	0.24209	0.62400			3.50		
112	3. 9765	1.1989	0.059982	0.11994	0.83000			D SI		
155	2.3555	0-71017	0.035532	0.071 047	0.96000			\$\frac{1}{2}		
127	3.5313	1.0646	0.053267		1.0900			7		
137	3.7214	1.1219	0.056134	0.11224	1-2200			00		
147	3.6813	1.1099	0.055530	0.11104	1.3500			10		
		*******						7.40		
	rf	-KE-1506	******				S	(A)		
<b>บาวแกลอ</b> -	PE	PL/PO	PL/PTF	PE /PTP	X COMPA			73		
107	8.0265	2.4199	0.12107	0.24209	-140000		Č	<b>&gt;</b>		
112	3.9762	1,1989	0. 059982	0.11994	1.0000			2		
122	2.3555	0.71017	0.035532	0.071047	-1.0000					
127	4. 5313	1.0646	0.053267	0.10651	-1.0000					
137	3.7214	1.1219	0.056134	0. 12224	-1.0000					
142	3.6819	1.1099	0.055530	9:11104	-1.0000					
152	3.5313	1.0646	0-053267	0.10651	-1.0000					
157	3.5313	1.0646	0.053267	0.10651	-1.0000		v = = =============================			+
7400TT10W	IL PRESSURE	RATIOS - FAI	NOZZIZ FLAP		···					
VD WOPD	PL	PL/PD***	XPL/PTF	PE /PTP	X/DPAX					
152	3.5313	1-0646	0.053267	0.10651	-1.0000					
157	3.9313**	1.0848	0.093267	0.10851	-1.0000					
>¤DVIT INW	IL PRESSURE	#47265 + 20	DEC SHRIDO (1	TCATTON -						<del></del>
AU NUMB	PL -	PL/P0	PE /PTF	ET INTE	X/DMXX					
167	3.5368	1.0661	0.053342	g#10000	-1.0000					
	3,9513	1.0646	0.053267	0-19651	-1.0000					
172	. /	PATTOS . 80	DEG SIMBUD 11	DCATTON -					<del></del>	
	K-bus 220ms				`					
> <del>270111100</del>		· m /pn····		- 91 7979	* ************************************					
<del>SANDITION</del> VO NORD	PL	PL/PD	PL / PTF	P[ 7PTP	X/MAX			and above 1 cm. A		
-172 -> <del>2001TTN</del> -182 -182 -187		PL/PO 1.0088 0.99319	0.050475 0.049192	Pt /PTP 0.10093 0.098361	1.0000 -1.0000	مستاه د مستخدی		minute for a second		

NASA-LEWI	S PRELIMI	NAPY DATA	06/28/79	CADDELL	REC 10/18/79 01:24:38.484	FAC BROWL	PGM C034	ROW 17 ROG 1235
>ADDIT ION	AL PRESSURE	RATIOS , PRI	IMARY PLUG					
VD WOPD	PL	PL/PO	PL / PTF	PL/PTP	x/DMAX			
32	11.257	3.3684	0.16882	0.43676	0.43200			
37	6.2370	1.8663	0.093537	0.24199	0.53000			
47	7.2874	2.1806	0.10929	0.28274	0.62900			
52	7.4424	2.2269	0.11161	0.28876	0. 72 700			
	ME LKE230ME		OW SPLITTER I.	•		· · · · · · · · · · · · · · · · · · ·		
VD WORD	PL	PL/PO	PL/PTF	PL /PTP	X/DMAX			
62	8,5725	2. 5651	0.12856	0.33260	0.42200			· · · · · · · · · · · · · · · · · · ·
67	11.727	3.5090	0.17587	0.45499	0.69200		- <del></del>	
>ADDITION	AL PRESSURE	RATIOS . FIG	W SPLITTER O	. D.		The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa		and to again agree the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of
OROW OY	PL	PL/PD	PL/PTF	PL /PTP	X/DMAX		-	
77	26. 677	7.9824	0.40008	1.0350	0:56400		fray is the state market continue.	
82	8.2425	2.4664	0.12361	0.31980	0.63500			
95	3.7692	1.0658	0.073468	0.23033	0-69200	<del></del>		
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107	6.0825	2.4105	0.12121	0.31359	0.62400			
12	3.9978	1.1998	0.059923	0.19903	O. #3000			
. 22	2.3690	0.70885	0.035528	0.091913	0.96000			
27	3.9392	1.0578	0: 05301 n	0.13726	1.0900			
137	2.9446	0.88110	0-644161	0.11425	1.2200			
142		0.87661	0.043939	0.11367	1.3900			
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39 1.9 19 1.9		.31	10.84	2.60	0.000								0.9741		
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47 1.0		.31		12.66									0.9814		
43 1.9		1.72	29.24		0.000								0.4964		
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52 j.g		• 72	27.39		0.070	0.150	0,661	0.989	J. 9425	0.9844	0.9972	1.0017	1.0027	1.4917	
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14 1.0		.50	24.79		0.020	0.159	0.961	0.989	1.0044	0.9889	0.9916	1.0070	1.0075	1.4978	, , , , , , , , , , , , , , , , , , , ,
40 1.00		.43	_	10.65									1.0061		
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77 1.9		32	72.37	_	0.020								1.0048		

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12	14.526	4.3545	0.71559	0.43730	0.43200	· · · · ·	-
37	8.0097	7.4767	9.12107	0.24139	3.53000		
47	9.3636	?.P133	0.14155	0.28188	J.62700		
77	9.5796	7.8779	0.14480	0.28835	2.72700		~
>4001T104	AL PRESSUPE	PATINS , FIC	W SPIJITEP J	• D•			
VD 40P0	PL	PE / PO	PI /PTF	PL/PTP	X/DMAX		
45	10.993	3.3729	0.16619	0.33004	0.42200		
67	11.349	3.4796	0.17155	0.34167	0.69200		
>4221TION	AT PRESSURE	RATIOS . FLO	M SULITIES D	. D.	mer	e e e e e e e e e e e e e e e e e e e	
O SUP UN	PL	PI /PN	PI /PTF	PL /PTP	KIDMAK		
77	26.612	7.9956	0.40229	0.P0113	0.56400	-	
-7	8.1537	2. 449F	0.12326	0.24546	0.63500		
, 7	3.5467	1.0656	0.052614	0-10-77	3. f 9203		
NOT TICK	AL PPESSURE	PATINS . FJF	CTO SHADING		••		•
AU HUBD	PĹ	PI / PN	PL /PTF	PL /PTP	XZPHAX		a more on a grown a single
.07	6.8095	2.0456	0.10297	0.20494	0.62400		
17	3.9170	1.1749	0.059212	0. 117°7	3. 83022		
27	2.2704	).69615	0.034623	0.068550	0.96900		and the same and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of t
127	3.5766	1.05%	0.343311	7.13617	1.0900		
42	3.6467	1.0957	0.055127	0.10978 0.10858	1.2200 1.3500		
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117	6.4085	2.0456	7.10292	0.20408	-16000	a naka kabupatan sa sa sa sa sa sa sa sa sa sa sa sa sa	
27	3.9170 2.2934	1.1749 3.68815	0.059212 0.034623	7.11792 0.068950	1.0000		
79	5.5266	1.0596	0.057311	0.10/17	-1.0000 -1.0000		
37	3. 1467	1.0957	0.055127	0.110.78	-1.0000		
47	3.6364	1.0436	0.054522	8.10F5B	-1.0000		
52	3.5316	1.0611	0.057387	0.10632	-1.0000		
57	3.5417	1.0641	0.053538	0.10662	-1.0000	· · · · · · · · · · · · · · · · · · ·	
ANTIT TOW	AT PRESSURE	HAT PRITTER	HITTLE FLAP	<del></del>			
	a	PI /PI	PI JOYF	PE /PTP	KIDHAK	e e e	
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÷.	12.675	3.7091	0.19011	0.43774	0.43200			
17	A.7369	2.0973	0.10495	0.24143	0.53000			
47	9.1768	2.4569	0.12254	0.24262	9.62400			
<u> </u>	P. 1669	2.5779	7.12540	C+28879	2.32799	essere superior and provide a superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the superior of the	ditahunggananan di mula bundan kanyan dipa mendi	Martin Statement Statement and a ring to consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and consultation and
MOLTECOA	AL PRESSIPE	PATENS , FLC	M SPLITTEP I	•n•				
NU MUED	Pt	PI /PO	PL/PTF	ol \646	X/DMAX			
62	0.6364	7.8894	0.14484	0.73241	0.42200			
F. 7	11-131	3.3962	0.16095		3.65200	en a spekkenskakenenska i renku ako makka d	M. Marana — rain	Millionia opi, ammerika angalika dina angapapanganak angalika antagapa
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ያስ ቁቦቃስ	Pi	PL/PO	Pt /PTF	PI /PTP	X/DMAY			
7.7	76.791	9.0774	0.41165	0.92495	0.5/400			
* ?	8.2114	2.4614	0.12317	0.24335	7.63500			······································
7	3.5507	1.0673	0. 057408	0.12284	0.69200			
MOT TECOD	AL PRESSIPE I	PATINS . FUE	CTTP SHPTID			~		
n wash	PL	PL / PIT	PI /PTF	PL /PTP	Y/DMAX			
97	6.8569	2.0583	0.10300	0.27694	0.62400			
12	3.9510	1.1343	0.059261	FE 1 . 0	Q-63000			
.22	2.3147	0.69382	9.034719	0.079870	0. 96300			and the same
27	3.5357	1.0598	0.053037	0.12200	1.0990			
37 42	3,3196	0.99231	0.049655 0.047554	0.11423 0.10940	1.2700 1.3500	* - · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · ·	=7 -100 + <del>=</del> -1
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nany trubb	Pl	PL ZPN	PL/PTF	ni /ete	Y /(may			
יייי	6.8669	7.0583	0.13700	0.23494	-1,2000	•		
12	2.9510	1.1843	145270.0	0.13633	20000			
	2.3147	3.69382	0.074719	0.079870	-1.0000			
.22	5357	1.0598	0.053077	0.12200	-1.0000			
2? 27 21	3.34.76	3.99231	0.049655	0.13423	-1.0000			* 15
7? 27 27 27 42	3.3176 3.1735	9. 99231 9. 95032	0.049655	0.13423	-1.0000 -1.0000			- 0
7? 77 71 47	3.31.76 3.1735 3.5457	9. 99231 9. 95032 1. 0628	0.049655 0.047554 0.057187	0.13423 0.13940 1.12235	-1.0000 -1.0000 -1.0000			
77 77 77 47 63	3.54.76 3.54.76 3.54.67 3.54.67 3.65.17	3.99231 3.99032 1.0628 1.0643	0.049655 0.6475*4 0.05*18? 0.05*25?	0.13/23 0.13/40 0.12234 0.12252	-1.0000 -1.0000		-	
77 77 77 47 63	3.54.76 3.54.76 3.54.67 3.54.67 3.65.17	3.99231 3.99032 1.0628 1.0643	0.049655 0.047554 0.057187	0.13/23 0.13/40 0.12234 0.12252	-1.0000 -1.0000 -1.0000		-	
27 27 27 47 63 63 67	3.54.76 3.54.76 3.54.67 3.54.67 3.65.17	3.99231 3.99032 1.0628 1.0643	0.049655 0.647554 0.052187 0.052257 HATTIE FLAR	0.11423 0.7940 0.12235 0.12252	-1.0000 -1.0000 -1.0000		-	
22 27 27 27 42 63 63 67 67 600 [1 ] [14]	3.5167 3.5106 3.177 3.5457 3.5517	3.90231 3.96032 1.0628 1.0643	0.049655 0.047554 0.052187 0.053257	0.11973 0.75940 7.12235 0.12252	-1.0000 -1.0000 -1.0000 -1.0000		-	
22 27 27 27 42 63 63 67 60 67 60 67	5357 3.3106 3.1775 3.5467 3.5567 71 PRESSURE	3.99231 3.95032 1.0628 1.0643	0.049655 0.647554 0.052187 0.052257 HATTIE FLAR	0.11423 0.7940 0.12235 0.12252	-1.0000 -1.0000 -1.0000 -1.0000			
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27   27   27   42   63   67   67   67   68   68   68   68   68   68   68   68	53-57 3-31-75 3-17-75 3-54-57 3-55-37 PI 3-64-57 3-55-97	0.99231 0.99332 1.0628 1.0643 PATIOS FAR PLOFE 1.0628	0.049655 0.047564 0.057187 0.057187 0.057187 0.057187	0.11473 0.10940 0.12235 0.12252 PI/PTP 0.12252 PTATYON	-1.0000 -1.0000 -1.0000 -1.0000		-	
22 27 27 42 63 67 200111040 00 WORD 67 20 WORD 67	5357 3.3176 3.1775 3.5467 3.5667 7.6667 7.6597	0.99231 0.95032 1.0628 1.0643 PAYIOS FAR PAYIOS FAR 1.0628 1.0628 PAYIOS - 20	0.049655 0.047564 0.057187 0.057187 0.057187 0.057187 0.057187 0.057187 0.057187	0.11473 0.10940 6.12235 0.12252 PI /PTP 0.12252 PEATYON	-1.0000 -1.0000 -1.0000 -1.0000 */OMAY -1.0000 */OMAX -1.0000		-	- · · · · · · · · · · · · · · · · · · ·
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72 77 77 42 63 67 60 60 60 60 60 60 60 60 60 60 60 60 60	5157 3.7106 3.1715 3.5467 3.5517 PI 3.6657 3.6537 EI POPTSTIRET I	0.99231 0.99032 1.0628 1.0643 PATIOS FAR 1.0643 PATIOS FAR 1.0628 1.963 PATIOS FAR 1.9643 1.1643 1.1643	0.049655 0.047564 0.057187 0.057187 0.057187 0.057187 0.057187 0.057187 0.057187	0.11473 0.10940 0.12235 0.12252 PL/PTP 0.12252 PTATYON PL/PTP 0.12252 C.12252	-1.0000 -1.0000 -1.0000 -1.0000 */OMAY -1.0000 */OMAX -1.0000			
122 27 27 42 53 54 57 60 60 60 60 60 60 60 60 60 60 60 60 60	5357 3.5106 3.1775 3.5467 3.5467 7.5507 2.6507 2.6507 2.6507	0.99231 0.99032 1.0628 1.0643 PATIOS FAR 1.0643 PATIOS FAR 1.0628 1.963 PATIOS FAR 1.9643 1.1643 1.1643	0.049655 0.647544 0.053187 0.053257 0.053187 0.053187 0.053187 0.053187 0.053257 0.053257	0.11473 0.10940 0.12235 0.12252 PL/PTP 0.12252 PTATYON PL/PTP 0.12252 C.12252	-1.0000 -1.0000 -1.0000 -1.0000 */DMAY -1.0000 */DMAX -1.0000			
122 27 27 42 42 63 63 67 67 70 Urph	5357 3.3106 3.1775 3.5447 3.5447 7.4447 7.4447 7.45307 2.45307	0.99231 0.95332 1.0628 1.0643 PAYIOS FAR PAYIOS FAR 1.0628 1.0628 1.3633 PAYIOS FAR 1.3643 1.3643 1.3643	0.049655 0.047564 0.057187 0.057257 HATTIE FLAD 0.057187 0.057187 0.057187 0.057257 0.057257	0.11473 0.10940 0.12235 0.12252 PI /PTP 0.12252 PTATYON 1/PTP 0.12252 C.12252	-1.0000 -1.0000 -1.0000 -1.0000 */DMAX -1.0000 -1.0000 */OMAX -1.0000 -1.0000			

AVC 2-1 EMIZ	DD F [ 14]	INAPY DATE	76/11/79	CADUELL	REC 10/18/79 04:15:51.579	EAC AXEXI	P64 L034	RDG 1250
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AND MERCO	PĮ	PL /P I	DI ADTE	Pt /PTP	¥.\U~¥.			
3 7	11.241	3, 3533	0.16536	0.43642	0.43200			
37	9. 21.10	1. 9549	0. 397518	0.24142	0.53999			
47	7.2728	7.16.96						
			0.1993#	O. 20277	9.62970			
.,	7.432A	2.2173	0.11179	G. 26854	J. 72700	makakan makan ugu sak mapu sa manusi. Sa mapagaba		
>VOOTT 1044	PPFSSHRE	PATINS . FEE	M ZDETAALD I	• n•				
AU MUSU	PI	PL/PO	PI /PYF	PI /PTP	X/DMAX			
67	8.5573	2,5528	9.17879	0.33224	J. 42200			
17	11.776	3. 36 37	0.16959	0.4377P	0.69200			
APOLTIOUS<	PRESSURE	PATIOS . FLO	M SPETTER O	. D.				
ለስ ሐሳቤቱ	PI	Pf / PO	PL / PTF	PI /PTP	W/DMAX			
77	76.723	7.9719	0.40191	1.0375	0.56400			
97	A.1775	2.4395	0.12259	0.31749	0.63500			
<del>- c2</del>	3.5675	1.7641	0.053656	0.13651	0.69200	· · · · · · · · · · · · · · · · · · ·		
APOT TICOAK	L PRESSURE	PATINS EJE	PTEP SHADUM	v =				
מארי מעו	PL	P( / P()	PI /PTF	PI /PTP	X/OMAY			~ • •
107	6.4379	2.9399	0.19284	0.26548	0.62409			
117	1.9127	1.1732	0.050149	0.15269	0.02700	· · · · · · · · · · · · · · · · · · ·		····
127	2.2918							
	7.2918	በ. ሉዋ?ሉዓ	0. 034469	0.048980	0.96000			
			* A * S # S = -					
127	3.4375	[. )552	0.053204	0.17735	1.0900			
127 137	3.4375 3.0023	(.)552 0.99563	0.045154	0.11656	1.2200			
127	3.4375	[. )552						* * *
127 137 147	3.5375 3.0323 5.9672	(.)552 0.99563	0.045154	0.11656	1.2200			
127 137 147 SASSIYIMU	3.4375 3.0323 5.9672	(.)552 0.97563 0.85513	0.045154 0.043127	0.11656 ñ.11132	1.2200	-		
127 137 147 <b>545513300</b> <b>50</b> HIBD	3.4375 3.0323 5.4672 BARCOIDE	(.)552 0.57563 0.65512 PARINE . EM	0.045154 0.043122 ERFAY INTE	0.11656 ñ.11132	E-2200 L-3500			
127 137 147 54551710M	5.4375 3.0323 5.4672 Entreme	[.)454 0.97563 0.85543 BANIOS , EM PL/PG 2.0399	0.045154 0.043122 PL/PTF 0.10284	0.11656 f. 11132 Pt /PTP 0.26548	E-2200 L-3500 X/DHAX -1-3000			
127 137 147 SASSIXIAMI No. 40 Ph 10	9.4375 3.0323 5.4672 E 885550FF PL 6.8379 3.9327	[.)55% 0.57563 0.655% PATION FOR PI / Pri 2.0399 1.1737	0.045154 0.043122 ERFOY INTE PLYPTE 0.10284 0.059146	0.11656 0.11132 Pt /PTP 0.2654P 0.15269	E.2200 1.3500 X/DMAX -1.3000 -1.0000			
127 137 147 <b>SANTYINM</b> <b>DQ</b> MCPN 107 112 122	9.4375 3.0123 5.4672 PL 6.8379 3.9327 2.2318	[.)55% 0.87563 0.855% PATINE EM PL/PN 2.0399 1.1737 0.68369	0.045154 0.043122 EBCDV INLEY PL /PTF 0.10284 0.059146 0.034469	0.11656 0.11132 P1 /PTP 0.2654F 0.15269 0.088980	X/DNAX -1.3500 -1.0000	•		
127 137 147 <b>SANTITION</b> <b>SOLUTION</b> 100 HI PRI 112 112 127	9.4775 3.0123 2.4672 1. MAFECURE PL 6.4379 3.9327 2.2314 3.5375	1.)55% 0.97563 0.855% BATTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS FOR PLANTOS F	0.045154 0.043122 EBCOV INTE PL/PYF 0.10284 0.059146 0.434469 0.553204	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0889P0 0.13735	X/DMAX -1.3040 -1.0000 -1.0000	•		
127 137 147 SANSTYIMU: Vo. HC P.D. 107 112 127 127	5.4775 3.0123 2.4672 1.4672 1.667379 3.9327 2.2318 3.5375 3.0223	1.)55% 0.97563 0.855% PATION FOR PI /PG 2.0399 1.1737 0.68369 1.055% 0.89563	0.045154 0.045122 ERFOY INLEX PL/PYF 0.10284 0.059146 0.034469 0.053704 0.045154	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.098989 0.13735 0.11656	X/DNAX -1.3500 -1.0000 -1.0000 -1.0000			
127 137 147 SASSITIONE Vo. ur. Ph 110 112 122 127 127 147	9.4375 3.0123 2.4672 PL 6.4379 3.9327 2.2314 3.5375 1.0223 2.8022	1.)55% 0.87563 0.87563 0.855%  ANTICE FOR PI / Pri 2.0399 1.1737 0.68369 1.055% 0.89563 0.89563	0.045154 0.045122 EBCDY INLEX PL /PTF 0.10284 0.055146 0.035469 0.053274 0.045154 0.043122	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0886P0 C.13735 0.11656 0.11656	1.2200 1.3500 X/DMAX -1.3000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147 SASSITIONE Vo. ur. Ph 110 112 122 127 127 147	9.4775 3.0123 2.4672 1.8672 1.668379 3.9327 2.2318 3.5375 1.0233 2.87827 3.5575	1.)55% 0.97563 0.855% PATION FOR PI /PG 2.0399 1.1737 0.68369 1.055% 0.89563	0.045154 0.045122 ERFOY INLEX PL/PYF 0.10284 0.059146 0.034469 0.053704 0.045154	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.098989 0.13735 0.11656	X/DNAX -1.3500 -1.0000 -1.0000 -1.0000			
127 137 147 SEASTY INSE 100 112 127 127 127 147 147	9.4375 3.0123 2.4672 PL 6.4379 3.9327 2.2314 3.5375 1.0223 2.8022	1.)55% 0.87563 0.87563 0.855%  ANTICE FOR PI / Pri 2.0399 1.1737 0.68369 1.055% 0.89563 0.89563	0.045154 0.045122 EBCDY INLEX PL /PTF 0.10284 0.055146 0.035469 0.053274 0.045154 0.043122	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0886P0 C.13735 0.11656 0.11656	1.2200 1.3500 X/DMAX -1.3000 -1.0000 -1.0000 -1.0000 -1.0000	• • • • • • • • • • • • • • • • • • • •		
127 137 147 SANSTY INME 100 112 127 127 127 127 127 127 127	9.4775 3.0123 2.4672 PL 6.4379 3.9327 2.2314 3.5375 3.5575	1.)55% 0.80563 0.855% BANIOS FOR Pi / Pri 2.0399 1.1737 0.68369 1.055% 0.89563 0.8557% 1.0613 1.0613	0.045154 0.045122 ERCOVILLEY PL /PTF 0.10284 0.059146 0.034469 0.253204 0.045152 0.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0886P0 C.13735 0.11656 0.11656 0.11656 0.11656 0.11656	1.2200 1.3500 X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147 SANTYIMU: No. 4: Ph 10 112 127 127 127 142 142 142 147	9.4775 3.0123 2.4672 PL 6.4379 3.9327 2.2314 3.5375 3.5575	1.)55% 0.80563 0.855% BANIOS FOR Pi / Pri 2.0399 1.1737 0.68369 1.055% 0.89563 0.8557% 1.0613 1.0613	0.045154 0.045122 ERCOV INLEX PL/PTF 0.10284 0.059146 0.053204 0.045154 0.045154 0.053505 0.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0886P0 C.13735 0.11656 0.11656 0.11656 0.11656 0.11656	1.2200 1.3500 X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147 SARRITINUI 100 W. P.D. 110 112 122 127 137 147 147 147 147 147 147 147 147 147 14	9.4475 3.0123 2.4672 PL 6.4379 3.9327 2.2314 3.5475 3.5575 1 PDF 55186F	1.)55% 0.97563 0.855% PATION FOR PI / PG 2.0399 1.1737 0.68369 1.055% 0.89563 0.855% 1.0613 1.0613	0.045154 0.043122 PL/PTF 0.10284 0.059146 0.034469 0.053704 0.045154 0.045154 0.053505 0.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0989990 0.13735 0.1165 0.14632 0.13812 0.13812	E.2200 i.3500 X/DMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147 SKASTYIMU  NO W. P.D. 110 112 127 127 127 147 147 147 147 147 147 147 147 147 14	9.4775 3.0123 5.4672 1.4672 1.4672 1.667377 2.2314 3.5375 1.4023 2.4023 2.4023 1.5575 1.5575	1.)55% 0.97563 0.855% PATION FOR PI / PG 2.0399 1.1737 0.66369 1.055% 0.89563 0.955% 1.0613 1.0613	0.045154 0.043122 ERCOV INTER 0.10284 0.059146 0.034469 0.539704 0.045154 0.045154 0.053505 0.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0PR9P0 0.13735 0.1165 0.1452 0.13812 0.13812	1.2200 1.3500 X/DMAK -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147 147 100 w: Pf 110 127 127 127 127 127 147 147 147 147 147 147 147 147 147 14	9.4775 3.0123 5.4672 1.4672 1.667379 3.0327 2.2318 3.5575 1.6575 1.5575 1.5575 1.5575	1.)55% 0.97563 0.95573  DATION FOR  Pi / Pri 2.0399 1.1737 0.69369 1.055% 0.89563 0.9557% 1.0613 1.0613 PAYTON FAR  Pi / Pri 1.7613 1.7617	0.045154 0.043122 ERECY INTE 0.10284 0.059146 0.059146 0.053206 0.045154 0.043122 0.053505 0.057505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.098989 0.13735 0.1165 0.14132 0.13812 0.13812	1.2200 1.3500 X/DMAX -1.3300 -1.0300 -1.0300 -1.0300 -1.0300 -1.0300 -1.0300			
127 137 147  No with the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the prope	9.4775 3.0123 5.4672 1.4672 1.667379 3.0327 2.2318 3.5575 1.6575 1.5575 1.5575 1.5575	1.)55% 0.97563 0.95573  DATION FOR  Pi / Pri 2.0399 1.1737 0.69369 1.055% 0.89563 0.9557% 1.0613 1.0613 PAYTON FAR  Pi / Pri 1.7613 1.7617	0.045154 0.043122 ERCOV INLEY PL/PTF 0.10284 0.059146 0.053204 0.043132 0.053505 0.053505 0.053505 0.053505 0.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0886P0 0.11656 0.11656 0.11657 0.117812 0.13812 0.13812 0.13812 0.13812	1.2200 1.3500 X/DMAX -1.3000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	•		
127 137 147  SASSITION 107 112 127 127 127 127 127 127 127 127 12	9. 4475 3.0123 2.4672 PL 6. 4379 3.0327 2.2314 3.5375 3.5575 7 PRESSIBE	1.)55% 0.97563 0.955% PATION FOR PI / Pri 2.0399 1.1737 0.68369 1.055% 0.89563 0.855% 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613	0.045154 0.043122 EBCDV INLEY PL/PYF 0.10284 0.053146 0.053146 0.053505 0.053505 0.053505 0.053505 PL/PYF VAP 0.053505 N.053505 N.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0889P0 C.13737 0.11656 0.14132 0.13812 0.13812 0.13812 0.13812 0.13812	1.2200 1.3500 X/DMAX -1.3000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147  SANTITION 107 112 127 137 147 147 147 147 147 147 147 147 147 14	9.4775 3.0123 2.4672 PL 6.4379 3.9327 2.2314 3.5375 3.5575 1.6575 1.7575 1.7575	1.)55% 0.97563 0.97563 0.97563 0.97563 2.0399 1.1737 0.64369 1.0553 0.95533 1.0613 1.0613 1.0613 1.0613 1.0613	0.045154 0.043122 ERCOV INLEY PL/PTF 0.10284 0.059146 0.053204 0.043132 0.053505 0.053505 0.053505 0.053505 0.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.0886P0 0.11656 0.11656 0.11657 0.117812 0.13812 0.13812 0.13812 0.13812	1.2200 1.3500 X/DMAX -1.3000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147  NO W. P.D. 110 127 127 127 127 127 127 127 127 127 127	9. 4475 3.0123 2.4672 PL 6. 4379 3.0327 2.2314 3.5475 10233 2. 4672 3.5575 1 PRESSIBE	1.)55% 0.97563 0.97563 0.97563 0.97563 0.97563 0.1737 0.64369 1.0553 0.95533 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613	0.045154 0.043122 ERCOV INLEY PL/PTF 0.10284 0.059146 0.053204 0.043122 0.053505 0.053505 0.053505 PL/YTE TAP 0.053505 N.053505 N.053505 N.053505 N.053505	0.11656 0.11132 PI /PTP 0.2654P 0.15269 0.0PRGPO C.13735 0.11655 0.11632 0.13812 0.13812 0.13812 0.13812 0.13812	X/DMAX -1.JJJO -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147  500 W. P.D 110 112 112 112 117 147 147 147 147 147 147 147 147 147	9. 4475 3.0123 2.4672 PL 6. 4379 3.0327 2.2314 3.5475 10233 2. 4672 3.5575 1 PRESSIBE	1.)55% 0.97563 0.95573  PATION FOR  PI / PG 2.0399 1.1737 0.69369 1.0553 0.89563 0.95573 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613	0.045154 0.043122  ERECY INTER 0.10284 0.059146 0.03469 0.053704 0.043127 0.053505 0.053505 0.053505 0.053505 0.053505 0.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.098990 0.13737 0.1165 0.14132 0.13812 0.13812 0.13812 0.13812 0.13812 0.13812 0.13812	X/DMAX -1.33-00 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147  SANSTYIMM 100 W. P.D. 110 110 111 117 117 117 117 117 117 117	9. 4379 3.0123 2.4672 PL 6.4379 3.9327 7.2314 3.5375 3.5575 PDECCUPE PL 3.5575 PDECCUPE PL 3.5575 PDECCUPE PL 3.5575 PDECCUPE PL 3.5575 PDECCUPE	[.)55% 0.97563 0.95573  PATION FOR  Pi / Pri 2.0399 1.1737 0.69369 1.0553 0.95533 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613	0.045154 0.043122 ERECY INTER PL/PTF 0.10284 0.059146 0.059146 0.053705 0.043122 0.053505 0.052505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.053505 PL/YYLE TAP 0.0	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.098989 0.13737 0.1165 0.1165 0.1167 0.1167 0.11812 0.13812 0.13812 0.13812 0.13812 0.13812 0.13812 0.13812	X/DMAX -1.33-00 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 147  500 W. P.D 110 112 112 112 117 147 147 147 147 147 147 147 147 147	9. 4475 3.0123 2.4672 PL 6. 4379 3.0327 2.2314 3.5475 10233 2. 4672 3.5575 1 PRESSIBE	1.)55% 0.97563 0.95573  PATION FOR  PI / PG 2.0399 1.1737 0.69369 1.0553 0.89563 0.95573 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613 1.0613	0.045154 0.043122  ERECY INTER 0.10284 0.059146 0.03469 0.053704 0.043127 0.053505 0.053505 0.053505 0.053505 0.053505 0.053505	0.11656 0.11132 P1 /PTP 0.2654P 0.15269 0.098990 0.13737 0.1165 0.14132 0.13812 0.13812 0.13812 0.13812 0.13812 0.13812 0.13812	X/DMAX -1.33-00 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

RUN 20

MAKA-LEWI	S PRELIM	INVEA DVIV	06/11/79	CADDELL	PEC 10/18/79	04:20:56.299	FAC 9X6X1	PG4 C034	Run 20 PPG 1251
POLITICAN	AL PPESSUPE	PATINS PEI	MARY PLUG	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	··· <del>- 11  </del>				
מיירה פיאי	PL	PL / PO	PL/PTF	PI /PTP	X/DMAX				
37	16.293	4. 86 74	7. 21493	0.43642	0.43290				
~ 7	0.0730	2.6472	0.11454	0.24060	0.53000				
47	19.512	3.1475	0.13507	0.29171	J-62900				
		2.2047	2.142.93	9.24747	<u>3-7270⊋</u>				
SADDITION	At porssiper	PATIOS , FEC	M COLITIED I	. n.					
TO WOPD	Pl	Pt / PO	bl /bit	Pt /PTP	X/DMAX				
€2	12.336	3. 5854	0.16475	0.33059	J.42200				
<u>^7</u>	11. 752	3, 3615	0,14981	0. 30153	0. 69200				
POTTICAL	AL PRESSIME	RATIOSFLO	W SPLITTER O	• n•					
ማየነት ሁለት	PL	PL/PO	PI /PTF	PL /PTP	X/DMAX				
77	30.145	9,0058	0.47137	0.83784	0.56400				
87	9.7779	2.7717	0.12353	0.24863	0.63500				
C 7	7.5773	1.0697	2.067630	0.005#45	J.69200				
NOT TECOM	AL PRESSURE	PATINS . EJF	CYDR SHPRUD		<b>4</b>				
No Aust	PL	PI / PN	PL / PTF	PL /PTP	X /OMAX				
107	7.7483	2.3148	0.10316	0.20764	0.62400				
117	4.4728	1.3362	7.050553	0.11986	0.03000				
1 77	2.6716	J. 78319	0.034905	0.070254	3.96000				
127	3.5473	1.0657	0.047497	0.095597	1.0900	=	· ·		•
137	4.1126	1.2286	0.054757	0.11021	1.2200				
147	4.0676	1.2137	0. 054001	9.10887	1.3500		· • • • • • • • • • • • • • • • • • • •		· ·
>1021 1 10H	M ORCECHOE	***	COCON INFER			······································			
MAUF MAN	Pt	Pt /PT	PL /PTF	PI /PTP	x / Digit		•		
-111	7.7483	2.314P	J.10°16	0.20764	-140000				
-112	4.4778	1. 3362	0. (55551	0.11996	<b>/-1.0030</b>			•	
-127	2.6216	0. 79319	J. 07490E	0.070255	-1.0000				
-177	2.5673	1.0457	0.047467	0.095557	-1.0000				
-137	e-1158	1.2296	0.054757	0.34621	-1.0000				
-147	4.00	1.7137	7, 9549°1	10847	-1-0000				
-152	3.5723	1.9672	J. 247563	C.095731	-1.0000				
-157	3.5573	1.0657	0.047492	0.095597	-1.0000				
2×001110M	AL PPESSIPE	DATING FAR	HOTTHE FLAN						
WB ACED	PI	M YED	OI / 17 F	01 /PTP	x/n#Ax		-		- *
-157	3.5723	1.0577	2.247563	0.095731	-1.0000				and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
-157	3.5673	1.30	3. ~47407	0.095597	-1.0000				
\$255T <b>TT</b> 40	at burzellbr	महास्रोते र जा	तहर दक्किका ।	neatiny					
IAU AUBU	PL /	M /PI	M /PTF	Q JPTP	x/DMAY				· •
-1 + 7	3.578	1.74.72	0.047563	0266231	-1.0000				
-177	3/177	1.0667	j. 34763 j	C-ODERE	-1.0000				
ע <b>קון דו</b> רייגיד	AL UNECCIDE	PATTOR . NO	THE SHEET !	PERTINA -			-		
	Pt	PI / Pሾ	P( /PTF	PI /PTP	HIOMAY				
ነላስ ፈጥኮለ			-1 / 1 17	/- IF	~ runger				
1VD (101)			9.042200	1.007150	-1 0000				
1VN - 10 N -10 - 10 N	3.2571 3.2571	7.97155 7.95959	0.0433 <b>0</b> 0 0.042767	7.087150 6.086077	-1.0000 -1.00c0				

	5 <u>PRELIMI</u>	HAPY DATA	0//11/79	CADDETT	PEC 16/18/	79 74:21:35.966	FAC 98681	PGM C034 PDG 1252	
วงี้มวโป ได้สั	11 PRESSURE	PATINS , PET	LANKA BERR						
AVC HOED	PL	Pt / PO	PLOTE	PL/PTP	X/{MAX				
37	14,200	4. 22 83	). 1 APPR	0.47779	0.43200				
77	7.9378	2.3374	0.19417	0.24150	J. 5300J				
47	9.1773	2.7211	0.12200	0.28277	0.62900				•
57	9. 36.22	2.7861	0.12445	0.28947	J. 72799				<del></del>
SAPOLT TOM	of bordellor	PATIOS, , FLO	TH SPLITTER I	•P•					
AVO HOPO	PĮ	nd \letu	PI /PTF	PL /PTP	x/DMAX				
62	10.771	1.2056	0.14319	0.33189	0.42200				
<u>67</u>	11.231	3.3427	2.14930	0.34605	0.69200				·
>600111046	TE PPESSUPE	PATTINS , FLO	W SPLITTEP D	•,D•					
IVO SHED	Pŧ	PL /PI	PI /PTF	PL /PTP	X/DMAX				
77	30.152	R. 0729	J.40082	0.92905	0.56400	•	**		
P2	9.2723	2.7653	9.12357	0.28632	0.63500				
c 7	1.5076	1.0676	0.0476#9	0.11053	0.69200	<u></u>			***************************************
NOTT COAC	it perssiler	PATIOS . FJF	CTCP SHEDUO	nomical and reduced forms		** *			
VO WORL	PE	PL/PG	PL/PTF	PL /PTP	X / DHA X			• · · · · · · · · · · · · · · · · · · ·	
107	7.767F	2.3116	2.19376	0.23934	0.62400				
112	4.4778	1.3725	0. (55524	0.13757	0. A3000			<del> </del>	
127	2.6169	0.77872	0.034785	0.040/28	0.96000				
127	1.5674	1.0616	0. 347427	0.10992	1.0900			er v van aktiv v	
1 * 7	3.7274	1.1092	0.049550	U. 11485	1.2200				
1	3.5624	1.0601	0.047?55	0.10976	1.3500				
ZESSTYTOW	T. WESTINE	TTIES - KO	FARM INCH			<u> </u>			
_				- 61 / PTP	X/OHAY	••	A 10		
เสียงสัย	ři	m /65	D1 701E						
100 4000	PÎ	PI /PO	P) /P1#				•		
107	7.7679	2.3116	0.10326	0.23934	-1-0000				
117	7.7679 4.4779	2.3116	0.10326 0.050524	0.23934	-1-0000				
-107 -112 -122	7.7679 4.4779 2.6169	2.3116 1.3428 0.77872	0.10326 0.050524 0.034785	0.23934 0.13767 0.080628	-1.0000 1.0000 -1.0000				
-107 -112 -177	7.7679 4.4779 2.6169	2.3116 1.3425 0.77672 1.0616	0.10326 0.050524 0.634785 0.047422	0.23934 0.13767 0.080628 0.10992	-1.0000 -1.0000 -1.0000				
107 112 122 127 127 142	7.7679 4.4779 2.6169	2.3116 1.3428 0.77872	0.10326 0.050524 0.034785	0.23934 0.13747 0.080678 0.10997	-1.0000 -1.0000 -1.0000 -1.0000				
-107 -112 -122 -127 -127 -147	7.7678 4.4779 2.6169 2.5674 2.2276 3.5686	2.3116 1.3425 0.77672 1.0616 1.1092	0.10326 0.050524 0.054745 0.047422 0.049550	0.23934 0.13767 0.080628 0.10992	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 127 147	7.7678 4.4779 7.6169 1.5674 2.276	2.3116 [.2+28 0.77672 [.0616 1.1092 [.060]	0.10226 0.050524 0.050524 0.034745 0.047422 0.049550 0.047355	0.23934 0.13767 0.080678 0.1099 0.11465 0.10976	-1.0000 -1.0000 -1.0000 -1.0000				
107 112 122 127 127 147 147 152	7.7678 4.4779 7.6169 3.5674 7.276 3.5774 3.5774 2.5774	2.3116 1.3427 0.77672 1.0616 1.1092 1.0646 1.0646	0.10326 0.084554 0.034745 0.047425 0.049550 0.047355 0.047555	0.23934 0.13767 0.080628 0.1099 0.11465 0.11073 0.11023	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
-107 -112 -127 -127 -142 -157 -157 -2701*1000	7.7679 4.4779 7.6169 1.5674 1.276 3.5674 3.5776 2.5776	2.3116 1.3128 0.77872 1.0616 1.1092 1.0646 1.0646	0.10326 0.04554 0.034745 0.047425 0.049550 0.049555 0.047555 0.047555	0.23934 0.13767 0.080678 0.1099 0.11485 0.10976 0.11073 0.11073	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000				
-107 -112 -127 -127 -127 -127 -157 -157 -157 -2377***********************************	7.7679 4.4779 2.6169 1.5674 1.5674 1.5774 3.5774 2.5774	2.3116 1.3128 0.77672 1.07.16 1.1092 1.0801 1.0646 1.0646	0.10226 0.086524 0.034785 0.047422 0.049550 0.047555 0.047555 0.047555	0.23934 0.13727 0.040628 0.1099 0.11465 0.11023 0.11023	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000				
107 112 127 127 127 142 157 157 7 Annivimia	7.7679 4.6779 2.6169 1.5674 2.5674 3.5774 3.5774 2.5774	2.3116 [.3428 0.77672 1.0616 1.1092 1.0646 1.0646 PAYION . FAP	0.10326 0.04554 0.034745 0.047425 0.049550 0.049555 0.047555 0.047555	0.23934 0.13767 0.000078 0.1099 0.11465 0.1093 0.11023	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 127 127 147 147 157 157 5 Anni Yimia Vin unen 157	7.7679 4.4779 2.6169 3.5674 3.5774 3.5774 2.5774 [[	2.3116 1.3128 0.77672 1.07.16 1.1092 1.0646 1.0646 PAYION . FAP M /PM 1.0646 1.0646	0.10224 0.084524 0.034745 0.047422 0.04955 0.047555 0.047555 0.047555 FERRYLL FLAR	0. 23934 0. 13767 0. 000628 0. 1099 0. 11465 0. 1099 0. 11023 0. 11023	-1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000 -1,0000				
107 112 127 127 147 157 157 157 157 157 157 157 157 157 15	7.7679 4.6179 4.6179 2.6169 4.5674 3.5674 3.5774 3.5774 [[ nneccipe	2.3116 [.3428 0.77072 [.0616 1.1092 [.0646 [.0646 ].0646 PAYIO FAP M./PO [.0646 [.0646]	0.10224 0.04524 0.047427 0.047427 0.049550 0.047555 0.047555 F MOTTLE FLAT	0.23934 0.13767 0.000028 0.1099 0.11465 0.11023 0.11023 0.11023 0.11023	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
107 112 127 127 147 157 157 157 157 157 157 157 157 157 15	7.7678 4.4779 2.6169 2.5674 3.5674 3.5774 3.5774 2.5774 11	2.3116 1.3128 0.77672 1.07616 1.1092 1.0646 1.0646 PAYION FAP M /PF 1.0646 1.0646 1.0646 1.0646 1.0646	0.10324 0.040524 0.0407427 0.040755 0.040755 0.047555 0.047555 0.047555 0.047555 0.047555	0. 23934 0. 13767 0. 000678 0. 1099 0. 11073 0. 11023 0. 11023 0. 11023 0. 11023 0. 11023	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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VD WOPD	PL.	PL / PO	PI /PTF	PL /PTP	×/DMA×			
3.7	15.467	4.6569	0.18734	0.43777	0.43200			
77	A.5367	2,5622	0.10397	0.24085	0.53000			
47	9.74/1	2.5957	7.12051	0.28161	0.62900			
53	10-176	3. 2652	2,12339	0.20012	2.72799	en un e de de su la comitación de la companión de la companión de la companión de la companión de la companión		
>ADDITION	INT PRESSURE	PATIOS , FLO	W SPLITTEP I	.n.				
AU AUBU	Pl	PI /PI	Pt / PTF	PL /PTP	#/DMAX			
47	11.495	3.5725	0.14170	0.33112	0.42270			•
47	11.130	3, 3524	0,13486	0.31514	0.69200			
>40017.104	ML PRESSUPE	PATINS, FLO	W SPLITTER O	• D ₂	- · · · ·			
VD WORD	PL .	PL /PO	PI /PTF	PI /PTP	X/DMAX			
77	32.777	9. 4721	0.39713	0.97831	0.56400			
82 97	10-161	3.0604	0.12311	0.28769	0.63500			
97	3.5413	1.0666	0.042907	0.10026	0.69200			
MULTICOR	AL PRESSUPE	PATIOS . FJE	CTCR SHPOUD		and the second of the second	e <del>ndang</del> e .	· •	
ORON ON	PL	PL/PD	PI /PTF	PL /PTP	X/DHAX			• • · · · · · · · · · · · · · · · · · ·
[1)7	R.491A	2.5577	0.10789	0.24043	0.62400			
117	4.9019	1.4764	0.059393	0.13879	0.83000			
123	2.8458	9.85714	0.034401	0.080574	0. 96000			
127	7.5263	1.0621	0.042775	0.099840	1.0900			
127 142	4.0415	1.2173	0.048969	0.11443	1.2200			
_	3.8664	1.1645	0.046847	0.13947	1.3500			
<del>&gt;409                                    </del>	AI POF SCHIEF	PATIOS - FOO	ENLUA IMEX					
_			PL / PTF	PI /PTP	X/DMAX	•	• • • • • •	
•	PL	PL/PN						
127	A.4018	2. 55 77	0.10289	0.24043	-1-9000			
127	A.4918 4.9019	2.5577 1.4764	0.17289 0.059393	0.13879	-16 V0000		. a., y amend	
127 112 122	4.9018 4.9019 2.8459	2.5577 1.4764 0.85714	0.17289 0.059393 0.034481	0.13F79 0.080574	-1.0000 -1.0000			
127 112 127	8.4018 4.9019 2.8459	2. 55 77 1. 4764 0. 85714 1. 0621	0.17289 0.059393 0.034481 0.742725	0.13F79 0.080574 0.09848	-1.0000 -1.0000 -1.0000			
197 112 127 127 137	8.4018 4.9019 2.8458 5263 4.7415	2. 55 77 1. 4764 0. 85714 1. 0621 1. 2173	0.17289 0.059393 0.034481 0.742725 7.048969	0.13F79 0.080574 0.059848 0.1343	-1.0000 -1.0000 -1.0000			
197 112 127 127 137	8.4018 4.9019 2.8459 5263 4.7415 3.866	2. 55 77 1. 4764 0. 85714 1. 0621 1. 2173 1. 1645	0.10289 0.059393 0.034481 0.042725 0.048969 0.046847	0.13P79 0.080574 0.139848 0.1343 0.1047	-1.0000 -1.0000 -1.0000 -1.0000			
197 112 127 127 137 147 157	8.4018 4.9019 2.8458 5263 4.7415	2. 55 77 1. 4764 0. 85714 1. 0621 1. 2173 1. 1645 1. 0621	0.17289 0.059393 0.034481 0.742725 7.048969	0.13P79 0.080574 0.059848 0.11443 0.40647 10.059840	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
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197 112 122 127 137 142 152 152 153 167	#.4918 4.9019 2.8459 5263 4.7415 3.5263 3.5363 AL PARESSIRE	2.5577 1.4764 0.85714 1.0621 1.2173 1.1645 1.0621 1.2651	0.17289 0.050393 0.034481 0.047725 0.046847 0.046847 0.042775 0.042775	0.13P79 0.080574 0.099849 0.11543 0.20647 0.099840 0.13012	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.3500			
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197 112 127 127 137 147 157 157 157 157 157 157 158 177 177 177	PL 3.5263 3.5363 AI PRESSIRE	2.5577 1.4764 0.85714 1.0621 1.2173 1.1645 1.0621 1.2651 PAYING FAR 91 / PR 1.0621 1.0651 1.0651 1.0651	0.17289 0.050393 0.034481 0.742725 7.048847 0.042725 7.042847 1.07711 FLAB 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725	0.13P79 0.080574 0.080574 0.1547 0.11547 0.069840 0.13012  PI /PTP 0.099840 0.10012 0.0012 0.0012	1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000			
197 112 127 127 137 147 157 157 157 157 157 2407111000 152 157 25507111000 167 177	P. 4918 4.9019 2.8459 2.8459 4.7415 3.8763 3.5363 AL PRESSIRE PL 3.5263 3.5363 AL PRESSIRE PL 3.5263 3.5363 AL PRESSIRE	2.5577 1.4764 0.85714 1.0621 1.2173 1.1645 1.0621 1.2651 PAYINS FAR PLANT 1.7621 1.0651 PAYINS - 20 PLANT 1.0651 1.0651 1.0651	0.10289 0.050393 0.034481 0.042725 0.046847 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725	0.13P79 0.080574 0.080574 0.1547 0.11447 0.1059840 0.13012 PL/PTP 0.099840 0.10012 0.10012 0.09840	1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000			
107 112 127 127 137 147 157 157 VO WORD 152 157 VO WORD 167 167 177 VO WOD 167	PL STATE PER STATE PL 3.5263 AL PRESSIRE PL 3.5263 AL PRESSIRE PL 3.5263 AL PRESSIRE PL 3.5263 AL PRESSIRE PL 3.5363 AL PRESSIRE PL 3.5363 AL PRESSIRE PL 3.5363 AL PRESSIRE PL 3.5363 AL PRESSIRE PL 3.5363 AL PRESSIRE PL 3.5363 AL PRESSIRE PL 3.5363 AL PRESSIRE PL 3.5363	2.5577 1.4764 0.85714 1.0621 1.2173 1.1645 1.0651 1.0651 1.0651 1.0651 1.0651 1.0651 1.0651 1.0651	0.17289 0.050393 0.034481 0.742725 7.048847 0.042725 7.042847 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042726 PI / PTF 0.042786 PI / PTF 0.042786 PI / PTF 0.042786 PI / PTF 0.042786	0.13P79 0.080574 0.080574 0.199749 0.11343 0.1647 0.099840 0.13012 PI /PTP 0.099840 0.10012 0.09082	1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
Vn WARA 152 157	P. 4918 4.9019 2.8459 2.8459 4.7415 3.8763 3.5363 AL PRESSIRE PL 3.5263 3.5363 AL PRESSIRE PL 3.5263 3.5363 AL PRESSIRE	2.5577 1.4764 0.85714 1.0621 1.2173 1.1645 1.0621 1.2651 PAYINS FAR PLANT 1.7621 1.0651 PAYINS - 20 PLANT 1.0651 1.0651 1.0651	0.10289 0.050393 0.034481 0.042725 0.046847 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725 0.042725	0.13P79 0.080574 0.080574 0.1547 0.11447 0.1059840 0.13012 PL/PTP 0.099840 0.10012 0.10012 0.09840	1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000   1.0000			

SASA -1 FWI	Հ Իսենքակ	INARY DATA	06/11/79	CADDELL	PEC 10/18/79	94:24:37.625	FAC AVGVI	PGM C034	RDG 1256	
SADST TON	AL PRESSUPE	PATIOS , PPI	MARY PLUG				ayan ayyandan ayang ii kisa Mari yu Akhari u ii ii gaba			<b>.</b>
AVD STOPD	PI	PI / PO	<b>ሚ/</b> ፆ <b>ኛ</b> ፑ	PL /PTP	X/DMAX					
32	14.714	4.2171	0.15891	0.43663	0.43700					
2.7	7.7393	2.3261	0.003171	0.24084	0.53900					
47	0.0342	2.7196	0.10000	3.28147	0.62900					
5.9	9.2399	2.7922	0.11136	U. 28786	0. 72700					
> ADD 1 T 10W			W SPLITTEP I			etracultura (tr. 1800), matematika (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800), eta (1800),	ellum enger till der i der Serte en elle til en till der ett beste till der ett beste till der ett beste forst	transfermine a committee committee and	**************************************	
WAD MUND	PI	of \bu	M /ble	PI /PTP	XAMMAX					
€2	10.623	3. 1967	9.12404	0.33097	0.42200					
47	11.137	3.3515	0.13424	0.74790	J. 6920 ¹ 3					
SATOLL LUA	AL PPESSIME	PATINS . FLO	W SPLITTER O	. n.	y de Nager	-				
AVD WYPD	PI	PL / PG	PL /PTF	PL /PTP	X/DMAX					
77	37.471	9. 8917	0.39620	1.3242	0.56400	•				
47	10.203	3.0704	0.12298	0.31790	0.63500					
77	1,8539	1.0695	0.042797	0.11063	0.49200	**************************************			<del></del>	
>Annit Inh	AL PRESSURE	RATTOS . EJE	CTOR SHROUD							
AVO WORD		31.480			L'ANDAGE					
-	PL	P[ /P/]	PI / PTF	PI /PTP	Y/IMAY					
107	A. 5595	2.5757	0.10717	0.26668	0.62400					
112	4.0308	1.4838	0.059432	0.15363	0.000 A.O					
122	2. 97:34 3.52 <b>47</b>	J. 86378	0.03459R	0.089433	0.96000					
127		1.0609	0.042495	0.10985	1.0900					
137 142	3.7357	1.1242 1.0855	0.045027	0.11639	1.2200					
-				0.11137	טוירניו					
<del></del>	At PAFSCHAE	******	tucon Infer	<del></del>						
AVO PUCETS	PI	PL /PO	PL /PTF	PI /PTP	X/DHAX		• -			
-107	8.5595	2.5757	0.19317	0.26668	-1,0000					
-117''' 🥆	4,0334"	1. 4938	0. 059472	0.15763	1.3003					
-127	2.8704	0.8637R	0.074598	0.089433	/-i.0030					
-177	375,22	7.08.70	0.042495	0.10985	-1.0000					
-117	1.7767	1.1242	0.045027	0.13039	-1.0000					
-147	مردن ه. د مردن د	1.0305	9.047279	0,4711A7	-1.0030					
-152	3.5757	1.0540	0.042616	<b>70.11016</b>	-1-0000					
-1 = 7	3.5757	1.7640	0.042616	0.11016	-1.0000			•		
22 <b>2414</b> 444	VI beteriet	RATTINS FAR	NOTTIFFE A							
evo wren	Pį	P( /P()	MIPTE	PL /#T9	x/DMAX					
-152	3.5357	1.0540	9.042616	0.11916	-1.0000					
-157	3.5357	1. 2542	0. 4. 7616	0.11016	-1.0000				1 w 10 m	
Zinalaluis.	AT PPFSSIPF	PATES - 20	ार्टा सम्बद्धाः इ.स.च्या	PCATTON			<del></del>			
ልሃስ ሠበድማ	rt /	PH 707	P[ /PTF	PLATE	x/OHÀX "					
-1+7	5492	1.3455	0.742676	0.1031	~1.J000					
-177 -177	5/17	1.0655	5.647676	0.110	-1.0000					
	אר וישר אדי און	PATTING - BR	गरह राक्लाम ११	\						-
SETTITUDE:			a distribution	****	_					
אַחודדוירדאַכּ										
AND HOMO	PI	PI /PÑ	ቦ፤ /ቦፕኖ	P[ /P ]P	XADEMA					
		PI /PB 0.48267	PE /PTF 0.439361	Pt /P TP 0.10174	X/DHAY -1.2200					

MASA-LEWIS		ALLIADY DATA	06/11/20	CADDELL	DEC 10/18/70 0/-35-// 033	CAP Aware		Pur 20
		INARY DATA	06/11/79	CADDEII	REC 10/18/79 04:25:44.920	FAC RYGXI	PGM CO34 P	ng 1257
>ADD1110M	AL PRESSUPE	PATINS . PPI	MANY PLUS			<del> </del>		
<b>1 ሆን</b> ዘብ <b>ቦ</b> ቦ	PI	PI / PO	P( / D) F	PL /PTP	X/GMAX			
32	19.196	5.7550	0.21162	0.43753	0.43200			
. ?7	19.551.	3.1648	0.11638	9.24961	0. 530QJ			
. 47	12.354	7.7757	0.13627	0.29177	J•629GO			
	15*410	7, 7951	0.13919	0.29777	0.72700			····
>40017189/	AL POESSIRE	RATIOS . FLO	W SPLITTER I	• n•	· · · · · · · · · · · · · · · · · · ·			
AVD HOPD	PL	PL /PO	PL /PTF	PL/PTP	X/DHAX			
62	14.517	4.3544	0.16912	0.33105	0.42200			
67	11.145	3, 3431	0.12293	0,25416	0.69200			· <del>- ·- ·- ·</del>
>AODITION	L PRESSUPE	RATIOS , FLO	H SPLITTER O	).n.				
AVO HORD	PL	PL /PO	PL / PTF	PL /PTP	XAMITX			
77	35.734	10.718	0.39414	0.81489	0.56400			
P 2	11-180	3.3536	0.12332	0.25496	0.63500			
63	3.5623	1.0685	U* 036583	0.081237	J• 6 4500			
>AnniTin4	L PRESSIRE	RATIOS . FJF	CTOR SHROUP		and the second statement of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	- Section (1) - 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AVO NOST	PL	PI / PO	PL /PTF	PI /PTP	X/DMAX	a agreement a service of the service of the		
107	9.3516	2. 8050	0.10315	0.21326	0.62400			
112	5.4027	1.6206	0. 650597	0.12321	0. 83700			
122	3.1421	1.95 249	0.034658	0.071654	0.96000			
127	3.5573	1.0670	0. (30237	0.001123	1.0900			
137	4.8627	1.4586	9.953635	0.11089	1.2200	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	and the same of the same of the same of	
142	4. TRZT	1.4346	0. 152753	0.10907	1.3500		_	
	nt but denne	#A1105 - FOR	fethe Infet			· · · · · · · · · · · · · · · · · · ·		
AVI WIPE	Pt	PL/PI)	PL / PTF	Pt /PTP	X/DHAX		5 5	
-107	9.351	2. 4950	0.10315	0.21326	-140000		0.3.	
-112	5.4027	1.6206	0.050502	C.12321	-1.0000 1.0000		Z 2	
-122	3.1421	0, 94249	0,034658	0.071654	-1.0000		40 VA	
-127	3 5573	1.9570	0.030237	0.001123	-1. 7000	-	0 0	
-137	4.0427	1.4586	0.053635	0.11089	-1.0020		<b>5.4</b>	
-147	4.792	1.4346	0.052753	0610907	-1.0000	A	<b>*</b>	
-157	3.5573	1.0685	0.039292	0.041237	-1.0000	2	<u> 5</u>	
-157		1.0670	0.039733		-1.0030			
	IL PRESSIPE		NOTE FLAS			۲۵)	•	
AND HUKD	PL	PI /PII	PL/PTF	PI /PTP	X /MAX			
-157	3.5623	1.7695	0.039252	0.081277	-1.0000			
-157	7,5573	1. 36 78	D. 030541.	0.001123	-1.0055			
SAINIT INV	L PRESSIBE	REYMS . 20	DEC SHE DOO	<b>NEATION</b>				
VAU AUDD	PL /	M /M	M /htf	EI /PTP	X/DMAX			
-167	3.5525	1.2655	0.039182	05011009	-1.0030			
-172	3,01523	1.0655	0.0391#2	0.074.009	-1.0000			
	M DOFSCHAF	RATIOS , 80	तहत् रामगणा ।	ULYALUM /				
יייו דוריייג								
AVO NOTO	Pt	PI /PI)	PI /PTF	PL /PTP	XAMAX			
	Pt 3.7472	Pt 7P0 0. 97400	M /PTF 0.035816	PL/PTP 0.074050	-1.0000	· · · · ·		

AVEV-FAIL	, DBEI,14	JUARY DATA	06/11/79	CADDELL	REC 10/18/79 04:27:37.679 FAC 88681 PGP C034 PNG 1258
SASSITIONS	I POFSSIPF	PATINS . PRI	MARY PLUG		
AVD HOPD	PĮ	M / PO	PI /PTF	PI /PTP	X
32	17.279	5. 1539	0.18821	0.43697	0.43200
37	0.5338	2.8349	0.10353	0.74034	0-53060
47	11.132	7.3776	0.17126	0.29151	0.62500
5?	11. 362	3.3491	2.12376	0.28732	3.7270J
			······································		J. 12 IVJ
>ADDITIONAL	AL PRESSURE	PATINS . FLO	M SPLITTER T	.D.	
AVD WORD	PL	Pt /PT	PI /PTF	PI /PTP	x/nmax
£7	13.714	7.8921	0.14177	0.32912	1.47290
67	11.782	3.3157	2.12072	0.28025	J.69200
>40317 304/	AL PPESSIRF	MATIOS . FLO	W SPLITTER C	. n.	
					# # # # # # # # # # # # # # # # # # #
AVD HOPD = 7/	PL 34 344	M /PO	PL / PTF	PL /PTP	X/OMAY
	36.065	17.759	7. 392#€	0.01204	3,56490
A ?	11.317	3.3757	0.12327	0.28419	0.63530
/	3.5821	1.06#5	0. 635020	0.0905#6	0.69200
ンとうつじてけつび	e ppessibe	PATINS . FJF	CTCP SHPRUR		en en en en en en en en en en en en en e
AVD YPPD	PI	PL /PI	PI /PTF	PL/PTP	X/OMAX
107	9.4538	2.8200	0.10298	0.2340#	0.62400
112	5.4717	1.6372	0. 050604	0.13837	0. #3000
122	3-1-29	0.94919	0.034662	0.090470	
127	3.5571	1. 1540	C. CARREA	0.093206	
137	4.5320	1.3519	0. 049347	0.11461	1.2200
142	4. 23 73	1.2037	3.047244	0.10968	1.350Q
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		ALTION CON			
WI HIPD	PL	PL /P1	PI /PTF	PI /PTP	x70mpd
107 unpn	PL 9.4538	PL /PTI 2. 829G	0.10208	0.2390F	x/nwar -1_0000
107 -107	PL 9.4538	Pt /Pri 2. 820G 1.6322	PI /PTF 0.10298 0.759874	0.2390A 0.17#37	-1.0000 1.0000
107 -107 -111	PL 9.4538 5.4717 3.1820	PL/PT 2.827G 1.6327 0.94919	PI /PTF 0.10298 0.759894 0.034662	0.7390R 0.17837 0.080470	-1.0000 -1.0000
101 unpn -107 -111 122	9, 4538 5,4717 3,1820	PL/PH 2.8290 1.6327 0.94919 1.0540	PI /PTF 0.10298 0.759874 0.034662 0.038856	0.7390R 0.13837 0.080470 0.090278	-1.0000 1.0000 -1.0000
107 -107 -111 -122 -127	9.4538 5.49[7 3.1820 3.567[ 4.329	PL/PT 2.829G 1.6327 0.94919 1.0440 1.3510	PI /PYF 0.10208 0.75674 0.054672 0.03886 0.03886	0.73908 0.13837 0.080470 0.090276 0.11461	-1.0000 -1.0000 -1.0000 -1.0000
107 -107 -111 -122 -127 -127 -142	91 9.4538 5.47[7 3.1820 4.527 4.527 4.1270	PL/P1 2, 82 90 1, 6 32 9 0, 94 91 9 1, 10 4 6 1, 35 1 9 1, 20 37	PI / PYF 0. 10208 0. 759874 0. 034876 0. 038876 7. 645367	0.2390F 0.17837 0.080470 0.09027F 0.11461 5.1096F	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000
107 107 112 122 127 142 142	9. 4538 5.4717 3.1820 4.5471 4.529 4.329 3.5671	PL/PT 2. R29G 1.6327 0.94919 1.0440 1.3519 1.7937 1.0640	PI / PTF 0. 10298 0. 105984 0. 074642 0. 074642 0. 074643 7. 04724 0. 034856	0.7390R 0.13837 0.080470 0.09020K 0.11461 0.090206	-1 0000   -1 0000   -1 0000   -1 0000   -1 0000   -1 0000
107 107 112 122 127 142 142	91 9.4538 5.47[7 3.1820 4.527 4.527 4.1270	PL/P1 2, 82 90 1, 6 32 9 0, 94 91 9 1, 10 4 6 1, 35 1 9 1, 20 37	PI / PYF 0. 10208 0. 759874 0. 034876 0. 038876 7. 645367	0.2390F 0.17837 0.080470 0.09027F 0.11461 5.1096F	-1 0000   -1 0000   -1 0000   -1 0000   -1 0000   -1 0000
vi unpn 107 111 122 127 127 142 157	9. 4538 5.4717 3.1820 4.5471 4.529 4.329 3.5671	P(/P1) 2.8296 1.6322 0.94919 1.0540 1.3510 1.2937 1.0640 1.0677	PI / PTF 0. 10298 0. 105984 0. 074642 0. 074642 0. 074643 7. 04724 0. 034856	0.7390R 0.17837 0.080470 0.090278 0.1141 5.10968 0.090206 0.090459	-1 0000   -1 0000   -1 0000   -1 0000   -1 0000   -1 0000
wh unpn -1107 -117 -127 -127 -142 -152 -152 -152	94538 54717 2-1820 2-5471 4-329 4-329 3-5671 3-5771	PL/PT 2. 8296 1.6327 0.94919 1.0540 1.351 1.7937 1.0640 1.0677	PI / PTF 0.10298 0.074642 0.074642 0.074642 0.074643 7.04434 0.034946	0.23908 0.17837 0.080470 0.090208 0.11461 0.10468 0.090206 0.090459	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
VI UNPO 107 117 127 127 127 142 142 142 143 144 145 147	91 9,4538 5,4717 3,1820 3,5471 4,5270 4,1270 3,5671 3,5771	PL/PT 2. R27G 1.6327 0.94919 1.0540 1.3510 1.7737 1.0640 1.0677	PI /PTF 0.10208 0.759874 0.074642 0.078876 7.645367 7.645367 0.638856 0.038965	0.2390R 0.17837 0.080470 0.090276 0.11461 0.090206 0.090206 0.090459	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
VI UNPO -1107 -111 -122 -127 -142 -142 -142 -142 -144 -142 -144 -142 -144 -144	P( 9.4538 5.4717 2.1820 5.5471 4.3270 4.3270 1.55771 1.55771 1.55671 7.5671	PI/PT 2. R29G 1.6322 0.94919 1.0540 1.3510 1.2937 1.0640 1.0677	PI / PTF 0. 10298 0. 10298 0. 0.7598/14 0. 0.746/2 0. 0.746/2 0. 0.74744 0. 0.38966 0. 0.38965 PT/ / PTF 0. 0.74866	0.2390R 0.17837 0.080470 0.040276 0.1247 5.1046R 0.040206 0.040206	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
WI WIPD -107 -117 -12? -12? -14? -14? -162 -163 -164 -167 -167	PL 9,4538 5,4717 2,1820 1,5471 4,329 4,329 3,5671 3,5771 11 PPESSIPE PI 3,5671 2,5771	PL/PT 2. 8296 1.6327 0.94919 1.0540 1.3510 1.7937 1.0640 1.0677 PAYING FAM	PI /PTF 0.10208 0.759874 0.074642 0.078876 7.645367 7.645367 0.638856 0.038965	0.2390R 0.17837 0.080470 0.040276 0.1247 5.1046R 0.040206 0.040206	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
Wn unpn -107 -117 -127 -127 -127 -127 -127 -127 -12	P( 9.4538 5.4717 2.1820 5.5471 4.3270 4.3270 1.55771 1.55771 1.55671 7.5671	PL/PT 2. R29G 1.6327 0.94919 1.0440 1.3510 1.7937 1.0640 1.0477 PAYITO FAR 1.0540 1.0540 1.0540	PI / PTF 0. 10298 0. 10298 0. 0.7598/14 0. 0.746/2 0. 0.746/2 0. 0.74744 0. 0.38966 0. 0.38965 PT/ / PTF 0. 0.74866	0.2390R 0.17837 0.080470 0.09020R 0.1461 0.09020R 0.09020R 0.09020R 0.09020R	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
With unpn	PL 9,4538 5,4717 2,1820 1,5471 4,329 4,329 3,5671 3,5771 11 PPESSIPE PI 3,5671 2,5771	PL/PT 2. R29G 1.6327 0.94919 1.0440 1.3510 1.7937 1.0640 1.0477 PAYITO FAR 1.0540 1.0540 1.0540	PI / PTF 0. 10298 0. 759874 0. 0746/2 0. 0746/2 0. 0746/2 0. 0746/3 7. 547244 0. 638866 0. 038966	0.2390R 0.17837 0.080470 0.09020R 0.1461 0.09020R 0.09020R 0.09020R 0.09020R	-1.0000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
WIN HUPD -107 -117 -127 -127 -147 -147 -147 -147 -157 -157 -157 -157	P( 9,4538 5,4717 2,1820 1,5771 4,327) 4,3270 3,5671 3,5771 11 PPFSSIPF	PI/PT 2. R2 9G 1. 6 32 2 0. 94 91 9 1. 0540 1. 35 10 1. 2937 1. 0640 1. 0677  PI/TTO, FAM M/PT 1. 0540 1. 0577	PI / PTF 0. 10298 0. 10298 0. 074662 0. 074662 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666	0.2390R 0.17837 0.080470 0.09027A 0.1241 5.1096R 0.090206 0.090206 0.090459	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
WI WIPD -107 -117 -127 -147 -147 -147 -147 -157 -157 -157 -157 -157 -157 -157	PL 9.4538	PI/PT 2. 827G 1.6327 0.94919 1.07460 1.3510 1.2937 1.0640 1.0677  PIYTH FAM M /PT 1.0540 1.0537	PI / PTF 0. 10298 0. 10298 0. 7559294 0. 074662 0. 074662 0. 074666 0. 074744 0. 034966 0. 034966	0.2390R 0.17837 0.080470 0.090276 0.090206 0.090206 0.090206 0.090206	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000  **/BMAX* -1.0000 -1.0000  **/BMAX* -1.0000
AVI UIPI -107 -117 -12? -12? -14? -14? -14? -15? -15? -15? -15? -15? -15? -15?	PI 9.4538 5.4717 2.1820 2.5671 2.5671 3.5771 II PPESSIDE PI 2.5671 2.5771 III PRESSIDE PI 3.5771	PI/PT 2. 829G 1. 6327 0. 94919 1. 0546 1. 3510 1. 2937 1. 0640 1. 0677  PAYTON FAM M /PT 1. 0546 1. 0555 1. 0655	PI / PTF 0. 10298 0. 759894 0. 074662 0. 074662 0. 074666 0. 074744 0. 034965 0. 034965 PPTT FLAP 0. 034965 PPTT FLAP 0. 034965 0. 034965	0.2390R 0.13837 0.08027R 0.12471 0.12471 0.12471 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000  **/BMAX* -1.0000 -1.0000  **/BMAX* -1.0000
AND MIPD -107 -111 -122 -127 -142 -152 -152 -157 -157 -157 -157 -157 -157 -167 -167 -167 -167 -167	PI 9.4538 5.4717 3.1820 3.5471 4.5229 4.3279 3.5671 3.5771 II PRESSIDE PI 3.5771 III PRESSIDE PI 3.5771 III PRESSIDE	PI/PT 2.8296 1.6329 0.94919 1.0540 1.3510 1.2937 1.0640 1.0677  PIYITO FAR  PAYETS 20  PAYETS 20  PAYETS 20  PAYETS 30	PI / PTF 0. 10298 0. 10298 0. 074642 0. 074642 0. 074643 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 0747244 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0. 074724 0.	0.2390R 0.13837 0.080677 0.090276 0.1261 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
AVI UIPIN -107 -111 -122 -127 -142 -142 -152 -157 -157 -157 -27117   1741 AVI UIPIN -162 -172 -173 -174 -174 -174 -174 -174 -174 -174 -174	P( 9.4538	PI/PT 2. R2 9G 1. 6322 0. 94919 1. 0540 1. 3510 1. 2937 1. 0640 1. 0677  PI/ITT FAM M /PT 1. 0540 1. 0557  PAYRIS . 20 PI/PT 1. 0555 1. 0671	PI / PTF 0. 10298 0. 10298 0. 10298 0. 0759874 0. 074672 0. 074676 0. 074724 0. 074965 PITTY DELETE 0. 074965 DEG SHEPTIME TO 0. 074911 0. 074911 0. 074915 DEG SHEPTIME TO 0. 074911 0. 074911 0. 074911 0. 074911 0. 074911	0.2390R 0.13837 0.08027R 0.13461 0.09027R 0.090206 0.090206 0.090459  PL/PTP 0.090206 0.090313 0.050459	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000
AVI UIPIN -107 -111 -122 -127 -142 -152 -152 -157 -157 -157 -157 -157 -157 -157 -167 -167 -167 -167	PI 9.4538 5.4717 3.1820 3.5471 4.5229 4.3279 3.5671 3.5771 II PRESSIDE PI 3.5771 III PRESSIDE PI 3.5771 III PRESSIDE	PI/PT 2.8296 1.6329 0.94919 1.0540 1.3510 1.2937 1.0640 1.0677  PIYITO FAR  PAYETS 20  PAYETS 20  PAYETS 20  PAYETS 30	PI / PTE 0. 10298 0. 10298 0. 759894 0. 074662 0. 074662 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666 0. 074666	0.2390R 0.13837 0.080677 0.090276 0.1261 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206 0.090206	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000

!!!!		HARY DATA	16/11/70	CADDELL	REC 10/18/79 04:28:07.020	FAC 9Y6KI	PG# (034	RUN 20 eng 1259
			•	( 1000 11	MEC T.M.P.S.1.4 24-54-11-05.1	PAC 400K	Pto- 11734	mins 85.14
27 1.21 (110) (4	T LETT 2 20162	PATINS . PRI	46P V 11 UM			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		
AU ALBU	PI	PI / PO	M /PTF	PE /PTP	X/DMAX			
32	1 6. 523	4.6752	0.16847	9.43696	0.43200			
² 7	P.5505	2,5522	0.092779	9. 24965	0.53900			
47	10. 324	2.9501	0.10965	0.24181	0.62990			
52	12,229	3.0512	0.11087	0,:8757	0.72700			
>100111001	H. PRESSIPE	PATINSFLO	n chîîlile î	, n <b>,</b>		*		
/D WIRD		PL/PD	M. /PTE	PL/PTP	X/DMAX			
52	11.748	3.5043	0.12733	0.33027	0.42200			
67	11.069	3,3016	2.11997	0.31117	0.65200			
NOT TICOR	F BEEZZIBE	RATIOS . FLD	N SPLITTEP O	.n				
VO WORD	PI	Pt /Pfi	PI /PTF	PL/PTP	X/DMAX	<b>.</b>		
/7	36.273	10.808	0.79274	1.0187	0.56400			
R2	11.359	3.3880	0.12311	0.31932	0.63500			
92	3.5745	1.0663	0.038745	0.10040	9.69200			
AND IT INNA	I PRESSIME	RATIOS . FJF	TTP SHPOUR					
N MUKU	PI	PI / PI	PL/PTF	PI /PTP	X/DMAX			
107	9.5191	2. #395	0.17314	0.26762	0.62400			
12	5.4950	1.6392	0. 055567	0.15440	0. 83000			
17?	3.1943	0.95285	0.034624	0.085805	0.96000			· · · · · · · · · · · · · · · · · · ·
27	3.5595	1.0618	0. 038542	0.19007	1.0900			
137 142	4.1397 3.9797	1.7349	0.044872	0.11639	1.2230 1.3500			
ADDLE LOW		64110E - FP8	CARRY IN CT					
						and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		constant to the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the contr
VID BORD	Pl 9.5191	P) /PD 2.8395	PL/PTF 0-10314	PI /PTP	Y/DHAX	•		
115	5,4950	1.6392	0.059562	0.26762	-1,0000 1,0000			
177	3.1943	0.95295	0.034624	0.089805/	-1.0000			
27	35595	1.0618	0. C3858?	2.10207	-1.0000			
37	4.1397	1.2349	2.044872	0.11639	-1.0000			
42	3.0797	1.1871	0.047177	0611199	-1.0000	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		
52	3.5495	1.0648	0.038691	0.19035	-1.0000			
57	3. 5645	V. 04 33	3.01*636	0.13021	-1.0000	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the s	
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n woen	PŁ	M /90	PL /PTF	" Pi /ÞTP	x/ŌMĀX	· • • ·		and a second second of the
152	3.5695	1.0648	G-038691	0.12235	-1.0000			
£7	3.5645	1.0635	0.438636	0.10031	-1.0000			
	IL PPFSSIRE	PANTIC . 20	`					
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	3,5595	1.0648	0.038691	0.10075	-1.0000		- w .	
	7			0.19035	-1.0000			
77	<b>/</b>	BITTING - NO	DEG SHEPTOP TI	LEALUM.				
77	3417774G				•			
יז ו הערודוריה	Pp	P) /PI)	· PI /₽TF ····	PI /PTP	X/MA			a. Mar en region principio.
167 172 527517171934 VD 2020 187			PF /PFF 0.035437 1.035057	Pt /PTP 0.091915 0.090930	X/1944 -1.0070	and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and t		war alak waan nagaliin ah gara war a

	PRFE INT	HARY DATA	96/11/79	- CANNETI	REC 10/18/79 04:28:55,719 FAC 98681 PG# CO34 9RG 1246
•		PATIOS . PPI			
TAU AUDU	PI	P/P/)	M /PTF	PI /P TP	······································
32	19.275	5. 7865	0.10724	0.43718	J-43200
37	10.563	3.1794	0.10837	0.24021	0,53000
47 52	12.391	3.7295 3.9392	7.12712 0.12984	0.28178	0.62 <del>90</del> 0 2.72700
	12.655				3012100
>ADDIT HIMA	PRESSUPE		M CHITTED I		
AVD HUBD	PL	Pt /PO	PI /PTF	PI /PTP	X/DMAX
62	14.568	4.3847	0.14944	0.33128	7.42200
<u>67</u>	11.763	3.3297	0.11350	0.25157	0.69200
SAUDIT FOUNT	PRESSURE	RATIOS , FLO	W SPLITTER P	• n•	المراجعة المستعلم المستعلى المستعلم المستعلم المستعلم المستعلم المستعلم المستعلم المستعلم المستعلم المستعلم
AVD HORD	PI	PI /PN	PL /PTF	PI /PTP	x/dmax
77	30,130	11.477	0.30120	0.86711	0-56400
82	12.026	3.6198	0.12739	0.27349	0.63500
92	3.5529	1.0494	0.036450	0.000753	
JAPOLTJORAC	PRESSIPE	PATINS . EJE	CTOP SHPMIN		And the second support to the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second
AVD YORD	PL	FL/PN	PI /PTF	PI /PTP	X/DMAX
197	10.049	3.0246	0.10310	0.22852	0.62400
112	5.4122	1.7494	0. C594 31	0.13217	0.43000
1??	3.3728	1.0152	0.034603	0.076699	
1 ? 7	3.5528	1.0694	0.036440	0.060793	
137	4.9876	1.4997	0.051119	0.11331	1.2200
142	4.8176	1.4482	0.044375	0.10944	1.3500
<del></del>		AATION TO			
	PI	PLTPN	PL/PYF	PI /PTP	X/CMAY
-107	10.049	3.0246	0.13310	0.27=52	-1.0000
-112	5.4122	1.7494	7. 0596 31	0.13217	>r.0000
-122	3.3728	1.0152	0.734603	0.076699	
-127	324524	1.0494	0.036450	0.040797	
-13 ⁷ -147	4.0126	1.4496	0.051119	0.11351	-1.0000 -1.0000
-147 -157	3.5428	1.0463	0.034347	0.10944	
-157	3.5428	1.0663	0.056347	0.085565	
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SECULT ICASE	PPFSTIRE	PATIOS FAN	WOTTER FLAT		•
	PE	9E 7#17	W/PTF -	PE /PTP	X/MAXX
-152	3.5428	1.0663	0.034347	0.080565	
-1=7	3.5675	1.7663		0.090565	-1:0000
	नमाररमस्य	WATTON . 20	गात रामगोग्	TEATTON -	
TEPTI FICES		P 791	PI /PTF	PLZPTP	- XZOMAKI
	Pl		0.03/347	0.060565	
AVD HOPD	PI 3.5478/	1.0663			
4VN 40PN -167		1.0663	0.036347	ः ०.००७५८	-1.0000
4VN 40PN -167	3.5478	1.0663			-1.3030
4VN 40PN -167 -172 	3.5478 3.5474 0155101	1.0663 PATENS - 40	7.636347	TEATTON	
AVN HIPN -167 -177 -XANTITINIAL	3.5428 3.5429 PFSSIBT	1.0663 PATENS : 40	NEG SIMPLIFITE OLIPPE	PI /PTP	X/DWAX
4VN 40PN -167 -177 -177	3.5478 3.5474 0155101	1.0663 PATENS - 40	7.636347	TEATTON	x/n=1.2000

445 1-L E4 IS	PRELIMI	HAGY DATA	06/11/79	CADDELL	PEC 10/10/79	04:31:29,172	FAC BYEKE	PG4 1034	ROW 20 PDG 1261
>400111094	PPESSIPE	RATIOS . PP1	HAPY PLUG					The Prince Strategie de la compa guarante de accepção	
ላስ ላርጀር	PL	PL/PO	PL/PTF.	PL /PTP	X/096 X				
32	14.789	5.5774	0.18816	0.4363	0.43200				
37	10,062	3,0300	9. 10352	0.24904	3.53000				
47	11.773	7.5455	0.12113	G.280C2	0.62900				
52	12,033	3, 6? 36	2.12383	0,29717	y <u>.72700</u>		····		
> VOOT A TOUNY	PPESSURE	PATIOS, R. FLO	W_SPLITTER I	en∙ .					
ላቦ 4ቦዶቦ	Pţ	PL/PD	PL /PTF	PI /PTP	X/DMAX				
£ ?	17.889	4. 1925	9.147.9	0.22140	J.42203				
67	11.000	2.3125	0.11317	0.76747	0.69209				
APPIT TOTAL	PPESSIPE	PAT105 FI 0	W SPLITTER C	. D.					
AU MUSD	PL	PL/PO	PL/PTF	PI /PTP	X/DMAX				
77	37. 954	11.399	7.39545	0.90322	J. =6400		. "		*
92	11.968	3.4041	0.12313	0.28557	0.63500				
92	3.5404	1.9662	0.024424	0.094477	0.69200				
jārnī tī (resk	PPFSSIRF	RATIOS . F.IF	CTOR SHEETING	-	made gave samble and a second of a	***			
VN WOPD	PL	PL /9/3	PI /PTF	PL /PTP	I/DMAX		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE S	
107	10.017	3.0165	0.19306	0.23901	0.62400				
11?	5,7483	1.7431	0. 554551	0.13811	0.43000			" · · · · · · · · · · · · · · · · · · ·	
122	3. 7605	1.0120	0.936574	0.090185	g. 960 <b>00</b>				
127	1.5404	1.0662	0.034424	0.084477	1.0900				
137	4.7943	1.4438	0.745325	0.11440	1.2200				
142	4.5795	1.3851	0.047321	0.10975	1.3500				
MOST TOWN	an f & Cum E	erting to	ENCON INTER						
Auturn	PL	PI /PN	PI /PTF	PI /PIP	X/044X		•		e e e e e e e e e e e e e e e e e e e
107	10.017	3.0165	90:01:06	0.23901	-1,0000				
112	5.7983	1.7431	0.254551	G. 13#11	1.0000				
72	3.3675	1.0120	0.034574	0.090195	-1.0000				
77	5404	1.0662	0.036424	0.084577	-1.0000				
177 14?	4.5004	1.4438	0.945375	0.13640	-1.0000				and the second of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract
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57	3.5434	1.0662	0.036424	0.094477	-1.0000				
	-				-110000				
ואנייתן דורר זי	PRESSUPE	PLYINS FAM	POTTE FEAR						
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57	3.5304	1.0631	0.036322	0.084238	-1.0000				
= 7	3.5404	1.3652	3036.634	0.094477	-1.0000		- · · •		
ואירן דוריי נ	PRESSIME	PAYERS . 20	nes simme i	UCTALUM			· · · · · · · · · · · · · · · · · · ·		
אה אהנה	PI /	PRI TEN	" PL/PTF	EL PPTP	X/DMAX				
167	2.5404	1.0462	0.036474	0.084477	-1.0000				
	354	1-3647	0.026273	0.006357	-1.0000		a company		
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177	PRESSIRE	PAYINS , AN	DEC SIMPLION	PEATIFIE >					
177 SEGNYTYVII	PPFSSIPE				DMAT				AND A CALL COMM
177 SEGNYTYVII	PI	PL/PII " "	M/PTF	PI /PTP "	#7 <b>PM</b> #X -1-0000				entage of the second second
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NISA-I FHIS	044 14	HARY DATA	26/11/79	CADDELL	REC 10/18/79	04:32:15-*49	FAC 9X6KI	PG4 C934	<i>Re</i> V 20 PDG 1242	
		PATINS . PPI		·			- 40, 341,48	164 1.954		
ነባ ሳበድቦ		PL /PP	m /PTF	PI /PTP					·	
2	PL 14.465	4.9340	0.16836	0.43696	x <b>/DMA</b> X ).4°2 <u>0</u> 0					
7	0. )484	2.7932	0.002779	0.24367	3.53039				•	
7	10.676	3.1675	7.17966	2.2.201	3.62593				•	
2	19.946	1.2330	2.11050	0.28784	1. 72 7:00					
ADDIT IDYA	I PRESSUPE	PATIOS , FLO	W SPLITTEP I	, n,						
D ALBD	PL	PI /PI)	PI /PTF	PL /PTP	X/DMAY					
2	12.418	3. 7016	0.12698	0. 32956	J. 42200	-	•			
7	10.970	3.2702	0.11214	0.29115	0.69200					
ANDIT ICHA	L PRESSIPE	RATIOS . FLO								
n when	PL	PL / PO	PL/PTF	PI /PTP	V /DMAY			*		
7	10.111	11.360	0.3897C	1.0114	Y/DMAX 0.56400					
2	12.963	3.5960	0.12375	0.32016	0.63500					
<u>.</u>	3.5438	1.0653	0. 036646	0.095113	0.69200		<del></del>	······································		
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		PATINS , FJE								,
กัษกลก	PI	PI./PI	Pt /OTF	PL /PTP	X/DMAX					-
07	10.097	3.0098	0.10324	0.26796	0.62400					
12	5. 4372	1.7400	0. C5 06 RA	0.15462	0.83000					
22	3.3989	1.0107	0.034653	0.089940	0.96000				-	
27	3.568R	1.06 7	0.076493	0.094715	1.0900					
37	4.3884	1.5081	0.044873	0.11646	1.2200					
42	4.2245	1.2605	0.043238	0.11272	1.3500					
		AASING . CON	• • • • • • • • • • • • • • • • • • • •							
y ALEU	PL	PL/PO	PE / PYF	PI 7PTP	X /MAY		•			
07	10.07?	3.0098	0.10324	0.26796	0000ھو1-					
12	5, 4372	1.7400	0. 25548#	0.15492	1.0000					
2? <del>27</del>	7.3889 5688	1.0102	0.034653	0.009940	-1.0000					
2 ' 37	4.3484	1.363#	0.034473	0.09477	-1.0000					
4)	4.728	1.2605	0.043235	0-11232	-1.0000	** ** **				
52	3.5778	1.0653	0.036544	0.094847	-1.0000 -1.0000					
57	7.5734	1.0653	0.036544	0.194847	-1.0000					
					214/120					
	PRESSIBE	RATIOS FAR								
<b>ሳ ተካ</b> ይሁ	PL	PI 7PI	VI I PALE	PE /PYP	X/IWAX					
52	3.5739	1.0653	0.034544	0.094847	-1.0000					
57	3.5738	1.0653	3503624	0.04447	-1.0000				-	
<u> ደጥ ፕሮሞ የ</u> ሶሜል	1 PRESSINE	PATINS . 70	DEC SHEDING	MEATTINE -						
	PL	PL 79H	MOPTE	N /PIP	X AMAX					
	3.5739	1.0653	0.034544	0.094947	-1.0000					
£.7		1.0666	~ ``^, 03 f 595	U* 0,60°C b D	-1.0000					
£.7	3.5769			_						
6.7 77	3.5769	-	तहत् दु <del>क्षणात् ।</del>	HEATENN -				······································		
נד יד <b>אייידדו</b> רמא	3.5769	-	neg simmin i	<del>ИГДТ   ИП</del> Ф1 /РТР	X/DNAX					
1 40PH 67 77 XH3TTTTTI 1 1:0PH 23	*.5769 PPF CSURE	<b>WATTER , NO.</b>			x/044x -1.0000	,				

NAS1-LEWI	S PRELIT	LHARY OATA	26/11/79	CADPELL	REC. 10/19/79 04:32:47.836 FAC 8X6X1 PGM C034 RNG 1263
>engli ion	AL PPESSURE	RATIOS . PRI	MAPY PLUG		
g 40H , 11V	PL	- m./en	PL/PTF	PLICTE	×/OMAN
2.7	16.413	4.8993	0.16749	0.43693	0.43200
37	9_0467	2. 7704	0.092315		0.53000
47	10.507	3.1602	0.10#04	0.28126	0.62900
57	10.897	3.2257	0.11027	0.2870R	J.,72700
HUI TICONS	AL PRESSURE	RATIOS + FLO	W SPLITTER I	, O _•	
AU ALED		PL/PO	PL/PTF	. M./PTS	x/max
17	12.437	3.7127	0. 12691	0.33039	0.42200
<u>67</u>	17.951	3,2689	0.11174	0.29093	0.69200
No. Linuré	AL PRESSURE	PATINS . FLO	W SOLITIER D	, D ₂	The control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the co
VP HOPP		PI / PO	M/PIF	PI /PTP	X/DMAX
P2	30.131 12.083	11.382 3.6066	0.38910 0.12330	1.0130 0.32099	0.56400 0.63500
97	3, 5743	1.0669	0.036473	0.094953	0.69200
>APRIT TON	AL PRESSURE	RATIOS . EJE	CTOR SHPOUD		
VO HOPD	Fi	Pt /P0	Pt /PTF	PI /PTP	X/DMAX
107	19.114	3.0189	0.10320	0.26#6#	0.62400
112	5.8497	1.7461	0.059697	0-15540	u.e 3000
177	3.4046	1.0162	0.034741	0.090444	0.96900
127	3,5593	1.9424	0.036320	0.094555	1.0900
137	4.3929	1. 7092	0.044723	0.11643	1.2200
142	4.2241	1.2620	0.043144	0.11232	1,3500
<del>&gt;1991 \$ 1000</del>	of the state	****** + **	FOUNT SHEE		
AUAGAD	PL	PI /PO	PL/PTF	PI /PTP	Y/MAX
107	10.114	3.01.09	0.10220	0.26868	
112	5.8407	1.7461	0.05969?	0.15540	1,0006
127	3,4046	1.0624	7.034741 0.036370	0.090444	-1.0000 -1.0000
127	4.342A	1.3082	0.036370	0.14643	-1.0000
147	22	1.26.20	0.043144	0.11232	-1.0000
152	3.5693	1.0654	0.036422	C.094820	-1.0000
1 = 7	3,5643	1.04 39	2.036371	0.054687	-1.0000
SEDDITION	AL PPESSIPE	PATION FAI	NOTTE FLAP	<del> </del>	
AL AUGU	Pt	PI /PI	MIPTE -	PLIPTH	X/DMAX
152	3.5693	1.9654	0. C36422	C.094A70	-1.0000
157	*********	1.063	yoʻbata 11.	0.0546#7	-1.0000
>4771717N	FF DELCCIME	PEYMS . 20	DEC SHRMDE	USAS IUM	
AU MUBL	Pİ	FL/96	M 7PTF	7919	X/MAX
-172 -172	3,576	1.0669	0.036473 0.036371	0.094663	-1.0000 -1.0000
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IVIT YUMD - 18-	Pi 3.2698 3.2399	9[ /PH 0. 9760 <u>1</u> 0. 94707	PL/PYF 0.033266 0.033060	# 0.086864 0.086069	x/mex -1.0090 -1.0060

>Angli Ind		PATIOS . PPI	96/11/79 MAPY PLUG	CADDELL	#FC 10/18/79 04:3	13: 34. 543	FAT RESEL	PGM C034	PNG 1264
ለሁ <i>ተ</i> սቢ-ս	Pf	PI /PO	PI /PTF	PI /PTP	X/DMAY				
32	19.495	5.5744	0.18876	0.43641	0.43700	•			
37	10.164	3.0360	0.10352	0.23543	0.53000				
47	11.929	1, 5544	0.17119	0.25075	0.62900				•
£7	12.154	3.6303	0.12379	9.2 ME 7P	J. 72700				
>+00 TT 10%	AT PRESSURE	PATINS . FLO	M ZOLÍTTED I	• N•					•
חקחע מע	PL	PL/PN	PI /PTF	P1 /PTP	x/DPAX				
+2	17.978	4.1754	0.14237	0.32984	J-42200			·· •·•	*
4.7	10.947	7.2699	0.11149	0.25831	3.69203				
>400   T   10%	L PPESSIPE	PATINS . FIN	W SPEETTER C	.D.	A to a software the said was an all the said was		* * **		
<b>งก พกสก</b>	Pŧ	PL / PO	PL /PTF	PL /PTP	X/DMAX				
77	30. (72	11.405	0.3PAR7	0.40045	0.56400			4	= +
97	12.049	3,6110	0.12312	0.28525	0.43500				
• ?	3.5622	1.3640	0.736281	0.084056	0.69200				
ADDE TERM	N PRESSIPE	PATINS . FUE	CTOP SHROUD"		A company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the comp				the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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/ቦ ሠብ#በ ኒበን					X/IMAX				
	10.114	3.0211 1.7455	0.10301 3.056515	0.23865 0.13788	0.62400				
17	T. 8435				7. #3000				
127	3.3975	1.0148	0.034602	0.070168	0.96000				
27	7.5427	1.0440	0.736241	0.0840=4	1.0900				•
137 142	4.4502	1.4448	0.049399	0.11445	1.2200				
-		1. 3771	0.047365	0.10974	1.3530				
ALL MARKE	PE	P1 / P7	M /PTF	PL JPTP	XIOMAY		•		
27	10.114	3.0711	0.19391	0.23465	-1,0000		agent of the same state of the		
115	5.8435	1.7455	0.059515	0.1374#	1.0000	-			
22	3.3975	1.014F	0. ¢34692	0.000160	-1.0000				
27	A-24.55	1.0640	0.036281	0.084356	-1.3000				
127	4. 572	1.4488	0.349399	0.13445	-1.0000				
147	4.65%	1.3491	0.047365	0.10074	-1.6995				
57	3.54?2	1.0440	0.036281	0.084056	-1.0000		and a second of the second		
F7	3.5672	1. 76.40	3.0367	<b>0.094356</b>	-1.0000				
AUSTA LUM	I BEFCIIBE	HAT PHITTER	HTTTLE FLAG						<u> </u>
IN HOPE	PE	M 780	MI IPTE	PIZPTP	X/IMAX				
E 7	3.562?	1.2642	0.036281	0.084056	-1.0000				
57	3.5627	1.0530	3 036271	0.046056	-1.0000				1941 I.M. # ## 9#
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AD ADRID	01	PI /#7	PE/PYF	PI /PTP	3 Fra 1 T				
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	3.5672	1.7640 1.7626	0.5362PL 0.336230	7.084056 3.083938	-1.0009 -1.0000	• • • • •	•		. •
147								<u></u>	
<del>6-7</del>   77	ा लग्दरराज्य	PATING AN	THE CHAPTER IT	PEATIFIN >					
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>ADDITION	AL PRESSING	PATINS , PPI	THAPY PIUG					e an include a single experience and the single experience and
ያሳ አሳክስ	PL	PI / PO	nj / PTF	Pt /PTP	K/DMAK			
32	15.357	4.5267	3.16417	0.43677	0.43200			
37	#.4EE7	2.54 BE	9. 392634	0.240*0	3. 53000			
47	9,9363	7. CR 54	3.10451	0.29193	J.62900			
52	13.116	3,0597	0,11091	0,28780	0.12100			
>407   1   1014	AL PRESSIPE	R41195 , FIT	NY SPLITTEP 1	, n _e	. N. S. Assenti . W. Mar			المناعد الوشاء المفود الماجو
VD WORD	PL	PL/PG	PL/PTF	FL/PTP	X/DMAX			
62	11.625	3.5335	0.12774	0.33074	0.42200	The second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the sect		20 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10 to \$10
f 7	19.921	3.2912	0.11962	0.31069	7.69200			
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งง พบษฏ	PL	PL/PO	PL/PTF	PL /PTP	X/DMAX			
77	35.619	19.732	0.39007	1.0131	0.564 <b>9</b> 0			
<del>82</del> 92	11.741 3.5407	1.3875	0.12313 0.038785	0.31979	0.63500 0.69200	· · · · · · · · · · · · · · · · · · ·	<del></del>	
				0.19573	0,642.00			
>AND	al pressure	RATIOS , EJF	FCTCP SHPCUD				_	
U MUSE	PL	PL/PI	PI /PTF	PI /PTP	x/nmax			
107	9,4165	2. 83 7R	0.10315	0.26790	0,62400			
112	5.4766	1.6354	0.059442	0.15439	0. 43000			
17?	3.1505	0.94944	0.034510	0.089629	0.96000	- Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Marketines - Mar		African consistence of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of
127	3.5257	1.0625	0.039620	0.10031	1.0900			
137	4.0911	1.2329	0.044813	0.11630	1.2209			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
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77	35.522	17.705	). 303AQ	0.40981	0.56490	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
97	11.209	3,7779	0.12335	0.28709	0.63500		
67	3.4409	1.0671	0.038965	0.090492	J-69200		
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vio พก่ศัก	<u> FE</u>	PL/PO	PI /PTF	PL /PTP	X/D4AX		The following of the second second second second second second second second second second second second second
197	9.3666	2.8226	0.19307	0.23998	0.62400		
117	5.4102	1.6304	C. 05<535	0.13857	0.83000		
122	3.1469	0. 74 825	0.734619	0.090576	0.96300		
127	3.5309	1.0641	0.034455	0.090436	1.0400		Control to the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Contro
177	4.4706	1.3472	0.049156	0.11450	1.2200		
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VAL WORD "	PT	PI /PI	MYPE	PE/PTP	1,1006	n nag <del>arawa</del> ar naka <del>wa</del> na m <del>aka maka maka na</del> na	A section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the sect
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127	3.5309	1.0641	0. 038855	0.040936	-1.0000	<del></del>	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
137	4.0176	1.3472	5.04919£	0.11450	-1.0000		
144	4.2847	1. 2915	7. 047[6]	1/10/77	-1.0050	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th
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AND MORD	<b>P</b> L	m_/pn	PL/PTF	PL/PTP	K/OMAX			
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37	10.521	3.1660	Q. 11566	9.24950	3.53000			
47	12.313	3.7065	0.13537	0.24158	3.62900			
52	12.573	3.7947	0.13822	0.28752	9.72793		-	
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07	3,5508	1.0689	0.039036	0.041109	J-692JO			
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172	3.1558	0.94995	0. 034693	0.072166	0.96000			
127	3.5458	1.0673	0.038941	0.041045	1.0906			
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107	9, 3821	7. #24?	0.10314	0.21455	-1,4000			
4115	4.4203	1.6316	0. (55538	0.12394	1.0000			
122	3.1550	7,44,995	0.034693	0.077166	-1.0000			
177	4.7455	1.0673	0. 634901	0.091995	-1.0000			
147	4.770	1.4360	0.053489	0.13/26 0./13909	-1.0000 -1.0000	- Marie and a company and the	principality in the second of their second principality and second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second or second	Company of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the contro
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	PI	PL/PA	PL/PTF	PI /PTP	x/PMax				
32	18.164	F. 4784	2. 21 701	0.43730	0.43200				
37	0.0977	2.9739	7.11982	0.24051	0.53000				
47	~11.671	3.4912	0.14026	0.29153	0.62900				
52	11.751	3.5546	D.1477R	J. 28778	J.72709				
					0012107				
AND IT I DOA	L PRESSUPE	RATIOS . FLC	W SPLITTEP I	• 71 - 12					
VD WOPD	Pt	PL/PN	PL/PTF	PL/PTP	X/DMAX				
45	13.749	4.0940	9.16495	0.23108	0.42200	•			•
7 م	10.757	3.2149	0.12053	0.26000	J.69200		<del></del>	<del> </del>	
ANDITIONAL	L PRESSUPE	RATIOS . FLO	W SPLITTEP O	• D•					
AD MUED	PL	PL/PO	PI / PTF	PL/PTP	x/DMAX				•
77	32.829	9.7752	0.79385	0.79053	2.56402				
A2	10-372	3.0677	0.17360	0.24809	. 0.63500				
92	3.4790	1.0657	0.047937	0.086184	0.69200	·	- <del></del>	<del> </del>	·
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VO WORD	PL	M / PO	PL/PTF	PI /PTP	X/DMAX				
107	R. 5835	2.5558	0.10298	0.20469	0.62400				
112	4.9643	1.4782	0, 059557	0.11954	0.83000			<del></del>	
122	2.8887	3.86914	0.034656	0.069541	0.96300				
127	3.5740	1.0642	0.047877	C.086063	1.0900				
137	4.5893	1.3665	0.055058	0.11051					
145	4.5193	1.3457	J. 35421A		1.2200				
•				0.10883	1.3500				
Anni I Inni	- PPECCIPE	PATIOS - FC	COOK INC.						
ALCHUED	PL	PI / PO	PLIPTE	PI /PTP	X/MAX		•		
107	P.5835	2,5558	0.10298	0.20669	-1.1000			.0	
112	4.9543	1.4792	7.756557	0.11954	1.3000				
122	2.8997	0. 96014	0.034656	0.069561	-1.0000				
127	3.5740	1.0642	0. 942877	0.086063	-1.0000		<del> </del>	(***	
137	4.5893	1.3665	0.95505R	0.11051	-1.0000				
147	4.510	1.3457	0.95421A	DC10443	-1.0000			\$7,55°	
152	3.5640	1.0612	0.042757	0.085822	-1. 2000		€	<b>^</b> ∧^	
157	3.5745	1.0642	0.742877	EAD380.0	-1.0000			Y. Cz	-
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A TOTT TONAL		BATIFA TAN		•			JA 6	<b>)</b>	
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le.	7.5540	1.0617	0. 642757	0.085822	-1.0000		· 🚓		
157	3.5747	1.065	3,042877	0.086063	-1.0000				some geställen. 14 m m m P. P 6 . 18
SANTITIONAL	E PRESSURE	PAST 5 . 20	गरत दामनाग्र ।	PCATION					
vn waph	PI /	PL JPN	MIPTE	OF VEAD	X/DHAX		· · · · · · · · · · · · · · · · · · ·		, and a second second second second second
167	2.57/6	1.7642	0.042677	0.006063	-1.0000				
172	3,4600	1.3627	9.742817	0.076943	-1.0000				and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
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חיזיייייי	PI	PL / PO	PI /PTF	P /FTP	XYIMAX				
	3.2539	<b>ን ዓሉ ጽጽ</b> ዋ	0. C390 <b>37</b>	0.078354	-1.0 <b>0n</b> q				
197	7.7130	3. CEK94	0.030557	0.077391	-1.3300				

4054-1 54 [	2 boef la	MERY MATE	06/11/79	C#00F[]	PEC 10/18/79 04:41:32.3	73 FAT THENS	PG4 1934	FOW 20 PRG 1271
יירן דורפיי	AL PPT SSIPE	P41105 . PP	MARY PLUG			The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		
VI) HEES	r)	21 / P1	714\ P	PĮ /P YP	x /DMA v	profession and the second		
3.7	12.577	3.7771	3.16875	0.43701	0.43203			
y ÷	4.3537	2.09.75	0.053760	0.24152	0.53000			
47	A.1353	2.4432	9.19615	0.2P2tP	G. 62900			
57	9,3372	2, 4720	2.11137	0.28941	).72700			
>2001T104	AL PRESSUPE	PATING . FLE	W SPLITTER I	.n.				
vo woep	PL	PI /PS	PL /PTF	PI /PTP	X/D#AX			
*** ****** £7	9.5444	7.4724	7.12832	0.37734	0.42200			· • • ·
67	10.734	3,2235	0.14401	0.37294	J.69200			
			W SPLITTEP C					
	et ny styne.			PL /PTP	W. Frank W.	en enem in gevenere griver v		and the second of the second
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P.2	9.2247	7.7704	0.12277	0.32053	0.63500			
<del>7</del> 2	3.5507	1.9664	0.247641	0.12338	0.69200		· — · · · · · · · · · · · · · · · · · ·	
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117	4.4309	1. 3307	0. 055451	0.15396	0.93000			
122	7.5903	2.77492	2.234627	0.089657	0. 96000	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t		the same many or a real or a region
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127 142	3.3556 3.2156	1.0078	0.045023 0.643144	0.11660	1.2200			
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VI UPEN 137 112 122 127 127 127 127 127 127 127 12	7.6655 4.4339 2.5803 2.5803 2.5257 3.5256 3.214 2.5407 3.5357 41 PRESSIDE P1 3.5407 3.5357 41 PRESSIDE	PI / PT 7 . 3021 1. 3397 0. 77492 1. 0549 1. 0549 1. 06572 1. 0434 1. 0619 RETITE . 30  II / PT 1. 0624 1. 0619  II / PT 1. 0619  II / PT 1. 0619  II / PT 1. 0619  II / PT 1. 0619  II / PT 1. 0619  II / PT 1. 0619  II / PT 1. 0619 II / PT 1. 0619 II / PT 1. 0619 II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT II / PT	0.10285 0.055651 0.034620 0.047205 0.047205 0.047205 0.047306 0.047439 0.047439 0.047439 0.047439 0.047439 0.047439	0.26635 0.15396 0.089657 0.12254 0.12254 0.12303 0.12286 PI/PTP 0.12303 0.12286 PI/PTP 0.12303 0.12286 PI/PTP 0.12303 0.12286	-1,000 1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000 -1,000			

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>400ET INNA	I PRESSUPE	PATINS . PPT	MAPY PIUG					
MAUN GAV	PL	ጣ / ቃበ	PL/PTF	PL /PTP	x/DMAX			
32	14.73R	4. 2270	0.18908	7.43R17	0.43200	· · · · ·	*	
37	7.7429	2. 32.92	0.10479	0.741+8	<b>0.53000</b>			
47	9.0573	7.7746	0.12200	0.2 A2 71	0.62900	- **		
57	9.2472	2.7902	0.12449	0.28848	0.72700		<del>- //</del>	
ANDITIONA	L PRESSUPE	RATIOS . FLO	W SPLITTER 1	. D.		-		• • · ·
AVP HOPP	PL	PL/PG	PI / PTF	PL/PTP	Y/DMAX	•		
62	10.646	3.2026	0.14340	0.33231	0.42200		* *	•
67	10.711	3.2221	0-14427	0.32433	0.69200			
APPRITECTAS	I PRESSIME	RATINS . FIR	W SPLITTER P	· n.				
AVD HORD	PL	የL/ዋን	Pt/PTF	PL /PTP	X/DMAX			
77	29.435	P. 9546	0.39647	0.91877	0.56400			
P2	9.1722	2.7592	0.12354	0.28630	0.63500			
92	3.5429	1.0658	0.047729	0.11059	0.69200			
SAPOTT FORAC	L PRESSUPE	MATINS . EJE	CTOP SHROW					
AVI HORD	PL	Pt /PI	PL /PTF	PL /PTP	X/DMAX			
107	7.6479	2.3006	9. 10371	0.23872	3. 62403			
112	4.4131	1.3276	0.059442	0.13775	0.#3000			
172	2.5774	0.77532	0.034715	0.080448	0.96000			
127	3.5279	1.0597	0.347455	0.10996	1.0900			
127	3.6679	1. 1734	0. 249404	0.11449	1.2200			
149	3.5129	1.0567	0.047316	0.10965	1.3500			and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
-> TOUL LION	f wedine	*47195 + F7*	FA499   FILT					,
AVIL MOPO	P(	PE 7 PA	PI /PTF	PL /PYP	x/DMAX			
-107	7.6479	2.3706	0.10301	0.23972	-1.9000			
-112	4.4131	1.3276	0. 059447	0.13775	24.0000			
-122	2.5774	1.3276	0.034715	0.089448	-1.0000			
-127	5779	1. 7597	0.04745)	3.10996	-1.0000	<del></del>		<del></del>
-127 -137	3.4579	1.1734	0.049404					
-142				0.1149	-1.0000			
-142 -15?	3.5126	1.0567	0.047316	0.11043	-1.0000 -1.0000			
-1-7	3.5329	1.0620	0.047545	0.11027	-1.0000			The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
~		PATTA - FAU						
AVN HUBB	bl.	PL / PA	PI /PTF	PL /PTP	X/DMYX			
-152	3.5379	1.0643	2. 047653	0.11043	-1.0000			
-157	7.5329	1.73	047585	0. [1327	-1.0000			· · · · ·
<u>&gt;₹~~111048</u>	T PRESSIPE	PATINE . 20	गम्द उस्लेख्या	PEATIN				
GROW OVE	PL /	M YM7	THEFT T	RE /PTP	XADMYX	- · · · · · · · · · · · · · · · · · · ·		
-167	2.5379	1.2628	0. 94 7585	201 1027	-1.0000			
	1.5	1.0628	0.047545	0.11027	-1.0000	. ****		
-1 / /		PATTOS . TO	NEC SHEEUN T	METTINN -				
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AVD HOPE	PL	" PL / PÖ "	Pt / PŤŤ	PI /PTP	X/IMA H	-		6 AN L 18 1901
אנירו ז דריר אכ <u>ר</u>	PL 2.2177		Pt /PTF 0.943340 0.042969	Pt /PTP 0.10044 0.049343	x/max -1.0000 -1.0000			± 40 € €

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"451-EF415	PPFLI4J	HAPP DATA	06/11/75	CADUETI	PEC 10/18/70	04:42:41.724	eac gapai	PG4 C034	#NG 1273	
APPOINTED !	PRESSURE	PATINS PPI	MARY PLUG	<del></del>						
rn waten	PL	PL / PO	PI /PTF	PI /PTP	X/DMAX					
1.7	14.703	4.8754	2.21726	P. 43768	J. 4320J					
. 7	P. 9750	2.5955	0.11973	0.24105	0.53000					
•7	10.435	3.1300	7.13606	0.28107	0.62900					
<u> </u>	10.00	3,7)76	2.14321	0.29795	<u> 12707</u>					
JAPOT TI COA	PRESSIRE I	RATIOS FLO	W. SPLETTER T	, r.						
/D W/IRD	PL	PL/P1	PL/PTF	PL /PTP	X/DMAX					
2	12.270	3.6719	0.16460	0.33143	0.47200				•	
.7	10.720	3, 7256	0.14381	9.24957	0.69299					
ANDETERNAL	PRESSUPE	RATIOS L FI	W.SPLITTER C	, n			<del></del>			
O HORD	PL	PL / PO	OL/PTF_	PI /PTP	Y/DMAX					
77	29.596	P. 9755	0.39704	0.79947	J.56400		* *			
?	9.2250	2,775A	0.12375	0.24919	0,63500			· · · · · · · · · · · · · · · · · · ·		
7	3.5573	1.0703	0.047717	0.0960#2	0.65200					
ANDET ÍDÁÁL	PRESSURE	RATIOS , FJF	CTOR SHPINIO	· · · · · · · · ·			<b></b>			
n ween	PŁ	PL /PI	PL/PTF	PL/PTP	X/DMAX				Marine Marine Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company	
07	7.6947	2.3123	0.10309	0.20758	0.62400					
12	4.4378	1.3353	3.059534	0.11968	0.63000					
77	2.5959	0.77807	0. 2346.49	0.069#49	0.96000				was entra production	
27	3.5369	1.0443	0.047449	0.095541	1.0900					
137	4.0975	1.2314	0.054901 0.054096	0.11055	1.2230 1.3500				mark a market two	
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		*******								
	PI	PL /PT	PL/PTF	PI /PTP	¥/04/4			· · · · · · · · · · · · · · · · · · ·		
0,	7.6847	2.3123	2.10109	0.2075	-1 0000					
112	4.4378	1. 1353	0.059534	0.11988	1.0000					
5,	2.5458	1.0643	0.0346#9	0.049849	-1.0000				<del>/</del>	
127 1 <b>37</b>	4.0025	1.2314	0.054901	0.14055	-1.0000 -1.0000					
47	4.037	1.2134	J. 05400h	0.10093	-1.0000					+
52	3.5419	1.0658	0.047516	0.095676	-1.0900					
E7	3. 5369	1.0643	0. 04 7449	0.095541	-1.0000		raine an in in make dissert	ere ere <del>eller ere e</del> e de la contraction de la research		
ANNIT INNAL	PERSONE	RATIOS	HATTLE FLAD							·
ก หกุยกั "	Pt	PI /PI	PIPTE	"PL/PTP"	X/DMAX	<b>.</b>				
57	3.5419	1. 3550	0.047516	0.095676	-1.0000					
e 7	3. 4169	1.05/15	"" JSQL744A"	0.095541	-1.0000		41 41 1 <b>10 10 10</b>	The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th		ar min
PROTTIONAL	PRESSIPE	Mns . 20	DEC SHAPING LI	PCATION						
	PL ·	PL /PN	M /ote	NI PTP	X/OPAX			approx.		
f	3.5119	1.0658	0.047516	0.095676	-1-0000					
7 ?	365369	1. 1643	0.347443	0.005541	-1.0030		and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th	•		
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PV24-f EMI	5 PRFL141	PIER PERE	26/11/79	CADDELL	RFC 10/18/79 04:44:	20.759 FAC 8X6X1	PGM F034 PPG 1274
>400111040	N PPFSSUPF	PATIOS . PET	MARY PIUG		······································		
AVP HORD	P1	Pt /PO	PI / PTF	PI /PTP	X/DMAX		
32	11.191	3. 3620	0.16926	0.43728	0.43700		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
27	6.1856	1.8587	0.093552	0.24169	0.53000		
47	7.2703	2.1600	0.10-20	0.29211	0.6290)		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
52	7.3899	2.2700	0.11177	0.28875	0.72700		
MOTTION	AL PRESSIPE	RATIOS . FLO	W SPLITTER 1	• n•	••		— par park
Au Aubb	PI	PL / PO	PL /PTF	PL /PTP	X/DMAX		
45	8.5197	2.5592	0.12884	7.33267	0.42200	· · · · <del>-</del>	# # ** *** * * * * * * * * * * * * * *
67	10.682	3.2090	0.16155	0.4177R	0.69200		
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77	26.337	7.9171	0.39833	1.0291	0.56400		
P2	P. 1303	2.4452	9,12319	0.31803	0.63500		
47	3.4413	1.0460	0.053710	0.13876	0.69200		
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107	6.9053	2.0444	0.10292	0.26591	0.62400	24	
112	3.9213	1.1780	0. 059306	0.15322	0. 83000		
12?	2.2911	0.68827	0.034651	0.009521	J. 96000	<b>⋌</b> ⋑ ≀	Č.
127	1.5763	1.0593	J. 053312	n.13774	1.0900	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th
137	7.9862	9.49711	0.045164	0.11666	1-2200	.~` <b>^` 4</b> °	,
14?	2.8562	^ ก็สรัสดิริ	0.043199	0.11160	1.3500	· · · · · · · · · · · · · · · · · · ·	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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107	4.8053	7.9444	0. 10292	0.26591	-1-0000		and the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contra
113	3.9213	1.1780	0.059306	0.15322	1.0000		
122	2.2911	0.68P27	0.034651	0.039521	-1.0000		
127	3,5273	1.0593	0.05337	0.1377	-1-0000		
137	2.9462	0.99711 7.85865	0.045164	0.1166	-1-0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	A CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR
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167	7.5413	1.0824		0.13837	-1.0000	y a long of the outer of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the c	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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72	12.699	3.7825	7. [#44)	0.43715	2.43200
37	7.0179	2.0904	0.10485	0.24159	0.53nng
47	P.2114	2.4457	0.12273	9.2.217	0.62900
52	9.3912	2.4094	0.12542		
				C.2APA6	0.1270)
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VO WORD	rt	PI /P/I	M /PTF	PL /PYP	y/rmax
62	9.6543	2.8756	0.14429	0.33234	0.42200
<u>+7</u>	10.669	3.1775	0.15944	U.36722	V.692VO
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<u>92</u>	8.2514 3.5909	1.0666	0.12333	0.17327	0.6350C 0.69200
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מפחע מעו	PI	PL /PO	M /PTF	PL /PTP	X/DMAY
107	6.8761	2.0517	0.10295	0.23712	0.62400
112	3.97.7	1.1927	0. C57349		
				0.17669	0.83000
127	2.3214	0.69145	0.234657	0.079911	
137	3.5609 3.3710	1.04.07 0.98920	0.053273 0.045679	0.1225P 0.11452	1.0900 1.2200
142	3.1911	0.94757	9.047546	0.10951	1.3500
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107	6.8881	2.0517	0.10295	0.23712	-1.0000
1112	3.9707	1.1427	0.050349	9-13669	-7.0000
125	2.3214	J. 69145	0.034697	0.079011	<u></u>
177	5609	1.0407	0.053223	0.12759	-1.0000
-177	3.346	). 94 970	0.047638	0.115-2	-1.0900
142	3.1917	0. 94752	0. 74 7546	1991ء	-1.0000
157	3.5709	1.0636	0.053373	12292	-1.0000
157	3.5759	1.0641	0.053447	0.12310	-1.0000
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-152	3.4709	1.2636	Q. 053373	0.12292	-1.00 <del>00</del>
157	1.5759	1.0651	0.452447	0.12310	-1.0000
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37	8.0454	2.3994	2.12269	0.24100	0.53000		
47	9.4149	2.8091	0.14129	0.28225	0.62900		••
52	9.6187	2.7687	0.14479	0.28824	0.72700		
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107	6.8514	2.9434	0.19274	0.20531	3,62400		
1112	3.9528	1.1789	0.040297	0.11845	3.83003	······································	
122	2.3179	0.49129	0.034771	0.069459	0.96000		
127	1,5579	1.0598	0.453244	0.10647	1.0900	there is also seen the territory of the contract of	and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and th
137	3.6679	1.0939	0.055022	0.10091	1.2200		
143	3.6579	1.0020	0.054423	0.1071	1.3500	transport communication and subgroupers subgrouped to subgroup to a subgroup of the subgroup.	التا بالجدو مجما والمسجداليس التعاليس
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122	2.3179	2.60129	0.934771	0.069459	1.9000		
1:7	35529	1. 3596	2.057208	0.10647/	-1.0000		
127	2, 6529	1.0930	3.055022	0.10991	~1.0930		
147	3.6279	2.0820	0.044473	0.17671	-1.0000	in the companies of the property of the property of the property of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the co	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
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167	3.5624	1.0426	5, 357448	3.N677	-1.0000	<b>271</b> A	
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124	2.2579	7.97144	0.045873	0.097628	-1.0008		
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10.154   3.0469   3.11094   0.20123     10.172   3.1662   0.17744   0.33014     10.597   3.1662   0.17744   0.33014     10.597   3.1662   0.17744   0.39014     10.597   3.1662   0.17744   0.39014     10.597   3.1662   0.17744   0.39014     10.597   3.1662   0.17744   0.29040     10.597   3.1932   0.39287   0.1076     10.172   3.1932   0.39287   0.1076     10.174   3.1932   0.39287   0.1076     10.174   3.1932   0.39287   0.1076     10.174   3.572   1.0694   0.2440     10.174   3.572   1.0694   0.30417     10.174   3.572   0.094487   0.1163     10.174   3.572   0.094487   0.1163     10.174   3.572   0.094487   0.1163     10.174   3.572   1.0619   0.34177   0.1103     10.174   1.2372   0.094487   0.1163     10.174   1.174   0.094487   0.1163     10.174   1.174   0.094487   0.1073     10.174   1.174   0.094487   0.1073     10.174   1.174   0.094487   0.1073     10.174   1.174   0.094487   0.1073     10.174   1.0649   0.3872   0.1073     10.174   1.0649   0.03872   0.1073     10.174   1.0649   0.03872   0.1073     10.174   1.0649   0.03872   0.1073     10.174   1.0649   0.03872   0.1073     10.174   1.0649   0.03872   0.1073     10.174   1.0649   0.03872   0.1073     10.174   1.0649   0.03872   0.1073     10.174   1.0649   0.03872   0.1073     10.175   1.0649   0.03872   0.1073     10.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.1073     11.175   1.0649   0.03872   0.03872   0.1073     11.175   1.0649   0.03872   0.03872   0.1073     11.175   1.0649   0.03872   0.03872   0.1073     11.175   1.0649   0.03872   0.03872   0.03872     11.175   1.0649   0.03872   0.03872   0.1		13.113	7.0017	0.007784 3.13887	0.24034	0.5330J J.6240A			
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1.317   1.0176   0.39287   1.0176   1.0176   1.2176   1.2176   1.2176   1.2176   1.2176   1.2176   1.2176   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1.2076   1	ěI I I		SULL	SPLITTER	Ü,	•	;		
16.179   10.795   0.39287   1.0176     16.4792   1.0494   0.0338915   0.10081     16.4792   1.0494   0.0338915   0.10081     16.4792   1.0494   0.0338915   0.10081     16.4792   1.0494   0.0338915   0.10491     16.4793   1.049   0.034847   0.10491     16.4794   1.1970   0.019447   0.10912     16.4794   1.1970   0.01944   0.10912     16.4795   1.049   0.03484   0.10912     16.4796   1.1960   0.03484   0.10912     16.4796   1.1960   0.03484   0.10912     16.479   1.1960   0.03484   0.10912     16.470   1.1960   0.03484   0.10912     16.470   1.1960   0.03487   0.10912     16.470   1.1960   0.03487   0.10912     16.470   1.1960   0.03487   0.10912     16.470   1.1960   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.10912     16.470   1.0649   0.03487   0.00412     16.470   0.03487   0.00412     16.470   0.03487   0.00412     16.470   0.03487   0.00412     16.470   0.03487   0.00412     16.470   0.00412   0.00412     16.470   0.00412   0.00412     16.470   0.00412   0.00412     16.470   0.00412   0.00412     16.470   0.00412   0.00412     16.470   0.00412   0.00412     16.470   0.00412   0.00412     16.470   0.00412   0.00412     16.470   0.0041	5	*	64/E	A / PTE	77 47 12	X /DMA X			
11.177  3.5792  1.06594  0.038015  0.10081  1.1710441 PRESSURE PATTINS , EJITTIN SHROUN  1.2792  1.2792  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.2794  1.279		36.129	13.795	0.39287	1.0176	0-56400		: :	,
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ADDII IOMAL D. WORD DI 12 22 27 27	PPESSURE 14.396 14.391 14.376 14.376	PATIOS . FOR PL /PC 0.99456 0.59421 0.99456 0.99749	PL/PTF 0.54983 0.54964 0.54965 0.54983 0.54869	PL/PTP 0.93048 0.93016 0.93048 0.9285	X/DMAR 0-39903 0-43100 0-44900 0-52200		•		
80011 10MA1 0 WORD 17 12 27 27 37	PPESSURE 14.396 14.391 14.376 14.376 14.356 14.356	PATIOS FOR PL/PC 0.99456 0.59421 0.99387 0.9956 0.99749 0.98662	PL/PTF 0.54983 0.54964 0.54965 0.54983 0.54869 0.54565	PL/PTP 0.93048 0.93016 0.9294 0.92055 0.92306	X/DMAX 0.39803 0.43100 0.44900 0.52260 0.52800		•		
BODII IOMAL ) WORD ) 7 12 ? ?	PPESSURE 14.396 14.391 14.376 14.376 14.356 14.356 14.271	PATIOS FOP PL /PC 0.99456 0.59421 0.99387 0.9956 0.99749 0.98662 0.90732	PL/PTF 0.54983 0.54964 0.54965 0.54983 0.54983 0.54869 0.55136	PL/PTP 0-93048 0-93016 0-9264 0-92855 0-92306 0-93307	X/DMAR 0.39903 0.43100 0.44900 0.52200 0.52200 0.58800		•		
ODII IOMAL ) WORD )? 2 2 7 7 8 3 7	PPESSURE 14.396 14.391 14.376 14.376 14.356 14.356	PATIOS FOR PL/PC 0.99456 0.59421 0.99387 0.9956 0.99749 0.98662	PL/PTF 0.54983 0.54964 0.54965 0.54983 0.54869 0.54565	PL/PTP 0.93048 0.93016 0.9294 0.92055 0.92306	X/DMAX 0.39803 0.43100 0.44900 0.52260 0.52800		•		
ODII IONAL WORD 17 22 27 17 17 22	PRESSURE 14.396 14.391 14.376 15.386 14.376 14.271 14.425	PATIOS FOP PL /PC 0.99456 0.59421 0.99387 0.9956 0.99749 0.98662 0.90732	PL/PTF 0.54983 0.54964 0.54983 0.54983 0.54869 0.54565 0.55136	PL/PTP 0-93048 0-93016 0-9264 0-92855 0-92306 0-93307	X/DMAR 0.39803 0.43100 0.44900 0.52200 0.52200 -1.0000				
ODII IONAL WORD 17 22 27 27 27 27 27 27 27 27 2	PRESSURE  14.396 14.396 14.376 15.386 14.356 14.271 14.435 14.425	PATIOS . FOP PL/PC 0.99456 0.59421 0.99456 0.99749 0.98662 0.99732	PL/PTF 0.54983 0.54984 0.54984 0.54983 0.54983 0.54983 0.54983 0.5469 0.54583	PL/PTP 0.9304R 0.93016 0.93048 0.92655 0.92306 0.53307 0.53307	X/DMAX 0.39803 0.43100 0.44900 0.52200 0.52200 0.58803 -1.0000				
ODII IONAL WORD 17 12 17 17 17 17 17 17 17 17 17 17	PRESSURE  PL 14.396 14.396 14.376 14.376 14.376 14.271 14.425 PRESSURE  PL 14.425	PATIOS . FOR PL/PC 0.99456 0.59421 0.99456 0.99749 0.98662 0.99732 0.99732	PL/PTF 0.54983 0.54984 0.54983 0.54983 0.54983 0.54983 0.54889 0.54583 0.55134 0.55134	PL/PTP 0.93048 0.93016 0.92948 0.92955 0.92306 0.93307 0.93307	X/DMAX 0-39903 0-43100 0-44900 0-52200 0-52200 0-58909 -1-0000 X/DMAX -1-0000				
ADDII IONAL D WORD D7 12 12 12 13 13 14 14 14 14 14 14 14 14 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16	PRESSURE  14.396 14.396 14.376 15.386 14.356 14.271 14.435 14.425	PATIOS . FOP PL/PC 0.99456 0.59421 0.99456 0.99749 0.98662 0.99732	PL/PTF 0.54983 0.54984 0.54984 0.54983 0.54983 0.54983 0.54983 0.5469 0.54583	PL/PTP 0.9304R 0.93016 0.93048 0.92655 0.92306 0.53307 0.53307	X/DMAX 0.39803 0.43100 0.44900 0.52200 0.52200 0.58803 -1.0000				
10011 10NAL 10 MORD 17 12 12 12 12 13 14 15 16 16 16 16 16 16 16 16 16 16	PRESSURE 14.396 14.396 14.376 14.376 14.376 14.376 14.425 PRESSURE PL 14.425 14.425	PATIOS . FOR PL/PC 0.99456 0.59421 0.99456 0.99749 0.98662 0.99732 0.99732	PL/PTF 0.54983 0.54984 0.54983 0.54983 0.54983 0.54983 0.54789 0.55134 0.55134 0.55136	PL/PTP 0.9304R 0.93018 0.92784 0.93048 0.92855 0.92306 0.93307 0.93307	X/DMAX 0-39903 0-43100 0-44900 0-52200 0-52200 0-58909 -1-0000 X/DMAX -1-0000				
ADDII IDHAL D MORD D7 12 27 27 37 62 27 37 62 52 53 40 40 40 40 40 40 40 40 40 40 40 40 40	PRESSURE  PL 14.386 14.386 14.376 19.386 14.356 14.425 14.425 PRESSURE  PL 14.425 PRESSURE	PATIOS . FOP  PL/PO 0.99456 0.59421 0.99387 0.9956 0.99749 0.98662 0.00732 0.90732 PL/PO  PL/PO	PL/PTF 0.54983 0.54964 0.54963 0.54983 0.54983 0.54869 0.55136 0.55136 0.55136 0.55136	PL/PTP 0.93048 0.93048 0.9264 0.93048 0.92855 0.92306 0.53307 0.92307 PL/PTP 0.93307 0.93307	X/DMAH 0.39903 0.43100 0.44900 0.52200 0.52200 0.52200 0.58909 -1.0000 -1.0000 -1.0000				
ADDII IDHAL D MORD D7 12 27 27 37 62 27 37 62 52 53 40 40 40 40 40 40 40 40 40 40 40 40 40	PRESSURE  14.396 14.391 14.376 14.376 14.376 14.271 14.425 14.425 PRESSURE  PRESSURE	PATIOS . FOR PL/PO 0.99456 0.59421 0.99366 0.99249 0.98662 0.99732 PATIOS . FAM	PL/PTF 0.54983 0.54964 0.54965 0.54983 0.54983 0.54869 0.54545 0.55136 0.55136 0.55136 0.55136	PL/PTP 0.93048 0.93048 0.92955 0.92306 0.93307 0.93307 0.93307	X/DMAX 0.39903 0.43100 0.44400 0.52200 0.52200 0.58909 -1.0000 -1.0000				
ADDII IDNAL D. WORD 17 12 27 27 27 37 62 62 63 64 64 64 64 65 7 67 67 67 67 67 67 67 67 67	PRESSURE  PL 14.386 14.386 14.376 19.386 14.356 14.425 14.425 PRESSURE  PL 14.425 PRESSURE	PATIOS . FOP  PL/PO 0.99456 0.59421 0.99387 0.9956 0.99749 0.98662 0.00732 0.90732 PL/PO  PL/PO	PL/PTF 0.54983 0.54964 0.54963 0.54983 0.54983 0.54869 0.55136 0.55136 0.55136 0.55136	PL/PTP 0.93048 0.93048 0.9264 0.93048 0.92855 0.92306 0.53307 0.92307 PL/PTP 0.93307 0.93307	X/DMAH 0.39903 0.43100 0.44900 0.52200 0.52200 0.52200 0.58909 -1.0000 -1.0000 -1.0000				
ADDII IONAL D WORD D7 12 27 37 62 62 63 64 64 64 64 65 65 65 65 65 65 65 65 65 65 65 65 65	PRESSURE  PL 14.386 14.381 14.376 14.376 14.386 14.376 14.425 14.425 PRESSURE  PL 14.425 14.425 14.425 14.425 14.425 14.425	PATIOS . FOP PL/PO 0.99456 0.59451 0.99456 0.99749 0.98662 0.99732 PATIOS . EAN PL/PO 0.99732 RAVIOS . 20 PL/PO 0.99732	PL/PTF 0.54983 0.54984 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54589 0.55136 0.55136 0.55136 0.77190 0.77190 0.77190 0.75136 0.77190 0.75136	PL/PTP 0.93048 0.93016 0.92644 0.93048 0.92755 0.92306 0.93307 0.93307 0.93307 7.93307 PL/PTP 0.93307 0.93307	X/DMAX 0.39903 0.43100 0.44900 0.52200 0.52200 0.52200 -1.0000 -1.0000 1.0000 1.0000				
ADDII IONAL  O WORD  O 12  27  27  27  27  27  27  27  27  27	PRESSURE  14.386 14.386 14.376 15.386 14.356 14.425 14.425 PRESSURE  PL 14.425 14.425 PRESSURE  PL 14.425 14.425 PRESSURE  PL 14.425 PRESSURE  PL 14.425 PRESSURE  PL 14.425 PRESSURE  PL 14.425 PRESSURE	PATIOS . FOP PL/PC 0.99456 0.59451 0.99456 0.99749 0.98662 0.99732 PATIOS . 20 PL/PC 0.99732 PATIOS . 20 PATIOS . 20 PATIOS . 20	PL/PTF 0.54983 0.54984 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.55136 0.55136 0.55136 0.55136	PL/PTP 0.93048 0.93016 0.9264 0.93048 0.92755 0.92306 0.53307 0.53307 0.93307 0.93307 0.93307 0.93307 0.93307	X/DMAX 0.39803 0.43100 0.44490 0.46690 0.52200 0.52200 0.58800 -1.0000 -1.0000 x/DMAX -1.0000 1.0000				
ADDIT TOMAL D WORD OF 12 27 27 27 27 27 27 27 27 27 27 27 27 27	PRESSURE  PL 14.396 14.396 14.376 15.386 14.356 14.425 14.425 14.425 PRESSURE  PL 14.425 14.425 PRESSURE  PL 14.425 14.425 PRESSURE  PL 14.425 14.425	PATIOS FOR PL/PO 0.99456 0.59421 0.99367 0.99249 0.98662 0.99732 0.99732 PL/PO 0.99732 PL/PO 0.99732 PL/PO 0.99732 PL/PO PL/PO	PL/PTF 0.54983 0.54984 0.54983 0.54985 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.55136 0.55136 0.55136 0.55136 0.55136 0.55136	PL/PTP 0.93048 0.93016 0.97684 0.93048 0.92855 0.92306 0.53307 0.93307 0.93307 7CATION PL/PTP 0.93307	X/DMAX 0.39803 0.43100 0.44490 0.52200 0.52200 0.58803 -1.0000 -1.0000 x/DMAX -1.0000 1.0000				
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D WORD 77 12 77 12 77 12 77 27 27 37 42 42 42 63 67 67 72 ADDITIONAL POPE 67 72 ADDITIONAL POPE 67	PRESSURE  PL 14.386 14.381 14.376 14.376 14.376 14.425 14.425 14.425 PRESSURE  PL 14.425 14.425 14.425 14.425 14.425 14.425 14.425 14.427	PATIOS FOR PL/PO 0.99456 0.59421 0.99367 0.99249 0.98662 0.99732 0.99732 PL/PO 0.99732 PL/PO 0.99732 PL/PO 0.99732 PL/PO PL/PO	PL/PTF 0.54983 0.54984 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983 0.54983	PL/PTP 0.93048 0.93016 0.97684 0.93048 0.92855 0.92306 0.53307 0.93307 0.93307 7CATION PL/PTP 0.93307	X/DMAX 0.39803 0.43100 0.44490 0.52200 0.52200 0.58803 -1.0000 -1.0000 x/DMAX -1.0000 1.0000				

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Miùl 11CC V	II PRESSIPE	PATINS . PPI	MIN MAN					
AU NUBU	et.	Pt / 90	PI / PTE	PL /PTP	X/DMAX		·	<del></del>
??	13.922	9, 96259	0.45664	0.76444	0.72200			•
27	14.721	1.0746	0.40609	0.81375	0.82900			
67	15.985	1.0429						
52			0.40477	0.02027	0.91990			
	15.185	1.0499	9.49894	J.P3375	1.0170			
>A701 T 10NA	I PPFSSIPF	PATIOS . FIR	W SPI ITTER I	1.n.				
en waren	PI	Pt /Pf)	PI /PTF	PI /PTP	X/OMAX			ere e genden grodge kann i de
52	14.571	1.0073	0.47791	9.80005	0.42200			
67	14.107	9. 97526	0.46269	J.77458	0.67900			
ANDITIONA	L PRESSIPE	RATIOS . FLO	M SPLITTEP I	P. D.			······································	<del></del>
VO WORD	•	m /00	<b>24</b> / 875	01 /DTD	V/0004			on market comments of the co
	Pl 12 211	PL /PN	PL /PTF	91 /PTP	X/DMAX			
77	12.311	0.85107	0.40377	0.67594	9.50000		-	man caretracture exercise to a second con-
??	16.926	1.1632	0.551AP	0.92388	0.58300			
92	14,402		<u> </u>	Q. 7 9074	0_67999	<del></del>		· · · · · · · · · · · · · · · · · · ·
TOO! 1 IOM	· sarççune	AATION - FJF	<del>cia cuanu</del>	<del></del>		-		
O WORD	7	PL/P0	PL/PTF	21.427	X/DMAX			
107	14.377	99380	0.47153	0.78937	-1.0000			
		2. 97320	30 37120					
112	<u> </u>			0.75082	-1.0999		<del></del>	
	14.357	7.000	N-03021	0.79400	-1.0000			
27	14.372	0.99355	0.47137	0.70910	-1.0000			
	-16.332	0.00070						
137		ე. <del>99</del> 979	0.47004	0. 76690	-1-0000			
137	14.262	0.99596	0.46777	0.78307	-1.0000			The Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Co
عسست	14.262		r.46777		-1.5000			
ADPLY IONA	14.262 L PRESSURE	0.99596 <u>Patins . Fr</u> e	0.46777 ERITOY INLEY	0.78307	-[.0000			. Print Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carlo Carl
ADPITIONA MORD	14.262 L <u>PRESSUPE</u> PL	0.98596 <u>8atjos " Fr</u> e Pl/Po	PL/PTF	0.78307 PL/PTP	X/IMAX			
ADPITIONA TO WORD	14.262 L PRESSUPE PL 14.377	0.98596 <u>Patins , fr</u> p PL/PR 0.99389	0.46777 ERFDY INLET PL/PTF 0.47153	0.78307 PL /PTP C.78937	x/max 0.39000			
ADPITIONA m word 137	14.262 L_PRESSUME PL 14.377 14.367	0.98596 <u>PATIOS . FCP</u> PL/PO 0.99389 0.99320	PL/PTF 0.47153 0.47120	0.78307 PL/PTP 0.78937 0.78882	X/RMAY 0.39000 2.43103	•		
ADPITIONA m word 107 112	14.262 L PRESSURE PL 14.377 14.367 14.352	0.98596 <u>PATIOS . FCP</u> PL/PO 0.99389 0.99320 0.99217	PL/PTF 0.47153 0.47120 0.47071	0.78307 PL/PTP r.78937 r.78882 0.78890	X/RMAY 0.39000 2.43103 0.44900			
ADPITIONA IN WORD 107 12 12 22	14.262 L_PRESSUME PL 14.377 14.367	0.98596 <u>PATIOS . FCP</u> PL/PO 0.99389 0.99320	C.46777  ERFOY IMLEY  PL/PTF 0.47153 0.47120 0.47071 -0.47137	0.78307 PL/PTP 0.78937 0.78882	X/RMAY 0.39000 2.43103			
ADPITIONA IN WORD 107 12 22 27	14.262 L PRESSURE PL 14.377 14.367 14.352	0.98596 <u>PATIOS . FCP</u> PL/PO 0.99389 0.99320 0.99217	PL/PTF 0.47153 0.47120 0.47071	0.78307 PL/PTP r.78937 r.78882 0.78890	X/RMAY 0.39000 2.43103 0.44900			
632 0 MORD 07 12 27 27 27 42	14.262 L PRESSURE Pt 14.377 14.367 14.352 14.372	0.98596 PL/PD 9.99389 9.99320 0.99327 9.99355	C.46777  ERFOY IMLEY  PL/PTF 0.47153 0.47120 0.47071 -0.47137	0.78207  PL/PTP C.78937 O.78882 O.78800 O.78910 O.78690	X/RMAH 0.39000 2.43100 0.44900 0.99600 0.52200	•		
63 6DPITIONA D WORD 37 12 27 27 27	14.262 IL PRESSUPE PL 14.377 14.367 14.352 14.372 14.332 14.762	0.48596 PL/PD 9.99389 9.99370 0.99217 9.99355 9.99079	PL/PTF 0.47153 0.47153 0.47120 0.47071 9.47137 0.47006 0.46777	0.78207 PL/PTP C.78937 O.78882 O.78800 O.78910	X/RMAX 0.39000 2.43103 0.44900 0.46000			
ADPITIONA IN WORD 37 12 22 27 27 37	14.262 L PRESSUPE PL 14.377 14.367 14.372 14.372 14.332 14.262	0.48596 PL/PD 0.49389 0.49370 0.49371 0.49375 0.49574 0.48596	PL/PTF 0.47153 0.47120 0.47071 9.47137 9.47106 0.46777	0.78207  PL/PTP C.78937 O.7882 O.7882 O.78910 G.78690 O.78307	X/RMAY 0.39000 2.43103 0.44900 0.52200 0.52200 0.58000			
63 PD WORD 07 12 22 27 27 37 42	PRESSURE 14.377 14.367 14.352 14.372 14.372 14.372 14.392 14.762	0.48596 PATINS . FIP PL/PN 0.99389 0.99320 0.99217 0.99355 0.99079 0.98596	PL/PTF 0.47153 0.47153 0.47071 9.47071 9.47006 0.46777 0.47204	0.78207  PL/PTP	X/RMAY 0.39000 2.43103 0.44903 0.52200 3.58000			
ADPITIONA IN HORD 107 112 127 27 27 37 142 142 143 143 144 145 145 146 147 147	PRESSURE 14.377 14.367 14.352 14.372 14.372 14.372 14.392 14.762	0.48596  PL/PR 0.99389 0.99320 0.99217 0.99355 0.99079 0.98586 0.99666	PL/PTF 0.47153 0.47153 0.47071 9.47071 9.47006 0.46777 0.47204	0.78207  PL/PTP	X/RMAY 0.39000 2.43103 0.44903 0.52200 3.58000			
63 ADPIT IONA IN WORD 37 12 27 27 27 42 42 53 53 40 40 40 40 40 40 40 40 40 40	PRESSUPE PL 14.377 14.367 14.352 14.372 14.332 14.62 14.414 1.0055400	0.48596  PL/PR 0.99389 0.99320 0.99217 0.99355 0.99079 0.98586 0.99666	PL/PTF 0.47153 0.47153 0.47171 0.47071 0.47071 0.47006 0.46777 0.47006	0.78207  PL/PTP C.78937 O.78937 O.78900 O.7890 O.7890 O.7890	X/NMAY 0.39000 2.43103 0.44900 0.52200 0.52200 0.50000			
20017 IOMA 70 HORD 107 12 12 127 27 27 27 442 45 45 467 467 467 467 467 467 467 467 467 467	PRESSUPE PL 14.377 14.367 14.372 14.372 14.372 14.416 14.416	0.48596  PATINS . FIP  PL/PN 0.99389 0.99320 0.99217 0.99355 0.99079 0.98596 0.995465	PL/PTF 0.47153 9.47120 9.47137 9.47137 9.47204 0.46777 0.47204	0.78207  PL/PTP C.78937 9.78882 0.78820 0.7890 0.7890 0.78307 0.79124	X/RMAY 0.39000 2.43103 0.44903 0.52200 3.58000 -1.0000			
ADDITIONA IN WORD 12 27 27 27 27 27 27 27 27 27 2	PRESSUPE  PL 14.377 14.367 14.352 14.372 14.332 14.762 14.416 14.416 14.416 15.416	0.48596  PL/PR 0.99389 0.99320 0.99217 0.99355 0.99079 0.98596 0.98596 0.98596	PL/PTF 0.47153 2.47120 0.47071 2.47137 0.47006 0.46777 0.47204 0.4777 0.47204	PL/PTP C.78937 C.78937 C.78930 C.78900 C.7890 C.78307 C.79106 P1/PTP C.79156	#/PMAX 0.39000 2.43100 0.44900 0.52200 0.52200 0.52000 1.0000			
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32	12.759	0.83445	0.33565	0.56497	J. 72200				
7	14.908	1.0316	0.41494	0-69843	2-82600				
. 7	15.711	1.0871	0.43730	0.73606	0.91900				
57	15.911	1.1709	3.44285	0.74540	1.0170			•	
ADDIT ION	AL PRESSURE	RATENS . FIT	W SPLITTER I	. P.					· · · · · · · · · · · · · · · · · · ·
/n wrmn	Pl	P1 / P()	PL/PTF	PL/PTP	Y/DMAX				
52	14.713	1.0181	0.40953	0.68932	0.42200				
7	12.518	0.96621	0.34643	0.586 48	0.67000				
MOIT FOR	I PPESCIME	PATERS . FEC	W SPLITTER	. 7.	A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR O	And the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	······································		
IN WORD	PL	PL/PO	PI / PTF	M./PTP	F/DMAX	•			enter ser i e la communicación
77	8-2714	0.57234	0.23022	0.38751	0.50600				and the second of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
12	20.659	1.4295	0.57501	0.96786	9.58700				
2	15.384	0.99532	9.40036	2.67389	0.67000				
<b>VUDITION</b>	IL-PRESSURE	PATIOS - EJE	CTOP SHIPOUR				Commission of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the State of the	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	garrige behindhare sambander. Dan blev vedtere – et an
D WIND	7	PL/PD	PL/PTE	PLEBA	X/DHAY.		and all the same and the same and the same and the same and the same and the same and the same and the same and		
107	14.334	0.49187	0.39892	0.67156	-1.0070				
112	14.329	179162	237884 _	0.67132					
127	14.329	2-20145	29884	0.67132	-1.0000				
77	14.349	7.99290	J. 39034	9.67226	-1.0009				
L37	14:514	0.99046	0.39862	0.03062	-1.0000				
32	14.265	0.98703	9. 39703	0.66829	1 0000				
MCLTICCAS	L PRESSURE	PATIOS . FOR	FRODY INLET						
D NUED	PL	PL/PO	PL/PTF	PL/PTP	T/DMAT			er sam "-innyamenya desir edilar kiri ani rikamenyafar	
197	14.334	0.99187	0.39897	0.67156	0.39000		•		
112	14.329	0.99152	0.39884	0-67132	0.43100	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			
177	14.329	0.99152	0.29684	0.67132	9.44960			•	
27	. 14.349	2,99290	0.39939	0.67226	0.48600				
77	14.314	0.99048	0.79842	0.67062	0.52200			\$3 2	
42	14.265	3.99703	0.39703	9.46828	0.58800		andre and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second se	35	
<del>  42</del>	<del></del>	<del> 3. 39635</del>	<del></del>	<del>91(7459</del>				~ ~	
<del>^</del>	<del> 14,349</del>	<del></del>	<del></del>	731 1459-	-1:0070			- <del>- 2</del> 23	
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ח שחפח	PL	7.790	_B/999	PL/PTP	Y/DMAX			7	
52	14.399	2. 99635	0.67078	0-67459	-1.0000	· ·	rader pres per les de l'establishes qui reflecces	2	* ************************************
5.7	14.199	0.99635	0.49078	0.67459	1-0000			S.P.	
	IL PRESSIPE	RATERS . 20	UEČ ZHAUŽU I	OCAT LON_				<u> </u>	
O MORD	Pŧ	PI / PG	PL/PTF	91 /PTP	Y FIMA Y			32	
67	14.399	0.99635	0.40078	0.67459	0.79300				and the second section of the second second section (second second
77	14.399	0.99635	0.40078	0.67459	0.84400				ayanan makang ayyang na 189 mai 1898 milang dipanggan sa 1898 milang na 1886
MOTT FOCK	IL PRESSIME	PATINS . NO	NEG SHRMUN L	CAT IN				4_41_41.	
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ND HORD	PL	PL /PD	PL /PTF	PL /PTP	Y/NAX		
32	8-1464	2.56431	0-19172	0.30773	0.72200		
37	16.458	1.1398	2.36702	0.62155	0.82000		atter kommunik krait ar hamperiole at the too too ordinante dans as one exhapped on one of the address of the owner.
7	17.675	1.2241	0. 29417	0.66752	0.91500		
2	17.630	1.2209	9. 39317	0.66587	1.0170		் சார் அறித் முன்றார் புச் <del>முற்றுக்கு இது இது பாழுக்கு படியாக முன்ற புக்கிய முன்ற முன்ற</del> முக்கிய கூடிய பிடிய கூறிய
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2	18.244	1.2634	C. 40685	0.68899	0.42200		ப் பார்கள் காரண்கள் கொள்ள கொள்ள கொள்ள கொள்ள கொள்ள குடியும் முறும்
7	15.749	1.0937	0.35122	0.59479	2. ( 7003		
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7	10.560	0.73129	0.23549	0.39880	0.50800		
12	14.976	1.0371	0.23599	0.56559	0.58309		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
2	14.362	0.99565	0.32029	0.54241	0.67000		
<del>10011 1000</del>	<del>(                                    </del>	AATINS , CUF	<del>(: Trin SHREWS</del>			1 119 9 9 9 9 9 1	
n werd	7	PL/PO	PL/PTF	PLANTE	X/DMAX		
Oï	14.302	99069	0. 31.090	0.54015	-1.0000		
12	14.297	0.000	0.31885	0.53996	-1.0000		
72	14.297	A-94014	TOTAL BRS	0.53996	-1.0000		
27	مجدد مؤا	0.99187	0.31940	Q. 54090	-1.0000		
37	14.287	0.98945	9.31862	0.2000	-1.0000		
47	14.258	0.99739	0.31796	0.53845	-1-0000		
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D 40ED	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX		
70 MUNED 07	PL 14.302	PL /PO 0.99049	PL/PTF 0-31896	0.54015	0.39800		•
70 WORD 107 12	Pt 14.302 14.297	PL/PN 0.99049 0.99014	PL/PTF 0-31896 0-31885	0.54015	0.39 <b>00</b> 0.43100		
70 WORD 97 12 27	PL 14.302 14.297 14.297	PL /PN 0.99049 0.99014 0.99014	PL/PTF 0.31896 0.31885 0.31885	0.54015 0.53996 0.53996	0.39 <b>900</b> 0.43100 0.44900		
n wnen 97 12 27	PL 14.302 14.297 14.297	PL/PN 0.99049 0.99014 0.99014 0.99157	PL/PTF 0.31896 0.31885 0.31885 2.31940	0.54015 0.53996 0.53996 0.54090	0.39800 0.43100 0.44900 0.4600		
70 WORD 97 12 27 27	PL 14.302 14.297 14.297 14.322	PL/PN 0.99049 0.99014 0.99014 0.99197 0.98945	PL/PTF 0.31696 0.31685 0.31685 2.31950 0.31667	0.54015 0.53996 0.53996 0.54090 0.54090	0.39800 0.43100 0.44900 0.46600 0.52200		
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70 WORD 97 12 27 27 37 42	PL 14.302 14.297 14.297 14.297 14.247 14.258	PL/PN 0.99049 0.99014 0.99014 0.99197 0.9845 0.98738	PL/PTF 0.31896 0.31885 0.31885 2.31940 0.31867 0.31796	0.54015 0.53996 0.53996 0.55099 0.53958 0.53855	0.39800 0.43100 0.44900 0.52200 0.52800		
ID WORD 07 12 27 27 37	PL 14.302 14.297 14.297 14.322 14.247 14.258	PL/PN 0.99049 0.99014 0.99015 0.99187 0.9845 0.98738	PL/PTF 0.31896 0.31885 0.31885 2.31940 0.31867 0.31796	0.54015 0.53996 0.53996 0.55090 0.53958 0.53855	0.39800 0.43100 0.44900 0.48600 0.52200 0.5800		
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D WORD  12 27 27 27 37 42 52 52 53 4001710NA 10 WORD  67 72 4001710NA	PL 14.302 14.297 14.297 14.322 14.297 14.258 14.343 14.2901 PPF \$SUPE PL 14.397 14.397 14.397 14.397 14.397 14.397	PL/PN 0.99049 0.99014 0.99014 0.99187 0.9845 0.98738 0.98738 0.98738 0.99636 PATINS 20 PL/PN PATINS 20 PL/PN	PL/PTF 0-31896 0-31885 0-31885 0-31867 0-31796 0-32085 0-32085 0-32085 0-32085 0-32086 0-32086 0-32086 0-32086	0.54015 0.53996 0.53996 0.54099 0.43948 0.53845 0.54355 0.54335 0.54335 0.54335 0.54356 0.54356	0.39600 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		
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D WORD  07 12 27 27 27 37 62 52 52 50 MOPD 57 57 50 MOPD 67 77 ADD   Y   DNA	PL 14.302 14.297 14.297 14.322 14.258 14.347 14.307 PPF \$SUPE PL 14.397 14.397 14.397 14.397 14.397 14.397 14.397	PL/PN 0.99049 0.99014 0.99014 0.99187 0.9845 0.98738 0.98738 0.98738 0.99636 PATINS 20 PL/PN PATINS 20 PL/PN	PL/PTF 0-31895 0-31885 0-31885 2-31950 0-31867 0-31796 0-32005 0-32009 0-32009 0-32006 0-32006 0-32006 0-32006 0-32006 0-32006 0-32006 0-32006 0-32006	0.54015 0.53996 0.53996 0.54099 0.43948 0.53845 0.54355 0.54335 0.54335 0.54335 0.54356 0.54356	0.39600 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		

والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحافظة والمحا

MASS-LEWIS	S PRF1 141	THAMA DULY	06/12/79	CARRETT	REC 10/24/79	9 07:37:35.823	ESC MAPAI	PG4 F934	RUN 22	
>AODITIONA	N. PRESSUPE	PATIOS . PRI	WARY IN U.C.							
yn ugen	PL	PLZPP	Pt / PT F	PI /PTP	Y/DMAX					
32	13.837	0.95886	0-26680	0.45291	J. 72200					
36 37	16.101	1.1150	0.31047	0.52703	0.0200)					٠
47	12.794	0.48661	0.74669	0.41878	0.62007					
41 E2	19.790	1.3021	0.74664	0.61593	1.0170					
- <i>e</i> 	196190	1. 2021	110 10723	**********	T+01 1.1					
NODET IONA	IL PRESSIME	PATINS . FLO	M COFTALED I	. P.						
งก พกจก	PL	PL/PO	PI /PTF	PL /PTP	X/DMA%					
62	21. 428	1.4849	0.41318	0.70139	0.42200					
67	18.455	1.2789	0.35586	0.60409	0.67000					
>AOD I T TONA	L PPESSUPE	PATENS . FLO	W SPLITTER O	- D.		·				_
VD WOPD	PL .	PL/PO	Pt /PTF	PI /PTP	X/DMAX		to the second of			
77	12.220	0. 84694	0.23563	0.40000	0.50900					
7 7 A 2	17.373	1.2039	0.33499	0.56866	0.50300 0.58300					• • • • • • • • • • • • • • • • • • • •
92	14.360	0.99516	0.27690	0.47005	0.67000					
ADDIT INNA	IL PRESSURE	PATIOS . EJE	CTOR SHROUD							
NO METO		7L/P8-	PL/PTF		-XADRAX		<del></del>			
107	14-250	0, 98963	0. 27536	0.46756	-1.0000					
112	15.271	98894		-0.36711	-1.0000				<del></del>	
127	14.261	0. 94H.	9.77407	0.46678	-1.0300			_		
127	14.295.	0-09057	0. 51265	0.46793	-1.0000					
137	15-251	0.98755	0-27478	U-MAGG	-1.0000			<b>**</b> **********************************		
1 - 1				0.0 11.000	- 100000					
	14.211	0. 98479	0.27401	0.46515	1.0000			70.4		
142	14.211	0. 98479	0.27401					হুর		
142	14.211		0.27401					হুর		
ADDITIONA	14.211	0. 98479	0.27401	0.46515 PL/PTP				23		
ADDITIONA VO.WORD	14.211 IL PRESSURE	0.98479 RATIOS . FOR	0.27401	0.46515 PL/PTP	1.0000			POOR		
ADDITIONA VO. WORD	14.211 ML_PRESSURE PL 14.290	0. 98479  RATIOS FUR PL/PQ 0. 98963	0.27401 ERDDY INLET PL/PTF 0.27536	0.46515 PL/PTP 0.46746	X/DHAX. 2 000991		•	POOR Q		
142 ADDITIONM VO WORD 107 112	14.211 NL PRESSURE PL 14.240 14.271	0. 98479  RATIOS . FUR PL/PO 0. 98963 0. 98894	0.27401 EEDDY INLET PL/PTF 0.27536 0.27517	PL/PTP 0-46744 0-46711	X/DMAX. 5. 19800 0.43100		•	POOR QL		
142 ADDITION VO WORD 107 112 122	14.211 AL PRESSURE PL 14.240 14.271 14.261	0.98479  RATIOS . FOR  PL/PO 0.98963 0.98894 0.98825	0.27401	PL/PTP 0-46744 0-46711	X/DMAX. 5. 19800 0.43100 0.44900		•	POOR QUA		
142 PADD LT.IQMA VD. WORD 107 112 122 127	14.211 NL PRESSURE PL 14.240 14.271 14.761 14.295	0. 98479  RATIOS FUR  PL/PO 0. 98963 0. 98894 0. 98825 0. 99067	0.27401 RENDOY INLEY PL/PTF 0.27536 0.27517 0.275497 0.27565	PL/PTP 0-46744 0-46711 0-46678 0-46793	X/DMAX 5. 19800 0.43100 0.44900 0.48600		•	POOR QUAL		
142 PADDITIONA VO. WORD 107 112 122 127	PL 14.240 14.271 14.271 14.271 14.295 14.251	0.98479  RAYIOS FUR  PL/PO 0.98963 0.98894 0.98825 0.99067 0.98755	0.27401 ERDDY INLEY PL/PTF 0.27536 0.27517 0.27565 0.27565	PL/PTP 0-46744 0-46711 0-46678 0-466793 0-46646	X/DMAX 1 19800 0.43103 0.44903 0.48600 0.52200		•	POOR QUAL		
PADDITIONA 70 WORD 107 112 122 127 137 142	14.211 NL PRESSURE PL 14.240 14.271 14.761 14.295	0. 98479  RATIOS FUR  PL/PO 0. 98963 0. 98894 0. 98825 0. 99067	0.27401 RENDOY INLEY PL/PTF 0.27536 0.27517 0.275497 0.27565	PL/PTP 0-46744 0-46711 0-46678 0-46793	X/DMAX 5. 19800 0.43100 0.44900 0.48600		•	POOR QUALIT		
142 PADD LY IQNA 70 WORD 107 112 122 127 127 137 142	PL 14.240 14.271 14.261 14.295 14.251 14.211	0.98479  RATIOS . FUR  PL/PQ 0.98943 0.98894 0.98825 0.99067 0.98755 0.98779	0.27401 PL/PTF 0.27536 0.27517 0.27497 0.27565 0.27478 0.27401	PL/PTP 0.46744 0.46711 0.46678 0.46678 0.46646 0.46515	X/DMAX 1 19800 0.43103 0.44903 0.48600 0.52200 0.58803		•	POOR QUAL		
142 PADDITIONA VO WORD 107 112 122 127 137 142	PL 14.290 14.271 14.261 14.295 14.211 14.211 14.211	0. 98479  RATIOS FUR PL/PU 98963 0. 98894 0. 98725 0. 99067 0. 98755 0. 98479 0. 98479	0.27401 PL/PTF 0.27526 0.27517 0.27565 0.27565 0.27478 0.27401 0.27401 0.27401	PL/PTP 0.46744 0.46741 0.46678 0.46679 0.46646 0.46515	X/DMAX 2. 19800 0.43100 0.44900 0.48600 0.52200 0.58800			POOR QUALIT		
142 >ADD LYIQMA VD. WORD 107 112 127 137 142 142 147	PL 14.240 14.271 14.271 14.261 14.271 14.271 14.271 14.271 14.271 14.271 14.271 14.271 14.271	0. 98479  RATIOS FUR PL/PU 98963 0. 98894 0. 98725 0. 99067 0. 98755 0. 98479 0. 98479	0.27401 PL/PTF 0.27526 0.27517 0.27565 0.27565 0.27478 0.27401 0.27401 0.27401	PL/PTP 0.46744 0.46741 0.46678 0.46679 0.46646 0.46515	X/DMAX 2. 19800 0.43100 0.43100 0.44900 0.52200 0.58800 1.0000			POOR QUALIT		
2ADDITIONA VD WORD 107 112 127 127 137 142 152 157	PL 14.240 14.271 14.261 14.271 14.261 14.271 14.271 14.271 14.271 14.271 14.271 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272 14.272	0. 98479 RATIOS FOR PL/PO 98963 0. 98894 0. 98825 0. 99067 0. 98755 0. 99479 0. 94779 0. 94779	0.27401 PL/PTF 0.27536 0.27517 0.27565 0.27565 0.27678 0.27478 0.27401 0.27401 0.27401	PL/PTP 0.46744 0.46711 0.46678 0.46679 0.46646 0.46515	X/DMAX 5. 19800 0.43100 0.44900 0.44900 0.52200 0.58800 1.0000		•	POOR QUALIT		
142 PADDITION VD WORD 107 112 122 127 137 142 152 157 VD WORD 152	PL 14.240 14.271 14.261 14.295 14.261 14.295 14.261 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300 14.300	0. 98479 RATIOS FOR PL/PO 0. 98963 0. 98894 0. 98925 0. 99067 0. 98755 0. 98479 0. 98479	0.27401 REDDOY INLEY PL/PYF 0.27536 0.27517 0.27497 0.27497 0.27478 0.27401 0.27401	PL/PYP 0.46744 0.46711 0.46678 0.46679 0.46646 0.46515 0.47103 0.47119	X/DMAX 2. 19800 0.43100 0.43100 0.44900 0.52200 0.58800 1.0000		•	POOR QUALIT		
ADDITIONA VD. WORD 107 112 122 127 137 142 152 157 VD. WORD 152	PL 14.290 14.271 14.761 14.295 14.211 14.749 14.390 14.395	0. 98479  RATIOS . FOR PL/PO	0.27401 REDDOY INLEY PL/PYF 0.27536 0.27517 0.27565 0.27447 0.27401 0.27401 0.27401 0.27748 0.27748 0.27757	PL/PYP 0.46744 0.46711 0.46678 0.46678 0.46646 0.46515 0.47103 0.47119	X/DMAX 1 19800 0.43103 0.44903 0.48600 0.52200 0.58803 1.0000		•	POOR QUALIT		
ADDITIONA  VD WORD  112  122  127  142  152  157  VD WORD  157  ADDITIONA	PL 14.290 14.271 14.261 14.271 14.261 14.271 14.271 14.271 14.271 14.271 14.390 14.390 14.395	0. 98479  RATIOS . FOR  PL/PO . 0. 98996 3  0. 98894 0. 98825  0. 99067 0. 98755  0. 99479  0. 44723  0. 99174	0.27401 REPORY INLEY PL/PTF 0.27536 0.27517 0.27565 0.27479 0.27401 0.27401 0.27748 0.27748 0.27748 0.27748 0.27757	PL/PTP 0.46744 0.46711 0.46678 0.46673 0.46615 0.46515 0.47103 0.47119	X/DMAX 19800 0.43103 0.44903 0.52200 0.52200 1.0000 1.0000		•	POOR QUALIT		
VD WORD 157 142 127 137 142 147 147 147 147 147 147 147 147 147 147	PL 14.290 14.271 14.261 14.295 14.261 14.211 14.390 14.395 14.395 14.395 14.395 14.396 14.396	0. 98479 RATIOS . FOR PL/PO	0.27401 REPORY INLEY PL/PYF 0.27536 0.27517 0.27565 0.27477 0.27407 0.27401 0.27401 0.27401 0.27746 0.27746 0.27746 0.27747 0.27748 0.27748 0.27757	PL/PYP 0.46744 0.46741 0.46678 0.46678 0.46646 0.46515 0.47103 0.47119  PL/PYP 0.47103 0.47119	X/DMAX 2. 19800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 1.0000 X/DMAX -1.0000			POOR QUALIT		
VD WORD 152 127 137 142 127 137 142 152 157 2001110NA	PL 14.290 14.271 14.761 14.295 14.271 14.761 14.295 14.211 14.799 14.390 16.395	0.98479 RATIOS . FOR PL/PO	0.27401 REPORY INLEY PL/PTF 0.27536 0.27537 0.27565 0.27447 0.27401 0.27401 0.27748 0.27748 0.27757 DEG SHRPUN 1 PL/PTF 0.27748	PL/PYP 0.46744 0.46711 0.46678 0.46678 0.46686 0.46515 0.47103 0.47119  PL/PYP 0.47103 0.47109	X/DMAX ( 19800 0.43100 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000			POOR QUALIT		
2ADDITIONA VD. WORD 107 112 127 137 142 147  VD. WORD 157 2ADDITIONA VD. WORD	PL 14.290 14.271 14.261 14.295 14.261 14.211 14.390 14.395 14.395 14.395 14.395 14.396 14.396	0. 98479 RATIOS . FOR PL/PO	0.27401 REPORY INLEY PL/PYF 0.27536 0.27517 0.27565 0.27497 0.27565 0.27478 0.27401 0.27401 0.27401 0.27748 0.27748 0.27748 0.27748 0.27757 DEG SHROUN 1 PL/PYF	PL/PYP 0.46744 0.46741 0.46678 0.46678 0.46646 0.46515 0.47103 0.47119 PL/PYP 0.47103 0.47119	X/DMAX 2. 19800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 1.0000 X/DMAX -1.0000		•	POOR QUALIT		
VD WORD 152 142 142 142 142 142 142 142 142 142 14	PL 14.290 14.271 14.261 14.295 14.251 14.211 14.390 14.395 PL 14.390 PL 14.395	0.98479 RATIOS . FOR PL/PO	0.27401 REPORY INLEY PL/PTF 0.27536 0.27517 0.27565 0.27565 0.27479 0.27401 0.27401 0.27401 0.27757 DEG SHROUD 1 PL/PTF 0.27757	PL/PTP 0.46744 0.46711 0.46678 0.46679 0.46646 0.46515 0.47103 0.47119  PL/PTP 0.47103 0.47119	X/DMAX ( 19800 0.43100 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000			POOR QUALIT		
VD WORD 157 142 127 137 142 152 127 200 157 200 157 200 157 200 157 200 157 200 157 200 157 200 157 200 157 200 157	PL 14.290 14.271 14.261 14.295 14.251 14.211 14.390 14.395 PL 14.390 PL 14.395	0. 98479  RATIOS . FOR  PL/PO . 0. 98963     0. 98894     0. 98825     0. 99067     0. 98755     0. 98479     0. 98775     0. 98775     0. 98775     0. 98778  RATIOS . 20  PL/PO . 0. 99758  RATIOS . 20  PL/PO . 0. 99758	0.27401 REPORY INLEY PL/PTF 0.27536 0.27517 0.27565 0.27565 0.27479 0.27401 0.27401 0.27401 0.27757 DEG SHROUD 1 PL/PTF 0.27757	PL/PTP 0.46744 0.46711 0.46678 0.46679 0.46646 0.46515 0.47103 0.47119  PL/PTP 0.47103 0.47119	X/DMAX ( 19800 0.43100 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000			POOR QUALIT		
142  ADD LYIQMA  VD. WORD  107  112  127  137  142  147  ADD LYIQMA  VD. WORD  152  ADD LYIQMA  ADD LYIQMA	PL 14.390 14.395 14.395 14.395 14.395 14.395 14.395 14.395 14.395 14.395	0. 98479  RATIOS . FOR  PL/PO	0.27401 REPORY INLEY PL/PTF 0.27536 0.27517 0.27565 0.27547 0.27565 0.27401 0.27746 0.27746 0.27747 0.27746 0.27757 DEG SHROUD 1 PL/PTF	PL/PTP 0.46744 0.46711 0.46678 0.46679 0.46515 0.47103 0.47119  PL/PTP 0.47103 0.47119  PL/PTP 0.47103 0.47119	X/DMAX 19800 0.43103 0.44903 0.48600 0.52200 0.58803 1.0000 1.0000 1.0000 1.0000 1.0000 X/DMAX 0.79300 0.84400			POOR QUALIT		
ADDITIONA  VD. WORD  107  112  127  127  137  142  142  142  142  142  147  240  240  240  240  240  240  240  2	PL 14.290 14.271 14.261 14.295 14.251 14.211 14.390 14.395 14.395 14.395 14.395	0.98479 RATIOS . FOR PL/PO	0.27401 REPUTY INLEY PL/PTF 0.27536 0.27517 0.27565 0.27479 0.27565 0.27479 0.27746 0.27746 0.27757 DEG SHROUN 1 PL/PTF 0.27757 DEG SHROUN 1 PL/PTF 0.27757	PL/PTP 0.46744 0.46741 0.4678 0.46678 0.46679 0.46679 0.46615 0.46515 0.47103 0.47119 PL/PTP 0.47103 0.47119 PL/PTP 0.47103 0.47119 PL/PTP 0.47103 0.47119	X/DMAX 2 19800 0.43100 0.44900 0.44900 0.52200 0.52200 0.58800 1-0000 1-0000 1-0000 X/DMAX 0.79300 0.84400 X/DMAX 0.79300			POOR QUALIT		
142  2ADDITIONA  VD. WORD  107  112  127  137  142  157  2ADDITIONA  VD. WORD  157  2ADDITIONA  VD. WORD  157  2ADDITIONA  VD. WORD  167  177  2ADDITIONA  VD. WORD  167  167	PL 14.290 14.271 14.261 14.295 14.261 14.211 14.390 16.395 14.390 14.390 14.390 14.395 14.395 14.395 14.395 14.395 14.395 14.395 14.395 14.396 PL 13.398 13.178	0. 98479  RATIOS . FOR  PL/PO	0.27401  RENDRY INLEY  PL/PYF 0.27536 0.27537 0.27565 0.27565 0.27567 0.27567 0.27567 0.27768 0.27768 0.27757  DEG SHROUN 1  PL/PYF 0.27768 0.27757  DEG SHROUN 1  PL/PYF 0.25833 0.25410	PL/PTP 0.46744 0.46711 0.46678 0.46679 0.46515 0.47103 0.47119  PL/PTP 0.47103 0.47119  PL/PTP 0.47103 0.47119	X/DMAX 19800 0.43103 0.44903 0.48600 0.52200 0.58803 1.0000 1.0000 1.0000 1.0000 1.0000 X/DMAX 0.79300 0.84400			POOR QUALIT		

,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就是一个人,我们就会一个人,我们就是一个人,我们就是一个人,我们就是一个人

MASA-I FWI		_				9 03:33:53,373		aum Edaf	PNG 1353
PATHETIN	ME BBESSIBE	PATEOS . PPI	MAPY PING						
AVD HOPD	PĮ	Pt /PO	PI /PTF	PL /PTP	X/DMAX	······································			
32	9.3540	0.64850	0.16343	0.27663	0.72200				
37	10.113	1.2559	0.31646	0.53566	0.82000				
47	14.221	0.99592	9.24846	J. 4205E	0. 91 900				
52	20. 294	1.3924	9.35089	0.59294	1.6170				
>ADDIT ION	AL PRESSUPE	PATINS . FLO	W SPLITTER	1.0.			· · · · · · · · · · · · · · · · · · ·		
AVN WOPD	PL	PL/PN	PI /PTF	PI /PTP	Y/DHAX				
62	23.039	1.5972	0.49250	0.68130	0.42200				
67	18.427	1.2775	0.32195	0.54495	0.67000				
>40717104	AL PPESSIPE	PATIOS . FLE	W SPI ITTEP (	P. N.					
AVP MOPS	PL	PL / PO	PL/PTF	PI /PTP	Y/DMAH	,			Management for any first or constructions
77	13.432	0.93125	0.23469	0.39724	0-50000				
92	19.171	1.3291	0.23494	0.56694	0.58300	1. •	The state of the second section of the second section of the second		
_ 02	14.356	9,99526	0.25051	0.42554	0_67000				
								The second second second	
AVD WOPD	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	PL/P0	PL/PTF	11/220	X/DMAX				
-107	14.266	0.99903	0.24924	0.42188	-1.0000				
-112	14-261	0.2750	0.25915_	0.42174	-1-0000		<del></del>		
-12?	14-241	0.38740	N-24881	0.47115	-1.0000				
-127	14.236	0.99741	0.249=0	0.42247	-1.0000				
-137	14-351	0. 99799	0.74408	0.42144	1.0000				
سسنعات	14.716	0.98547	0.24#37	0.42941	-1.0090_	··	*		
>AODITION	AL PRESSIPE	RATIOS . FOR	FPINY IM FT						
AVP WOPP	PL	PL/PO	PI /PTF	PL /PTP	X/DMAX				
107	14.266	0.44903	0.74924	0.42188	0.39800		•		
117	14.261	0.99848	0.24915	0.42174	0.43100				
127	14.241	0.98730	0.74881	0.42115	0.44900				
. 127	15.296	0, 99041	0.24950	0.42247	0.46600				
127	14.251	D. 98799	0.24P9R	0.42144	0.52200			·	
142	14.216	0.98557	0.24837	0.42041	0.5000				
-152			0.35136	0_43538					
-167	14.346-		<del></del>	9.42549	<del>-1.0070 -</del>				
	AL PRESSING	043105 FA	mussie eivi						
AVD WOPD	PI	PI 7917	PL/PTF	PL /PTP	X/DMAX				
-152	14.391		9.25125		-1.0000				
-157	14.396	0.09733	0.25133	9.42543	-1:0440				
<del></del> ,	AL PRESSIPE	PATINS , 20	DEG SHRMID I	OCATION	-		· was a second of second of		
AV1 WOPD	P1	PL/PT	PL /PTF	PL /PTP	X/PMAX 0.79300				· · · · · · · · · · · · · · · · · · ·
167	14.351	ე. 99699	0.25125	0.47578					
17?	14.346	0.49733	0. 25133	0.42543	9. 84400				
34301T10M	AL PPESSIPE	PATINS 1. 80	NEG SHEMUN !	ucation					
	et.	P( / Pf)	PI /PTF	PL /PTP	X/DMAX				
TAU MUOU			0.23564	0.39886	0.79300				
	13.487	0_ 93505							
TAU MUNU	13.487 13.298	0.92191	0.23233	0.39325	J. #4400				

	S PRFLIM	INARY DATA	96/13/79	CANDETI	REC 10/24/7	9 03:34:46.902	FAC AXAX1	PGM TO34	PNG 1354	
PAUDITION	IAL PRESSUPE	RATIOS . PPI	MAPY PING				er register i register			
AVD HORD	PL	PL/PN	PL / PTF	PL/PTP	X/DMAX	<del> </del>				
32	9.3447	0.64762	0-16221	0-27445	0.72200					
37	19.298	1.2619	0.31607	0.53478	0.82000					
47	14.321	0.99252	0.24859	0.42062	0- 91 900					
52	27-164	1.3975	9.35002	0.59223	1.0170					
>ADDIT TON	AL PRESSIRE	PATIOS , FLO	W SPLITTER I	. D.						
LVD WOPD	PL	<b>ዖ</b> L / <del>ዖ</del> በ	PI /PTF	PI /PTP	XAMAX					
ŧŻ	23.158	1.6049	0.40199	0.68015	0.42200					
67	14.427	1.2768	0.31979	0.54108	9.67000					
VADOLT 104	A1 09551195	PATIOS . FLO	W COL 17750 C							
-4	-C 'FRI 330FT			* 1/4						
HENR CAL	PL	ቦቲ / Pቦ	PI /PTF	PL/PTP	Y/DMAX					
77	13.558	0.93961	0.23534	0.39819	0.50800					
R2	19.316	1.3307	2.33530	0.56731	0.58300					
92	14-356	0.99494	0-24920	0.42164	0.67000					
24091710H	AL PRESSURE	PATING . EJE	CTON SHIPOUD		······································	• · · · · · · · · · · · · · · · · · · ·				
VD WORD	PL	PL/PO	PL/PTF .	. PL/PIP	X/DMAX					
-107	14-271	-0.98906	7.24773	7.41915	-1.0000					
112	<u> 14-261</u>	0.98897	0.25756	0-41886						
-127	14.256	0. 92703	11076767	0.41871	-1.0000					
-127	14.291	7.99045	7.24805	0.41974	-1.0000					
-137	14.256	0.98803	7.24747	0.41874	1.0000					
152	14.221	0.98561	0.24686	0.41769	-1:0000					
TANTALIAN.	M.M. J.J.L. alabyti.h.	RATIOS . FCF			v 40.44 v					
NO HORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX					
107	14.271	0.98906	0.24773	0.41915	0.39M00		•			
							•			
107 112	14.271 14.261	0.98906 0.98937	0.24773	0.41915 0.41886	0.39M00 0.43100	· /	•			
107 112 122	14.271 14.261 14.256	0.98906 0.98837 0.98803	0.24773 0.24756 0.24747	0.41915 0.41086 0.41071	0.39800 0.43100 0.44900		•			
107 112 122 127	14.271 14.261 14.256 14.291	0.98906 0.98937 0.98903 0.99045	0.24773 0.24756 0.24747 0.24808	0.41915 0.41886 0.41871 0.41974	0.39M00 0.43100 0.44900 0.48600	/ A	•			
107 112 122 127 127	14.271 14.261 14.256 14.291 14.256	0.98906 0.98937 0.98803 0.99045 c 98803	0.24773 0.24756 0.24747 0.24808 0.24747	0.41915 0.41886 0.41871 0.41974 0.41871	0.39800 0.43100 0.44900 0.48600 0.52209		•			
107 112 122 127 127 137 142	14.271 14.261 14.256 	0.98906 0.98837 0.98803 0.99045 C 28803 0.98561	0.24773 0.24756 0.24747 0.24808 0.24747 0.24686	0.41915 0.41886 0.41871 0.41974 0.41771 0.41769	0.39800 0.43100 0.44900 0.48600 0.52209 0.58800		•			
107 112 122 127 127 137 142	14.271 14.261 14.256 14.256 14.291 14.256 14.221	0.98906 0.98937 0.98803 0.99045 0.98561 0.98561	0.24773 0.24756 0.24747 0.24808 0.24747 0.24686	0.41915 0.41886 0.41871 0.41974 0.41971 0.41769	0.39M00 0.43100 0.44900 0.52200 0.5800 1.0000		•			
107 112 122 127 127 147 142	14.271 14.261 14.256 14.256 14.256 14.256 14.221	0.98906 0.98937 0.9803 0.98045 C.28803 0.98561 0.9757	0.24773 0.24756 0.24757 0.24808 0.24747 0.24686 0.24901	0.41915 0.41886 9.41871 0.41974 0.41971 0.41769 9.42267	0.39800 0.43100 0.44900 0.48600 0.52209 0.58800					
107 112 122 127 127 147 142	14.271 14.261 14.256 14.256 14.256 14.256 14.221	0.98906 0.98937 0.98803 0.99045 0.98561 0.98561	0.24773 0.24756 0.24757 0.24808 0.24747 0.24686 0.24901	0.41915 0.41886 9.41871 0.41974 0.41971 0.41769 9.42267	0.39M00 0.43100 0.44900 0.52200 0.5800 1.0000					
107 112 127 127 127 137 142 163 163 163 164 165 167	14.271 14.261 14.256 14.256 14.256 14.256 14.271 14.301 14.301	0.98906 0.98937 0.98803 0.98045 0.99045 0.990561 0.99737 0.99737	0.24773 0.24756 0.24747 0.24808 0.24747 0.24686 0.24481 0.24981	0.41915 0.41886 9.41871 0.41974 0.41769 9.42267 0.92267	0.39800 0.43100 0.44900 0.548600 0.52209 0.58800 1.8000					
107 112 122 127 127 142 142 153 163 164 165 167 167 168 179 179 179	14.271 14.261 14.256 14.256 14.256 14.251 14.301 14.301 PL 15.301	0.98906 0.98937 0.9803 0.99045 C 28803 0.99561 0.99737 0.49737	0.24773 0.24756 0.24747 0.24808 0.24747 0.24686 0.24901 2.24901	0.41915 0.41866 0.41871 0.41971 0.41771 0.41769 0.42267 0.42267	0.39800 0.43100 0.44900 0.52209 0.52209 0.58600 1.8000 X/DMAX -1.0000					
107 112 127 127 127 137 142 163 163 163 164 165 167	14.271 14.261 14.256 14.256 14.256 14.256 14.271 14.301 14.301	0.98906 0.98937 0.98803 0.98045 0.99045 0.990561 0.99737 0.99737	0.24773 0.24756 0.24747 0.24808 0.24747 0.24686 0.24481 0.24981	0.41915 0.41886 9.41871 0.41974 0.41769 9.42267 0.92267	0.39800 0.43100 0.44900 0.548600 0.52209 0.58800 1.8000					
107 112 127 127 137 142 142 143 143 144 145 147 149 149 149 149	14.271 14.261 14.266 14.276 14.276 14.276 14.271 14.301 14.301 Pt. 15.301 14.391	0.98906 0.98937 0.9803 0.99045 C 28803 0.99561 0.99737 0.49737	0.24773 0.24756 0.24747 0.24808 0.24747 0.24686 0.24481 0.24481 0.24481 0.24481	0.41915 0.41866 9.41871 0.41974 0.41769 9.42267 PI /PTP 0.42267	0.39800 0.43100 0.44900 0.52209 0.52209 0.58600 1.8000 X/DMAX -1.0000					
107 112 127 127 147 142 153 163 163 164 175 165 165 165 165 165 200 17100	14.271 14.261 14.256 14.256 14.256 14.271 14.391 AL PRESSUPE  AL PRESSUPE	0.98937 0.98937 0.9803 0.99045 C 28803 0.99561 0.99737 0.49737 0.99737 0.99737	0.24773 0.24756 0.24767 0.24808 0.24747 0.24686 0.24981 9.24981 MOTZLE FLAS 0.24981 0.24981	0.41915 0.41866 0.41871 0.41974 0.41771 0.41769 0.42267 0.42267 0.42267 0.42267	0.39800 0.43100 0.44900 0.52209 0.58600 1.8000 2.9009					
107 112 127 127 142 142 143 145 145 240017100	14.271 14.261 14.266 14.276 14.276 14.276 14.271 14.391 14.391 14.391  AL_PRESSUPE	0.98906 0.98537 0.98803 0.98045 0.99045 0.98561 0.99737 0.49737 0.49737 0.99737 0.99737	0.24773 0.24756 0.24756 0.24767 0.24808 0.24747 0.24686 0.24981 0.24981 0.24981 0.24981 0.24981	0.41915 0.4186 0.41871 0.41871 0.41871 0.41769 0.42767 0.42267 PI /PTP 0.42267 0.42267	0.39800 0.43100 0.44600 0.52209 0.52209 0.58800 1.8000 1.0009 X/DMAX -1.0000 1.0000					
107 112 127 127 137 142 152 153 150 150 150 150 150 150 150 150 150 150	14.271 14.261 14.261 14.276 14.276 14.271 14.276 14.271 14.301 14.301 14.391  AL PRESSUPE PL 14.391	0.98906 0.98937 0.98803 0.98045 0.99045 0.99561 0.99737 0.99737 0.99737 0.99737 0.99737	0.24773 0.24756 0.24747 0.24808 0.24747 0.24686 0.24481 0.24981 0.24981 0.24981 0.24981	0.41915 0.41866 0.41871 0.41974 0.41769 0.4267 0.42267 0.42267 0.42267 0.42267 0.42267	0.39800 0.43100 0.44900 0.52209 0.58800 -1.8000 -2.0009 X/DMAX -1.0000 1.0000					
107 112 127 127 142 142 143 145 145 240017100	14.271 14.261 14.266 14.276 14.276 14.276 14.271 14.391 14.391 14.391  AL_PRESSUPE	0.98906 0.98537 0.98803 0.98045 0.99045 0.98561 0.99737 0.49737 0.49737 0.99737 0.99737	0.24773 0.24756 0.24756 0.24767 0.24808 0.24747 0.24686 0.24981 0.24981 0.24981 0.24981 0.24981	0.41915 0.4186 0.41871 0.41871 0.41871 0.41769 0.42767 0.42267 PI /PTP 0.42267 0.42267	0.39800 0.43100 0.44600 0.52209 0.52209 0.58800 1.8000 1.0009 X/DMAX -1.0000 1.0000					
107 112 127 127 147 142 153 153 153 154 157 267 172	14.271 14.261 14.256 14.256 14.256 14.251 14.391 14.391 14.391 AL_PRESSUPE PL 14.391 14.391	0.98906 0.98937 0.98803 0.98045 0.99045 0.99561 0.99737 0.99737 0.99737 0.99737 0.99737	0.24773 0.24756 0.24767 0.24808 0.24747 0.24686 0.24981 9.24981 0.24981 0.24981 0.24981 0.24981 0.24981	0.41915 0.41866 0.41871 0.41974 0.41771 0.41769 0.42767 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267	0.39800 0.43100 0.44900 0.52209 0.58800 -1.8000 -2.0009 X/DMAX -1.0000 1.0000					
107 112 127 127 127 147 142 153 155 157 260017100	14.271 14.261 14.261 14.276 14.276 14.276 14.271 14.301 14.301 14.391 14.391 14.391 14.396 IAL PRESSUPE	0.98906 0.98937 0.98803 0.98045 0.29045 0.290737 0.290737 0.290737 0.290737 0.290737 0.290737 0.290737 0.290737 0.290737 0.290737 0.290737 0.290737	0.24773 0.24756 0.24747 0.24808 0.24747 0.24686 0.24481 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981	0.41915 0.41861 0.41871 0.41974 0.41769 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267	0.39800 0.43100 0.44900 0.52209 0.58000 -1.8000 -1.0000 1.0000 1.0000 0.79300 0.84400					
107 112 127 127 137 142 153 153 153 153 15401719N 150 157 157 157 2401710N 167 172 24017109	14.271 14.261 14.256 14.291 14.256 14.291 14.391 14.391 14.391 14.391 14.396  AL PRESSUPE PL 14.396	0.98906 0.98937 0.9803 0.9803 0.99045 0.28737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737	0.24773 0.24756 0.24757 0.24808 0.24747 0.24686 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981	0.41915 0.41866 0.41871 0.41974 0.41771 0.41769 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267	0.39800 0.43100 0.44900 0.52209 0.58600 1.8000 2.7009 X/DMAX 0.79300 0.84400					
107 112 127 127 127 137 142 153 167 200111109 167 172 >ADDITION 180 187	14.271 14.261 14.266 14.276 14.276 14.271 14.271 14.391 14.391 14.391 14.391 14.396  AL PRESSUPE PL 14.396  AL PRESSUPE PL 13.503	0.98906 0.98937 0.98803 0.99045 0.99045 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737	0.24773 0.24756 0.24747 0.24808 0.24747 0.24886 0.24981 0.24981 0.24981 0.24981 0.24972 DEG SHERUD 1 PL/PTF 0.24981 0.24972 DEG SHERUD 1	0.41915 0.41866 0.41871 0.41974 0.41771 0.41769 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267	0.39800 0.43100 0.44600 0.52209 9.58800 1.8000 1.0009 X/DMAX -1.0000 1.0000 0.64400					
107 112 127 127 127 142 152 152 152 26001710N 1VD WOPD 152 157 26001710N 167 172 26001710N	14.271 14.261 14.261 14.276 14.276 14.271 14.391 14.391 14.391 14.391 14.396  AL PRESSUPE PL 13.503 13.313	0.98906 0.98937 0.98803 0.98045 0.99045 0.997561 0.99757 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737	0.24773 0.24756 0.24747 0.24806 0.24747 0.24886 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981	0.41915 0.41866 0.41871 0.41974 0.41771 0.41769 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267	0.39800 0.43100 0.44900 0.52209 0.58600 1.8000 2.7009 X/DMAX 0.79300 0.84400					
107 112 127 127 127 142 152 152 152 26001710N 1VD WOPD 152 157 26001710N 167 172 26001710N	14.271 14.261 14.261 14.276 14.276 14.276 14.271 14.301 14.301 14.301 14.301 14.301 14.301 14.301 14.301 14.301 14.301 14.301 14.301 14.301 14.301 14.301	0.98906 0.98937 0.98803 0.99045 0.99045 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737 0.99737	0.24773 0.24756 0.24747 0.24806 0.24747 0.24886 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981 0.24981	0.41915 0.41861 0.41871 0.41974 0.41769 0.42767 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267 0.42267	0.39800 0.43100 0.44600 0.52209 9.58800 1.8000 1.0009 X/DMAX -1.0000 1.0000 0.64400	DSM 0-076646	CF9 9-0028631			

4454-I EWIS	PRELIM	NARY PATA	06/13/70	CADDE!!	REC 10/24/79 03:76:34.219	FAC RYSYI	PG4 C034	Russ 22
NOT T [ COA	IL PRESSUPE	RATIOS , PPI	MAPY PLUG					
yn ynen	PL	PI /PO	PI /PTF	PL /PTP	x/0max			
72	13.235	0-91648	0.25472	0.43247	0.72200			
27	16.118	1.1161	0.31022	0.52669	0.52000			
47	12.781	0.88504	0.24598	0.41764	0.91900			
57	10.907	1.3023	0.36196	0.61455	1.0170			
>engt tone	H PPFSSUFF	PATTOS , FLO	N SPLITTEP I	. n.	el de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya del companya de la companya del companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya del la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la			
AD MUND	Pl	PL/PG	PL/PTF	PI /PTP	x/DMAx		مهاليما مرما المحادد	* #* #* * #*** **** *
62	21.415	1.4830	0.41217	0.69979	0.42200			
57	18.413	1.2750	0.3543*	0.60167	0.67000			
APPIT INVA	L PRESSUPE	RATINE . FLO	W SPLITTER F	'. n.				
n Music	PL	PL/PO	PL/PTF	PI /PTP	X/DMAX	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		
77	12.302	0.85187	0. 23676	0.40198	0.50800			
12	17.465	1.2094	0.33614	0.57070	. 0.58303			
92	14.372	0.99525	0.27661	0.46964	0.67000			
ANCIT (NW	L MESSUAL	*******	CTOS CHAPUD					
ID WIPD	71	PL/PO	PL/PTF	PL/PIR-	X/DMAX			
07	14.287	0.98937	0.27498	0.466917	-1.0000			
112	15.273	0.99834	0.27560	0.46618	-1.0090			
122	14.273	0.98634	17.27465					
127	14.397	0.99075	0.27537	0.4663h	-1.0000 -1.0000			
137		0.99765	0.27450	P.46606	~1.0000			
سنفأ	14.218	0. 99454	0.27364	0.46459	-1.0000			
NO AUBO Mustificina	PL PL	RAT <u>ins , f</u> ne %/po	PL/PTF	PI /PTP	x/max			
107	14.287	0.98937	0.27498	0.46687	0.39800			
17	14.273	0.98834	0.27469	0.46638	0.43100	•		
122	14.273	0.98834	0.27469	0.46638	0.44900			
27	14.307	0. 99075	0.27537	0.46752	0.48609			
37	14.263	0. 98765	0.27450	0.46606	0.52200			
142	14.218	0.98454	0.27364	0.46459	0.58800			
192	14:377	3. 99897	10.27720	0.47040	-1.0000			
	14:407		0.2*729	<del>0247070</del>	<del>-1:000)</del>			
		<del>*************************************</del>						
	PL 14.397	7, 49607	0-27-10	PI /PTF 0.47046	X/P#AX -1.0000			الكالة الإرابيات ويهار والمارات المارات والمراب والمراب والمراب والمراب والمراب والمراب والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمرابع والمر
	14.407	0.99766	0. 27729	0.47079	-1.0000 -1.0000	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o		
152		#ATIOS . 20	DEG SHPOUD I	OCATION				
152 157	L PRESSUPE	C - 11 - 2 - 1 - 1 - 2 - 2 - 2 - 2 - 2 -			X/DMAX			
152 157			M /ATC	04 /B TB				
152 157	PL	PL/PO	PI /PTF	PL /P TP				
152 157 >4701TINN VD WORD 167	PL 14.492	PL / PO 0. 99732	0.27719	0.47062	0.79300			
152 157 2001TIGNA VD WORD 167 172	PL 14.492 14.402	M/P0 0.99732 0.99732	0.27719 0.27719	0.47062 0.47062				
VD WORD 167 172 >83311104A	PL 14.492 14.402	PL/PO 9. 99732 0. 99732 PATIOS_, RO	0.27719 0.27719 DEG_SHRPUD_1	0.47062 0.47067 PCATION	0.79300 0.84400			
152 157 VD HORD 167 172 PROTITIONA VO HOPD	PL 14.402 14.402 I PPESSIME	PL/PO 9.99732 0.99732 PATIOS , RO PL/PO	0.27719 0.27719 DEG_SHRPUD_1 PL/PTE	0.47062 0.47067 PLATION	0.79300 0.84400 X/DMAX			
152 157 VD WORD 167 172 0833111098 VD WORD LR?	PL 14.402 14.402 I PPESSIME PL 13.409	PL/PD 0.99732 0.99732 PATIOS_, RO PL/PD 0.92857	0.27719 0.27719 DEG SHRPUD_1 PI /PTE 0.25808	0.47062 0.47062 PLATION PL/PTP 0.43818	0.79300 0.84400 x/DHAX 0.79300			
152 157 VD WORD 167 172 VD WORD 189 VD WORD 189	PL 14.492 14.402 I PPESSIRE PL 13.409 13.205	PL/PO 9.99732 0.99732 PATIOS , RO PL/PO	0.27719 0.27719 DEG SHRPUD 1 PL/PTE 0.25808 0.25415	0.47062 0.47067 PLATION	0.79300 0.84400 X/DMAX			

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HESA-I FUIS	044614	MARY DATA	06/12/79	CADDELL	RFC 10/24/79	93:37:27.848	FAT AVEXT	PG# 5374	Rung 2.2	• •
SANDET FORME	PRESSIBET	PATINS . PRI	MANY PLUG				· · ·		The second second second	
LVD WORD	PL	PI / PO	PI / PTF	PE /PTP	X/D44X					
37	8.1936	0.56146	0.16183	0.30832	0.72203			, in a contrader or sometime.	· · · · · · · · · · · · · · · · · · ·	
37	16.486	1.1427	0. 76991	0.62724	9. 92000					
47	17-619	1.2207	3.39533	0.67034	0.91900		manager of the second		- compression and the second second second	
52	17.594	1.2183	0.39454	0.66901	1-0170					
JANNET INNAL	PRESCUPE	PATINS . FLO	W SM ETTER I	.D.						
VO WORD	PĮ	PI /PO	PI /PTF	P1 /PTP	Y/DMAY			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Contrago description of the Contrago	
£ 2	15.138	1.2567	0.49697	0-69009	0.42200					
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82	14.744	1.0354	0.33530	0.56856	0.58300	••				
92	14.370	0.99560	0.32242	0.54673	0.67000					
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VD WORD	PL	PL/PO	PL/PTF	PLEATE	X/DMAX					
107	14.310	B-09165	0.32108-	0.54445	-1.0000					
112	14.310	0.99145	32109	0.54445						
122	14.300	10000	9.32946	0. 54497	-1.0000					
127	14.332	0.99283	0.32153	0-54521	-1.0000	9 9				~
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177	14.390	9.9969R	9.322 <b>87</b>	0.5474#	0.74400		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of 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187	13.476	0.93370	0.30238	0.51273	0.79300					
197	13.271	0.91952	0.29774	0.53494	J. 84490	* * * * * * * * * * * * * * * * * * * *	,	and the second second second		
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	32	12.954	9.83465	0.33415	0.56219	0.72200									
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	47	15.743	1.0901	0.43640	0.73423	). 91 900									
	57	15,937	1.1035	0.44179	0.74331	1.0170	er in det de finder in net de de des enterprises de la comprese de de enterprises de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese del la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese del la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese del la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese del la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese del la co								
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	-107	14.350	3.99363	0.39789	0.66929	-1.0000									
<b>O</b>	112	14,350	0.09274	0.39752	0.66892	-1.0000									
_	-17?	14.335	2-04267	n. 99238	0.66859	-1.0000									
-	-127	14.353	1.99399	0.39794	0.66952	-1.0000									
	-137	14. 120	0.99156	0.39697	0.66789	-1.0000	To the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of th								
	-152	14.270	0.94611	0.39558	0.46556	-1.0000_									
	AVD WORD 197 117	PL 14.350 14.340	PL/PN U.99363 U.99294	PL/PTF 0.79780 0.39752	PL/PTP 0.66929 0.66882	X/DMAX 0.39800									
	122	14.335	7.99260	0.3973	0.66859	0.43100									
	127	14. 355	7. 79398	2,39794		0.44900 0.49600									
	127	14.320			0.66952										
	147		0.99156	0.79697	0.66789	9.52200									
	<del></del>	14.270 14:41 <del>0</del>	7.98811	0.39458	0.66556	3.5000	A A - Grand a state and of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the								
	-144	14:415	7479023		<del>- 0.47200</del> -	-1.0000 -									
		-													
	AVP WITER	PL	PI/PU	-	PL /PTP	x/DMAX									
	-152	14.510-	17. 9977A	0.30066	9-6720A	-1.0000									
		14.415	0.99813	0.39960	0.67231	-1.7090									
	>คากรารากษ	AL PRESSUPE	RAYINS 1 20	DEG_SIMPPLID_I	DCAT ION										
	AVP MOPD	Pl	P4 / P1	PL /OTF	PL /PTP	X /DMAX	A company and control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control								
	167	14.415	0.99513	0-30010	0.67231	J. 79300									
	177	14.415	0-99813	0.39960	0.67731	0.84400	grammer in the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second stat								
	>Analition	AT PPESSUPE	PATING & RO	DEG SHPCHIN I	UCAT ION										
	AVD SUPD	PL	PL/PN	, PI /PTF	PL/PTP	Y/DMAY	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s								
*	182	13.607	0.94214	0.3771#	0.63460	0.79300									
	187	13.477	ე" 9297D	0. 27220	0.62627	0.84400	والمراقب المراقب		. >rntjin s . 4f-31 572.		THRUST PAPAM	IFTFPS Stamm to 1.7	7710 5740	F 0.090650	nsp 6,927770

NASA-I FUTS	PRFLIM	HARY DATA	06/13/79	CADDELL	PFC 10/24	/79 03:42:04.953	FAC SECTI	PGM C034	RNG 1358
JAMDI TICOAK	DOESSIJRE	PATINS . PP	TANDA DI IIC						
VO HORD	PI	PL /#I	PL/PTF	PI /PTP	X/DMAY				
32	13.961	0.94566	0.46230	0.77561	0.72200				
37	14.799	1.0236	0.49006	0.82218	9. R2000				
47	15.048	1.0409	0.49832	0.83604	0.91900				
52	15.148	1.0478	0.50162	7.84158	1.0170				
JAMOIT FORAC	PRESSIME	PATINS , FLE	W SPLITTER I	. n.		<del></del>			
	••	~	M /PTF	PL /PTP	XICMAX				e e e unit qu'estante la jant de la la quipalité de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la com
AD MUBU	PL	PL/PN							
62	14.569	1.0078	0.48246	0.80943	0.42200		* * ****		
47	14.135	0.97773	0.46P0P	0.79531	0.67000				
>ADDITIONAL	PRESSIME	RATIOS . FLO	W SPLITTER C	.n.					
VB WOPD	PL	PL/PIT	PI /PTF	PL /P TP	XAMAX	· ·	1. 100 (a <del>ppendi</del>		in the same where the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and
77	12.369	0.85556.	. 0.40959	0.68718	2.50500		· · · · · · · · · · · · · · · · · ·		
92	16.660	1.1523	0.55167	0.92556	0.58300				
92	14.510	0.99672	0.47717	0.80056	2.67000				
<u> 100017 10004</u>	PPESSURE	847105 v EUL	670P SHRBUD	<del>,</del>		er a manager of the second of the second of the second of the second of the second of the second of the second			. <del> </del>
O SON ON	PE	PL/P3 .	PL/PTF	PLARTE	X/DMAX .				
197	14-375	99430	0.47601	0.79862	-1.0000	en commendad rest e com com com en en en			
		0-97301	-0.57568	0.79806	-1.0000				
112	14-365					<del></del>			<del></del>
122	14.355	0.5234	7.43535	0.79751	-1.0000				
127	14.375	0.99420	0.47601	0.79862	-1.0000	ne again i carage e again a como a como e acomo e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e como e c			
137	160334	0.99154	0.47469	0.796-0	-1.0000				
142	14.269	0. 99636	0.47221	0.79224	-1.0000	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			<del>,</del>
ALPOLITICOAS	PRESSURE	PATIOS . FOR	ENCOY INLET	···					
VO 4080	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX .				
177	14.375	2.99433	2.47601	0.79867	0.39R00				
112	14.365	9.97361	0.47569	0.79806	9.43100		· · · · · · · · · · · · · · · · · · ·		
122	14.355	0.99292	0.47535	0.79751	0.44900				
127	14-375	0.99432	2.47601	0.79862	0.58600				
137	14.335	2. 99154	0.47460	C.79640	0.52200				
142	14.269	0.98636	7.47221	9.79224	0.56800				
192	-14.425		9,47766	-0.00139	-1.0000	•			
197	14.427	-0,09741-	<del> %47750</del> -		-1-0000				
49011104A	- enessine	PATION: - FAR	MORRIE FLAR			<u>.                                    </u>			
			PL / DTF	PL/PTP	X/DMAX				
162	PL 14 425	0-99775	0.41766	0-80139	-1.0000				
157	14.425	0. 99741	0.47750	0.40111	-1.0000				
			DEG SHPTUD L			<b></b>	and the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of th		
VN 40PN	Pt 14 425	ሚ/PO 0.99775	PL /PTF 0.47766	P[ /PTP	X/DMAX 0.79300				
167	14.425			0.80139					
172	14.475	0.99775	0.4*766	C. #0139	9.84400			Marie Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commission of the Commis	
Jairol & Loug	baédZñbé	RATTOS 40	DEC SHROUD I	ULATION					
NO MUSD	PL	PL/PR	PI /PTF	PL/PTP	X/DHAX				
	13.721	0.94909	9.45437	C.76271	0.79300	• • • • • •			
	130121								
187	13.571	2.94012	0.45007	0.75510	J.84400				

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VASA-LEWIS	PRFE 14	INCRY DATA	06/13/79	CADDELL	REC 19/24/7	9 07:44:21.133	FAC WAVAI	P64 6734	RUN LZ
>470   T   ION	I PRESSIBE	RATIOS . PPI	MAPY PLUG						<u>-</u>
IVO WOPO	PL	PI / PA	PL/PTF	PL /PTP	X/DMA X				
32	14.219	3. 99237	3.54614	0.92186	J. 72200				
77	14.450	0.99941	0.55573	0.93806	3. 42000			-	
47	14.554	1.0967	0.55937	0.94421	0.9100				
£2	14.594	1. 2282	C. 56090	0.94689	1.0170				- <del></del>
>ADDITIONA	IL PRESSIPE	RATIOS , FLO	W SPLITTEP 1	'.n.					
AVD WORD	PL	PL /PO	PL / PTF	PI /PTP	x/DMAX				
52	14.349	0.99134	0.55113	0.93029	0.42200				
67	14.230	0.99375	9.54691	0.92317	0.67000				
>ATT IT TON	L PRESSURE	PATINS , FIR	W SPLITTER O	·.n.		· · · · · · · · · · · · · · · · · · ·			
AVO MURO	PL	PI /PT	PI /PTF	PI /PTP	X/DMAX				the same same comments of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the
77	12.544	0.86716	9-49209	0.91376	0.50800				
82	15.966	1.1938	0.61363	1.0358	0.54300				
92	14.415	0. 99651	0.55400	0. 93515	2.67202	· · · · · · · · · · · · · · · · · · ·			<del>~</del>
14001710W	A-PRESSURE	RATIOS y EJE	cto suppup	<del></del>				and the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contract of the second contrac	
AVD WOPD	P	PL/P0	PL/PTF	PL/PTP	X/DMAX.				
-107	14.390	0.99478	J. 55304	0.93353	-1-0000				
-112	14.380	0.99509	-0. 25266_	0.93288	-1.0000				
-122	14.375	0,99375	7.55247	0.93256	-1.0000	****			
-127	14.390	0.94579	0.55304	2.93353	-1.0000				
-137	-14:155	0.99237	0.55170	0.93126	-1.0000				
-142	14.275	0-98685	0.54863	0.92698	-1-9000				
SADDITIONS	<u>L PRESSUPE</u> PL	RATIOS . FOR	PL/PTF	PL/PTP	x/DMAX				
107	14.390	0.99475	0. 55304	0.43353	0.39800				
112	14.380	9.99479	0.55266	0.93288	0.43100				
122	14.375	0. 99375	0.55247	0.93256	0.44900				
127	14.390	0.99478	0.55704	0.93353	0.48600				
127	14.355	0.99237	0.55170	0.93176	0.52200				
142	14.275	9. 98685	9.54963	0. 52604	0.58800				
-157	14:435	<del></del>	9.55477	7.43/44					
-143	144439		9.55459	0.93612					
HN1 11004	t- establish	******	MOTTIE FLAS	<u> </u>					
4VN ພጥቃበ	PL	PI /PI	PITTE	el /PTP	Y/DMAX				
-157	16-434	7. 99789	0. 25477	0.93644	-1.0000				and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th
44	14.430	7.09754	0.55458	0.9617	1-0000				
>Anni tinna	L PPESSURE	PATINS , 20	NEG SHPNUD L	DEATION		·····			
AVO WOPD	<b>≠</b> L	PI /PT	PL /PTF	PL/PTP	Y/NMAX				
167	14-430	0.99754	0.55458	0.93612	0.79300				
172	14.475	0.99720	7.55430	0.93579	0.84400				and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
	L PRESSURE	PATERS_1, RO	DEG SHPNUM L	OCATION .			<del></del>		
>APPIT TOPA	Pt.	Pt / PT	PL / PT F	PI /PTP	x/fmax				
			0-53176	0.89760	0.79300		· · · · · · · · · · · · · · · · · · ·		
AVP WEDD		0, 95650	0-7110						
	13.836	0.95650 0.95029							
AVD WEDD Imp	13.836 13.746	0.95650 0.95029 Thrist Papan	0.52831	0.80178	0.84400				

		MARY DATA	06/13/79	CADRETT	REC 10/24/7	9 N3:45:37.546 FAC 4X6X1 PGP C034 PNG 1360
>4 201 T 10%	AL PRESSIBE	PATIOS . PEI	MAPY PLUG			· · · · · · · · · · · · · · · · · · ·
vo woko	PI	PI / PO	PL/PTF	PI /PTP	X/DMAX	
עאויא ניע 32	14.210	0.98328	0.54757	G.92124	u.72200	
32 37	14.459	1.0005	0.54718	0.93741	0.82000	
.7	14.544	1.0064	0.56045	0-94290	0.91900	
5 <b>2</b>	14.584	1.0392	0.56198	C.94549	1.0170	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t
72 		1.9376	*** 36174		1.0170	
40017104	AL PRESSUPE	PATTOS . FLO	W SPLITTEP I	.n.		
/ก พก⊅ก	PL	Pt /PO	PI /PTF	PL /PTP	X/DMAY	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
2	14.319	0.99068	0.55180	0.92835	U. 42200	
57	14.225	0.98432	0.54814	0.92271	0.67000	
ADDETERN	AL PRESSURF	PATIOS . FLO	M SPLITTER C	.0.	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	
IN WOPD		m /20	PI /PTF	PL /PTP	v / file A	
	PL	PL/PN			x/OPAX	
17 	12-518	0.86625	0.48240	0.81159	0.50000 .	
12	15.976	1.1055	0.61561	1.0357	0.58300	
?2	14.409	<u> </u>	0.55526	0.93417	0.67000	
4001710W	AL PRESSURE	NATIOS - CUE	CTER SHADUS	<del></del>		
IN MURD	71-	PL/PO	PL/PTF	PLEATE	X/DHAX.	
07	14.394	0.90436	0.55629	0.93256	-1.0000	
12	14,379	0.97502	0.55610	0.93223	-1.0000	
22	14.374	_0,49467	0-55191	0.43141	-1.0000	
27	150279	0.99502	0.55410	0.93223	-1.0000	
37	14.354	0. 99329	0. 55314	0.41042	-1-0000	
92	14.275	0.98777	0.55007	0.92544	-17-0000	
/D_HORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
107	14.384	0. 99536	0.55429	0.93256	0.39800	•
107 112	14.384	0. 99536 9. 99502	0.55429	0.93256 0.93223	0.39800	
107 112 127	14.384 14.379 14.374	0.99536 9.99502 0.99467	0.55429 0.55410 0.55391	0.93256 0.93223 0.93191	0.39800 0.43100 0.44900	
107 112 12? 127	14.384 14.379 14.374 14.379	0.99536 9.99502 0.99467 0.99502	0.55429 0.55410 0.55391 0.55610	0.93256 0.93223 0.93191 0.93223	0.39800 0.43100 0.44900 0.58600	
107 112 127 127	14.384 14.379 14.374 14.379 14.354	0.99536 9.99502 0.99467 0.99502 0.99329	0.55479 0.55410 0.55391 0.55410 0.55314	0.93256 0.93223 0.93191 0.93223 0.93062	0.39800 0.43100 0.44900 0.52200	·
107 112 127 127 137 142	14.384 14.379 14.374 14.379 14.354 14.275	0. 99536 9. 99502 0. 99467 0. 99502 0. 99329 0. 98777	0.55479 0.55419 0.55391 0.55510 0.55714 0.55007	0.93256 0.93223 0.93191 0.93223 0.93062 0.92544	0.39800 0.43100 0.44900 0.52200 0.55800	
107 112 12? 127 137 142	14.384 14.379 14.374 14.379 14.354 14.275	0. 99536 9. 99502 0. 99502 0. 99502 0. 99329 0. 98777	0.55429 0.55410 0.55391 0.55510 0.55314 0.55007	0.93256 0.93223 0.93191 0.93223 0.93062 0.92544	0.39800 0.43100 0.44900 0.5200 0.5200 0.58000	·
07 112 22 27 27 37 .42 53	14.384 14.379 14.374 14.379 14.354 14.275 14.474	0. 99536 9. 99502 0. 99467 0. 99502 0. 99329 0. 98777 0. 99613	0.55429 0.55410 0.55391 0.55391 0.55314 0.55907 0.55907	0.93256 0.9323 0.93123 0.93191 0.93223 0.93062 0.92544 0.93962	0.39800 0.43100 0.44900 0.52200 0.55800	
07 112 22 27 27 37 .42 53	14.384 14.379 14.374 14.379 14.354 14.275 14.474	0. 99536 9. 99502 0. 99502 0. 99502 0. 99329 0. 98777	0.55429 0.55410 0.55391 0.55391 0.55314 0.55907 0.55907	0.93256 0.9323 0.93123 0.93191 0.93223 0.93062 0.92544 0.93962	0.39800 0.43100 0.44900 0.5200 0.5200 0.58000	\$ <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del>
107 112 22 27 27 37 442 53 54 54 57	14.384 14.379 14.374 14.379 14.354 14.275 14.474	0. 99536 9. 99502 0. 99467 0. 99502 0. 99329 0. 98777 0. 99613	0. 55479 0. 55419 0. 55391 0. 55391 0. 55510 7. 55314 0. 55007 7. 57363 0. 77363	0.93256 0.9323 0.93123 0.93191 0.93223 0.93062 0.92544 0.93962	0.39800 0.43100 0.44900 0.5200 0.5200 0.58000	\$ <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del>
107 112 22 27 27 37 49 49 53 53 54 57	14.384 14.379 14.374 14.379 14.354 14.275 14.474 14.419	0. 99536 9. 99502 0. 99502 0. 99502 0. 99777 0. 99777 0. 99778	0.55419 0.55419 0.55391 0.55314 0.5507 0.55314 0.55087	0.93256 0.93223 0.93191 0.93223 0.93062 0.92544 0.93902	0.39800 0.43100 0.44900 0.52800 0.52200 0.55800 -1.0000	\$ <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del> <del>\$</del>
107 112 22 27 37 42 42 53 40017 10W	14.384 14.379 14.374 14.379 14.354 14.275 14.474 14.419	0. 99536 9. 99502 9. 99467 0. 99502 9. 99329 9. 99777 9. 99615 0. 99778	0. 55479 0. 55419 0. 55391 0. 55391 0. 55510 7. 55314 0. 55007 7. 57363 0. 77363	0.93256 0.93223 0.93191 0.93223 0.93062 0.92544 0.93982	0.39800 0.43100 0.44909 0.52200 0.52200 0.52800 -1.0000	
107 112 127 27 27 37 42 42 53 57 ADDLT FOW IN MPPD 52	14.384 14.379 14.374 14.379 14.354 14.275 14.474 14.419 M. PRESSURE. PL 14.424	0. 99536 9. 99502 0. 99467 0. 99502 9. 99329 0. 99777 0. 99613	0. 55479 0. 55410 0. 55391 0. 55391 0. 55314 0. 55007 0. 55383 0. 77784 0. 77784 0. 77784 0. 77784	0.93256 0.93223 0.93191 0.93223 0.93062 0.92544 0.93514 0.93514 0.93514	0.39800 0.43100 0.44400 0.52200 0.52200 0.52800 -1.0000	
107 112 127 27 37 42 42 53 49017 10W	14.384 14.379 14.374 14.379 14.354 14.275 14.444 14.444 14.424 14.424	0. 99536 9. 99502 0. 99467 0. 99502 9. 99329 9. 99777 0. 99613 9. 99778 PATIOS 20	0. 55479 0. 55410 0. 55391 0. 55314 0. 55007 0. 55007 0. 55007 0. 55007 0. 55507 0. 55507 0. 55507	0.93256 0.93223 0.93191 0.93223 0.93062 0.92544 0.93914 0.93982 PL/PTP 0.93514 0.93482	0.39800 0.43100 0.43600 0.52200 0.52200 0.58800 -1.0000 -1.0000	
107 112 127 27 37 462 57 40017 10W	14.384 14.379 14.374 14.379 14.354 14.275 14.474 14.419 M. PRESSURE PL 14.424 14.424 14.474 PL PRESSURE	0. 99536 9. 99502 0. 99467 0. 99502 0. 99777 0. 99613 0. 99778  E47105	0. 55429 0. 55410 0. 55311 0. 55314 0. 55007 0. 55707 0. 55709 0. 55709 0. 55709 0. 55564 0. 65509 0. 65509 0. 65509 0. 65509 0. 65509 0. 65509 0. 65509 0. 65509 0. 65509	0.93256 0.93223 0.93191 0.93223 0.93062 0.92544 0.95914 0.93962 PL/PTP 0.93514 0.93682	0.39800 0.43100 0.44900 0.5220 0.5220 0.58800 -1.0000 -1.0000 1.0000	
107 112 127 127 127 137 142 142 157 149 157 169 169 169 169 169 169	14.384 14.379 14.379 14.379 14.354 14.275 14.474 14:419  PL 14.424 14:410  PL 14.419	0. 99536 9. 99502 9. 99467 0. 99502 9. 99329 0. 98777 9. 994813 0. 99778  RATIOS	0. 55479 0. 55410 0. 55391 0. 55314 0. 55007 0. 55308 0. 55007 0. 55589 0. 55589 0. 25589 0. 25589 0. 25589 0. 25589 0. 25584	0.93256 0.93223 0.93191 0.93223 0.93062 0.92544 0.93916 0.93982 PL/PTP 0.93514 0.93682	0.39800 0.43100 0.44909 0.52200 0.52200 0.52800 -1.0000 -1.0000 1.0000 1.0000	
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กษณะก	PL	95 / PO	PI /PTF	24 /PTP	X /DHA X					
67	14.474	0.09674	0.36347	0.61397	9.79300					-
77	14.479	1. 99 709	0.36359	0.41418	0.84400		and the second according			
ADDITION	L PRESSURE	PATINS , BN	DEC SHPOUR I	OCATION						
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n waen	P(	PL / PG	Pt /PYF	M /PTP	X /DMAX				The second of the second of the second	
A7	13,590	0.93976	0.34269	3.57887	0.79300					
A7	13.391	0.97464	0. 33 791	n=5707 <del>9</del>	0-84400			and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	and the second and the second of	
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APPITTONA	f bbeccibe	PATIOS . PRI	MAPY PEUG					- · ·	
UB WURD	Pl	M /PO	PI /PTF	PI /PTP	*/OMAX			· · · · · · · · · · · · · · · · · · ·	
2	9.4725	0.65628	9-19807	9.33645	J. 72200			and the second	
7	14.293	J.09028	0.75987	0.50768	0.02000				
.7	18-275	1.2523	0.37795	0.64199	0-91900		Man F 11 F		
\$2	14.175	1.2592	0.38003	0.14553	1.0170				
AND TECNA	L PRESSIPE	PATINS . FLO	W SPLITTER I		от — — Метор очино Истологийн Иббиг и осий голин үзэр отхицогийн улсын харбаар харбаар үүд				
ባቁበዙ ሲነ	PL	PI / PO	PI / NTF	PI /PTP	x/pmay		- ·	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	
2	19-586	1.3570	0.40955	0.69568	0-42200				
.7	16.918	1.1721	0.35275	7. <i>€</i> 7088	J. 67000				
APOTT TOMA	PRESSIME	PATINS . FLO	W SPLITTEP P	. n.					
n wash	PL	P( / P()	PL / PT F	PI /PTP	x/DMAX	THE PERSON NAMED IN COLUMN TWO	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	***************************************	
17	11.294	0.78250	. 0.23617	. 0.40116	0.50800	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
2	16-200	1-1085	0.33455	0.56#7#	0.56300				
2	14.368	0-99547	0.30044	0.51033	0.67000				
4001 <u>1 104</u> 8	<del>L-PRESSURE</del>	PAT105 y Edit	CTOP SHPEUD			and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t			
ID HORD	PL	PL/PO	PL/PTF	PLEED	X/DMAX.	And the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			
97	14.293	0-99029	0. 29982	0. 50769	-1.0000				
12	14.278	3.99929	2.29856	0.50714	-1-0000				
22	14.243	7.98449	0.29462	0.50732	-1.0000				
27	14.300	0.99132	0. 29019	50021	-1.0000				
37	_44.7.73	7.98A9A	0.29846	0.50657					
42	14.230	J. 98648	0.29773	0.50573	-1-0000				
ADDITIONA	L PRESSURE	RATIOS . FOR	ERCOY IMLET	<del>, , , , , , , , , , , , , , , , , , , </del>					
D MUND	PL	PL/PO	PL/PTF	F_/PTP	X/DMAX	in in the part of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of		الماران المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراج	
<b>)</b> 7	14.273	0.99028	0.29887	0.50768	0.39800	•			
17	14.278	J. 98925	0.29856	0.50714	0.43109				
<b>2</b> 2	14-293	7.98959	0.29#67	0.50732	7.44 <b>90</b> 0				
27	14.338	J.99132_	0.29910	0.59P21	2.48600				
37	14.273	g. 98 896	9. 29946	0.50497	0.52200				
42	14.238	0.99648	0.2977?	0.50573	0.58909				
<del>43</del>	14+393	<del></del>	0.20096	0.21177	<del>-1.9000</del>				
47	t+ <del>790</del>	<del> 93 754</del>	<del>0. ?0107</del>	0.51140	-1.0000				
4 <u>0-4-7-40.94</u>	L PPESSURE	PAT175 _ FAM	MEERLE FLAT						
U AUBU	PL	PL/PO	- ALPTE	PL/PTP	X/OMAX	. A grant was a second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the		-	
52	14.393	J.99720	90006	A-51122	-1.0000				
.57	14.174	ŋ <b>. 99</b> 754	0. 30107	0.51140	-1 annoo				
APPET FORA	L PRESSURE	RATIOS 20.	NEG SHPTUD I	CAT ION					
n weed	PL	PL/PG	PĮ /PTF	PL /PTP	Y/DMAY			ya . Min ngan maja salam salah sa Andri Mandalam salah salah sa	
<i>(</i>	14.393	0.99720	V-500eV	0.51122	0.79300				
172	14.393	9.99770	9.30096	0.51122	0.84400			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
APPLI A LOUY	L PRESSUPE	RATIOS , RO	NES SHPRUN I	DCAT TON					
P 40PB	PL	P( /PO	M /PTF	PL/PTP	XAMOLX				
	13.465	7. 93 290	0.28156	0.47826	0.79300				
	10.400								
ρ7 ρ7	13.260	0. 91 872	0.27729	0.47000	0.84400				

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>400TT FONA	PRESSIPE	PATINS . PP	MARY OF UG				•		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
<b>ል</b> ስኮ ጣርቀይ	PL	Pt /PD	PL /PTF	PL /PTP	Y/OMAX				
32	9.3299	0.64631	2.19543	0.33101	J. 72200				
27	14.257	0.98759	9.79864	0.505#0	O.#2000				
47	19.379	1. 2524	0-27870	0.64140	0.91900				
<b>~</b> ?	18.193	1.2673	7-78110	9.64547	1.0170				
SAUDIT TONA	PRESSUPE	RATIOS . FLE	W SPITTER I	i., n.,		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon			
AVD WORD	Pl	Pt /PN	PI / PTF	91 /PTP	F/DMAX			• .	
62	19.629	1.3592	9-41109	C.69610	0.42200		and the same of the		
67	16.926	1.1725	2. 35456	0.69351	J.670G3				
APPET TONAL	PRESSIME	PATINS . FLE	M SPITTEP F	`• ?•					
AVD HOPD	PL	PL/PR	PI /PTF	PL /PTP	X/D4AX				- Caller - miller ridget var intrinstrukt - Laure trinspression var vivi
7"	11.262	0.78015	0.23591	0.39955	0.50800				
<b>A</b> 2	15.949	1.1062	0.33449	0.56652	0.58300				
92	14.366	2.99520	0.32093		0.67900		<del></del>		
redit there	- PAESCURE	*41105 . EJE	CTOP SHOUD	<del> </del>			n one out the second of the second participal with the second		e le con establishes establishes que che c
AAD AUBD	PL	PL/PO	PL/PTF	PL/PIP	X/DHAX		contact the amount that the amount of the formation		-
-197	14.291	0-99001	0.29937	7.30704	-1.0000				
-112	14.291	2.98932	0.20916	0.50668	1.0000				·
-122	14.291	0. 98932	0.70016	0.50668	-1.0060				
-127	14.306		0.2996	0-50757	-1.0000				
-137	15-246	0.98828	0.29884	0.50615	-1.0000				
-142	14. 232	J. 98587	0-20411	0.50491	-1.0000				<del></del>
>4001TIONA	PRESSURE	PATINS . FOR	FRITTY IN ET						
AVD WORD	PL	PL/PR	PL/PTF	PL/PTP	x/D=4x				
107	14.291	0.99001	0.29937	0.50704	0.39800				The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
112	14.741	0. 98937	9. 29916	0.57668	0.43100				
127	14.241	0.98932	0.29016	0.59668	0.44903				
127	14,396	0.99105	0.29968	9.59757	0.48690				
127	14. 766	0. 98979	3.29884	0.50615	0.52200				
142	14.232	). 9P 5P 7	9.29411	0.50491	0.58800				
-142	14.391	<del></del>	<del>0.39146-</del>	9:51058	-1.0000				
-157	-14:391	- 0; 99695 -	0. 37146 -	0.41654	-1.0000		may , or helder quality payments and an incidence of the second		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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-157	14.391	7.99693	0.30146	0.51058	-1.0000				
157	<b>-14.37</b> 1	0. 99603	0. 20146	C- 41048	1-0000			*	the head control of the control of the control of
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167	14.391	0.09693	9.70146	0.51058	0.79300				
177	14.391	)* <del>a</del> a9c3	9. 39146	0.51058	0.84400		·		AND THE OWNER, MAKE MAY WANT IN THE
>ATTITITES	PRESSIBE	PATTINS , RO	NEG SHRPUN I	DESTION					
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	17.463	7.93263	0.28201	0.47764	J. 79300				
102									
187	13.244	3.91776 THPIST PAPAM	9.77757	0.47003	J.84400				

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		PATENS . PPT	_						
VO WOPD	PL	PL/PN	PL/PTF	PI .'PTP	x/D=AX				
22	11.823	0.81924	0.29855	0.50534	0.72200			and the second second second second second	sample states and any
97	14.941	1.0353	0.37729	0.63866	0. # 2000				
47	16.174	1.1297	0.40840	0.69133	J. 91 9JJ				and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th
5?	16.439	1.1390	0.41508	0.70263	1.0170				
APPET FOR	PRESSUPE	RATIOS . FIR	M CAFTALES I	.n.					
IN WOPD	PL	PL / PO	PI /PTF	PL /P TP	X/DMAX				., ,
52	15.969	1.1065	0.4032-	0.68258	0.42200				المواقعة بسعامها والإسارية المقد
57	13.160	0.91190	0.33257	0.56253	0.67090				
AND T TONAL	PRESSIDE	RATIOS . FER	W SPEITTEP F	. D.	ga an annaga an 1990 Million — Malainthig Sanashagaghtan ang ar 1990 Million				
vn wnen	PL	PL / PG	PL /PTF	PI /PTP	X/DMAX		· w comme 415	· · · · · · · · · · · · · · · · · · ·	management - units contragation for a settle of
77	9.1334	0-63286	0.23063	0.39040	0.50800				
ż	18.957	1.3135	0.47868	0.81029	0.58300	<del>-</del>			
92	14.383	0.99659	O_36218	0.61478	0.67000				
POSTI IUMA	PRESSURE	84 <del>7105 v Edf</del>	ETOP SHROUD			er mer i			
VP WOPD	PL	_ PL/PG	PL/PTE .	PL/230	X/DMAX				
107	14.333	0.99313	0. ?6192		-1.0000				
112	14.323		-0.3E167	0.61222	-1.0000				
177	14.323	0.99244	0.36167	0.61772	-1-0000				
127	14.343	- 0.99392	0. 36217	7051307	-1.00.0				
137	14.318	0.00213	0.76154	10510.0	-1.0000				
142_	14.269	0.98864	0.36028	0.60987	-1.0000				Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Marine Ma
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VD MORD	PL	PL/PO	PL/PTF	PL/PTP	X/DHAX				
137	14.333	0.99313	0.36197	0.61265	0.39800		•		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
112	14.323	0.99244	9-36167	0.61222	0-43100				
127	1 +- 323	7.99244	0.36167	0.61772	0.44900				
127	14.353	2.99382	0.36217	0-61307	0.58600				·
137	14.319	2.99713	0.36154	0.61701	0.52200				
142	14-269	0.98864	0.3602*	0.60987	J. 58203				
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<del>  5  </del>	140493	<del>-9₆ 99</del> 797	Po 36364 -	0.61563	-1.0000				Andrewson was remarked through a series of the A
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32	11.995	2. 82982	0.33169	0.5565?	0.72200	
7	14.974	1.0290	0.41130	0.60061	3. 02030	
7	15.737	1.0887	0.43516	0.73669	0.91900	
2	15.942	1. 1029	0.44097	0.74019	1.0170	
MOTTECE	AL PRESSUPE	PATINS , FEE	W SPLITTEP	.n.		
0 4090	PL	PI / PO	PL/PTF	PI /PTP	X/DHAY	
2	14.894	1.0242	0.40936	0.69737	0.42200	المورد الموادد الموادي الموادي الموادي الموادي الموادي الموادي الموادي الموادي الموادي الموادي الموادي الموادي
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D WORD	PL	PL /PI)	91 /PTF	PL /PTP	X/DMAY	e de descrito e e a descritor e como es como e
7	8.2311	9.56736	0.22677	0.38078	0.50800	ட்ட நடைபட்டார் நடையும் இட்ட முறுவூர் பார். விறை வரை மான்ற ஆற்ற முற்ற நடையும் முறி பார்க்க அடியில் கட்ட ந
7	20-921	1.4494	0.57573	0.96673	0.58300	
2	14,390	0.99553	9.39791_	0.66214	161990	
CONTRACT	<del>le par ssurf</del>	44 <del>5145 , 646</del>	CTOR CHROUD	<del></del>		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
D HUBD	The	PL/PO	PL/PTF	PLEBTO	X/DMAX	
07	14.347	J. 9920A	0.39653	0.665A3	-1-0900	
12	14.335	0.79133	0. 39639	0.66559	-1-0000	
77	14.335	2-20177	39639	0.66559	-1.0000	
27	14.322	0.99777	3. 39671	0.66629	-1.0020	
37	14.325	0.99104	7.39612	0:04513	-1.0030	
32	- 14.275	0. 98759	0.39474	T8584.0	-1,0000	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
<b>VODIT TOR</b>	AL PRESSURE	PATIOS . FOR	EULA THEE			
D HUND	PL	PL/PN	PI /PTF	PLIPTP	K/DMAF	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
27	14. 140	9.99208	0.39653	0.66583	0.39007	•
12	14.335	9.90173	0.30639	0.66559	0.43100	y company or any and the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of
77	14.335	0. 99173	0.39639	0.66559	0-44900	
21	15.352	9-99277	0.396 91	0.66629	0.48630	
?7	14.325	3.99104	0.39612	0.66513	0.52200	
47	14.275	0. 98759	0.39474	0.66781	0.58800	TALL IN STATE OF THE SHEET OF THE PROPERTY WAS AND AND AND AND ADDRESS OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE
67	<del>- 14,495 -</del>	<del></del>				
mans Fr Tings	PL		• <del>• • • • • • • • • • • • • • • • • • </del>			
		0.99656	PI /PTF		X/2#3X	
				0.66884	1.9900 	
52	14.495		3 30044			
5? 57	14.475	0. 9960 T	1) , 30846	0.66007		- while a second on the grade department of the course of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the
5? 57 497[T][0%	14.475	0.99691	DEG SHAUD T	DCATION		
57 57 EDDITION	14.435 14.410 IL PRESSURE Pi	#ATENS 1 20 #L/PD	DEG SHPOUD (	DCATION PL/PTP	x/DMAX	
D WNPD	14.495 14.410 N. PRESSURE Pi 14.400	PATIOS , 20 PL/PO 0.99622	DEG SHPOUO L	PL/PTP O.66P61	x/DMAX J. 79300	
52 57 800   T T T T T T T T T T T T T T T T T T	14.495 14.410 AL PRESSURE Pi 14.400 14.430	# /PO 0.99622 0.99622	DFG SHPOUD L P1 /PTF 0.39819 0.39819	PL/PTP O.c6861 O.66861	x/DMAX	
52 57 8001110N/ 0 WOPD 67 72	14.495 14.410 AL PRESSURE Pi 14.400 14.430	# /PO 0.99622 0.99622	DEG SHPOUO L	PL/PTP O.c6861 O.66861	x/DMAX J. 79300	
52 57 #03[T][0NI 0 WOPD 67 72 #03[T][0NI N WOPD	14.405 14.610 AL PRESSURE PI 14.400 14.470 AL PRESSUPE	# /PO 0.99622 0.99622 PATINS , RO PI /PO	DEG SHPOUD 1  PI /PTF  O. 39P19  O. 39P19  DEG SHPOUD 1	DEATION  PLIPTP O.CORCL O.GGRGI OCATION  PLIPTP	#/DMAX J. 79300 9.84400	
52 57 ADDITION D MOPD 67 72 ADDITION D MOPD #2	14.405 14.610 AL PRESSURE Pi 14.400 14.400 AL PRESSURE PL 13.597	# /PN 0.99622 0.99622 PATINS , NO PI /PN 0.94064	DEG SHPOUD 1  PI /PTE 0.39819 0.39819  DEG SHPOUD 1  PI /PTE 0.37597	PL/PTP O.66861 OCATION  PL/PTP O.63131	*/DMAX J. 79300 9.84400 */DMAX J. 79307	
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ነኮ ዛበቃቦ	PL	Pt / PF	PL/PTF	PL /PTP	X/DMAX	
32	13.932	0.96425	0.53445	0.77613	0.72200	
17	14.716	1.0145	7. 56453	0.81981	0.82000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
7	14.940	1.0341	0-57315	0.83232	J. 91900	
52	15.030	1.0403	0.57660	0.83733	1.0170	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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MPT TECOM	AL PRESSURE	PATTINS . FLE	M CH ITTER I	· u•		
O NORD	Pl	Pt /PO	DEFPTF	PI /PTP	XJDMAX	
?	14.566	1.0381	0.55878	0.81146	<b>9.</b> 42200	
<b>57</b>	14.156	0.97980	0.54307	0.78865	0.67000	
MOD TEOOR	AL PRESSUPE	RATIOS . FLO	M COLITTED O	.n.		
n when	PL	PI /PI	PL / PTF	PL /PTP	X/DMAX	
7	12.568	0. 86 989	0-48215	0.70018	0-50800	
12	16.024	1.1091	0.61471	0.79768	0.58300	
2	14.406	0.99708	0. 55265	0.00256	0.67000	
427171CN	AL-PRESSURG	******* <del>* Ed</del>	CTOP SHADUD			
D WORD	PL	PL/PO	PL/PTF	P1_40-75	VARMAN	
10 WURU 197	14.371	0.99466	0.55131		X/DMAX	***************************************
12	14.371	0.99666		0.80061	-1.0000 -1.0000	
22	14.365	0.33505_S	20-5112	0.89033	-1.0000	
.27	14.374	0.99501	0,55150	6-80089	-1.0000	
37	14.346	0. 99 294	0. 55035	0.79577	-1.0000	
4	14.271	3.98775	0.54748	0.79505	-1.0099	
				4412505		
SAUSTITUM	IL PRESSIRE	RATIOS . FOR				
O WOPD	PL.	PL/PO	PL/PTF .	PL/PTP	X/DMAX	reductive that a different forms of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of
107	14.371	0, 97466	0.55131	0.80061	0.39800	•
.12 .	14.371	<b>3.</b> 99466	0. 55131	0. 80061	0.43100	
22	14.366	0.99432	0.55112	0.80033	0.44900	
.27	14-376	0.99501_		0.80089	0.48600	
37	14.346	9.99294	. 55035	0.79922	0.52200	
42	14.271	0.98775	,749	0.79505	0.58800	
53				0.00211	<del>-1.0000</del>	
47	14.421	9.99812	*******	0.0000		
TOOLS INVI	L PPESSURE	PATIOS EAN	NOZZLE ELAP			
D MubD	PL	PLIPS	TOPTE	PL/PTP	X/DMAX	
52	16-414	0. 99777	0° 22.114	- 0.B0311	-1.0000	
	14.421	0.99912	0.55323	0.40339	-1.6000	
ADDLT IONA	AL PRESSUPE	PATINS . 20	DEG SHPOUD L	OCATION		
r wake	PL	PL/PN	PI / PT F	PL /PTP	x/04AX	
67	14.416	0. 99777	0.55303	0-40311	0.79300	
.72	14.416	9.99777	0.55303	0.90311	0.84400	
ADDET LONA	L_PRESSURE	RATIOS . 50	DEG SHROUD L	DCATLON		
ስ ማስቀስ	PL	PL / PO	PI / PT F	PI /PTP	X/DMAX	
P.7	13.817	0. 95630	0.57005	0.76973	0.79300	<u>-</u>
		0.04004	3 53/63			
87	13.712	9.94904	0.52602	0.76389	J. 84400	

VASA-L FWI	2 bacila	INARY DATA	76/17/70	CARRETT	PEC 10/24/7	9 63:54:35.366	FAF AY641	PGW CO34 RRG I	367
>A1017 [PH	AL PRESSUPE	RATIOS . PP	MERY, PLUG						
VN WAPA	Pl	P; /P(1	PI /PTF	PI /PTP	×/DMAX				
32	12.651	0.87534	9.41858	7.50895	0.72700				
> 7	14.738	1.0336	0.49426	0.7041#	0.02000				
47	15.403	1.0658	9. 50563	0.72914	0.91900				
52	15.473	1.0775	0.51 425	Q. 73f 17	1.0170				
>400111004	AL PRESSURF	RATIOS . FLO	W SPLITTEP I	.n.					
/በ ቁብቀብ	PL	PL/PG	P) /PTF	PI /PTP	x/IMAx	Ÿ.	The second second second		
2	15.028	1.0398	0.49724	0.71043	9-42209				
57	13.530	0.93617	0.44766	0.63960	0.67000	· ••• •			
ADDIT TON	AL PRESSURE	PATIOS . FLO	W SPLITTER T	.n.	***************************************				
D WIRD	PL	PL/PN	PL /PTF	PI /PTP	X/DMAX			er comme a company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of	
7	12.331	0.85322	9-40609	0.50293	0.50800				
2	16.596	1.1403	0.54912	0.78456	0.58300				
2	14,399	0.99630	0.47542	0.68059	0-67000				
<del>1001110</del> 1	u <u>-eneggung</u>	AATIOS . 6JE	CTOR SHROUD	<del></del>			· · · · · · · · · · · · · · · · · · ·		
0 4000	PL	PL/29	PL/PTF	PLEED	X/DMAX				
.07	14.354	0.99319	0.47493	0.67856	-1.0000				
12	14,344	0.99290 >	0.57460	0.67509_	-1.0000				
27	14.344	0-00257	75-47463	0.67499	-1-9900				
.27	14,350	0. 99354	0.47509	0.67880	-1.0000				
137	14.319	7. 99077	0.47377	0.67691	_1-0000				
45	14.244	9.98559	0.47129	9.67337	-1-9000		. —		
ADD IT TOM	L PRESSURE	RATIOS . FOR	ERODY THEF		<del></del>				
n word	PL	PL/PTI	PL / PTF	PL /PTP	x/DMAX				
107	14.354	0. 9931 9	0.47473	0.67856	0.39800		•		
12	14.344	0.99250	0.47460	0.67809	9.43100				
22	14.344	0. 49250	0.47460	0.67009	0.44900				
77	14.359	0. 99354	0.47509	0.67690	0.48600				
77	14.319	0.99077	0.47777	0.67691	0.52200				
42	14.244	0. 94559	0.47129	0.67337	0-59800				
<del>43</del>	24.409	7. 40,00	0.47679	0. APT16	-1.0000				
<del>**</del>		<del></del>		0.98190	-1:0000 -				<del></del>
Hard-barre	e essime	PATENCE FAN	HULSTE LITE						
מקחש ח	PL	PL/PT		PI /PTP	Y/DMAX				
57 57	14.409 - 14.414	<del></del>	0.47675	7.44116 0.68140	-1.0000 -1.0000				
		PATINS . 20							
n worn		PL / PO	PI / PTF	PI /PTP	x/DMAX				
(6.7)	PL 14.414	0.99734	0.47691	P. A8140	G. 79300				
16.7 1 <b>7</b> 7	14.414	0.99734	9.4769ì	0.68140	0.84400				
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1854-k F#15	. bell4	HEPY DATE	36/12/70	CAUDELL	PEC 10/74/79 57:1	F5:34.527	FAC SEARS	600 CU34	auc late	
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2	13.525	3.72889	3.77141	C.4216F	3.72200					
17	14. 337	2.97025	5.38787	5.56125	3.42603					
7	15.821	1-0956	0.43204	0.63765	J. 91 900					
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?	14.370	1.1337	0.45775	9.57-25	1.0170					
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7	13.173	7.90951	9.36763	0.52618	3.67000					
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2	29.775	1.4387	0.57521	0.83275	0.58700			maria managan an	was to the contract of	
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<del>90017101</del> 4	t-MESSUME	*47195 - EJE	CTOR SHOULD	<del></del>			and the second of the second	mandada make in in the second record	THE THE SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND SECOND S	
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7454-1 FW15	PRFLIM	HAPY DATA	76/17/79	CAONFII	RFC 10/74/79 04:01:03.048	FAT AVENT	PGM E034	RUN 13 POG 1369	
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VO MORD	Pt	PL /P!!	PI / PTF	P) /PTP	Y/DMAX		<del></del>		
**	9.7757	2-62873	0.19555	0.29753	9. 72200				
37	13.549	3.04646	9.33494	3.44705	0.42000	•	<i>'</i>		
47	19.719	1.2633	9.40581	9.59669	9.91900				
52	18.677	1.2051	0.41604	0.41174	1-0177		-		
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62	29. 774	1. 4495	0.46275	0.48042	0-42200				
57	17-115	1.1868	0.34123	0.56655	7.67909				
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9.7	14.977	1.0386	0.73363	0.49955	0.5#390				
92	14.353	J.9952#	0.21972	0.47011	0.67000				
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37	17.874	1.2346	0.24438	0.49874	0.82000		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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62	24.619	1.7061	0.47435	0.68697	0.42200		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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VD HEFD	7	. PL/PD	PL/PTF	PL/PIP	X/DHAX		
107	14.274	0.98914	0.27502	0.39829	-1.0000		
	14.269	0.98579	27592	0.39915	-1-0000		
112							· · · · · · · · · · · · · · · · · · ·
127	14.274	2.98014	22502	0.39#29	-1.0000		
127	14.299	3.99097	0.27550	0.39898			
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VD WERD 167 112 122 127	PL 14.274 14.269 14.274 14.299	ML/PO 0.98914 0.98879 0.98914 	PL/PTF 7.27502 0.27492 0.27502 0.27553	0.39829 0.39815	0.39800 0.43100		
VD WCRD 107 112 122 127	PL 14.274 14.269 14.274 14.299 14.259	PL/PO 0.98914 0.98879 0.98914 0.99097 2.98810	PL/PTF 0.27502 0.27492 0.27502 0.27550	0.39829 0.39815 0.39829 0.39898 0.29787	0.39800 0.43100 0.44900 0.48600 0.52200		
VÖ MCRD 167 112 122 127 137	PL 14.274 14.269 14.274 14.299	ML/PO 0.98914 0.98879 0.98914 	PL/PTF 9-27502 0-27592 0-27502 9-27559 0-27473 9-27415	0.39829 0.39815 0.39829 0.32898	0.39800 0.43100 0.44900 0.48600		
VD MCRD 167 112 122 127 137	PL 14.274 14.269 14.274 14.299 14.229	M./PO 0.98914 0.98879 0.98914 0.99097 0.98602 0.99602	PL/PTF 9-27502 0-27492 0-27502 0-27559 0-27415 9-27415	0.39829 0.39815 0.39829 0.39898 0.29787 0.39702	0.3 9800 0.43100 0.44900 0.52200 0.52200		
VD MCRD 167 112 122 127 137	PL 14.274 14.269 14.274 14.299 14.259	PL/PO 0.98914 0.98879 0.98914 0.99097 0.98810 0.99602	PL/PTF 9-27502 0-27492 0-27502 0-27559 0-27415 9-27415	0.39829 0.39815 0.39829 0.39898 0.29787 0.39703	0.3 9800 0.43100 0.44 900 0.48600 0.52200 0.58900		
VD WCRD 107 112 122 127 137 142	PL 14-274 14-269 14-274 14-279 14-259 14-259 14-269	M./PO 0.98914 0.98879 0.98914 0.99097 0.98602 0.99602	PL/PTF 9-27502 0-27492 0-27559 0-27559 0-27473 9-27415 0-27773	0.39829 0.39815 0.39859 0.39898 0.398787 0.39702 0.40147	0.3 9800 0.43100 0.44900 0.52200 0.52200		
VD WCRD 107 112 122 127 127 137 142	PL 14-274 14-269 14-274 14-279 14-259 14-259 14-269	PL/PO 9-98914 0-98979 0-98914 9-99091 2-98810 9-99602 0-99710 8-99675	PL/PTF 9-27502 0-27492 0-27559 0-27559 0-27473 9-27415 0-27773	0.39829 0.39815 0.39829 0.39898 0.29787 0.39702 0.49143	0.39800 0.43100 0.44900 0.48600 0.52200 0.58900 1.9800		
VD WCRD 107 112 122 127 137 137 142 153	PL 14.274 14.269 14.274 14.299 14.259 14.229 14.269 14.274	#1/PO 1-98914 0-98974 0-98914 0-99091 1-98602 0-99710 0-99602 0-99710	PL/PTF 20-27502 0-27492 0-27502 0-27550 0-27550 0-27413 0-27415 0-27713	0.39829 0.39815 0.39829 0.39898 0.29787 0.39702 0.49145 0.49135	0.39800 0.43100 0.44900 0.48600 0.52200 0.58500 1.9800		
VD WCRD 107 112 122 127 137 142	PL 14.274 14.269 14.274 14.274 14.259 14.259 14.229 14.369 14.794	PL/PO 0.98914 0.98870 0.98914 0.99091 0.98602 0.99602 0.99710 0.99602	PL/PTF 2-27502 0-27492 0-27502 0-27550 0-27475 2-27475 0-27713	0.39829 0.39815 0.39829 0.39898 0.29787 0.39702 0.49143	0.39800 0.43100 0.44900 0.48600 0.52200 0.58900 1.9800		
VD WCRD 107 112 122 127 127 142 142 157 VD WCRD 152	PL 14.274 14.269 14.274 15.299 14.259 14.229 14.909 14.794 PL 14.389	PL/PO 0.98914 0.98870 0.98914 0.99091 0.98602 0.9910 0.99675 PAPED 0.99710 0.99710 0.99710 0.99710	PL/PTF  9-27502  0-27492  0-27550  0-27550  0-27415  0-27415  0-27713	0.39829 0.39815 0.39829 0.39898 0.29787 0.39702 0.49143 0.49135	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 1.9000 1.0000		
VD WCRD 157 112 122 127 137 142 142 157 VD WCRD 152 157 >ADDITION	PL 14.274 14.269 14.274 14.269 14.274 14.279 14.259 14.229 14.399 14.349 PL 14.389 14.375	PL/PO 9-98914 9-98914 9-99091 9-98602 9-9910 9-99602 9-9910 0-99675 PATINS 266	PL/PTF 9-27502 0-27502 0-27502 0-27503 0-27503 0-27415 0-27415 0-27713 0-27713 0-27713 0-27713 0-27713	0.39829 0.39815 0.39898 0.39898 0.39787 0.39702 0.40149 0.40135 0.40149 0.40149	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 1.9000 -1.0000		
VD WCRD 107 112 122 127 137 142 157 VD WCRD 152 157 VD WCRD 152 157 VD WCRD VD WCRD VD WCRD	PL 14.274 14.269 14.274 14.269 14.274 14.259 14.259 14.229 14.389 14.494  M. FRESSURE PL 14.389	PL/PO 9-98914 9-98914 9-9991 9-98602 9-9916 9-99675 PATINS 2 26 PL/PO	PL/PTF  9-27502 0-27492 0-27502 0-27550 0-27550 0-27415 0-27415 0-27713 0-27713 PL/PTF	0.39829 0.39815 0.39829 0.39898 0.29787 0.39702 0.49135 0.49135 PL/PTP 0.40149 0.40135	0.39800 0.43100 0.44900 0.48600 0.52200 0.58900 1.9000 -1.0000		
VD WCRD 107 112 122 127 137 142 157 VD WCRD 157 >ADDITION VD WCRD 167	PL 14.274 14.269 14.274 15.299 14.259 14.229 14.309 14.309 14.309	PL/PO 1-98914 0-98970 0-98914 2-99091 2-98602 0-9910 0-99675 PATIOS - 548 PL/PO 0-99675	PL/PTF  9.27502  0.27492  0.27553  0.27553  0.27415  4.27773  0.27713  HOTELE FLAS  PL/PTF  9.27713  PL/PTF  9.2771	0.39829 0.39815 0.39829 0.39898 0.29787 0.39702 0.40143 0.401435 0.40149 0.40149 0.40135	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 1.9000 -1.0000		
VD WCRD 107 112 122 127 137 142 157 VD WCRD 157 >ADDITION VD WCRD 167	PL 14.274 14.269 14.274 14.269 14.274 14.259 14.259 14.229 14.389 14.494  M. FRESSURE PL 14.389	PL/PO 9-98914 9-98914 9-9991 9-98602 9-9916 9-99675 PATINS 2 26 PL/PO	PL/PTF  9-27502 0-27492 0-27502 0-27550 0-27550 0-27415 0-27415 0-27713 0-27713 PL/PTF	0.39829 0.39815 0.39829 0.39898 0.29787 0.39702 0.49135 0.49135 PL/PTP 0.40149 0.40135	0.39800 0.43100 0.44900 0.48600 0.52200 0.58900 1.9000 -1.0000		
VD WCRD 107 112 122 127 137 142 157 167 2001710W	PL 14.274 14.269 14.274 14.269 14.274 14.299 14.259 14.229 14.389 14.389 PL 14.384 14.389	PL/PO 1-98914 0-98970 0-98914 2-99091 2-98602 0-9910 0-99675 PATIOS - 548 PL/PO 0-99675	PL/PTF  9-27502 0-27502 0-27502 0-27503 0-27503 0-27415 0-27415 0-27713 0-27713 DEG SHOUD 1 PL/PTF 0-27713	0.39829 0.39815 0.39898 0.29787 0.39702 0.40149 0.40149 0.40149 0.40149 0.40135 0.40149	0.39800 0.43100 0.44900 0.52200 0.52200 0.53300 1.0000 1.0000 1.0000		
VD WCRD 167 112 127 137 142 139 VD WCRD 152 157 >ADDITIONA	PL 14.274 14.269 14.274 14.269 14.274 14.279 14.259 14.259 14.279 14.389 14.389 14.384 14.384	PL/PO 9-98914 9-98914 9-99091 9-98602 9-99602 9-99602 9-99605 PATIOS - 568 PLAND 0-99675 9-99675 9-99675 9-99675 9-99675	PL/PTF 9-27502 0-27502 0-27550 0-27550 0-27550 0-27415 9-27713 0-27713 0-27713 DEG SIMMUD 1 PL/PTF 9-27723 DEG SIMMUD 1	0.39829 0.39815 0.39898 0.29787 0.39702 0.40149 0.40149 0.40135 0.40149 0.40135 0.40149	0.39800 0.43100 0.44900 0.52200 0.52200 0.58300 1.9000 1.0000 1.0000 1.0000 1.0000		
VD WCRD 157 112 122 127 137 142 142 157 VD WCRD 152 157 VD WCRD 167 167 177 VD WCRD 167 177 VD WCRD 167 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCRD 177 VD WCR	PL 14.274 14.269 14.274 14.269 14.274 14.299 14.259 14.229 14.389 14.389 14.384 14.384 14.389	PL/PO 9-98914 9-98914 9-99097 9-98602 9-99710 9-9602 9-99710 9-96675 PATIOS 2 20 PATIOS 3 80 PATIOS 3 80	PL/PTF  9-27502 0-27502 0-27550 0-27550 0-27473 0-27415 0-27713 0-27713 PL/PTF 0-27713 DEG SHPRUP L PL/PTF	0.39829 0.39815 0.39826 0.39886 0.29787 0.39702 0.40145 0.40145 0.40149 0.40149 0.40135 0.40149 0.40135	0.39800 0.43100 0.44900 0.52200 0.52200 0.53500 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		
VD WCRD 167 112 122 127 137 142 157 2001710W VD WCRD 152 157 >ADDITIONA VD WCRD 167 177 >ADDITIONA VD WCRD 167	PL 14.274 14.269 14.274 14.269 14.274 14.299 14.259 14.229 14.389 14.389 14.384 14.389	PL/PO 9.98914 9.98914 9.99914 9.99915 9.98602 9.99716 0.99675 PATINS 26 PL/PO 0.99675 9.99719 9.99719 PATINS 30	PL/PTF 9-27502 0-27502 0-27502 0-27503 0-27503 0-27515 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713 0-27713	0.39829 0.39815 0.39898 0.29787 0.39702 0.40149 0.40149 0.40149 0.40149 0.40135  OCAT [ON PL /PTP 0.40149 0.40149 0.40149 0.40149	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 1.0000 1.0000 1.0000 X/DMAX 0.79300 0.84400		
VD WCRD 107 112 122 127 137 142 157  VD WCRD 157  VD WCRD 167 177  >ADDITIONA VD WCRD 167 177  >ADDITIONA VD WCRD 167 177  >ADDITIONA VD WCRD 167 177	PL 14.274 14.269 14.274 14.269 14.274 14.279 14.259 14.299 14.389 14.389 14.384 14.389 14.389 14.389 11.00000000000000000000000000000000000	PL/PO 9-98914 9-98914 9-99097 9-98602 9-99710 9-9602 9-99710 9-96675 PATIOS 2 20 PATIOS 3 80 PATIOS 3 80	PL/PTF 9.27723 PL/PTF 9.27723 PL/PTF 9.27723 PL/PTF 9.27723 PL/PTF 9.27773	0.39829 0.39815 0.39826 0.39886 0.29787 0.39702 0.40145 0.40145 0.40149 0.40149 0.40135 0.40149 0.40135	0.39800 0.43100 0.44900 0.52200 0.52200 0.53500 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		

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AU HUBU	PL	PL/PO	PL / PT F	PLIPTP	X/DMAX		***************************************	**************************************	
32	17.447	0. 72484	0.18265	0.26564	0-72200				
37	23.143	1.4791	0.35282	0.51312	G. # 2003				The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
47	15.292	1.0610	0-26736	0-38883	0.91900				
57	20.560	1.4264	0. 35945	0.5277	1.0170				
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UD WOPD	Pt	PL/PO	PL/PTF	PL /PTP	X/OMAX	•			
62	26.667	1.8501	0.46622	0.67895	0.42200				
67	20.939	1.4458	0.36434	0.52987	0.67000				
>4071T1094	L PRESSIME	RATIOS . FLO	W SPLITTER I	·.O.			<del></del>		
AU MUBO	PL	PL/PG	PL /PTF	PL/PTP	X/DMAX	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			
77	13.374	0.92791	0.23381	0.34007	0.50900				
82	19.127	1.3270	0.33440	0.48633	0.58300	Property or the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Contr			
92	. 14.343	0.97513	0.25077	0-36470	0.67900				
	<del>- MESSINE</del>	441105 . EUC	Cton Chaun				. Victoria de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya del companya del companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya		
AU AUNU	PL	PL/PD	PL/PTE	PLANT	X/DHAX				
107	14. 263	0.98959	0.26094	0.36267	-1.0000				
112	14.245	2.9863	2.24911	0.36229	-1.0000				
122	14.743	2.98820	0.24902	0.36216	-1.0000				
127	16-eng	0.99132	0. 24941	0.36331	-1.0000				
137	14.24#	9.98855	0.24911	0.36229	-1.0700		ay in stage the transcription was the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the same the s		
245	14.223	0.98681	0.24867	0.36166	-1:0000				
>AODET EDNA	L PRESSUPE	RATIOS , FOR	ENDOY INLET						
yn wnen	PL	PL/PN	PL/PTF	PL/PTP	X/DMAX				
107	14.263	0.98958	0.24937	0.36267	0.39800	a		-	
112	14.248	0.98855	0.24911	0.36229	0.43100		•		
122	14.243	0.98420	0. 24902	0.36216	0-44900				
127	14-200	0.99132_	9.24981	0.36331	0.48600				
127	14.248	0.94855	0.24411	0.16229	0.52200				
142	14. 223	0, 99681	0.24867	0.36166	0.58800				
163	-14-378			0.30399	-1.0000				
157	14, 143			C.70772	1.0000	unic con establic constant a superior			The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
M22171044	<del>- rarssu</del> nc	P47103 _ F46							
ልሁ ማሁ <u>ሄ</u> ው 	PI	-EL/PR	P1_4.87#	PL /PTP	X/DMAX				
	14.370	-9-99139	0.25134	0.36559	-1.0000		. and the case with the entire transfer of		
12 7		0.99790	0.25141	0.36572	-1-00C0	way to			
15?		RATIOS . 20	DEG SHERIND L	JCATION					
157	I. PRESSURE	-			Y/OWAY				
157 >6991T (MAA VO. HORD	I. PRESSYME	PL / PO	PL /PTF	PL /PTP	Y/0MAX	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s			
157 >enoit inna vo hoen 167	I. PRESSURE	PL /PN 0.99790			X/0MAX U. 79300 O.84400				
157 >8901T YONA VO WORD 167 172	R. PRESSUME PL 14.383 14.393	PL/PN 0.99790	PL /PTF 0.25147 0.25147	PL /PTP 0.36572 0.36572	U. 79300				
157 >8001T (DNA VO. MORD 167 172 >ADDIT (DNA	PRESSURE PL 14.383 14.383	PL/PN 0.99790 0.99790 RETENS . 80	PL /PTF 9.25147 0.25147 DEG SHROUD L	PL/PTP 0.36577 0.36572 DCATION	0.79300 0.94400				
157 >eDOIT INNA VO. HOPD 167 172 >ADOIT INNA VO. HOPD	PRESSUPE PL 14.383 14.393 L PRESSUPE PL	PL/PN 0.99790 0.99790 RETTOS , RO PL/PN	PL/PTF 9.25147 0.25147 DEG SHROUD L	PL /PTP 0-36572 0-36572 NCATION PL /PTP	U. 79300 O. 94400				
VO ЧОРО 167 172 >АПОІТІОЧА VO ЧОРО 182	PRESSURE PL 16.383 16.393 U PRESSURE PL 13.589	ML/PN 0.99790 0.99790 RETTINS . RO M /PN 0.942P1	PL/PTF 0, 25147 0, 25147 DEG SHRPHO L PL/PTF 0, 23759	PL /PTP 0.36572 0.36572 NCAYION PL /PTP 0.34553	U. 79300 O. 84400 X/DRAX O. 79300				
157 >600]T INNA VO HOPD 167 172 >ADDIT IONA VO HOPD 182 187	PRESSURE PL 14.383 14.383 1. PRESSURE PL 13.589 13.424	PL/PN 0.99790 0.99790 RETTOS , RO PL/PN	PL /PTF 0. 25147 0. 25147 DEG SHRMID L PL /PTF 0. 23759 0. 27470	PL /PTP 0-36572 0-36572 NCATION PL /PTP	U. 79300 O. 94400				

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			04 43 3 4 70	CARDELL	0EC 1043/470	## +03+50 324	546 974Y	PG= C934	Run 22
4851-E FM 1	S PERFER	INARY DATA	06/13/79	( with Eli	WEL 10/24/14	64:93:59.724	FAC AXEAS	Prim (1/134	PNG 1372
MULTICUM	AL PRESSURE	RATINS . PPI	MARY PLUG						
IN WORD	PL	Pt / Pri	PL/PTF	PI /PTP	X/DMAY				
2	10.464	0.72528	0.18243	0.26520	0.72200				
7	20.243	1.4030	0.35291	0.51303	0.82000				
67	15.364	1.0649	9.26786	0.39939	0.91900			·	
52	20.562	1. 4252	0.35848	C.52113	1.0170				
ADDIT ICN	AL PRESSURE	PATIOS . FLO	W SPLITTER I	•n•					
/ก พก <b>ล</b> ก	PL	ምር ያዋብ	PI /PTF	PI /PTP	X/DMAX				
52	26.720	1.8520	0.46583	0.67718	0.42200				
57	20.892	1.4473	0.36405	0.52923	J.67000				
ADDIT ION	AL PRESSURE	PATIOS . FLO	W SPEETTER D						
						· · · - · ·			
IN MUBD	PŁ	PL/PO	PL/PTF	PL /PTP	X/DMAX				•
77	13-401	0.92886_	. 0.23364	0.33965	0.50800				
92	19-179	1.3293	0.33437	0.48608	0.56300				
	14_345	0.99429	0.25010	0.36357	0-67000		· · · · · · · · · · · · · · · · · · ·		
MOTTIGOR	AL PRESSURE	PATEOS V. EUC	CT CR SHPCUD	····					
D WORD	PL	PL/PO	PL/PTF	PLARTP	X/DMAX				
107	14.256	98805	0.24853	0.36129	-1.0000				
112	14.251	0.95771	25865	0.36116	-1-0000				
122	14.246	12-24731	70.74.235	0.36104	-1.0000				
27	14.295	0.99013	0.24905	Q_36205	-1.0000				
27	-14.265	0.98736	0.24835	0.36176	1.0000				
152	14-216	3.98529	9.24783	0.26028	-1:0000				
MODELE COR	AL PRESSURE	PATIOS . FOR	EPDDY INLEY				· · · · · · · · · · · · · · · · · · ·		
ሃሳ ዛበጽክ	PL .	PL/PD	PL/PTF	PL/PTP	X/DMAX				
07	14.256	0. 98805	0. 24853	0.36129	0.39800		•		
112	14-251	2.28771	0.24844	0.36116	0.43109				
122	14-246	0.98736	0.24835	0.36104	0.44900				
27	14-285	0.99013	0. 24905	0.36205	0-48600				
37	14.246	). 98736	0.24835	0.36104	0.52200				
142	14.216	0.98529	0.24783	0.36028	0.58800				
ļ-\$2	14.305	0 <del>, 99 70 5</del>	A. 25079	0.36458	1.0000				
	<u>t</u> 4.385	<del>) , 09</del> 795		0.3645A -	-1.0000			·····	<del> </del>
<u> </u>	L PRESSURE	RATIOS FAN	- NOZZ LE FLAT				····		
U HUPP	PL	-4-400		OL/PTP	X/DMAX		_		
52	14-395	- 0.99705	7-25079	0.36459	-1.0000				
57	14.385	0.99705	0. 75079	0.38454					<del></del>
איחן דן <i>כיר</i> א•	AL PRESSURE	PATIOS . 20	DEG SHROUD L	OCATION					· · · · · · · · · · · · · · · · · · ·
/P WORD	PL	Pt / PO	PL/PTF	PL/PTP	X/DMAX				
(67   67	14.380	0.99671	0.25071	0.36445	7.79300	*	· · · · · · · · · · · · · · · · · · ·		
172	14.395	0.99671	9.25079	0.36458	0.84400				
	_				V• 077VV	•			
MOT TECOP	PL PRESSUPE	RATIOS 50.	DEG ,SHRPUD .L	PCATEDN					
กา สมหา	PŁ	PL / PN	PL/PTF	Pt /PTP	X/DMAX	w			
LP2	13.586	0.94167	0. 23686	0.34433	0.79300				
		2 02001	0 00444	2 24242	0.04430				
147	13.421	0.93094 THRUST PAPAM	0.23416	0.34040	0.84400				

	pati la	NARY DATA	06/13/70	CARRELL	REC 10/24/75	04:05:41.314	FAC REGEL	PG9 C034	PNN 22
APPITIONA	1 DBESSIBE	PATING , PRI	MAPA UFIIG						· / · · · · · · · · · · · · · · · · ·
מאַמאַ מי	PL	PL/PH	PL /PTF	PL /PTP	X/DMAX			· · · · · · · · · · · · · · · · · · ·	
7	19.341	0.71621	0.19926	0.20019	0. 72200			<b></b>	
7	17, 979	1.2349	0.34756	0.49690	0.92000				
7	13.407	0.97856	9. 25934	9.37364	J. 91 900				
.2	19.307	1.3372	0.37203	0.53878	1.0170				
ANDI TECCY	L PRESSUPE	PATTOS . FLO	W SPLITTER I	• D•	V =	er annagagar fan i generalen Alle Britania en gegenellen.			
กษากะก	PL	PL / PO	PL/PTF	PI /PTP	X/DHAX				
2	24-633	1.7061	0.47466	0.68651	9.42200				
7	23.350	1-4095	0.39213	0.56715	0.67000				
ANDIT TONAL	L PRESSUPF	PATIOS . FIC	M COLITYPO D	. 0.					~ <del>~</del>
geny o	PL	PL/PR	M /PTF	PL /PTP	X/DMAX				
7	12.128	0. 84003	0.23371	0.33602	0.50800				
?	17.375	1.1996	0.33346	0.48279	0.58300				
?	14.350	0, 99391	0.27652	0.39994	0.6.7000				
1001 s sumi	<del></del>	<del></del>	<del>CTCP-SHPNUN-</del>						
NUB u	PE	PL/PO	PL/PTF	PLANTE	X/DMAK				
17	14.270	0.98838	0.27698	0.39771	-1.0000				
2	14_260	0. 99169	0.27479	0.39743	-1-0000				
"	14.755	0-98774	27469	0.39729	-1.0000				
?7	14,290	0.98976	0.27537-	0.39827	-1.0000				
• •	-14. 745	0. 98665	0.27450	0:99701	-1.0000				
20171011	14.715	0,98458	0, 27392 _	0.3961#		-			
		RATERS . FRE			w 25344 W	<del></del>		<del></del>	
7 WORD	PL 14.270	PL / PG 0. 98838	PL/PTF 0.27498	PL /PTP 0.39771	X/DMAX 0-39800		•		
2	14.269	0. 93769	0.27479	0.39743	0.43100		•		
2	14.255	0.98734	0.27469	0.39729	0.44900		<del></del>		
•	14. 290	0. 98976	0.27537	0.39927	0.48600				
7	14.245	0.98665	9. 27459	0.39701	0.52209				<del></del>
	14.215	0.9458	0.27392	0.3961#	0.58800				
				0.40077	-1.0000				
	246 244			- 0,40077					
	<del></del>								
<del></del>		AATIOS FAN	NOZZIE FLAR				·		
SDITIONAL		NATIOS FAN	NOTTIE FLAR	PI /PTP	x/DPAX				
HUBU POSTE LUMPI	POESSURE-	844105 <u>-</u> FAN		Pt /PTP 0.40077	x/DMAX -1.0000				
10015 (11144) 1 41180	PL PAGGSUME	NATIOS FAN	_0-/						
001510040 0 MORD 52	PL 14-330 14-390	M+105 FAN 	7.27710 1.27710	0.40077 0.40077	-1.0000				
INDESTRUMANTO SE SE SE SE SE SE SE SE SE SE SE SE SE	PL 14-390 14-390 1 PRESSURE	M7P0	0.27713 0.27710 0.27710 DEG SHPCHO L	0.40077 0.40077 O.40077 PL/PTP	-1.0000 -1.0000				
ADDITIONAL D. MORD S.Z. ADDITIONAL	PL 14-330 14-330 PRESSURE	M 7PA	0.27713 0.27713 0.27710 DEG SHPCUD L	0.40077 0.40077 0.40077	-1.0000 -1.0000				
INDESTIONAL HURD SP INDESTIONAL HURD HURD TO HURD	PL 14-390 14-390 1 PRESSURE	M7P0	0.27713 0.27710 0.27710 DEG SHPCHO L	0.40077 0.40077 O.40077 PL/PTP	-1.0000 -1.0000				
INDESTIONAL NUMBER SZ SZ SZ SZ SZ SZ SZ SZ SZ SZ SZ SZ SZ	PL 14-390 14-390 14-390 PRFSSURF PL 14-390 14-375	M 7P0	0.27710 0.27710 0.27710 DEG SHPCID 1 PI /PTF 0.27710 0.27700	0.40077 0.40077 0.40077 0.40077 0.40073	-1.0000 -1.0000 X/DMAX 0.79300				
LODITIONAL O MORD ST LODITIONAL O MORD T Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	PL 14-390 14-390 14-390 PRFSSURF PL 14-390 14-375	M / PM	# /PTF # /PTF  # /PTF  0.27710  # /PTF  0.27710  0.27710  THE SHPPLIN I	0.40077 0.40077 0.40077 0.40077 0.40073	-1.0000 -1.0000 X/DMAX 0.79300				
N MORD 52 57 APDET JANAJ D. MOPD 67 72	PL 14-390 14-390 14-390 14-390 14-390 14-395 PRESSURE	M / PO	# /PTF # /PTF  # /PTF  0.27710  # /PTF  0.27710  0.27710  THE SHPPLIN I	0.40077 0.40077 0.40077 0.40077 0.40063 0.40163	-1.000 -1.0000 X/DMAX 0.79300 2.84400				
ADDITIONAL DESTRICTIONAL ACCUST TOWARD FOR ACCUST TOWARD DESTRICTIONAL DESTRICTIONAL	PL 14-390 14-390 14-390 14-390 14-390 14-390 14-395 14-395 14-395 14-395 PL	MATIOS CAN MYPO 0.90599 0.90599 PATIOS 20 PL/PO 0.90564 PATIOS 90 PL/PO	0.27710 0.27710 0.27710 0.65 SHPCHD 1 0.27710 0.27710	0.40077 0.40077 0.40077 0.40077 0.40073	-1.0000 -1.0000 X/DMAX 0.79300 0.84400				

.7120 3.556 9.118 4.632 RESSUPE P 0.679 6.980 RESSUPE R 0.430 4.929 4.350	PI /PH 1.4326 1.1764 ATTHS , FLO PI /PH 0.72260 1.0343 0.99414	PL/PTF 0.19443 0.30253 0.40435 0.40435 0.41582 IM SPLITTER ( PL/PTF 0.46149 0.37895 IM SPLITTER ( PL/PTF 0.23277 0.33317 0.32024 ECTCR SHPOUD PL/PTF 0.31868 0.31926 0.31926	P1 /PTP U. 6.2.356 0.558P4  P. N.  P1 /PTP 0.34327 0.49137 0.47226  P1 /PTP 0.47017 0.46996 0.47078	X/DMAY  3.72200  9.82000  3.91500  1.0170  X/DMAX  3.42200  0.67000  X/DMAX  0.50800  0.58300  0.67000  X/DMAX  -1.0000  -1.0000  -1.0000				
.7120 3.556 9.118 9.637 9.637 9.6479 9.6490 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430	0.60357 0.03915 1.2552 1.2909 ATIOS . FIG PI /PG 1.6326 1.1764 ATIOS . FIG PI /PG 0.72260 1.0343 0.99414 PT103 . EJE PL/PG 0.08965 1.33939 0.99103 0.99103 0.99203	0.19443 0.30253 0.40435 9.41582 0.41582 0.41582 0.46149 9.37895 0.23277 0.33317 0.32024 0.31868 0.31868 0.31924	0.28672 0.44414 0.59629 0.61321 1.0. P1/PTP 0.62356 0.558P4 1.0. P1/PTP 0.34327 0.49137 0.47226 P1/PTP 0.47017 0.46996 0.47078	3.72200 9.82000 3.91500 1.0179  K/OMAX 3.42200 9.67000  X/DMAX 0.50900 9.67000  X/DMAX -1.0000 -1.0000 -1.0000				
.7120 3.556 9.118 9.637 9.637 9.6479 9.6490 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430 9.6430	0.60357 0.03915 1.2552 1.2909 ATIOS . FIG PI /PG 1.6326 1.1764 ATIOS . FIG PI /PG 0.72260 1.0343 0.99414 PT103 . EJE PL/PG 0.08965 1.33939 0.99103 0.99103 0.99203	0.19443 0.30253 0.40435 9.41582 0.41582 0.41582 0.46149 9.37895 0.23277 0.33317 0.32024 0.31868 0.31868 0.31924	0.28672 0.44414 0.59629 0.61321 1.0. P1/PTP 0.62356 0.558P4 1.0. P1/PTP 0.34327 0.49137 0.47226 P1/PTP 0.47017 0.46996 0.47078	3.72200 9.82000 3.91500 1.0179  K/OMAX 3.42200 9.67000  X/DMAX 0.50900 9.67000  X/DMAX -1.0000 -1.0000 -1.0000				
3.556 4.118 4.632 RESSUPE P 0.679 6.980 RESSUPE R 0.430 4.929 4.350 RESSURE P 4.285 4.280 4.300 4.300 4.300	0. 93 91 5 1. 25 52 1. 29 09 ATIOS . FLO PI /PO 1. 43 26 1.1764 ATIOS . FLO PI /PO 0. 72 260 1.03 43 0. 99 414 PTIOS . EJE PL/PO 0. 98 95 5 1. 93 93 93 94 94 95 30 0. 99 103 0. 98 93 0	0.30253 0.40435 0.41582 IM SPLITTER 1 P1/PTF 0.46149 0.37895 IM SPLITTER 1 PL/PTF 0.23277 0.33317 0.32024 ECTOR SHEDUD PL/PTF 0.21889 0.31868 0.31924	0.44f14 0.59629 0.61321 1.0. P1/PTP 0.62356 0.558P4 0.4727 0.49137 0.47226 PL/PTP 0.46996 0.47078	7.87090 3.91500 1.0170 K/NMAX 3.42200 0.67000 K/NMAX 0.50900 0.58300 0.67000 X/DMAX -1.0000 -1.0000 -1.0000				
9.118 9.632 RESSUPE P 0.679 6.980 RESSUPE R 0.430 4.929 4.350 RESSURE P 4.285 4.280	1.2552 1.2099 ATIOS , FLO PL/PD 1.4326 1.1764 ATIOS , FLO PL/PD 0.72260 1.0343 0.99414 PTIOS , EJE PL/PD 0.9965 1.93999 0.99103 0.99103 0.9920	U. 47435 9.41582 W SPLITTER 1 PI/PTF 0.46149 9.37895 W SPLITTER 0 PL/PTF 0.23277 0.33317 0.32024 CCTCR SHPOUD PL/PTF 0.31868 0.31924	0.596.29 0.61321 1.0. P1 /PTP 0.62356 0.558P4 P. D. P1 /PTP 0.34327 0.49137 0.47226 PL/PTP 0.47017 0.46996 0.47078	3.91500 1.0170 X/DMAX 0.42200 0.67000 X/DMAX 0.50000 0.58300 0.67000 X/DMAX -1.0000 -1.0000				
A.632  RESSIPE P  0.679 6.9R0  RESSIPE R  0.430 4.929 4.350  RESSURE P  4.285 4.780 4.300 4.300	1.2909 ATIOS . FLO PI /PO 1.4326 1.1764 ATIOS . FLO PI /PO 0.72260 1.0343 0.99514 PTIOS . EJE PL/PO 0.9965 1.93990 0.99103 0.99030	0.41582  PI /PTF 0.46149 0.37895  By SPLITTER ( PL/PTF 0.23277 0.33317 0.32024  CCTCR SHPOUD  PL/PTF 0.21889 0.31868 0.31924	P1 /PTP	X/DMAX 3.42200 0.67000 X/DMAX 0.50800 0.58300 0.67000 X/DMAX -1.0000 -1.0000				
RESSUPE P 0.679 6.980 RESSUPE R 0.430 4.929 4.350 RESSURE P 4.285 4.280	PI /PD 1.4326 1.1764 ATIDS , FLO PL /PD 0.72260 1.0343 0.99414 PTIDS	PI / PTF 0.46149 0.37895 IN SPLITTER O 23277 0.33317 0.32024 ICTCR SHPOUD PL/PTF 0.21889 U.31868 0.31924	PI /PTP	X/DMAX 3.42200 0.67000 X/DMAX 0.50900 0.59300 0.67020 X/DMAX -1.0000 -1.0000				
0.679 6.980 RESSURE R 0.430 4.929 4.350 RESSURE P 4.285 4.280 4.280	PI /PN 1.4326 1.1764  ATTINS , FL (1) PI /PN 0.72260 1.0343 0.99414  PTINS , EJE PL/PN 0.494930 0.99103 0.99203	PI/PTF 0.46149 9.37895 IN SPLITTER C PL/PTF 0.23277 0.33317 0.32024 PL/PTF 0.31868 0.31924	P1 /PTP U. 6.2.356 0.558P4  P. N.  P1 /PTP 0.34327 0.49137 0.47226  P1 /PTP 0.47017 0.46996 0.47078	3.42200 0.67000 X/PMAX 0.50900 0.58300 0.67000 0.67000 -1.0000 -1.0000				
0.679 6.980 RESSIPE R 0.430 4.929 4.350 RESSURE P 4.285 4.280 4.280	1.4326 1.1764 ATIOS . FLO PL/PO 0.72260 1.0343 0.99414 PTIOS . ESE PL/PO 0.98965 1.93930 0.99103 0.99103 0.98930	0.46149 9.37895 By SPLITTER O PL/PTF 0.23277 0.33317 0.32024 CTCR SHPOUD PL/PTF 0.31868 0.31924	0.68356 0.558P4 7.7. Pt /PTP 0.34327 0.49137 0.47226 PL /PTP 0.47012 0.46996 0.47078	3.42200 0.67000 X/PMAX 0.50900 0.58300 0.67000 0.67000 -1.0000 -1.0000				
6.980 RESSURE R 0.430 4.929 4.350 RESSURE P 4.285 4.280 4.280	1.4326 1.1764 ATIOS . FLO PL/PO 0.72260 1.0343 0.99414 PTIOS . ESE PL/PO 0.98965 1.93930 0.99103 0.99103 0.98930	0.46149 9.37895 By SPLITTER O PL/PTF 0.23277 0.33317 0.32024 CTCR SHPOUD PL/PTF 0.31868 0.31924	0.558P4 P. N. Pt /PTP 0.34327 0.49137 0.47226 PL /PTP 0.47017 0.46996 0.47078	X/DMAX 0.50900 0.58300 0.67000 X/DMAX -1.0000 -1.0000				
0.430 4.929 4.350 RE33URF P	1.1764 AYINS , FLO PL/PN 0.72260 1.0343 0.99414 P7193 , EJE PL/PN 0.98965 1.93939 0.99103 0.99103 0.9920	PL/PTF 0-23277 0-33317 0-32024 CCTCR SHPOUP PL/PTF 0-31868 0-31668 0-31924	Pt /PTP 0.34327 0.49137 0.47226  Pt /PTP 0.47017 0.46996 0.47078	X/DMAX 0.50900 0.59300 0.67000 X/DMAX -1.0000 -1.0000				
0.430 4.929 4.350 RESSURF P 4.285 4.280 4.280	PI/PI 0.72260 1.0343 0.99414 PTIDS V ESE PI/PI 0.9995 0.9995 0.99103 0.99103 0.98930	PL/PTF 0.23277 0.33317 0.32024 CTCR SHPOUD PL/PTF 0.31868 0.3168 0.31924	PL /PTP 0.34327 0.49137 0.47226  PL /PTP 0.47017 0.46996 0.47078	0.50900 0.58300 0.67000 X/DMAX -1.0000 -1.0000				
0.430 4.929 4.350 RESSURF P 4.285 4.280 4.780 4.304	0.72260 1.0343 0.99414 P7193 v EJE PL/PD 0.98965 1.93939 0.99103 0.99103 0.99930	0.23277 0.33317 0.32024 CTCR SHPOUD PL/PTF 0.31868 0.31868 0.31924	0.34327 0.49137 0.47226 0.47226 0.47017 0.46996 0.47078	0.50900 0.58300 0.67000 X/DMAX -1.0000 -1.0000				
0.430 4.929 4.350 RESSURF P 4.285 4.280 4.780 4.304	0.72260 1.0343 0.99414 P7193 v EJE PL/PD 0.98965 1.93939 0.99103 0.99103 0.99930	0.23277 0.33317 0.32024 CTCR SHPOUD PL/PTF 0.31868 0.31868 0.31924	0.34327 0.49137 0.47226 0.47226 0.47017 0.46996 0.47078	0.50900 0.58300 0.67000 X/DMAX -1.0000 -1.0000				
4.295 4.295 4.295 4.290 4.290 4.290 4.290	1.0343 0.99414 P7193 V EJE PL/PD 0.98965 1.95939 0.494730 0.99103 0.99630	0.33317 0.32024 CCTCR SHPOUD PL/PTF 0.21889 0.31868 0.31924	0.49137 0.47226 PL#PTF 0.47017 0.46996 0.47078	0.58300 0.67000 X/DMAX -1.0000 -1.0000				
4.295 4.295 4.295 4.290 4.290 4.290	0.99414 P7103 v EJE PL/PD 0.98965 0.947930 0.99103 0.99103	0.32024 ETCR SIPPUD PL/PTF 0.31868 0.31868 0.31924	0.47226 PL#PTF 0.47012 0.46996 0.47078	X/DMAX -1.0000 -1.0000				
4.285 4.280 4.280 4.280 5.305 4.280	PL/PD 0.98965 0.98939 0.99103 0.99103 0.98930	PL/PTF 0.31868 0.31868 0.31968 0.31924	0.47017 0.46996 0.46996 0.47078	-1.0000 -1.0000 -1.0000				
4.285 4.280 4.280 4.280 5.305 4.280	PL/PD 0.98965 0.98939 0.99103 0.99103 0.98930	PL/PTF 0.31868 0.31868 0.31968 0.31924	0.47017 0.46996 0.46996 0.47078	-1.0000 -1.0000 -1.0000				
4.295 4.290 4.290 4.305 4.200	0.9995 0.99930 0.99103 0.98930	0.31868 0.31868 0.31868 0.31924	0.47017 0.46996 0.46996 0.47078	-1.0000 -1.0000 -1.0000				
4.780 4.780 4.305 4.280	0.99999 0.99930 0.99103 0.98930	0.31868 0.31968 0.31924	0.46996 0.46996 0.47078	-1-0000 -1-0000				
4.780 <u>4.305</u> 4.280	0.99930 0.99103 0.98930	0.31924	0.46996	-1.0000				
4.240	0.99103 0.98930	0.31924	0.47078					
4.2MD	0.98930		0.47078	-1.0000				
		7. 31 96 B		70000				
<b>₹.245</b>	0.98689		0.46486	-1.0000				
		9.31799	0.46881	-1-0000	-			
RESSUPE R	ATIOS FOP	EBOOY_IMLET						****
	PL/ PO	PL/PTF	PL/PTP	X/DPAX				
4.285	0. 98965	0.31 PRO	0.47012	0.39800		•		
4.280	0.98930	0.31868	9.46956	0.43100				
4. 2 AO	0.98933	0.31868	0.46996	0.44900				
4.305	0.99103	0.31924	0.47078	0-48600				
					1.1			
				W 4004 A W				
				-67ac.			and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	
	PL/PN			X/DMAX				
4.390	0.99522	2091 • 0	C-47325	3.84400				The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
RESSIME P	ATERS RO	NEG SHPPUD J	CCAZEON					
	PE / PG	P[ /nTF	PL /PTP	X/NMAX				
3.486	0. 93431	0.30097	0.44384	0.79300			· ·	
3.291						_		
						~ ~ ~		
444 P. 45 P. 44 P. 33	390 390 390 4.390 6.390 RESSURE P	#.245 0.98688 #.390 0.99628 #.390 0.99622 #.390 0.99622 #.390 0.99622 #.390 0.99622 #.390 0.99622 #.390 0.99622 #.390 0.99622 #.390 0.99622	#245 0.9868 0.31790 #270 0.9962 0.32091 #2599 0.99622 0.32091 #2599 84103 FAM MCZZLE FLA  #270 0.99622 0.32091 #5550PE PATINS 20 DEG SHRCUM #270 PL/PN PL/PTF #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091 #4.390 0.99622 0.32091	#245 0.98688 0.31790 0.46881 #370 0.44482 0.22041 0.47325 #370 0.44482 0.22041 0.47325 #25392 Ref123 FAM MOZZLE FLAP  #270 PL/PTP PL/PTP #3.390 0.47325 0.32041 0.47325 #ESSUPE PATINS 20 DEG SHROUD INCATION  #270 PL/PTP #3.390 0.47325 #3.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325 #4.390 0.47325	1.245   0.98660   0.31790   0.46881   0.58900     1.700   0.4462   0.32641   0.47325   1.48880     1.390   0.47327   0.47327   1.0000     1.5399   0.47325   0.47325   0.47325   0.47325     1.390   0.47325   0.32041   0.47325   0.4000     1.5390   0.99622   0.32041   0.47325   0.47325   0.47325     1.0900   0.47325   0.47325   0.47325   0.47325     1.390   0.49622   0.32041   0.47325   0.47325   0.47325     1.390   0.49622   0.32041   0.47325   0.47325   0.47325     1.390   0.49622   0.32041   0.47325   0.47325   0.84400     1.486   0.43431   0.4007   0.44384   0.79300     1.486   0.43431   0.4007   0.44384   0.79300     1.486   0.43431   0.4007   0.44384   0.79300     1.486   0.43431   0.4007   0.44384   0.79300     1.486   0.43431   0.4007   0.44384   0.79300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49300     1.486   0.43431   0.4007   0.44384   0.49400     1.486   0.43431   0.4007   0.44384   0.49400     1.486   0.43431   0.4007   0.44384   0.49400     1.486   0.43431   0.4007   0.44384   0.4400     1.486   0.43431   0.4007   0.44384   0.4400     1.486   0.43431   0.4007   0.44384   0.4400     1.486   0.4407   0.4407   0.4407   0.4407     1.486   0.4407   0.4407   0.4407   0.4407     1.486   0.4407   0.4407   0.4407   0.4407   0.4407     1.486   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.4407   0.44	1.245   0.9868   0.31790   0.46881   0.58900     1.780   0.4442   0.2201   0.47325   -1.0000     1.599   0.99022   0.9291   0.47325   -1.0000     1.599   0.99022   0.32091   0.47325   -1.0000     1.390   0.90622   0.32091   0.47325   -1.0000     1.580PE PATIOS   20 DEG SHRQUD   DCATION     1.470   PL/PTP   X/DMAX     1.390   0.90622   0.32091   0.47325   0.79300     1.390   0.99622   0.32091   0.47325   0.84400     1.390   0.99622   0.32091   0.47325   0.84400     1.486   0.93431   0.30097   0.44384   0.79300     1.486   0.93431   0.30097   0.44384   0.79300     1.486   0.93431   0.30097   0.44384   0.79300     1.486   0.93082   0.29662   0.43743   0.84400     1.486   0.93431   0.30097   0.44384   0.79300     1.486   0.93082   0.29662   0.43743   0.84400     1.486   0.93431   0.30097   0.44384   0.79300     1.486   0.93631   0.92082   0.29662   0.43743   0.84400     1.486   0.93431   0.30097   0.44384   0.79300     1.486   0.93631   0.92082   0.29662   0.43743   0.84400     1.486   0.93431   0.30097   0.44384   0.79300     1.486   0.93631   0.92082   0.29662   0.43743   0.84400     1.486   0.93631   0.92082   0.29662   0.43743   0.84400     1.486   0.93631   0.92082   0.29662   0.43743   0.84400     1.486   0.93631   0.92082   0.29662   0.43743   0.84400	1.245	### 1996   0.31790   0.46881   0.58900   ###################################

ASA-I FWI	2 OBELIA	INARY DATA	06/13/79	CANDETI	PEC 10/24/79 04:07:37.336	FAC AVAKE PGM CO34 RDG 1375
**************************************	NE DRESSURE	PATIOS . PPI	MARY PLUG			
ባ ቁስቃስ	PL	Pt / PO	PI /PTF	PI /PTP	X/DMAT	
?	7.1593	0.49631	0.18002	0.26370	9.72200	
7	14.595	1.0194	0.36649	0.53685	9.82000	•
7	16.791	1.1618	9.42139	0.61727	J. 91 900	
2	17.265	1.1953	0.43355	0.63508	1.0170	
APDIT ION	AL PPESSIPE	PATINS , FLO	M COLITAND	. n.		
n wash	PL	PL /PD	of \ultr	PI /PTP	X/DMAX	the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
2	19.366	1.2716	0.46124	0. £ 75££	0.42200	ம் <b>ந</b> ாக அடிக்கும் அன்ற கண்டு பட்டை நாகள் முறைந்தில் கொழுத்துள்ளும் நடித்து நடி
7	14.340	0.09278	0.36009	0.52749	0.67000	
HUD LI COT	I metcelle	PATIOS . FLO	W SPLITTEP I	. n.		
n 40Ph	PL	PL/PO	PL/PTF	PI /PTP	x/DMAX	Communication (Communication Communication C
7	9.0973	0.42981	0.22844	0.33463	0.50R00	
?	18.234	1.2623	0-45786	0.67070	0.58300	
?	14.160	0.99416	9.36060	0.52022	J.67900	
1091 T 10W	<del>11-00555105</del> -	PATT95 - y - FJE	CTOR SHPOHO			to the first throughout the first throughout development of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of the continue of th
D MUND	PL	PL/PO	PL/PTF	PLAPTE	X/DPAX	
17	14.305	99036	9.25922	0.52620	-1.9000	
12	14.295	0.03767	T. 35897	0.52583	-1.3000	
77	14.290	0.98972	02-35884	0.52565	-1.0000	
?7	150324	0.99105	0.35947	0.57657	-1.0000	
37	14.285	0.98808	0.35872	0.52542	-1.0000	
49	14.225	0.98483	0.35721	0.52326	-1-0000	
MOUTICE	L_PRESSURE	PATINS . FOR	ENCOY INLET			
D MORD	PL	PL/PO	PL/PTF	PL /PTP	X AMO X	
07	14.335	0. 99036	0.3592.1	0.52620	0.39000	•
17	14.295	0.98967	0.75497	0.52583	0.43100	
? >	14.290	0.08932	0.35884	0.57565	0.44900	
27	14.315	0.99105	0. 35947	0.52657	0.48600	
37	14.285	0.98898	0.35P72	0.57547	0.52200	
<b>5</b> ?	14.225	0.98483	0.35721	0.52726	0.56800	
<del></del>	141 345		<del>0. 36122 -</del>	····· ••• • • • • • • • • • • • • • • •	<del>-1-0000</del> —	
	14.300	<del>610424</del>	0-36119	··· ·· · · · · · · · · · · · · · · · ·	-1.0000	Commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of th
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HUBU	PL	PETPA	- PAPER	PI /PTP	X/DMAX	
57	14.395		7.76127	0.52914	-1.0000	
51	14.340	0.99554	0.36117	C. 57896	-1.0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
199 <b>1 T TON</b>	L. PRESSURF.	PATIOS 20	DEG_SHROUD_I	ULAT EDM		
HUBD.	PŁ	PL / PD	PL / PTF	PL /PTP	×/DMAX	
47	14.383	0. 90554	0.36110	0.52896	0.79300	
77	14.385	0.99589	0.36127	0.52914	G. 844Q0	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
10 TT 10 M	L PRESSIME	PATINS , NO	OEG SH®OUD <u>.I</u>	DCATION		
מפרש ר	Pt	Pt / PO	PI /PTF	P! /PTP	Y / DMA K	
P 2	13.576	0.93900	0.34092	0.49070	0.79300	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
	13, 392	0. 92711	0.33628	0.49260	0.84400	
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NOT TENCA	I PRESSIPE	PATINS . PP	MARA LINE					- · -	
AU AUBU	Pt	PI / PP	PI / PTF	PL /PTP	Y/DMAY				
32	9.8522	0.68392	0.27445	0.39667	9. 72200				
27	13.947	0.95521	0.38773	0.55981	0.02000				•
47	15.769	1.0913	C. 43 793	0.63295	0.91900				
52	16.373	1.1793	0.45276	0.45439	1.0170				
									<del></del>
ANDET FONA	I PRESSURE	PATERS . FEE	W SPLITTER I	.n.				•	
VD ሣብጽበ	PL	<b>የ</b> ቲ / ውባ	Pt /PTF	Pt /PTP	XANITAX				
62	16. 547	1.1659	0.46787	0.67622	J-42200				
.7	13.118	0.90786	0.36431	0.52655	J- 67000				
APPLT TONA	L PRESSUPE	PATINS . FLO	W SPLITTER C	- D.	· +				
yn wnep	PL	PL / PO	PL/PTF	PL /PTP	X/DMAX				
77	8,0940	0.56017	0.22479	0.32489	0.50500				
12	20.830	1.4416	0.22717	0.03610	0.58300	**	·		A STATE OF STREET, SE AND STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STREET, STORY STORY STREET, STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY STORY ST
2	14.371	0.99458_	0.39911	0_57684	0.67000				
		PATIOS - EJE							
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VO WORD	PE	PL/PN .	PL/PTF	91 (377	X/DMAX.				
107	14.316	0.9907#	0. 39750	0.57444	-1.0000				
L12	16-311	2.99743	-0.39745	0-57555					
122	14.311	0.00003	0.39745	0.57444	-1.0000				
27	14-331	0.99181	0.39100	0.57524	-1.0000				
137	14.336	0.09000	0.39731	0.57424	-1.0000				
ستستجما	14.246	0. 99594	0.39565	0.57184	-1-0000				
MOTITION :	L PRESSURE	RATIOSFOR	EBODY INLET						<del></del>
VO MORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX				
197	14.316	9.9907N	0.79759	0.57464	0.39800		•		
11?	14.311	0.99043	0.39745	0.57444	J-43100	a			
22	14.311	0, 99043	0.39745	0.57444	0-44900				
	14.33L	0.99181	. 0.39800	0.5.7526	0.58600				
137	14.336	0. 00000	0.37771	0.57424	0.52700				
42	14.246	0.08594	2.39565	0.57184	0.58900				
42	14+396	<del></del>	<del></del>	0.57785	-1.0000				
47	-14.541	<del> 0. 44546</del>	7, 39987	0.97769	1.0000				
ADDITICNA	L PRESSUPE	RATIOS EAN	NOZZLE FLAP					······································	
D AUDD	PL	ምL / ምር	PL/PTF	PL /PTP	X/DMAX	-		* * * * * * * * * * * * * * * * * * *	
47	14.396	9.99631	0.39980	0.57785	-1.0070				
57	14.391	0. 99596	0.30067	0.57765	-1.0000			and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th	
₩ <del>0</del> 01110M	PRESSURE	PATIOS_#_ 20	n <u>EG SHPNU</u> N L	neat tem			<u> </u>		
ID AUDD	Pl	M/PD	-TIPIE	PL /PTP	F/DMAX				
67	_14-391-	0.99596	0.39967	P.57765	0.79300				
33	14.396	0. 99562	0.30053	0.57745	J.#4400 -				
A77171044	1 PRESSUPE	MATINS , 80	DEG SH≢∩UD L	OCAT JON					
n Hubb	PE	P( / P()	PL /PTF	PI /PTP	X/DMAX				
(4) M(-1-1)	13.592				0.79300	-			
[ 7 7 [ <b>P</b> 7		0.9496#	0.3774# 0.37291	C.54558					
	13.427	0.92978 THRUST PAPAM		0.53897	0.84400				
VCOTION &									

		INAPP DATA	06/13/79	rannell	REC 10/24/79 04:09:28.809	FAC REARI	PGM C034 RNG 1377	
Secret Literature	AL PRESSIPE	PATINS . PPE	MARY PLUG					
VP WERD	Pl	PL /PN	PL / PTF	PL /PTP	K/DMAE			
32	12.557	0. 96 86 9	0.41174	0.59984	0-72200			
27	14.928	1.0327	9.48945	0.70122	9. 82009			
47	15.403	1.2655	0.50503	0.72349	0.91900			
K ?	15.577	1.0776	0. 51 076	0.73169	1.0170			
>4DOITION	AL PPESSIPE	PATIOS . FIC	W SPLITTEP I	. n.				
VD WORD	<b>?</b> 1	PL / PO	PL /PTF	PL /PTP	X/DMAX	~		
62	15.048	1.0410	0.49341	0.706 *4	0.42200			
67	13.501	0.93396	0.44268	0.63416	0.67000	. ***	Yes transfer to the period of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the compan	•••
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VN WORD 77	PL 12 247	PL /PG	PE /PTF	0.57695	X/DMAX 0.50600			
45 45	12.293 16.675	0.94970 1.1501	0.40274 0.54513	0.71092	0.5000		management of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th	
72 72	14.339	0.99562	0.55515	0.67589	9.47000			
	X7.JZX	942323&	Neglibe	WALIZEZ .	······································			
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107	14.744	0.99232	0.47034	0.67378	-1-6000			
112	15.344	0.99232	9. 57924_	0.67379	_1.0000			
122	14.334	2.44167	0.47001	0.673%	-1.0000			
127	14.149	0.99266	C. 47050	0.67462	-1.0000			
137 152	14,315	7.99024 0.98437	0.46936 0.46657	0.6:/3#	-1.0000 -1.0000			
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112	14.344	0.99232	0.47034	0.67378	0.43100			
	14.334	0. 99162	0.47001	0-67332	0.44900			
127		2.99266	. 9.47059	0.67402	3.48600			
	14.349			0.6723#	J.52200			
127	14.315	0.99024	0.46936	U+C+23~				
127 137			0.46936 0.46697	0.44839	0.58800			
27  37  42  52	14.315 14.230 	0.99924 0.98437	0.46657	0.44839	-1.0000	en per la laga la mala del mala accessor en considerado mando en mala del del del del del del del del del del	IX issiliativamentitis y (viii) 1989 — issa assa assa vaga vaga issa vervasta dalet viivo hispitaleiseis	
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27 137 142 162 163 163 PROSET (NO. WORD) 157	14.315 14.230 14.696 14.699 M PRP53URS PL 14.634 14.679	0.9924 0.98437 0.98437 0.99680 PATING _ CAN	0.46657 0.47239 0.47247 1.407745 5440 0.47259 0.47259	0.6769 0.6766 0.6769 01.7979 0.6769 0.67693	1.0000 -1.0000 x/max -1.0000			
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162 14.411 0.99720 0.55365 0.80338 -1.0000  DADDIT TOMPL PRESSURE RATERS 20 DEG SUPEUD LOCATION  VID HOPD PL ML/PD ML/PTF PL/PTP X/DMAX  157 14.411 0.99720 0.55365 0.80338 0.79300  172 14.411 0.99720 0.55365 0.80338 0.84400  DADDIT TOMPL PRESSURE RATERS 90 DEG SUPEUD LOCATION  VID HOPD PL ML/PD ML/PTF PL/PTP X/DMAX  VID HOPD PL ML/PTF PL/PTP X/DMAX  102 13.812 0.95577 0.53064 0.77000 0.79300  187 13.697 0.94783 0.52623 0.76360 0.84400	107 112 127 127 137 142	14.371 14.366 14.366 14.376 14.371 14.341 14.281	0.47444 0.99410 0.99410 0.99479 0.99237 0.98823	0.55192 9.55192 0.55231 0.55096 0.54866	0.80153 0.79549 0.79615	0.44900 0.48600 0.52200 0.58800	
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VD WORD PL PL/PD PL/PTF PL/PTP X/DMAX 167 16.411 0.99720 0.55265 0.80338 0.79300 172 14.411 0.99720 0.55365 0.80338 0.84403 >ADDITIONAL PRESSURE RATIOS . 80 DEG SHPCUD LOCATION  VD WORD PL PL/PTF PL/PTP X/DMAX 102 13.412 0.95577 0.53064 0.77000 0.79200 147 13.697 0.94783 0.52623 0.76360 0.84400	107 112 127 127 137 142 142 142 142 142 142 142 142 142 142	14.376 14.366 14.366 14.376 14.376 14.411 14.411 14.411 14.411	0.97444 0.99410 0.99419 0.99237 0.99237 0.9923 0.99729 0.99729	0.55192 0.55192 0.55231 0.55096 0.54866 0.54866 0.9909 0.9909	C. #00## C. #01#3 C. 79649 C. 79615 C. #027# C. #023#	0.44900 0.418600 0.52200 0.52800 -1.0000 -1.0000	
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157	107 112 127 127 137 142 143 143 1449 1449 1449 1449 1449 1449 1	14.371 14.366 14.366 14.376 14.371 14.411 14.411 14.411 14.411 14.411	0.97444 0.99410 0.99479 0.99237 0.99237 0.99723 0.99729 PATIOS # FRN PLABO 0.99729	0.55192 9.55192 9.55231 0.55096 0.54866 9.5999 0.9989 WOFFEE FEAT	C. FOOPR C. BO153 C. 79549 O. 79615 O. FOOTR O. FOOTR PL /PTP C. FOOTR T. FOOTR	0.44900 0.418600 0.52200 0.52800 -1.0000 -1.0000	
172 14.411 0.99720 0.55365 0.60338 0.84400  >ANDITIONAL PRESSURE RATERS . 80 DEG SHRCUD LOCATION  VN HOPD PL PL/PTF PL/PTP X/DMAX  100 13.812 0.95577 0.53064 0.77000 0.79300  187 13.697 0.94783 0.52623 0.76360 2.84400	107 112 127 127 137 142 142 143 143 1449 145 145 145 157 20017 10M	14.376 14.366 14.366 14.376 14.376 14.411 14.411 14.411 14.411 14.411 14.411	0.97444 0.99410 0.99419 0.99237 0.99237 0.9923 0.99729 PATIOS # FAN D.99720 0.99720 0.99720	0.55192 0.55192 0.55231 0.55096 0.54866 0.54866 0.54866 0.54866 0.55365 0.55365	C. FOOPR C. BO153 C. 79549 O. 79615 O. ROSTB O. ROSTB OL /PTP C. FO33R D. FO33R	0.44900 0.418600 0.52200 0.52800 -1:0000 -1:0000 -1:0000 -1:0000	
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VN HNPN PL PL/PTF PL/PTP X/DMAX 1°2 13.412 G.95577 G.53064 G.77000 G.79300 197 13.697 J.947P3 G.52623 G.76360 J.P4400	107 112 127 127 137 142 142 142 142 142 142 142 142 142 142	14.371 14.376 14.376 14.376 14.371 14.411 14.411 14.411 14.411 14.411 14.411 14.411	0.97444 0.99410 0.99479 0.99237 0.99233 0.99723 0.99729 PP71773 # FPN PL/RO 0.99720 RATIOS # 20 PL/PO 0.99720	0.55192 0.55192 0.55231 0.55096 0.54966 0.54966 0.54966 0.55365 0.55365 0.55365 DFG SIMPLUD 1	C.FOOPR C.BO153 C.79549 O.79615 O.RO338 O.RO338 O.RO338 OCATION PL/PTP O.RO338	0.44900 0.48600 0.52200 0.52800 -1.0000 -1.0000 -1.0000 -1.0000	
1° 13.412 0.95577 0.53064 0.77000 0.79200 197 13.697 0.94782 0.52623 0.76360 0.84400	107 112 127 127 137 142 142 143 143 143 143 143 143 143 143 143 143	14.371 14.376 14.376 14.376 14.376 14.411 14.411 14.411 14.411 14.411 14.411 14.411 14.411 14.411	0.97444 0.99410 0.99419 0.99237 0.99237 0.99233 0.99729 PRTIOS # FFR 0.99720 0.99720 0.99720 0.99720 0.99720 0.99720	0.55192 0.55192 0.55231 0.55096 0.54866 0.54866 0.55365 0.55365 DEG SHECUD 1 PL/PTE 0.55365	C. FOOPR C. BO153 C. 79549 O. 79615 O. ROSTB O. ROSTB O. ROSTB O. ROSTB O. ROSTB O. ROSTB O. ROSTB O. ROSTB O. ROSTB	0.44900 0.48600 0.52200 0.52800 -1.0000 -1.0000 -1.0000 -1.0000	
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12	9.7268	0.67460	0.20329	0.29715	0.72200			
27	15, 202	1.0547	0.21772	0.46461	<b>3. #2</b> 500		<i>'</i>	
47	13.925	9.96573	9-29103	0.42539	J. 91900			
52	19, )89	1.3230	0.30401	C. 58315	1.0170	•		
>APPLT TOPA	L PRESSIME	PATINS . FER	W SPLITTER I	I.D.	<ul> <li>A commissionage : A again place white introduction of more cash Ministra, it offers</li> </ul>			
INU MUBU	21	Pt /P/I	PL /PTF	PL /PTP	x/NAX	•	en i appropriate i appropriate i appropriate i	
62	22.377	1.5519	J. 46 768	0.68360	0.42200			
67	18.440	1.2789	0.38541	0.56334	J-67000	* * * ** ** ** ** ** ** ** ** ** ** **	e e e e e e e e e e e e e e e e e e e	-
>ADDIT IONA	L PRESSURE	PATIOS . FLO	M SPI ITTEP E	i.n.				
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77	11.165	0.77431	9.23334		0.50800			
P2	15.921	1.1042	0.33274	0.341 <i>9</i> 7 0.48636	0-58300	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		~
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112	14.264	2. 9992	29312	0-43575	-1-0000			
177	14.264	2-9976	0.20012	0.42575	-1.0000			
127	15=204	0.99134	0.29974	0-43567	-1-0000			
-137	16.259	0.98892	0. 29*01	0.43-60	-1.0000			
ستستعد	14.224	7.98649	9.2972F	0.43453	-1.0000	·	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t	
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112	14.264	3.98976	0.29P12		0-44900			
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112 122 127 127 137 142 153	14.264 14.264 14.294 14.259 14.259 14.374	7.98926 0.98926 0.99134 0.98892 0.98649	0.79812 0.29874 0.29801 0.29778 0.70041 0.30041	0.4357¢ 0.43667 0.43560 0.43453	0.48500 0.52200 0.58800			
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32	15.295	1.0356	0.55651	0.93923	0.72200			- · · · · · · · · · · · · · · · · · · ·
77	15.510	1.0197	0.56473	0.05243	0.82000			
47	15.590	1.0250	3. 56" 24	0.05734	J. 91900			m was one and a
£ 5	15-625	1.0273	0.56851	0.95949	1.5.70			
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62	15.390	1.0112	0.55960	0.94445	3.42200			
67	15.305	1.0062	0.55687	0.93984	0.67000			. I data i tel in indistribution in an indistribution and indistribution and indistribution and indistribution in the indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistribution and indistrib
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-107	14.785	0.97235	0.53795	0.90792	-1.0000			
-112	14-700	0.98646		0.90270	-1-0000			
-127	14.715	0.96349	0.52641	0.90362	-1.9090			
-127	15.000	U.9861A	0.5457	0.92112	-1.0000	·	The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th	nga in managan 1988 alikuwan malamananananankalika katalah katalah katalah malamanan (katalah manaka) (katalah ma
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112	14.700	0.96646	0. 53486	0.99270	0.43100			
122	14.715	0.96745	0.53541	0.90362	0.44900			and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t
127	15-303	0.98618	0.54577	0.92112	0-48600			
137	15.000	0.98618	0.54577	0.97112	0.52200-			
142	14.865	0.97731	0.54086	0.91263	0.58800			
153	14.535	1+0010		0. 93974	-1-0000			
	17.237	1.0013	0.5414	0.93524	=1.0000			
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172	15-230	1.0013	0. 55414	0.93524	0. 54400		in the the course three collections directly and the second	At the last one production distance and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the
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>ADDITIONA LVD HORD 187	PL 14.565	0.95759	0.52905	0.87441	0.79300		Associate and the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of	ann i fheir ainn ann an a-mhair, mheann an an an t-mheann agus ann ar t-mheann ann an t-mheann air an t-mheann
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UND D PL	-12.		1.0017	0.47544	0.79479	dest		1		
WIRD PL RIPED 81/876 PL/879 X 15.289 1.0004 0.47482 0.79575 15.299 1.0010 0.45513 0.79575 15.299 1.0010 0.45513 0.79677 0.79677 0.71710NAL PRESSURE PATIOS 4 NO DEG SHPRING LOCATION X 15.299 0.96176 0.45659 0.76504 17.100 4 0.45601 0.74579	hul alcov		22		Pration					
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1017 IONAL PRESSURE PATIOS 8 NO DEG SHORING LOCATION	72	15.249 15.299	1.0010	0.474#2	0.79575	3. 79303 3. 84400				
MORO PI PP PP PL/PTF PI/PTP X 14.639 0.96176 0.45650 0.76504 1 14.329 0.93755 0.44501 0.74579 TITCH 4 MVACIBER TUBLIST PARRENETEDS	MOTITION		ATINS 4 MO	SHerijn	MUILEUM					
14,329 0,9375 0,44501 0,74579	142	4.639	7 / Pn 0.96176	PL/PTF 0.45650	91/PTP 9.76504	x/OMAX 0.79300		CAP - MARTIN - OF PROPERTY COMMITTEE - P. LEG. 1 VANAGE - THE ST.		
		14.329		\$	0.74579	00*98*0				

ANZ V-1 EM I.	c skefla	IMARY DATA	76/17/79	CARREIT	PFE 10/24/79	C4:4P:05,679 FAF AX6V1 PGW C034 PNG 1382
PULLLUNK	AT DRESSIBE	PATINE . PP1	mibA bill			
ayo ⊯nen	PL	P( / PO	M /PTF	PL /PTP	ANDMAA	
3.7	13.443	9.89177	0.35140	0.59183	J. 72200	
37	16.347	1.0736	0.42784	0.72057	J. 82999	
47	17. 332	1-1172	3.44522	0.74994	3.51900	
52	17.217	1-1293	) <b>.</b> 45705	0.7575#	1.0170	
SATTITION	AL PPESSIPE	RATIOS . FED	W SPLITTEP 1	.n.		
AVD WORD	PŁ	PL / PO	PE /PTF	PL /PTP	I/DMAX	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
62	15.842	1.0392	0.41412	0-69747	3.42200	
67	13.792	0.90473	0.36055	0.60773	0.67000	
MRITTONA C	AL PPFSSIRE	RATIOS . FLE	W SPITTTE F	.D.		
AVD WOPD	Pt	PL/PN	PI /PTF	9{ /PTP	X/DMAX	The first angular of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the secon
77	8.7423	0-57344	0-22852	0.38488	0.50800	
62	22.577	1. 759	0.58816	0.00058	0.58300	a y mark a some mer i a some an er a phone or a phone of the some of a share well and a substitution of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source of the source
92	15-252	1 1005	0.29871	2.671.50	0-67999	
->427171700	AL PPESSUPE	PATEOS 1 ESE	CTCR SIFEUD			
AVD WOPD	P	PL/ PG	PL/PTF	PLEATF	X/DMAX	
-107	14.977	97589	7.38890-	0.65499	-1.0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
	14-817	0.97199	-9-39734	0.65235	-1.0000	
112 -122	14- 952	0.97429	0. 8425	0.64389	-1.0000	
-127	15.137	39307	0.39491	0.6512	-1.0000	
-137	15-1-2	0.99327	0°26282	2.6666	-1.0000	
-142	15.097	2.99031	0.39465	0.56468	-1-0000	
NOT TECCO	AL PRESSUPE	PATICS . FOR	EBODY_INLET			
AVD WORD	PL	Pt /PD	PL / PTF	PL/PTP	X/DMAX	. way a supply of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the statement of the s
107	14.877	0.97589	0.78890	0.45495	0.39 <del>8</del> 99	•
112	14.917	9.97195	0.38734	0.65235	0.43100	
	14. 952	0.97425	O. 38FZ5	0.65789	0-44900	
122		2.99297	2.39491	0.66512	0.48600	
122 127	15-197					
	15-197 15-142	0.99327	0.29543	7.66666	0-52200	
127 137 142			0.295#3 0.39465	0.66469	0-52200 0-58800	
127 137 142	15-142	0.99377	0.39465 		0.58800 -1.7900	and the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of the companion of th
127 137 142	15-142 15-297	0.99327 0.99031	0.39465	0.66469	0.58800	
127 137 142 153	15.142 15.297 15.252 15.252	0.99327 0.99031 1.0305	0.39465 0.3947 0.3947	0.66469	0.58800 -1.7900	
127 127 142 142 143 143 144 145 147 147 147	15.142 15.297 15.252 15.252 ML PRESSUPE	0.99377 9.99031 1:0905 1:0911 RATIOS = EAN	0.39465 0.39497 0.39497 HOLLLE TLAS	0.664.9 9.67199 0.87196	0.58800 -1.0939 -1.0939	
127 127 142 142 143 -147 ->ABOLT 1876 AVD WORD 9	15.142 15.297 15.252 15.252 ML PRESSUPE PL 15.257	0.99377 9.99031 1:0905 1:0911 RATIOS - EAN	0.39465 0.3947 0.3947 HOLLE LAT 0.39419	0.664.9 9.49199 0.67194 PL/PTP 0.67150	0.58800 -1.7900 -1.0979 X/DMAX -1.7000	
127 127 142 142 143 143 144 145 147 147 147	15.142 15.297 15.252 15.252 ML PRESSUPE	0.99377 9.99031 1:0905 1:0911 RATIOS = EAN	0.39465 0.39497 0.39497 HOLLLE TLAS	0.664.9 9.67199 0.87196	0.58800 -1.0939 -1.0939	
127 137 142 143 167 	15.142 15.297 15.252 ML PRESSUPE PL 15.257 15-242	0.99377 9.99031 1:0905 1:0911 RATIOS - EAN	0.39465 0.3947 0.3947 HORRE SLAT PLANT 0.39497	0.66469 9.47159 0.67104 PL/PTP 0.67150 0.67164	0.58800 -1.7900 -1.0979 X/DMAX -1.7000	
127 137 142 157 147	15.142 15.297 15.252 M. PRESSUPE PL 15.257 15.262 AL PRESSUPE PL	0.99377 0.99031 1.0004 1.0011 PATIOS : EAN 1.0394 1.0011	0.39465 0.39497 0.39497 0.39497 0.39497 0.39497 0.4960400 L	0.664.9 9.77199 0.87196 PL/PTP 0.67186 0.67186	0.58800 -1.9900 -1.0979 X/DMAX -1.9090 L.9090	
127 137 142 142 143 144 145 157 167  AND WIPD -159 -167  >ADDITING	15.142 15.297 15.252 ML ERESSUPE PL 15.257 15.262 AL PRESSUPE PL 15.252	0.99377 0.99031 1.0905 1.0911 RATIOS : IAN 1.0304 1.0911 PETIOS : 29 PL/PO 1.0905	0.29465 0.39477 0.39497 0.39497 0.39497 DEG SHROUN L	PL/PTP	0.58800 1.7900 -1.0979 X/DMAX -1.9090 1.0090 X/DMAX 0.79300	
127 137 142 157 147	15.142 15.297 15.252 M. PRESSUPE PL 15.257 15.262 AL PRESSUPE PL	0.99377 0.99031 1.0004 1.0011 PATIOS : EAN 1.0394 1.0011	0.39465 0.39497 0.39497 0.39497 0.39497 0.39497 0.4960400 L	0.664.9 9.77199 0.87196 PL/PTP 0.67186 0.67186	0.58800 -1.9900 -1.0979 X/DMAX -1.9090 L.9090	
127 137 142 142 143 1457	15.142 15.297 15.252 M. PRESSUPE PL 15.257 15.252 4L PRESSUPE PL 15.252 14.252	0.99377 0.99031 1.0905 1.0911 RATIOS : IAN 1.0304 1.0911 PETIOS : 29 PL/PO 1.0905	0.39465 0.39477 0.39477 92111 147 0.39479 0.39497 0.39470 0.39470 0.39470	0.664.9 9.771.99 0.871.94 PL/PTP 0.671.50 0.671.50 0.671.50	0.58800 1.7900 -1.0979 X/DMAX -1.9090 1.0090 X/DMAX 0.79300	
127 137 142 142 142 143 147 149 147 147 147 147 147 149 140 140 140 140 140 140 140 140 140 140	15.142 15.797 15.252 ML PRESSUPE PL 15.257 15.252 AL PRESSUPE PL 15.252 15.252 AL PRESSURE PL	0.99377 9.99031 1.0905 1.0911 PATIOS : FAN 1.0905 1.0905 1.0905 1.0905 1.0905 1.0905 1.0905 1.0905 1.0905	0.39465 0.39477 0.39477 0.39479 0.39497 0.39497 0.39497 0.39477 0.394770 0.394770 0.394770	0.664.9 9.671.99 0.671.50 0.671.50 0.671.60 0.671.50 0.671.50 0.671.50	0.58800 -1.7900 -1.0979 X/DMAX -1.7000 -1.0000 X/DMAX 0.79300 0.84400	
127 137 142 142 143 144 145 147 147 147 240 WORD 147 177 240 WORD 187	15.142 15.297 15.252 ML PRESSUPE PL 15.257 15.252 4L PRESSUPE PL 15.252 14.252 AL PRESSURE PL 14.597	0.99377 9.99031 1.0305 1.0305 1.0305 1.0305 1.0305 1.0305 1.0305 PATIOS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS 20 PLANDS	0.39465 0.39477 0.39477 0.39479 0.39497 0.39497 0.39470 0.39470 0.39470 0.39470	0.66469 9:7159 9:7159 9.67150 9.67150 9.67150 9.67150 9.67150 9.67150	0.58800 -1.7900 -1.0779 X/DMAR -1.7000 1.0000 X/DMAR 0.79300 0.84400	
127 137 142 142 142 143 147 147 240 WORD 147 177 240 WORD 147 177 240 WORD 147 177 240 WORD 147 177	15.142 15.297 15.252 ML PRESSUPE PL 15.257 15.262 AL PRESSUPE PL 15.252 14.252 AL PRESSURE PL 14.252 AL PRESSURE	0.99377 9.99031 1.0905 1.0911 PATIOS : FAN 1.0905 1.0905 1.0905 1.0905 1.0905 1.0905 1.0905 1.0905 1.0905	0.39465 0.39477 0.39477 0.39479 0.39477 0.39477 0.39477 0.39477 0.39477 0.39477	0.664.9 9.671.99 0.671.50 0.671.50 0.671.60 0.671.50 0.671.50 0.671.50	0.58800 -1.7900 -1.0979 X/DMAX -1.7000 -1.0000 X/DMAX 0.79300 0.84400	

45 A-1 EW 15	PRFL 14	THAPY DATE	06/13/79	CARRELL	PFC 10/24/79 04:40:72	.954	FAC RYEVE	PG4 C93	14 R	DG 1343	
ANDITIONAL	perssipe	PATINS . PP	MARY PILLS								
ሰ ዛባፆը	PL	PL / PO	PL/PTF	PL /PTP	* /DMA X						
5	9.3568	3. 55246	9-17584	0-29767	0.72200						
7	17.949	1.1932	0.37001	0.63991	0. 02000						
7	15.994	1.2442	0.39747	0-67284	0.91900						
2	14.449	1.2439	0. 39736	0.67266	1.0170				-		
ADDITIONAL	PRESSURE	PATING . FLO	M SPLITTER I	.0.					<del></del>		
n wnen	PŁ	PI /PI)	PI /PTF	PL /PTP	X/DMAX						
2	19.249	1.2676	0.40493	0.68547	0.42200						
7	16. 329	1.0754	0.34352	0.58152	0.67000		_		-		
ADD ET TONAL	PRESSUPE	PATTINS , FLO	M SPE STTEP O	.n.	~						
n MUSED	PL	PI /PII	PI /PTF	Pt /PTP	Y/DMAX						
7	11.125	9.73261	0-23403	0.39617	0.50800						
2	15.845	1.0434	0.33332	0.56425	0.58300						
2	15.190	1.0003	0.31955_	0.54093	0.67909						
1221 T10WH	PRESSUPE	##1105 v Edi	ETT SHRRYS	<del></del>							
D 40RD	PL	PL/PQ	PL/PTF	PLZETP	X/DHAX						
97	14.835	97693	0.31208	3.52829	-1.0000						
i.2	15.935	2.97552	_0.1135_	0.52704	-1-0000						
22	14.930	7.9249	0.71167	0.52011	-1.0000						
27	15.095	7.99339	0.31734	0.53719	-1.0000						
	15-160	0. 99701	0-3184G	0 53CT	1.0000						
37 52	15.195 PRESSUPE	0.99701 1.0206 RATIOS <u>-</u> EUP	0.31 649 0.31 965 ENTRY INLET	0.5367* 0.54111	-1.0000 -1.0000						
LODITIONAL	15.195 L <u>PRESSUPE</u> PL	1.0206 .RATIOS EDP PL/PD	0.31965 FRITTY THLET PL/PTF	0.54111 PL/PTP	-1-000Q_ X/DMAX						
ADDITIONAL D. HORD	15.195 PRESSUPE PL 14.835	1.0996 RATIOS <u>* F</u> PP PL/PD 0.97693	0.31965 FACTIV [HLET PL/PTF 0.31208	0.54111 Pt /PTP 0.52829	T/0000 X/MAX 0.39900						
ADDITIONAL D. MORD 37	15.195 PRESSUPE PL 14.835 14.900	1.0006 RATIOS . FOP PL/PO 0.97693 0.97462	0.31965 FAMY [HLET PL/PTF 0.31208 0.31134	0.54111 PL/PTP 0.52829 0.52704	*/DMAX 0.39800 0.43100		•				
37 52 ADDITIONAL O WHEN 07 12 27	15.195 PRESSUPE PL 14.835 14.900 14.930	1.0006 RATIOS . FOP PL/PO 0.97693 0.97462 0.97660	0.31965 FACTO [HLET PL/PTF 0.31208 0.31134 0.31197	0.54111 PL/PTP 0.52829 0.52704 0.57811	x/DMAX 0.39800 0.43100 0.44900		•				
ADDITIONAL D. MORD D. 7 12 22	15.195 PRESSUPE PL 14.835 14.900 14.930 15.095	1.0006  RATIOS _ FOP  PL/PO	0.31965 FAITH INLET PL/PTF 0.21208 0.31134 0.31197 0.31734	PL/PTP 0.52R29 0.52704 0.52711	*/DMAX 0-39900 0-43100 0-44900 0-48699		•				
37 52 8001710HAL 0 HORD 07 12 22 27	15.195 PRESSUPE PL 14.835 14.900 14.930 15.095	1.0006 RATIOS . FOP PL/PO 0.97693 0.97462 0.97660 0.99339 0.99701	0.31965 FAMV [MLET PL/PTF 0.31208 0.31134 0.31197 0.31734 0.31849	PL/PTP 0.52R29 0.52R29 0.52R11 0.53R19 0.53915	X/DMAX 0.39900 0.43100 0.44900 0.48609		•				
37 ADDITIONAL D WIRD 07 12 27 27	15.195 PRESSUPE 14.835 14.909 14.930 15.095 15.149 15.149	1.0006  RATIOS . EDP  PL/PD 0.97693 0.97462 0.97660 0.99339 0.99701 1.0006	0.31965 FATTY [HLET PL/PTF 0.31208 0.31134 0.31197 0.31734 0.31849 0.31849	PL/PTP 0.52829 0.52794 0.57811 0.53719 0.53915 0.54111	#/DMAX 0.39900 0.43100 0.44900 0.46600 0.52200						
37 52 8001110085 0 MIRD 12 12 22 27 27	15.195 PRESSUPE PL 14.835 14.900 14.930 15.095 15.140 15.195	1.0706  RATIOS . FOP PL/PO	0.31965 FACTIV [NLET PL/PYF 0.21208 0.31197 0.31197 0.31849 0.31849 0.31965	PL/PTP 0.52R29 0.52R79 0.52R11 9.53R19 0.53R15 0.5411	X/DMAX 0.39000 0.43100 0.44900 0.46690 9.52200 2.58900 -1.0000		•				
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ADDITIONAL DEPO	15.195  PRESSUPE PL 14.475 14.470 14.470 15.095 15.195 15.195 15.200 15.200 15.200 PRESSUPE PL 15.205 15.270 PRESSUPE	1.0006  RATIOS . FOP PL/PO O. 97693 O. 97462 O. 97660 O. 99339 O. 99701 1.0006 1.0010 1.0010 1.0010 1.0010 1.0010 PATIOS . 20 PL/PO PATIOS . 70 PL/PO	0.31965 EARTY INLET PL/PTF 0.31208 0.31134 0.31197 0.31734 0.31849 0.31965 0.71974 0.31976 0.31976 0.31976 DEG SHPRUD I PL/PTF	0.54111  PL/PTP 0.52829 0.52704 0.57811 0.53719 0.53719 0.54170 0.54170 0.54170 0.54120 0.54120 0.54129 0.64129 0.64129 0.64129 0.64129 0.7410N PL/PTP 0.54146	#/DMAX 0.39900 0.43100 0.44900 0.48600 9.52200 2.58500 -1.0000 -1.0000 -1.0000 1.0000 #/DMAX 0.79300 0.84400						
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MACA-I FWIS	BO F! 14	IMARY DATA	06/13/79	CADDETT	PEC 10/24/79	04:50:44.265	FAC MYSYL	PGP C034 PNG 1384
SAPPLE TOTAL	perssinc	RATIOS . PPI	SHIG Adve					e e e e e e e e e e e e e e e e e e e
ND 4080	PI	የር / ዖቦ	PI /PTF	P1 /PTP	X/DMAX			
32	14.481	0.95059	0.26347	0.44638	0.72200			
27	16.756	1.0990	0.30486	0.51615	9.82900			
47	15-611	1.0248	0.28433	0.45368	0.91900			
57	20.38)	1.3778	0.37089	0.62779	1.0170			
JANOT TEONAL	PRESSUPE	PATINS . FLO	W SPEETTER E	. 7.	·			
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2	22.780	1.4953	0.41445	9.79171	0-42200			
7	19.450	1.3030	0.36116	0.61147	0.67000			
JAPEN TICOA	PRESSUPE	RATIOS . FLO	W SPLITTEP F	·. n.			· · · · · · · · · · · · · · · · · · ·	
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7	12-536	0.84260	0-23354	0.39540	0.50800			
2	14.366	1.2056	0.33414	9.56574	0.58300			
2	15-266	1-0321	0_27775	0.47026	0.67000		· · · · · · · · · · · · · · · · · · ·	
4221110WL	PRESSURE	PATIOS . EJE	GT CK SHE COS					
D WORD	1	PL/PD .	PL/PTF	-PLIFTP	X/DMAX		······································	
37	14.951	97488	7.22921	0.45748	-1.0000			
12	14.791	0.9709	2.26911	0.45563_	-1-0000			
22	14.816		N. 76056	0.45640	-1.9000			
27	15000	1.99063	0.27457	0-46487	-1.0000			
.37	19.141	0. 99391	3. 27549	0.46751	1.0000			
44	15.181	0.99654	9.27620	0.46764	-1-0000			
APOLT LONAL.	PRESSUPE	PATIOS . FOR	ERCOY INLET					
D WORD 1	PL	PL/ PO	PL/PTF	PL/PTP	X/DMAX	-		
77	14.951	0.97488	0.27020	0.4574	0.39800		•	
12	14.791	0.97094	0.26911	0.45563	J. 43100	÷		······································
22	14.816	0.97258	0.24956	0.45640	0.44900			
27	15. 391	0. 99063	0.27451	0.46487	0-48600			
77	15.141	0.99391	n. 2754A	0.46641	<b>9.5220</b> 3			
47	15.191	0.99654	0.27629	0.46764	0.58700			
<del></del>	- <del>150251</del>	t++n1t	no 2774A	0,44980	1-0004			
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52  AVD 62 67  AVD 77 67  -101  -112 -127 -137 -143  AVD AVD	DOTTIONAL WORD POST FORMAL WORD 7	PRESSUPE PL 23.748 20.188 PRESSURE PL 13.534 19.384 15.224 PRESSURE PL 14.769 14.769 14.769 14.784 15.054	1.3719  PATINS , FLM  PL/PM 1.5623 1.3201  PATINS , FLM  PL/PM 2.09034 1.2752 1.9015  P-1103 y E3P  PL/PM 0.97554 0.97554 0.97258 0.97258	0.36005 PL /PTF 0.41003 0.34857 PL /PTF 0.23367 0.26295 PL /PTF 0.25603 0.25500 0.25500	0.6115P 0.69693 0.59247 0.59747 0.39718 0.56885 0.446.78	1.0170  X/DMAX 5.42200 0.47000  X/DMAX 0.50800 0.58300 9.67000  X/DMAX -1.0000 -1.0000					
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62 67 77 77 77 77 77 92 92 	DOTTIONAL WORD P	23.748 20.198 PRESSURF 13.534 19.394 15.225 PRESSURF 14.769 14.769 14.774 15.054 15.004	1.5623 1.3281 PATINS , FLM PL/PM 2.89034 1.2752 1.9015 PL/PM 0.97554 0.97169 0.97258	0.41003 0.34 957 W SM ITTEP D PL/PTF 0.23367 0.33467 0.26295 CTCR SMPOUP PL/PTF 0.25603 0.25500	0.69693 0.59247 0.59247 0.39718 0.56885 0.44678	x/DMAX 0.50800 0.57000 0.57300 9.67000 x/DMAX -1.0000 -1.0000					
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AVD 777 77 77 92 92 	WORD P	13.534 19.384 15.224 PRESSUPF 14.879 14.769 14.784 15.054 15.054	PL/PD 2.89034 1.2752 1.9015 PL/PD 0.97554 0.97169 0.97258	PL/PTF 0.23367 0.33467 0.26295 CTCR 3MPOUP PL/PTF 0.25603 0.25500	PI /PTP 0.39718 0.56885 0.446.78  PL /B3P 0.41519 0.43342	0.50800 0.54300 9.67000 X/DHAX -1.0000					
77 82 -92 -92 	WORD 7	13.534 19.394 15.224 PRESSUPE 14.879 14.769 14.784 15.054 15.054	2.89034 1.2752 1.9015 ************************************	0.23367 0.33467 0.26295 0.76295 0.76603 0.25500 0.25500	0.39718 0.56885 0.44678 PL/B3P 0.43519 0.43519	0.50800 0.54300 9.67000 X/DHAX -1.0000					
P?92	WORC 7	19.394 15.224 PRESSUPF 14.879 14.789 14.784 15.054	1.2752 1.9015 ************************************	0.33467 0.26295 0.26295 0.25603 0.25500 0.25500	0.56AR5 0.44678 PL/B3P 0.43519 0.43342	0.58300 9.67990 X/DMAX -1.0000 -1.9990					
- 92 - Avo - 107 - 112 - 127 - 127 - 127 - 127 - 143 - 240 Avo	WORC 7	15.224 PRESSUPT 14.879 14.169 14.784 15.054 15.099	1.0015 PL/PD 0.97554 0.77169 0.97258	PL/PTF 0.25603 0.25500 25726	PL /B3P 0.41519 0.43342	X/DHAX -1.0000 -1.0000					
AVD AVD AVD AVD AVD AVD AVD	WORC 7	14. 979 14. 769 14. 784 15. 054 15. 099	0.97554 0.97554 0.97258 0.97258	PL/PTF 0.25603 0.25500 0.25526	0.43519 0.43342	-1.0000 -1.0000	-				
AVD AVD AVD AVD AVD AVD AVD	WORC 7	14. 979 14. 769 14. 784 15. 054 15. 099	0.97554 0.97554 0.97258 0.97258	PL/PTF 0.25603 0.25500 0.25526	0.43519 0.43342	-1.0000 -1.0000					
-101 -112 -127 -137 -143 	7 2 7 7	14.769 14.784 15.054 15.099	0.97554 0.97169 0.97250 0.99034	0.25603 0.25500 25526	0.43519 0.43342	-1.0000 -1.0000					
	? ? ?	14.769 14.784 15.054 15.099	0.97250	25526	0.43342	-1.0000					
-127 -137 -142 >AG	7 7	15.054		0.25526	0.43386	-1.0000					
-137 -143 	7	15,000									
>AC			0.99339	0.26969	0.44179	-1.0000 -1.0000					
AVD		25.144	0,99626	0.26147	0.44443	1.0000					
	DOLT TONAL	PRESSUPE	RATIOS . FOR	ERODY INLET							
101		r	PL/PO	PL/PTF	PL/PTP	x/DMAX					
112		14.929	0.97554 0.97150	0.25603 0.25500	0.43519	0.39P00 0.43100		•			
127		14.769	0.97258	0.25526	0.43342 0.43386	0.44900					
127	7 <u></u>	15, 254	0.99034	0.25092	9.44179	0.58600					
137 142		15.399 15.144	0.99330 0.99626	7.26069 0.26147	0.44311 0.44443	0.52200 0.5 <b>88</b> 00					•
<del>-1-7</del>		13.219	1.0012	0.70277	0.44603	<del>-1:0000</del>					
-1-11	<del>,</del>	17.217	1:0012	7624777	0.44667						
<del>721</del>		PRESSUPE	RETTING . PAR	APTILE PLAN							
AVO	WARA P	1	PJ /PHI	PI /PTP	PL /PTP	x/DMAX					(
-152		15.219	1.0012	0.2621	C. 64663	-1.0000					
-157	7	ستعلقعط	1.0012	0.26777	0.4467	1-0000			man and manager spaces are sure surely a		
>nř	DOTT TOWAL	PRESSUPE	RATINS . 20	DEG SHANUN I	CCATION						
AVP	WITE P	<b>પ</b>	PL /PN	PL/PTF	PL /PTP	X/DMAX					
167		15.219	1-0012	7.26277	0.44663	0.79300					
177	•	15.219	1.0012	0.26277	0.44663	0_84400		· - · · · - · · <del>-</del> · · <del>-</del>			
>Af	IAPOIT TECO	PRESSURE	RATIOS + 80	DEG SHPOUN t	PCATION						
		ч.	Pt / PO	PI /PTF	PI /PTP	X/[MAX					
192		14.624	0.96205	0.25749	0.47517	0.79300					
1 P 7		14.284 MEASIRED	O. 9796# THPHST PAPAM	0.24662 FTFRS	0.41919	0.84400					
	11134.8			STOMA IC 3.1	149 FT	PF 2.3001	DS# 2.3651	CE4 0.992129	n .		`

	PRF(, \$4)	INARY DATA	06/13/79	CADDELL	MEC 10/24/79 04:53:31.13	FAC 9X6Y1	PG4 C034 PNG 1346	
-470 TT 1044	E UBESSIDE	PATINS . PRI	MARY PEUG				Act of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of	America
n unan	- PL	ም፤ / ምብ	PI /PTF	PI /PTP	X/DMAX			
	13.857		0.23960	0.40631	0.72200			
32		0.91271		0.52875		w in the control of the control of	Control for a 18 or American a ferrance on the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the cont	
7	19-746	1.1890	0. 712/7		0.42000			
7	14.377	0.94183	0.24738	0.41919	<b>0.91</b> 900		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	
12	20. 455	1.3779	0.36060	9.61195	1.0170			
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D WOMB	PL.	PL /PO	PL /PTF	PL /PTP	X/DMAX			-
2	23.774	1.5651	0.41107	0-69658	0.42200		- Mary 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	
7	20.179	1.3278	0.34876	0.59000	J.67000			
APPIT TERRA	L PPESSUPE	PATINS . FER	W SPEITTEP F	.n.	. Jan Bedi Prim improvinteratus indeximation despendente in a			
กษาคา	PĘ	Pt /P1)	PI /PTF	PI /PTP	X/DMAX	the second of the second of the second of	And the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	
7	13.527	0.89049	3.23389	0.39634	0. 50800			
2			0.33459	0.56697	0.58300	a state of part of a	name on a comment of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the secon	and the second
2	19.353 	1.2739	0-26285	0.56697	0.58309			
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n word	PL	PL/PG	PL/PTF	PLANTE	X/DMAX			
07	14.817	0-97540	0.25619-	0.43413	-1.0000			
12	14.747	0.97079	7.25498	0.43208	-1.0000			
27	14.762	7,9247#	11.25424	0.43252	-1.0000			
27	15.032	0.99955	0.25991	0-64043	-1.0000			
37	14:177	0.99251	C. 26669	0.44179	-1.0000	and a state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the		
43	15-122	0.99548	0.26147	0-44397	-1.0000			
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	L PRESSUPE.	entios Fee		Mindratecture manage of managements to a second				
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D WORD	Pt	PL/P0	PL/PTF					
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D WORD 37	Pt 14.417 14.747	PL/PG 3. 97540 U. 97379	PL/PTF 0.25619 0.25698	0.43413	0-39800 0-43100			
D WORD 17 12 27	Pt 14.817 14.747 14.762	PL/PD 1. 97540 U. 97979 0. 97178	PL/PTF 0.25619 0.25698 0.25524	0.43413 0.43209 0.43252	0.39800 0.43100 0.44900			
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D WORD 37 12 22 27	Pt 14.417 14.747 14.762 15.032	PL/PG 1. 97540 U. 97779 0. 97178 D. 98955 3. 99 251	PL/PTF 0-25619 0-25698 0-25524 0-25991 0-76069	0.43413 0.43208 0.43252 0.44043 0.44175	0-39809 0-43103 0-44993 0-48600 9-52230			
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D WORD 17 12 27 27 37 42	Pt 14.417 14.747 14.762 15.932 15.177 15.122	M./PO 1. 97540 U. 97979 O. 97178 D. 98955 3. 90251 U. 93548	PL/PTF 0.25619 0.25498 0.25524 0.25991 0.26147 0.26147	0.43413 0.43208 0.43252 0.44175 0.44175 0.44377	0.39800 0.43103 0.44900 0.52200 0.52200 0.58900			
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D WORD  17  12  27  27  37  42  42  47  48  49  69  69  69  67  67  67  67  67  67  6	Pt 14.817 14.747 14.762 15.332 15.177 15.122 15.191 19.191 PRESSUPF	PL/PO 1. 97540 U. 97979 0. 97178 D. 98995 3. 99 251 0. 93548 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701	PL/PTF 0.25498 0.25594 0.25991 0.26147 0.26147 0.26268 PMIZZE FLAT 0.7624 0.76268 DEG SHPDUD 1	0.43413 0.43208 0.43208 0.43208 0.44175 0.44175 0.44517 0.44517 0.44512 0.44512	0.39809 0.43103 0.44993 0.48600 9.52200 0.58900 1.0000 -1.0000 -1.0000 -1.0000			
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D WORD  17  12  27  27  37  42  42  42  57  40  40  40  40  40  57  APD 17 JONAS  67	Pt 14.747 14.747 14.762 15.032 15.177 15.122 15.191 19.191 PRESSURE Pt 15.191 15.191 PRESSURE Pt 15.296	PL/PO 1. 97540 U. 97540 U. 97579 0. 97178 D. 98955 1. 90281 0. 97548 1. 9001 1. 9701 1. 9001 RATIOS20 PL/PO 1. 9011	PL/PTF 0.25498 0.25594 0.25594 0.25991 0.26147 0.26147 0.26268 MUZZE FLAT 0.76268 DEG SHPRUR I PL/PTF 0.26294	0.43413 0.43252 0.43252 0.43252 0.44175 0.442 7 0.44572 0.44512 0.44512 0.44512 0.44515 0.44556	0.39809 0.43103 0.44993 0.48600 3.52230 0.58900 1.00793 X/DMAX -1.0000 -1.0000			
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D WORD  17  12  27  27  37  42  57  40  67  And It Jones  67  72	Pt 14.747 14.747 14.762 15.932 15.177 15.122 15.191 19.191 15.191 15.191 15.191 15.296 15.296	PL/PO 1. 97540 U. 97540 U. 97579 0. 97178 D. 98955 1. 90281 0. 97548 1. 9001 1. 9701 1. 9001 RATIOS20 PL/PO 1. 9011	PL/PTF 0.25498 0.25594 0.255991 0.26147 0.26147 0.26268 PRIZZE FLAT 0.7624 0.76268  PEG SHPRUR 1 PL/PTF 0.26294 0.26276	0.43413 0.43208 0.43252 0.49043 0.44175 0.443 7 0.443 7 0.44312 0.44512 0.44512 0.44512 0.44512 0.44512 0.44526	0.39809 0.43103 0.44993 0.48600 3.52230 0.58900 1.00793 X/DMAX -1.0000 -1.0000			
D HORD 17 12 27 27 37 42 37 42 57 42 57 ADDITIONAL	Pt 14.747 14.747 14.762 15.932 15.177 15.122 15.191 19.191 15.191 15.191 15.191 15.296 15.296	PL/PO 1. 97540 U. 97979 0. 97178 D. 98995 3. 99251 0. 93548 7. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701	PL/PTF 0.25498 0.25594 0.255991 0.26147 0.26147 0.26268 PRIZZE FLAT 0.7624 0.76268  PEG SHPRUR 1 PL/PTF 0.26294 0.26276	0.43413 0.43208 0.43252 0.49043 0.44175 0.443 7 0.443 7 0.44312 0.44512 0.44512 0.44512 0.44512 0.44512 0.44526	0.39809 0.43103 0.44993 0.48600 3.52230 0.58900 1.00793 X/DMAX -1.0000 -1.0000			
D WORD  17  12  22  27  37  42  42  47  40  40  40  40  40  40  40  40  40	Pt 14.817 14.747 14.747 14.747 15.032 15.177 15.122 15.191 15.191 15.191 15.191 15.191 15.191 15.196 L PRESSUPE.	PL/PO 1. 97540 U. 97979 0. 97178 D. 98955 1. 99251 0. 93548 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 RATIOS 20 PL/PO 1. 9701 RATIOS 20 PL/PO 1. 9701	PL/PTF  0.25498 0.25524 0.25931 0.25969 0.26147 0.26147 0.26167 0.26268  PL/PTF  DEG SHPRUM L PL/PTF  DEG SHPRUM L PL/PTF	0.43413 0.43208 0.43252 0.43252 0.44175 0.44175 0.44517 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512	0.39800 0.43103 0.44993 0.48600 2.52200 0.58500 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
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D MORD  7  12  22  27  37  42  42  57  ADDITIONAL  67  72  ADDITIONAL  67  72  ADDITIONAL  67  72  ADDITIONAL  67  72  ADDITIONAL	Pt 14.817 14.747 14.747 14.747 15.932 15.177 15.122 15.171 17.171 15.171 15.171 15.171 15.171 15.171 15.171 15.171 15.171 15.276 15.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176 17.176	PL/PO 1. 97540 U. 97979 0. 97178 D. 98955 1. 99251 0. 93548 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 1. 9701 RATIOS 20 PL/PO 1. 9701 RATIOS 20 PL/PO 1. 9701	PL/PTF 0.25498 0.25594 0.25594 0.25991 0.26147 0.26147 0.26268  MUZLE FLAP 0.76268  PEG SHPRIM I PI/PTF 0.26276  PEG SHPRIM E PL/PTF 0.25248 0.2651	0.43413 0.43208 0.43252 0.43252 0.44175 0.44175 0.44517 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512 0.44512	0.39800 0.43103 0.44993 0.48600 2.52200 0.58500 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

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2	14.76)	0.07186	7.26 # 69	0.45597	0. 72200					
7	16.792	1.1949	3.20569	2.51837	3.42000					
, <del>,</del>	15.255	1.0244	0.27791	0.47126	0. 91 900					
2	20.319	1.3379	0.37017	0.62772	1.0170					
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2	22.759	1.4985	9-41462	0.70306	0.42200					
7	19.439	1.3963	9. 36143	0.61296	0.67000					*****
ANTIT TOTAL	PRESSURE	RATIOS , FLO	W SPLITTER C	. 0.				<del></del>		
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2	15.225	1.0312	G-27700						<del></del>	
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07	14.430	17-07-649	7.26562	0.45721	-1.9090	- · · · · · ·				
12	14.735	0.97021	26844	0.45520	-1.0000					
7 7	14.765	0.92219	n. 78498	0.45613	-1.0000					
77	15-735	7.99996	0.27390	9-46447	-1.0000					
37	15:190	7, 99350	0.27400	0.46617	-1.0000					
42	15-149	0.99688	0.77591	0.46771	-1-7000	-	a gip , in the state of the control of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	description of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of t		manus of the second of the
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	<u>PRESSIPPE.</u> PL	#[/#G	PI /PTF	PL /PTP	X/OHAX		wa	a anamangang akka sanjabah-be agang angga		
D WORD		PL/PR 0.97669		0.45721	X/0MAX 0.39800			a. anamangang adas sanjahada dal agang masan		Figure Springer of 1 or 1
D #GR9 07	PL	PL/PN	PI /PTF	PL/PTP 0.45721 0.45520				a accompagn agin caginah da Agogo wanta		
0 #QR9 07 12 22	PL 14.900 14.735 14.765	PL/PN 0.97449 0.97021 0.97219	M /PTF 0.26962 0.26844 0.26898	0.45721	0.39800					
D WGRD 07 12 22 27	PL 14.500 14.735	PL/PR 0.97449 0.97021	M /PTF 0.26962 0.26844 0.26898	0.45721	0.39800 0.43100					
D WORD 07 12 22 27	PL 14. 500 14. 735 14. 765 15. 335 15.090	PL/PN 0.97649 0.97021 0.97219 0.91996 0.99359	M /PYF 0.26962 0.26844 0.26898 0.27390 0.27490	0.45721 0.45520 0.45613 0.46647 0.46617	0.39800 0.43100 0.44900 0.46800 0.52200					
0 wgR9 37 12 22 27 37	PL 14. 500 14. 735 14. 765 15. 335 15.090 15.140	PL/PN 0.97449 0.97021 0.97219 0.97396 0.99359	M /PTF 0.26962 0.26844 0.26898 0.27390 0.27490 0.27581	0.45721 0.45520 0.45613 0.46547 0.46617 0.46771	0.39800 0.43100 0.44900 0.58600 0.58600					
D WORD 07 12 22 27 37 42	PL 14.800 14.735 14.765 15.035 15.090 15.140 170.779	PL/PN 0.97649 0.97021 0.97219 0.9359 0.99689	M /PYF 0.26962 0.26844 0.26898 0.27390 0.27590 0.27581	0.45771 0.45520 0.45613 0.46617 0.46617 0.46771	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800					
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n when	PI	PL/PO	PI /PTE	PL /PTF	X/DMAY				
2	6.3279	0.54498	0.17539	0.29698	J. 72200				
7									
	18.929	1.1408	0.38002	0.64348	0.82000				
.7	18.934	1.2381	0.39846	3.67471	0.91900				
2	18.924	1.2394	O.39888	0.47543	1.0170				
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n Mubu	PL	PL/PG	PL /PTF	PL /PTP	x/DMAX				
2	19.196	1.2571	0.40458	0.68506	0.42200				
7	16.234	1.0633	0.34219	0.57942	0.67999				
ATTIONAL	PRESSIME	PAYENS , FLE	W SPLITTEP F		- more farmer arming the electropic appropriate from the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control o				
D WORD	Pŧ	92 / PO	PL /PTF	PL /PTP	X/DMAX		again agus 1 agus ann an an an an an an an an an an an an		
7	11-093	2.72652	0.23361	0.39591	0.50800				
ż	15.909	1. 0354	0.33322	0.56425	0.58300				
ž	15.264	2-93972	0.33173	0.54479	0.47000			· · · · · · · · · · · · · · · · · · ·	
40 <u>0111044</u> 6	PRESSURE	******* * E3E	CTOR SHEDUD		<del></del>				
				21 (27	Y 40MAY				
D WERD	PE	P) / PO	PL/PTF	PL/BSP	X/DMAX				
7	14.919	0.57712	0.31446	0.53248	-1.0000				
12	14-866	0.97372	ــ دود اوسوب	0.53051					
77	14.999	0.07514	7:31383	0.53141	-1-0000				
27	15.149	99219	0.31931	0.54069	-1.0000				
37	15.210	0.99677	0.32079	0.54910	-1.0000				
4?	15.274	1.0904	0.32195	0.54515	1-3000				
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ADDITIONAL	L. PRESSURE.	RATIOS FOR	EBODY INLET	0.54515	1-1000				
ADDITIONAL	L_PRESSURE	RATIOSFOF	PL/PTF	0.54515 PL/PTP	X/DMAX				
ADDITIONAL	L. PRESSURE.	RATIOS FOR	EBODY INLET	0.54515	1-1000				and dynamics and
DOLLIONAL DAURD	PRESSURE	PL/PD 9.97712	PL/PTF 0.31446	0.54515 PL/PTP 0.53248	X/DMAX 0-39900				
ADDITIONAL D WORD D7 12	PL 14.919	RATIOSFOF	PL/PTF 0.31446 0.31330	0.54515 PL/PTP 0.53248 0.53051	X/DMAX 0.39#00 0.43190				
ADDITIONAL D. WORD 07 12 22	PL 14.919 14.964 14.889	PL/PD PL/PD 0-97712 0-97352 0-97516	PL/PYF 0-31446 0-21330 0-31783	0.54515 	X/DMAX 0.39900 0.43190 0.44590				
A221TIONAL D WORD 07 12 22 27	PL 14.919 14.964 14.889	PL/PD 0.97712 0.9752 0.97516 0.99219	PL/PTF 0-31446 0-21330 0-31783 0-31931	PL/PTP 0.53248 0.53051 0.53161 0.55169	X/DMAX 0.39700 0.43190 0.44900				
A221110NAL 0 HORD 07 12 27 27	PL 14.919 14.964 14.889 15.149 15.219	PL/PD 0.97712 0.97352 0.97556 0.97519 0.99677	PL/PTF 0-31446 0-31330 0-31283 0-31931 0-32079	0.54515 PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319	X/DMAX 0-39800 0-43190 0-44900 0-52200				
A 221 T IONAL D WORD 27 12 27 27 27	PRESSURE 14.919 14.964 14.889 15.149 15.219 15.274	PL/PD 0-97712 0-97352 0-97516 0-99219 0-99677 1-9004	PL/PTF 0-31446 0-21330 0-31783 0-31931	PL/PTP 0.53248 0.53051 0.53161 0.55169	X/DMAX 0.39700 0.43190 0.44900				
37 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PRESSURE 14.919 14.964 14.889 15.149 15.219 15.274	PL/PD 0.97712 0.9752 0.9756 0.99219 0.99677 1.9704	PL/PTF 0.31446 0.31330 0.31383 0.31931 0.32079 0.32195	0.54515 PL/PTP 0.53748 0.53051 0.53161 0.54069 0.54319 0.54515	X/DMAX 0-39900 0-43190 0-44900 0-52200 0-52800				
771110NAL 7 WORD 77 12 22 27 27 27 27	PRESSURE 14.919 14.964 14.869 15.149 15.219 15.276	PL/PD 0-97712 0-97352 0-97516 0-99219 0-99677 1-9004	PL/PTF 0-31446 0-21330 0-31331 0-31931 0-32079 0-32195 0-22175	PL/PTP 0.53248 0.53051 0.53161 0.54069 0.54319 0.54515 0.74461	X/DMAX 0.39800 0.43190 0.44903 0.4200 0.5200 0.5200				
ADDITIONAL D WORD D7 12 27 27 27 27 27 27 27 27 27 27 27 27 27	PRESSURE  14.919 14.964 14.889 15.149 15.274 17.279 17.209	PL/PD 9-97712 9-97752 0-97516 0-99219 9-99677 1-9704 0-99972 9-99972	PL/PTF 0-31446 0-21330 0-31381 0-31931 0-32079 0-32195 0-32173	PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319 0.54515 0.74479	X/DMAX 0.39400 0.43190 0.44903 0.42200 0.52200 0.58000 -1.0000				
D WORD  O WORD  O YOU  O YOU  O YOU  O YOU  O WORD  O WORD  O WORD	PRESSURE  14.919 14.964 14.664 15.149 15.219 15.274 17.239 17.209	PL/PD 0.97712 0.97752 0.97550 0.97519 0.99219 0.99677 1.9704 0.99972 P47193: # FAM 0.99973	PL/PTF 0.31446 0.21330 0.31331 0.31931 0.32079 0.32195 0.22173	PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319 0.54515 0.54479	X/DMAX 0.39800 0.43190 0.44593 0.52200 0.52200 0.58800 -1.0000				
O HORD  O HORD  O HORD  O HORD  O HORD  O HORD  O HORD	PRESSURE  14.919 14.964 14.889 15.149 15.274 17.279 17.209	PL/PD 9-97712 9-97752 0-97516 0-99219 9-99677 1-9704 0-99972 9-99972	PL/PTF 0-31446 0-21330 0-31381 0-31931 0-32079 0-32195 0-32173	PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319 0.54515 0.74479	X/DMAX 0.39400 0.43190 0.44903 0.42200 0.52200 0.58000 -1.0000				
DOLITIONAL D. WORD D. T. T. T. T. T. T. T. T. T. T. T. T. T.	PRESSURE  14.919 14.964 14.889 15.219 15.274 17.259 17.269  PL 15.259	PL/PD 0.97712 0.97752 0.97550 0.97519 0.99219 0.99677 1.9704 0.99972 P47193: # FAM 0.99973	PL/PTF 0-31446 0-21330 0-31931 0-31931 0-32195 0-22175 NPZZZZ ELAP 0-32163 0-32177	PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319 0.54515 0.54479	X/DMAX 0.39A00 0.43190 0.44593 0.48600 0.52200 0.58800 -1.0000 -1.0000				
ADDITIONAL D WORD DT 12 27 27 27 27 27 27 27 27 27 27 27 27 27	PRESSURE  14.919 14.964 14.864 15.149 15.274 17.279 17.209  PL 15.259 15.259 15.254  PRESSURE	PL/PD 0.97712 0.97752 0.97550 0.97519 0.99219 0.99677 1.9004 0.99972 P47193 # FPM PL/PD 7.99939 0.99972 P47195 # 20	PL/PTF 0-31446 0-21330 0-31931 0-31931 0-32195 0-22175 NPZZZZ ELAP 0-32163 0-32177	0.54515  PL/PTP 0.53748 0.53051 0.53141 0.54069 0.54319 0.54515 0.74461 0.54461 0.54479	X/DMAX 0.39A00 0.43190 0.44593 0.48600 0.52200 0.58800 -1.0000 -1.0000				
ADDITIONAL D WORD DT 12 27 27 27 27 27 27 27 27 27 27 27 27 27	PRESSURE  14.919 14.964 14.889 15.219 15.274 17.239 17.209  PL 15.259 15.259 15.254  PRESSURE	PATIOS FOR PL/PD 0. 97712 0. 97712 0. 97516 0. 99219 0. 99677 1. 9704 0. 99972 PATIOS 20 PL/PD	PL/PTF 0-31446 0-21330 0-31283 0-31283 0-31931 0-32195 0-22173 NOTELE FLAT 0-32177 DEG SHROUN   PL/PTF	PL/PTP 0.53748 0.53751 0.53161 0.54069 0.54319 0.54515 0.74461 0.54479 PL/PTP 0.54461 0.54479	X/DMAX 0.39800 0.43190 0.44903 0.42200 0.52200 0.58800 -1.0000 -1.0000 -1.0000				
ADDITIONAL D WORD D7 12 27 27 27 27 27 27 27 27 27 27 27 27 27	PRESSURE  14.919 14.964 14.864 15.149 15.274 17.279 17.209  PL 15.259 15.259 15.254  PRESSURE	PL/PD 0.97712 0.97752 0.97550 0.97519 0.99219 0.99677 1.9004 0.99972 P47193 # FPM PL/PD 7.99939 0.99972 P47195 # 20	PL/PTF 0.31446 0.21330 0.31331 0.31931 0.32079 0.32195 0.22175 0.22175 0.22175 0.32175	0.54515  PL/PTP 0.53748 0.53051 0.53141 0.54069 0.54319 0.54515 0.74461 0.54461 0.54479	X/DMAX 0.39900 0.49190 0.44902 0.48600 0.52200 0.58800 -1.0000 -1.0000				
ADDITIONAL D WORD DT 12 27 27 27 27 27 27 27 27 27 27 27 27 27	PRESSURE  14.919 14.964 14.889 15.149 15.219 15.276 17.259 17.259 17.259 PRESSURE  PRESSURE  PL 15.269 15.264	PL/PD 0.97712 0.97752 0.97552 0.97556 0.99219 0.99677 1.9004 0.99972 P47195 2.20 PL/PD 1.9000 0.99972	PL/PTF 0-31446 0-31330 0-31283 0-31283 0-32195 0-32175  NOTICE CLAP PL/PTF 0-32163 0-32173  DEG SHROUD   PL/PTF 0-32184 0-32173	PL/PTP 0.53748 0.53051 0.53141 0.54069 0.54515 0.54461 0.54461 0.54479 PL/PTP 0.54467 0.54479	X/DMAX 0.39800 0.43190 0.44593 0.48600 0.52200 9.58800 -1.0000 -1.0000 -1.0000				
ADDITIONAL D WORD D7 12 27 27 37 42 27 37 42 27 40 40 40 40 40 40 40 40 40 40 40 40 40	PRESSURE  14.919 14.964 14.889 15.149 15.219 15.274 17.299 17.209 PRESSURE  PL 15.259 15.754  PRESSURE  PL 15.269 15.264  PRESSURE	PL/PD 0-97712 0-97712 0-97752 0-97516 0-97516 0-99219 0-94677 1-9704 0-99972 PATIOS 1-PN 1-97939 0-99972 PATIOS 20 PL/PD 1-9700 0-99972 PATIOS 3-90	PL/PTF 0.31446 0.21330 0.31931 0.31931 0.32195 0.32173  NOCCLE CLAP PL/PTF 0.32163 0.32173  DEG SHROUD 1 PL/PTF 0.32184 0.32173  DEG SHROUD 1	PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319 0.54515 0.74461 0.54479 PL/PTP 0.54461 0.54479 PL/PTP 0.54467 0.54479	X/DMAX 0.39800 0.43190 0.44503 0.42200 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 3.79303 3.94400				
ADDITIONAL O WORD OT 12 77 27 27 37 42 27 37 42 27 40 52 77 40 52 40 60 77 77 40 40 60 77 72 40 40 60 77 72 40 40 60 60 60 60 60 60 60 60 60 60 60 60 60	PRESSURE  14.919 14.964 14.964 14.889 15.149 15.274 17.279 17.209  PRESSURE  PL 15.259 15.259 15.264  PRESSURE  PL 15.269 15.264	PL/PD 9-97712 9-97712 9-97712 9-977516 9-99219 9-99677 1-9704 9-99972 PATIOS 1-PM 1-99939 0-99972 PATIOS 1-20 PL/PD 1-97000 0-99972 PATIOS 1-90 0-1/PD	PL/PTF 0.31446 0.21330 0.31331 0.31931 0.32195 0.32195 0.32175 0.32173 DEG SHROUN I PL/PTF 0.32184 0.32173 DEG SHROUN I PL/PTF	0.54515  PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319 0.54515 0.74461 0.54479 PL/PTP 0.54467 0.54479 PL/PTP 0.54467 0.54479	X/DMAX 0.39900 0.49190 0.44503 0.48600 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX 0.79303 J.94400				
ADDITIONAL O WORD OT 12 77 27 37 40 40 52 77 AD WORD 77 AD WORD 77 72 AD WORD 77 AD WORD 77 AD WORD 77 AD WORD 77 AD WORD 77 AD WORD 77	PRESSURE  14.919 14.964 14.889 15.149 15.274 17.279 17.209  PRESSURE  PRESSURE  PL 15.269 15.264  PRESSURE  PL 15.269 17.264  PRESSURE  PL 15.264  PRESSURE  PL 15.264	PATIOS FOP PL/PD 0. 97712 0. 97712 0. 97716 0. 99219 0. 99677 1. 9704 0. 99972 PATIOS 20 PL/PD 1. 9700 0. 99972 PATIOS 20 PL/PD 1. 9700 0. 99972 PATIOS 90 PL/PD 0. 995518	PL/PTF 0-31446 0-21330 0-31283 0-31283 0-31283 0-32195 0-22173 PL/PTF 0-32184 0-32173 DEG SHPOUD L PL/PTF 0-32184 0-32173	PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319 0.54515 0.74461 0.54479 PL/PTP 0.54467 0.54479 PL/PTP 0.54467 0.54479 PL/PTP 0.54479 PL/PTP 0.54479	X/DMAX 0.39900 0.43190 0.44993 0.48600 0.52200 0.58800 -1.0000 -1.0000 -1.0000 X/DMAX 0.79303 J.94400				
ADDITIONAL O WORD OT 12 72 27 37 42 42 77 40 40 FORD 52 77 ADDITIONAL O WORD 77 72 ADDITIONAL O WORD 77 72 ADDITIONAL	PRESSURE  14.919 14.964 14.889 15.219 15.274 17.259 17.269 15.259 15.254  PRESSURE  PL 15.269 15.264  PRESSUPE  PL 14.584 14.584 14.214	PL/PD 9-97712 9-97712 9-97712 9-977516 9-99219 9-99677 1-9704 9-99972 PATIOS 1-PM 1-99939 0-99972 PATIOS 1-20 PL/PD 1-97000 0-99972 PATIOS 1-90 0-1/PD	PL/PTF 0.31446 0.21330 0.31231 0.31931 0.32195 0.22173 NPZZZZ ELAP PL/PTF 0.32184 0.32173 DEG SHROUN   PL/PTF 0.32184 0.32173 DEG SHROUN   PL/PTF 0.30740 0.22960	0.54515  PL/PTP 0.53248 0.53051 0.53141 0.54069 0.54319 0.54515 0.74461 0.54479 PL/PTP 0.54467 0.54479 PL/PTP 0.54467 0.54479	X/DMAX 0.39900 0.49190 0.44503 0.48600 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX 0.79303 J.94400				

VASA-LENT	S DREE 14	INARY DATA	06/13/79	CADDELL	REC 10/24/79 N6:57:49.9N9	FAC RESEL	Run PGM 1934 PNG 1389	
>ADDITION	AL PRESSIPE	P17175 . PP1	MAPY PEHG					
AVD WOPD	PL	P( /PG	PI /PTF	OI /PTP	X/DMAX			
37	13.426	2.57962	3.35118	0.59156	0.72200			
37	15.316	1.0705	0.42740	0.71966	0.82000			
47	16.996	1.1151	0.44521	0.74995	0.91900			
52	17.176	1.1269	1).44997	0.75790	1.0170			
>A00;1 104	AL PRESSURE	RATIOS . FLO	m Shi itteb i	. 9.				
AVO HOPO	PL	PL/PO	Pt /PTF	PI /PTP	X/DMAX			
62	15.401	1.0367	0.41391	0.69723	0.42200			
4.7	13.751	0.99224	0.36021	0.6067#	0.67000			
>ADDITION	AL PRESSUPE	PATINS , FLO	M SPLITTER F	· D.				
AND HORD		m /en	94 / 575	PI /PTP	w 40m a w			
AVO HOPD	PL	PI / PO	PI / PTF		X/DMAX			
77	0.7050	0.57114	9. 22 02	0.30411	0.50800		en mer en en en en en en en en en en en en en	
<b>P</b> 2	22.577	1.4776	0.58991	0.99370	7. 58300			
.92	15.241	1.0200	0.39924	0.67253	0-67900			
7200223014	AL PRESSURE	R47105 + E4E	<del>CTOR SHADUS</del>					·-· · · ·
AVD WOPD	PL	PL /PD	PL/PTF	PLANTS	X/DMAX			
-107	14.466	17.42539	0.38047	9.6559R	-1.0000			
			38785					
-112	<u> 14. 596 : .</u>	0.97146		0.65333	-1-0000			
-122	14.974	0.47217	U- 38405	0.65422	-1.0000			
-127	15-004	U. GRORT	0.39518	0344569	-1-0000			
-137	15.126							
		0. 99245	0.39623	0.66745	1.0000			
-Lagran	15.096	0.98983	0° 3021 u	0.66745	-1.0000			
-140 ->47717104/	15.096 AL PRESSIPE	0.98983 RATIOS . FOR	O. 3951 P	0.66569	1.300			
=140 _>477171044 AVD_WORD	15.096 AL PRESSIPE PL	0.98983 RATIOS - FOR PL/PO	n. 3951 P <u>Francy Inlet</u> Pl/PTF	0.66569 PL/PTP	x/D#AX			
-14	15.096 AL PRESSUPE PL 14.866	0.98983 RATIOS : FOR PI /PO 0.97539	0.3951 P ERODY INLEY PL/PTF 0.38942	0.66569 Pt /PTP 0.6559P	x/DMAK 2.39800			
=140 	15.096 AL PRESSUPE PL 14.866 14.976	0.98983 RATIOS . FOR PI /PO 0.97539 0.97146	0.3951 P FRMDY INLEY M. /PTF 0.38942 0.38785	PL /PTP 0-6559P 0-65333	X/DMAK 1.39900 0.43100			
>47717]044 AVD WORD 107 112 127	15.096 AL PRESSUPE PL 14.866 14.996 14.926	0.98983  RATINS . FOP  PI /PN 0.07539 0.97146 0.97277	0.3951 P FRITOY INLET MI /PTF 0.38785 0.38785	PL /PTP 0-6559R 0-65333 0-65422	x/DMAK 1.3980D 0.43100 0.44900			
>47717 JANA AVD WORD 107 112 127	15.096 AL PRESSUPE PL 14.866 14.976	0.98983 RATIOS . FOR PI /PO 0.97539 0.97146	0.3951 P FRMDY INLEY M. /PTF 0.38942 0.38785	PL /PTP 0-6559P 0-65333	X/DMAK 1.39900 0.43100			
>47717]044 AVD WORD 107 112 127	15.096 AL PRESSUPE PL 14.866 14.996 14.926	0.98983  RATINS . FOP  PI /PN 0.07539 0.97146 0.97277	0.3951 P FRITOY INLET MI /PTF 0.38785 0.38785	PL /PTP 0-6559R 0-65333 0-65422	x/DMAK 1.3980D 0.43100 0.44900			
>A991TINWA AVD WORD 107 112 127 127 127	15.046 AL PRESSIME PL 14.866 14.476 15.276 15.126	0.98983 RATINS : FOR PI /PN 0.97539 0.97146 0.97277 0.98983 0.99245	0.3951 P FRODY INLEY PL/PTF 0.38942 0.38785 0.3865 0.39518 0.39623	PL/PTP 0-6559R 0-65392 0-65392 0-65422 0-66569 0-66745	x/DMAK 2.39800 0.43100 2.44900 2.52200			
>47017 INWA AVD WORD 107 112 127 127 137 142	15.046 AL PRESSIPE PL 14.866 14.976 14.976 15.086	0.9P983  RATINS _ FOP  PI /PO 0.97539 0.97146 0.97277 0.9083 0.99245 0.9883	0.3951 P FRITOY INLET PL/PTF 0.38765 0.38765 0.3951 P 0.3951 P 0.3951 P	PL/PTP 0.6559P 0.65333 0.65422 0.66569	x/DMAK 7.39800 0.43100 0.44900 0.52200 0.58800			
>A991TINWA AVD WORD 107 112 127 127 127	15.046 AL PRESSIME PL 14.866 14.476 15.276 15.126	0.98983 RATINS : FOR PI /PN 0.97539 0.97146 0.97277 0.98983 0.99245	0.3951 P FRODY INLEY PL/PTF 0.38942 0.38785 0.3865 0.39518 0.39623	PL/PTP 0-6559R 0-65392 0-65392 0-65422 0-66569 0-66745	x/DMAK 2.39800 0.43100 2.44900 2.52200			
>A701T ION/ AVD WORD 107 112 127 127 137 142	15.046 AL PRESSUPE PL 14.866 14.976 15.176 15.176 15.276	0.9P983  RATIOS . FOP  PI /PO 0.97539 0.97146 0.97277 0.98983 0.99245 0.98983 1.9990 1.0705	0.3951 P FRITOY INLEY PL/PTF 0.38785 0.38785 0.39518 0.39623 0.30518 0.39623	Pt /PTP 0.6559P 0.6559P 0.6533 0.65622 0.66569 0.66569	x/DMAK 1.3980D 0.43100 0.44900 0.52200 0.52200 1.0000			
>A701T ION/ AVD WORD 107 112 127 127 137 142	15.046 AL PRESSIPE PL 14.866 14.976 15.276 15.276 15.276 17.241	0.9P983  RATIOS , FOR PI / PO 0.97539 0.97146 0.97277 0.98983 0.99245 0.9893 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9988 1.9988 1.9988 1.9988 1.9988 1.9988 1.9988 1.9988 1.9988 1.	0.3951 P FRITOY INLEY PL/PTF 0.38785 0.38785 0.39518 0.39623 0.30518 0.39623	Pt /PTP 0.6559P 0.6559P 0.6533 0.65622 0.66569 0.66569	x/DMAK 1.3980D 0.43100 0.44900 0.52200 0.52200 1.0000			
>A701TION/ AVD WORD 107 112 127 127 127 127 127 127 127 127 12	15.046  AL PRESSUPE  PL 14.866 14.976 15.046 15.046 15.086 17.248 14.248	0.9P983  RATIOS , FOP PI /PO 0.07539 0.97166 0.97277 0.09083 0.99245 0.98983 1.90905	0.3951 P FRIDY INLEY M./PTF 0.38942 0.38785 0.38637 0.39518 0.39518 0.39518 0.39518	PL /PTP	x/DMAX 1.39800 0.43100 0.44900 2.49600 0.52200 0.58800 -1.0000			
>A701TIONA AVD WORD 107 112 127 127 137 142 137 142 137 142 137 142 137 142 137	15.046 AL PRESSUPE PL 14.866 14.976 15.046 15.126 15.276 17.241 17.246	0.9P983  RATIOS , FOR PI / PO 0.97539 0.97146 0.97277 0.98983 0.99245 0.9893 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9998 1.9988 1.9988 1.9988 1.9988 1.9988 1.9988 1.9988 1.9988 1.9988 1.	0.3951 P FRIDY INLET M / PTF 0.38942 0.38737 0.39518 0.39518 0.39518 0.39518 0.39518	PL /PTP 0.6559P 0.6559P 0.65333 0.65422 0.6569 0.66764 0.66569 0.67799 0.67799	x/DMA x 1, 19900 0, 43100 0, 44900 0, 52200 0, 58800 119000			
>4771TION/ AVD WORD 107 112 127 127 147 142 -1-7 AVD WORD -152 -157	PL 14.866 14.866 14.976 15.176 15.176 15.286 17.291 17.298 M 27.291 17.298 M 27.291 17.298	0.9P983  RATIOS , FOP PI /PO 0.97539 0.97146 0.97277 0.98983 0.99893 1.9990 1.0703 PI /PO 1.0500 1.0003	0.3951 P FRIDY INLET M./PTF 0.38942 0.38737 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518	PL/PTP 0.6559P 0.6559P 0.6559P 0.6533 0.65422 0.66569 0.66744 0.66569 0.67779 0.67275	x/DMAX 9.39800 0.43100 9.49600 9.49600 0.52200 0.58800 -1.0000			
>A991710N/ AVD WORD 107 112 127 127 137 142 142 142 142 142 142 142 142 142 142	PL 14.866 14.876 15.276 15.276 17.278 17.278 15.261 15.266 15.266 15.276 17.278 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266	0.9P983  RATIOS _ FOP  PI /PO	0.3951 P FRODY INLEY PL/PTF 0.38785 0.38785 0.39518 0.39623 0.39628 0.39623 0.39628 0.39623 0.39628 0.39628	PL/PTP 0.6559P 0.6559P 0.65332 0.65422 0.66569 0.67275 PL/PTP 9:63263 0.67275	x/DMAK 7.39900 0.43100 2.44900 2.4500 0.52200 0.58800 -1:0000 -1.0000 -1.0000			
>A771TION/ AVD MORD 107 112 127 127 147 142 142 147 -147 >AVD MORD -157 >A771TION AVD MORD	PL 15_261   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266   15_266	0.9P983  RATIOS _ FOP  PI /PO 0.97539 0.97146 0.97277 0.98983 0.99983 1.9090 1.0703  PATIOS _ FOR  PATIOS _ 20  PI /PO	0.3951 P FRITTY INLEY PL/PTF 0.38937 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P 0.3951 P	PL /PTP 0.6559P 0.6559P 0.6559P 0.6569 0.66569 0.66569 0.67275 PL /PTP 9.67275  DCATION PL /PTP	X/DMAK 1.39800 0.43100 0.44900 0.52200 0.58800 1.0000 -I.0000 -I.0000			
>A991710N/ AVD WORD 107 112 127 127 137 142 142 142 142 142 142 142 142 142 142	PL 14.866 14.876 15.276 15.276 17.278 17.278 15.261 15.266 15.266 15.276 17.278 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266 15.266	0.9P983  RATIOS _ FOP  PI /PO	0.3951 P FRODY INLEY PL/PTF 0.38785 0.38785 0.39518 0.39623 0.39628 0.39623 0.39628 0.39623 0.39628 0.39628	PL/PTP 0.6559P 0.6559P 0.65332 0.65422 0.66569 0.67275 PL/PTP 9:63263 0.67275	x/DMAK 7.39900 0.43100 2.44900 2.4500 0.52200 0.58800 -1:0000 -1.0000 -1.0000			
>A771TION/ AVD MORD 107 112 127 127 127 142 142 1-7 >AVD MORD -152 -157 >A771TION AVD MORD 167 177	PL 14.866 14.976 15.241 15.246 15.276 15.241 15.266 15.276 15.241 15.266 15.241 15.266	0.9P983  RATIOS , FOP  PI /PO 0.97539 0.97146 0.97277 0.98983 0.98983 1.99983 1.9999 1.0103  PATIOS , FOR 0.903 PATIOS , 20  PI /PO 0.99967	0.3951 P FRITTY INLEY 0.38785 0.38787 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518	PL /PTP 0.6559P 0.6559P 0.65332 0.65422 0.66569 0.66765 0.66767 0.67273 PL /PTP 0.67231 0.67273	X/DMAK 1, 19800 0, 43100 0, 44900 0, 52200 0, 52200 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 58800 -1, 588000 -1, 588000 -1, 588000 -1, 5880000 -1, 58800000000000000000000000000000000			
>4771TION/ AVD WORD 107 112 127 127 127 127 147 -147 -157 -157 -157 -157 -157 -157 -157 -167 177 >4771TION/	PL 15.246  AL PRESSUPE PL 14.866 14.976 15.176 15.286 17.298  PL 15.246  AL PRESSUPE PL 15.236 15.241  AL PRESSUPE	0.9P983  RATIOS , FOP  PI /PO 0.97539 0.97146 0.97277 0.98983 0.99893 1.9990 1.0103  PATIOS , FO  PATIOS , FO	0.3951 P FRIDY INLET  M / PTF 0.38942 0.38937 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518 0.39518	PL /PTP	X/DMA X 1, 19800 0, 43100 0, 44900 0, 52200 0, 58800 -1, 00700  X/DMA X -1, 0000 -I, 0000 0, 79300 0, 84400			
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52	15.673	1.0260	0.56643	0.95747	1.0170	s entended of the term of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the
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	17.379	1.1331	0.62553	1.0574	J.5#300	
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07	14.863	0.97298	0.53716	0.00797	-1.0000	
12	14.783	0.96774	25.53425	Q.90309		
22	14.799	O-SHAT?	No53670	0.90400	-1.0000	
27	15.078	2. 99706	0.54497	0.92111	-1.0000	
37	15. 763	7.98608	0.54437	7. +3020	-1.0000	The second second second is a second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second
63	14.928 N PRESSURE	0.97724 RATIOS . FOR	0.53949 ERMY INLEY	0.01193	1,0000	
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62 ADD [T 10NA D WORD D7	PRESSURE PL 14.863	RATIOS . FOR PL/PO 0.97298	M /PTF 0.53714	Pt /PTP 0.90797	X/DMAX 0.39800	•
62 ADD <u>IT IONA</u> D WORD DT 12	N PRESSURE PL 14.863 14.783	PL /PD PL /PD D. 97298 D. 96774	M /PTF 0.53714 0.53425	P1 /PTP 0.90797 0.90309	X/DMAX 0.39800 0.43100	•
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ADD IT 10NA D. WORD D7 12 22	N PRESSURE PL 14.863 14.783	PL /PO PL /PO O. 9729R O. 96774 O. 96873	M /PTF 0.53714 0.53425	P1 /PTP 0.90797 0.90309	X/DMAX 0.39800 0.43100	•
ADD 17 10NA D WORD 17 12 22 27	PL 14.863 14.783 14.799	PL /PD PL /PD D. 97298 D. 96774	M /PTF 0.53714 0.53425 0.53479 9.54492	Pt /PTP 0.90797 0.90309 0.90400	X/DMAX 0.39800 0.43100 0.44900	
ADD 17 10NA D WORD D7 12 22 27	PL 14.863 14.783 14.799 15.978	PL/PD D. 97298 D. 96774 D. 96775 D. 9706 D. 97608	M /PTF 0.53714 0.53425 0.53470 9.54492 0.54437	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020	X/DMAX 0.39800 0.43100 0.44900 0.52200	
ADDIT 10NA D WORD D7 12 22 27 27 37	PL 14.863 14.783 14.799 15.078 14.929	PL/PD 0.97298 0.96774 0.96773 0.96706 0.9608 0.97724	M /PTF 0.53714 0.53425 0.53479 9.54492 0.54437 0.53949	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200	
ADD 17 10NA D. WORD 07 12 22 27 27 47 42	PL 14.863 14.783 14.799 15.978	PL/PD D. 97298 D. 96774 D. 96775 D. 9706 D. 97608	M /PTF 0.53714 0.53425 0.53470 9.54492 0.54437	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800	
ADDIT 10NA D. WORD 07 12 22 27 27 47 42	PL 14.863 14.783 14.783 15.979 15.063 14.929 15.798	PL/PD 0.97298 0.96774 0.96774 0.9673 0.97706 0.9706 0.97724 1.7729 1.7719	M /PTF 0.53714 0.53425 0.53425 0.54492 0.54437 0.53949 0.99287	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200	
ADDIT 10MA D. WORD 07 12 22 27 37 42 57	PL 14.863 14.703 14.709 15.970 15.063 14.929 15.99 15.99	PATIOS . FOP PL/PO 0.97298 0.96774 0.96873 0.98706 0.98608 0.97724 1.7719 1.7719	M /PTF 0.53714 0.53425 0.53479 0.54492 0.54437 0.53949 0.99297 0.55297	Pt /PTP 0-90797 0-90309 0-90400 0-92111 0-92020 0-91195 0-93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800	
ADDIT 10MA D WORD D7 12 27 27 37 42 57	PL 14.863 14.783 14.799 15.978 15.063 14.929 15.998 15.998 PL	PL/PD 0.9729R 0.96774 0.96774 0.96776 0.98706 0.97724 1.7719 1.7719 1.7715 PAYING 1.FR	M /PTF 0.53714 0.53425 0.53479 0.54492 0.54437 0.53949 0.39287 0.55787	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000	
ADDIT 10NA D WORD D 7 12 22 27 37 42 57 57	PL 14.863 14.783 14.783 14.799 15.979 15.063 14.929 15.798 15.798	PL/PD 0.97298 0.96774 0.96774 0.96773 0.98706 0.97724 1.7719 1.7719 1.7719 1.7719	M /PTF 0.53714 0.53425 0.53425 0.54422 0.54437 0.53949 0.9247 0.55787	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 -1.0000	
ADDIT 10NA 0 WORD 17 12 27 27 37 47 57 57 0 WORD 52	PL 14.863 14.783 14.799 15.978 15.063 14.929 15.998 15.998 PL	PL/PD 0.9729R 0.96774 0.96774 0.96776 0.98706 0.97724 1.7719 1.7719 1.7715 PAYING 1.FR	M /PTF 0.53714 0.53425 0.53479 0.54492 0.54437 0.53949 0.39287 0.55787	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000	
ADDIT 10MA D. MORD 07 12 22 27 37 37 57 57 50 MORD 52 57	PL 14.863 14.703 14.709 15.970 15.063 14.929 15.709 15.108 PL 15.298	PL/PO 0.9729R 0.96774 0.96774 0.96773 0.98706 0.97706 0.97724 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719	M /PTF 0.53714 0.53425 0.53425 0.54422 0.54437 0.53949 0.9247 0.55787	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 Pt /PTP 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 -1.0000	
ADDIT IONA D WORD DT 12 22 27 37 42 57 57 D WORD 52 57 ADDIT IONA	PL 14.863 14.703 14.709 15.970 15.063 14.929 15.709 15.108 PL 15.298	PL/PO 0.9729R 0.96774 0.96774 0.96773 0.98706 0.97706 0.97724 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719	M /PTF 0.53714 0.53479 9.54492 0.54437 0.53949 0.9297 0.55287	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 Pt /PTP 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 -1.0000	
ADDITIONA D WORD 12 22 27 37 37 37 37 40 52 57 ADDITIONA D WORD	PL 14.863 14.703 14.709 15.070 15.063 14.929 15.798 15.798 PL 15.298 L PRESSUPE	PL/PO 0.97298 0.96774 0.96774 0.96773 0.97706 0.9706 0.97724 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2.7719 2	M /PTF 0.53714 0.53425 0.53479 9.54492 0.54437 0.53949 0.55287 MUZZE PLAN 0.55287 DEG SHPOUD L PL/PTF	PI /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 PI /PTP 0.93456 0.0325K	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 10000 X/DMAX -1.0000	
ADDIT 10MA D WORD 17 12 22 27 37 37 40 57 57 ADDIT 10MA D WORD 67	PL 14.863 14.703 14.703 14.709 15.063 14.929 15.298 15.298 PL 15.298 L PRESSUPE	PL/PO 0.96774 0.96774 0.96776 0.9673 0.96706 0.97724 1.7717 1.7715 PATING 1.7717 1.7715 PATING 2.770 1.7717 2.77015 1.0015 PATING 20 PL/PO 1.0015	M /PTF 0.53714 0.53424 0.53424 0.53479 9.54492 0.54437 0.53949 0.9297 0.55287 0.55287 0.55287 0.55287	Pt /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 Pt /PTP 0.93456 OCATION Pt /PTP 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 X/DMAX -1.0000 1.0000	
ADDIT 10MA D WORD 07 12 22 27 37 37 37 37 57 NORD 52 57 ADDIT 10MA D WORD 67 72	PL 14.863 14.703 14.703 14.709 15.063 14.929 15.947 15.947 15.298 14. PRESSUPE PL 15.298 15.298 15.303	PL/PO 0.97298 0.96774 0.96774 0.96776 0.9706 0.97724 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 2.7719 2.7715 PAYINS 2.788 PL/PO 1.0015 1.0015 1.0016	## /PTF 0.53714 0.53425 0.53479 9.54492 0.54437 0.53949 0.55287 ### /PTF 0.55287 DEG SHPOUD L PL/PTF 0.55287 0.55287	PI /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 0.93456 0.93456 0.93456 0.93456 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 10000 X/DMAX -1.0000	
ADDIT 10MA D WORD D7 12 22 27 37 37 42 57 D WORD 52 57 ADDIT 10MA D WORD 67	PL 14.863 14.703 14.703 14.709 15.063 14.929 15.947 15.947 15.298 14. PRESSUPE PL 15.298 15.298 15.303	PL/PO 0.97298 0.96774 0.96774 0.96776 0.9706 0.97724 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 2.7719 2.7715 PAYINS 2.788 PL/PO 1.0015 1.0015 1.0016	M /PTF 0.53714 0.53424 0.53424 0.53479 9.54492 0.54437 0.53949 0.9297 0.55287 0.55287 0.55287 0.55287	PI /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 0.93456 0.93456 0.93456 0.93456 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 X/DMAX -1.0000 1.0000	
ADDITIONA D WORD DT 12 22 27 37 42 27 57 ADDITIONA D WORD 67 72 ADDITIONA D WORD	PL 14.863 14.703 14.709 15.978 15.063 14.929 15.708 PL 15.298 LL PRESSUPE PL 15.298 15.303 EL PRESSUPE PL	PL/PO 0.9729R 0.96774 0.96774 0.96776 0.98706 0.97724 1.7719 1.7715 PATING . FRE PL/PO 1.0015 PATING . 20 PL/PO 1.0016 PATING , PO PL/PO	M /PTF 0.53714 0.53425 0.53479 0.53492 0.54492 0.54497 0.55787 0.55787 0.55787 0.55787 DEG SHPOUD L PL/PTF 0.55287 0.55287	PI /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 0.93456 0.93456 0.93456 0.93456	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.52200 0.58800 -1.0000 X/DMAX -1.0000 1.0000 X/DMAX 0.79300 0.84400	
ADDITIONA D WORD DT 12 22 27 37 42 27 57 ADDITIONA D WORD 67 72 ADDITIONA D WORD	PL 14.863 14.703 14.703 14.709 15.063 14.929 15.298 15.298 15.298 15.298 15.298 15.298 15.298 15.298	PL/PO 0.97298 0.96774 0.96774 0.96776 0.98706 0.97724 1.7719 1.7715 1.7715 PATING . FRE PL/PO 1.0015 1.0015 1.0018 PATING , PO	M /PTF 0.53714 0.53425 0.53479 0.53479 0.54492 0.54492 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287	PI /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 0.93456 0.93456 0.93456 0.93466 0.93466	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 -1.0000 1.0000 1.0000 1.0000 1.0000	
ADDITIONA D WORD D7 12 22 27 37 42 37 57 ADDITIONA D WORD 67 72 ADDITIONA D WORD 67	PL 14.863 14.703 14.709 15.978 15.063 14.929 15.708 PL 15.298 LL PRESSUPE PL 15.298 15.303 EL PRESSUPE PL	PL/PO 0.9729R 0.96774 0.96774 0.96776 0.98706 0.97724 1.7719 1.7715 PATING . FRE PL/PO 1.0015 PATING . 20 PL/PO 1.0016 PATING , PO PL/PO	M /PTF 0.53714 0.53425 0.53479 0.53492 0.54492 0.54497 0.55787 0.55787 0.55787 0.55787 DEG SHPOUD L PL/PTF 0.55287 0.55287	PI /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 0.93456 0.93456 0.93456 0.93466 0.93466	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.52200 0.58800 -1.0000 X/DMAX -1.0000 1.0000 X/DMAX 0.79300 0.84400	
ADDIT 10MA O WORD OT 12 22 27 37 42 57 57 O WORD 52 60 FO WORD 67 72 ADDIT 10MA O WORD 67 72 ADDIT 10MA O WORD 67 72 ADDIT 10MA	PL 14.863 14.703 14.703 14.709 15.063 14.929 15.708 15.108 PL 15.298 15.298 15.303 PRESSUPE PL 15.298 15.303	PL/PO 0.97298 0.96774 0.96774 0.96776 0.9706 0.97724 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.7719 1.771	M /PTF 0.53714 0.53479 0.53479 0.54437 0.53287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287 0.55287	PI /PTP 0.90797 0.90309 0.90400 0.92111 0.92020 0.91195 0.93456 0.93456 0.93456 0.93456 0.93456	X/DMAX 0.39800 0.43100 0.44900 3.48600 0.52200 0.58800 -1.0000  X/DMAX -1.0000  X/DMAX 2.79300 0.84400	

MASA-L FWIS		PARY DATA	36/13/70	CANDETT	TEL 8772971	9 95:91:43.714	FAC REGEL	PG4 1034	PFG 139	•
> PORT TENCH	<b>P</b> RFCCIPT	PATIOS . PPI	MARA MILL							
vo ween	PĮ	PL/PO	U / DTF	PE /PTP	X/DMAX	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa				
32	12.342	). 84914	0.31002	0.52384	0.72200		-			
27	16.341	1.0735	7. 20102	9.66223	0. 82063					
47	17.485	1.1473	0.41887	0.70775	0.91900					
52	17.7)5	1.1617	0.42413	0.71665	1.0170					
·										
>A TICKA	uhe 22ilhe	PATINS . FLO	W Chillian I	- P-						
	Pt	PL / PO	PI /PTF	PL /PTP	X/DMAX					
62	16.900	1.1089	0.40486	0.68498	0.42200					
57	14-061	0. 92261	0.33685	0.56914	0.47000					
ADDITIONAL	PRESSUPE	PATIOS . FIG	W SPLITTER O	-0-						
						+	The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th			
	PL CALLE	PL /PO	PL /PTF	Pi /PTP	X/DMAX					
77	9.6415	0.63261	0-23097	0.39026	0.50800		1.11.12.94		de entre open nom .	-
7	21.433	1.4306	9-52731	0.88253	0.54300					
i2	15.241	1_0000	0.36511	0.61691	<u>0</u> 67000					
789017101ML	PRESSUPE	PATIOS , EJE	CTOR SHROUD							
VD WORD	PL	PL/P9	PL/PTF _		X/DHAX					
107	14.991	7-97.706	0-33673	0.60275	-1-0000					
12	140831	0.97312	0.35529	0-60032	-1-0000					
22	14.456	11.97476	0.79589	0.60133	-1.0000					
27	13.116	0.97142								
			9. 36211	every us	-1.0000					
22	15-166	0.99509	0. 36371	0.61388-	-1.0000					
162	15-166 15-171	0.99509 9.99542	0.36371 0.36343	0.613FF~ 0.61408	-1.0000		er communication or communication and	Alam (gaggaga - cos 😑 colonida Aliffi (Anggagaga ya capin) sa		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
	15-171		0.36343							Anny anglitación (n
ADDITIONAL	15-171	7.99542 PATIOS - FCP PL/PO	0.36343 EBOOY INLET PL/PTF							
ADDITIONAL	15.171 PRESSURE	7.99542 PATIOS FCP	0.36343 EBOOY INLET	0,61498	-1.0000					and adjusted to a supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of the supple of th
ADDITIONAL O WOPD	15•171 PRESSURE PL	7.99542 PATIOS - FCP PL/PO	0.36343 EBOOY INLET PL/PTF	0,61498 PL/PTP	-1.000Q X/DMAX 2.39000		-			est edition of a serger of
ADDITIONAL D WOPD	15-171 PRESSURE PL 14-691 14-631	9.99542 PATIOS FCP PL/PD 0.97706 0.97312	0.36343 EBOOY INLET PL/PTF 0.35673 0.25529	0.61408 PL/PTP 0.60275 0.60032	*/DMAX 2.3 9000 0.43100		•			
ADDITIONAL  O WOPD  O T  112	15-171 PRESSURE PL 14-691 14-631 14-656	0.99542 PATIOS ECP. PL/PO 0.97704 0.97312 0.97476	0.36343 EBOOY INLET PL/PTF 0.35473 0.25529 0.35589	0.61408 PL/PTP 0.60275 0.60032 0.60133	-1.0000 X/DMAX 3.3900 0.43100 G.44900					
PADDITIONAL /D WOPD     07   112   127	15-171 PRESSURE PL 14-891 14-831 14-856	7.99542 PATIOS ECP PL/PO 0.97704 0.97312 0.97476 979182	0.36343 ERODY INLET PL/PTF 0.35529 0.35529 0.35589 0.36211	PL/PTP 0.60275 0.60032 0.60133	X/DMAX 2-3 9800 0-43100 G-44900 Q-48600		-			
ADDITIONAL OF HOPD 112 127 27	15.171 PRESSURE PL 14.691 14.631 14.656 15.166	0.99542 PATIOS	0.36343 EBOOY INLET PL/PTF 0.35673 0.25529 7.35589 0.36211 0.36331	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61398	X/DMAX 3.39800 0.43100 G.44900 0.52200					
ADDITIONAL //D WOPD (07) 112 //27 127 137 142	15.171  PRESSURE  PL 14.891 14.851 14.856 15.116 15.166 15.171	7.99542 PATIOS ECP PL/PO 0.97706 0.97312 0.97476 2.99182 0.99509 0.99542	0.36343 EBOOY INLET PL/PTF 0.35673 0.25529 0.35589 0.36211 0.36331 0.26342	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61398	K/DMAK 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800					
ADDITIONAL (D WOPD (7 ) 112 / 7 2 / 27	15.171  PRESSUPE  14.891  14.856  15.116  15.166  15.171  19.291	7.99542 PATIOS FCP. PL/PO 0.97706 0.97312 0.97476 0.99509 0.99542 1.9700	0.36343 EBODY INLET PL/PTF 0.35529 0.35589 0.36211 0.36331 0.36343	PL/PTP 0.60275 0.60032 0.60133 C.61385 0.61388 0.61408	X/DMAX 2.3 9800 0.43100 G.44900 0.52200 0.57800		•			
ADDITIONAL  // WOPD   07   112   72   127   137   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142   142	15.171  PRESSURE  PL 14.891 14.851 14.856 15.116 15.166 15.171	7.99542 PATIOS ECP PL/PO 0.97706 0.97312 0.97476 2.99182 0.99509 0.99542	0.36343 EBOOY INLET PL/PTF 0.35673 0.25529 0.35589 0.36211 0.36331 0.26342	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61398	K/DMAK 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800	-				
ADDITIONAL //D WOPD   07   12   12   27   27   37   42	PRESSURE  PL 14.891 14.831 14.856 15.116 15.166 15.171 19.241	7.99542 PATIOS FCP. PL/PO 0.97706 0.97312 0.97476 0.99509 0.99542 1.9700	0.36343 EBODY INLET PL/PTF 0.35673 0.25529 7.35589 0.36211 0.36331 0.36343 7.76971 C.36925	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.6138R 0.61408 0.61408	X/DMAX 2.3 9800 0.43100 G.44900 0.52200 0.57800					
PADDITIONAL /D WOPD  07  12  12  127  137  42  197	15.171 PRESSUPE PL 14.891 14.831 14.856 15.116 15.166 15.171 19.241 19.241	7.99542 PATIOS ECP. PL/PO 0.9770A 0.97312 0.97476 0.99182 0.99509 0.99542 1.9709 1.0003	0.36343 ERODY INLEY PL/PTF 0.35573 0.25529 0.35589 0.36211 0.36331 0.36331 0.26442 7.76411 0.30723	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.6138R 0.61408 0.61408	X/DMAX 2.3 9800 0.43100 G.44900 0.52200 0.58600 -1.0000 1.0000					
ADDITIONAL //D HOPD (07 12 27 27 37 42 42 42 42 44 44 44 44 44 44 44 44 44	15.171 PRESSUPE PL 14.891 14.831 14.856 15.116 15.166 15.171 19.241 19.240 PRESSUPE PL 15.264	7.99542 PATIOS FCP. PL/PO 0.97706 0.97312 0.97476 0.99509 0.99542 1.9709 1.0003 RATISS I FAM	0.36343 ERODY INLEY PL/PTF 0.35573 0.25529 0.36211 0.36331 0.36342 2.76711 C.36223	0.61408 PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61388 0.61408 0.61408	X/DMAX 2.3 9800 0.43100 G.44900 0.52200 0.58800 -1.0000					
ADDITIONAL //D WOPD   107 112 127 127 137 142 157	15.171 PRESSUPE PL 14.891 14.831 14.856 15.116 15.166 15.171 19.241 19.241	7.99542 PATIOS ECP. PL/PO 0.9770A 0.97312 0.97476 0.99182 0.99509 0.99542 1.9709 1.0003	0.36343 ERODY INLEY PL/PTF 0.35573 0.25529 0.35589 0.36211 0.36331 0.36331 0.26442 7.76411 0.30723	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61388 0.61408 0.61408 0.61408	X/DMAX 2.3 9800 0.43100 G.44900 0.52200 0.58600 -1.0000 1.0000					
PADDITIONAL  (D WOPD (07) 12 (27) 27 (27) 37 (42) 97 (42) 97 (40) 60 HORD (67) 67 (57)	PRESSURE PL 14.891 14.831 14.856 15.116 15.166 15.171 19:241 19:246 PRESSURE PL 15.264 15.264	7.99542 PATIOS FCP. PL/PO 0.97706 0.97312 0.97476 0.99509 0.99542 1.9709 1.0003 RATISS I FAM	0.36343 EBODY INLET PL/PTF 0.35573 0.25529 0.36211 0.36331 0.36343 0.36343 0.36343 0.36343 0.36343 0.36523	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61388 0.61408 0.61408 0.61408 0.61411	X/DMAX 3.3 9800 0.43100 0.44900 0.52200 0.52200 0.5800 -1.0000 X/DMAX -1.0000		•			
ADDITIONAL //D WOPD //O7 12 12 27 27 37 42 37 42 57 ADDITIONAL	PRESSUPE  14.891 14.831 14.856 15.116 15.166 15.171 19.291 19:240 PRESSUPE  PRESSUPE	7.99542 PATIOS FCP. PL/PO 0.97706 0.97312 0.97476 0.99582 0.99542 1.9707 1.0003 RATIOS IAN	0.36343 EBODY INLET PL/PTF 0.35673 0.25529 0.36211 0.36331 0.26343 0.26343 0.26343 0.26343 0.36523 DEG SHROUN 1	0.61408  PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61398 0.61408 0.61408 0.61408 0.61408 0.61408 0.61408 0.61408	X/DMAX 2.39800 0.43100 0.43100 0.58600 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
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ADDITIONAL  (D WOPD   07   12   12   12   12   12   12   12   1	PRESSURE PL 14.891 14.891 14.831 14.856 15.116 15.166 15.171 19:241 19:246 PRESSUPE PL 15.264 PRESSUPE	7.99542 PATIOS FCP. PL/PO 0.97706 0.97312 0.97476 0.99509 0.99542 1.9709 1.0003 RATIOS IAM PL/PO 1.0007	0.36343 EBODY INLET PL/PTF 0.35573 0.25529 0.36211 0.36331 0.36343 0.36343 0.36343 0.36523 POLICE FLAT 0.36523 DEG SHROUD 1 M /PTF 0.36535	PL/PTP 0.60275 0.60032 0.60133 C.61385 0.61408 0.61408 0.61408 0.61408 0.61408 0.61408 0.61711 PL/PTP 0.61732	X/DMAX 2.3 9800 0.43100 G.44900 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000					
ADDITIONAL O HOPD OT 112 72 27 37 42 42 42 42 57 AMMENTATIONAL O HOPD 67 ADDITIONAL	PRESSUPE  14.891 14.831 14.856 15.116 15.166 15.171 19.241 15.246 PRESSUPE  PL 15.246 PRESSUPE  PL 15.251 15.251	7.99542 PATIOS FCP. PL/PO 0.97706 0.97312 0.97476 0.99542 1.9707 1.0003 RATIOS IAM PL/PO 1.0003 RATIOS 20 PL/PO 1.0007 1.0009	0.36343 EBODY INLET PL/PTF 0.35673 0.25529 0.36211 0.36331 0.36343 7.7671 C.36925 PPLLE:FLAT 0.36523 DFG SHARDE 1 M /PTF 1.36535 0.36511	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61388 0.61408 0.61408 0.61408 0.61408 0.61408 0.61408 0.61711 PL/PTP 7.61601 0.61711 PL/PTP 0.61737 0.61691	X/DMAX 2.3 9800 0.43100 G.44900 0.52200 0.52800 -1.0000 -1.0000 -1.0000					
ADDITIONAL O HOPD OT 112 72 27 37 42 42 42 42 57 AMMENTATIONAL O HOPD 67 ADDITIONAL	PRESSUPE  14.891 14.831 14.856 15.116 15.166 15.171 19.241 15.246 PRESSUPE  PL 15.246 PRESSUPE  PL 15.251 15.251	7.99542 PATIOS FCP. PL/PO 0.97706 0.97312 0.97476 0.99509 0.99542 1.9709 1.0003 RATIOS IAM PL/PO 1.0007	0.36343 EBODY INLET PL/PTF 0.35673 0.25529 0.36211 0.36331 0.36343 7.7671 C.36925 PPLLE:FLAT 0.36523 DFG SHARDE 1 M /PTF 1.36535 0.36511	PL/PTP 0.60275 0.60032 0.60133 C.61185 0.61388 0.61408 0.61408 0.61408 0.61408 0.61408 0.61408 0.61711 PL/PTP 7.61601 0.61711 PL/PTP 0.61737 0.61691	X/DMAX 2.3 9800 0.43100 G.44900 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000					
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r ween	PĮ	PL /PD	Pt /PTF	P1 /PTP	x/neax			<del></del>	
2	15.206	0.99869	9-55184	0.79668	2-72200				
7	15.937		0.57834	0.83494		· ·			
		1.0466			0-82000				
7	16-127	1-9591	0.58524	0.84490	G-91900	+			
<b>?</b>	14.315	1.9647	0.58833	0.84035	1.0170				
JANNET ECNA	PRESSIME	RATIOS . FLO	W SPLITTER 1	- n-					
n warp	PL	PE / PC	P1 / PTF	PL /PTP	X/DMAX				
:2	15.812	1.0384	0.57381	0.82839	0.42200				
7	15.441	1-0141	0.56037	0.80930	3.67000				
AND TIONA	PRESSUPE	PATINS . FLI	W SPLITTER I	'. n.	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s				
in MUSD	PL	PL / PO	PQ /PTF	PL /PTP	x/DHAX				
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2	17.342	1.1389	0.42935	0.90857	g. 58300			- "	
2	15.235	1.0007	0.55293		9-67000	***************************************		· · · · · · · · · · · · · · · · · · ·	
1000E	- PRESSUPE	PATIOS & EST	<del>CTOR SHADUS</del>			والمستقد المداعة المادات المادات	reduceração de Aria. O o conseguento e e, e e o consecuente despediações		
D MOPD	<u> </u>	PL/PD	PL/PTF	PL (239	X/DMAX				
97	14.836	0.97426	0.53741	0.77729	-1.0000	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	and the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of th		
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12	14.781							· · · · · · · · · · · · · · · · · · ·	
22 23	14.786	0. 97100	3 53659	0.77467	-1.9060				
?7	15.061	0.9R91A	0. 4	0.7890R	-1.0000	. In the second second			
	15.07	0.98982	0.54694	T-1804A	-1.0000				
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37 42	14.976	0. 98357	0.54349	0.7946	-1.0000		The comment of the comment of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the co	Secretary across states attacked and the secretary of the	
42	14.976		0.54349	0.79469					
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ADD J.T J.N.YAL N. WORN D. T	14.976 PRESSUPE PL 14.836	0.98357 PATINSFOR PL/PN 0.97438	0.54349 FBROY INLET PL/PTF 0.53841	0.794AT	x/DMAX 0-39800				
42 A2D J.T <u>IONAL</u> D. HORN D. T. 12	T4.976  PRESSUPF  PL  14.836  14.781	0. 98357  PATINSFOR  PL/PO 0.97438 0.97076	0.54349 FRIOV IMET PL/PTF 0.52841 0.53641	0.79467 PL/PTP 0.77720 0.77441	x/DMAX				
42 A2D J.T <u>IONAL</u> D. HORN D. T. 12	14.976 PRESSUPE PL 14.836	0.98357 PATINSFOR PL/PN 0.97438	0.54349 FBROY INLET PL/PTF 0.53841	0.794AT	x/DMAX 0-39800	•			
42 A3D [,T [,D,YAL D, HORD D, T 12 22	74.976  PRESSUPE  14.836  14.781  14.786	0.98357  PATINSECR PL/PN 0.97438 0.97076 0.97109	0.54349 PERMOY IMLET PL/PTF 0.52841 0.53641 0.57659	0.794ATP 0.7772° 0.77441 0.77467	X/DMAX 0.39800 0.43100 0.44900	*			
42 A20 J.T.J.O.YAL O. HORO 07 12 22 27	PRESSUPE PL 14.836 14.781 14.786 15.061	0. 98357  PATINSFOR  PL/PO 0.97438 0.97076	0.54349 FRIOV IMET PL/PTF 0.52841 0.53641	0.79467 PL/PTP 0.77720 0.77441	X/DMAX 0.39800 0.43100 0.44900 0.48600				
42 ADDITIONAL O WORD 07 12 22 27	74.976  PRESSUPE  14.836  14.781  14.786	0.98357  PATINS FOR  PL/PN 0.97438 0.97076 0.97109 0.928916	0.54349 PERMY IMEY PL/PYF 0.53641 0.53645 0.54658	PL/PTP 0.77720 0.77441 0.77467 Q.78909	#/DMAX 0.39800 0.43100 0.44900 0.52200	•			
42 ADDITIONAL D. WORD D7 12 27 27 37	74.976  PRESSUPE PL 14.836 14.781 14.786 15.061 15.071 14.976	0.98357  PATINS FOR  PL/PO 0.97438 0.97076 0.97109 0.98916 0.98987 0.98357	0.54349 PERMY IMET PL/PTF 0.53641 0.53641 0.57659 0.54658 0.54694	PL/PTP 0.7772° 0.77441 0.77467 0.78909 0.78960 0.78463	#/DMAX 0.39800 0.49100 0.44900 0.52200 0.52200				
42 ADD J.T. J.O.YAL O. WORD 12 22 27 27 37 42 42	74.976  PRESSUPE PL 14.836 14.781 14.786 15.061	0.98357  PATINSFOR  PL/PO 0.97438 0.97109 0.97109 0.98916 0.98982	0.54349 PERMY IMET PL/PTF 7.52841 0.53641 0.54658 0.54694	PL/PTP 0.77729 0.77441 0.77441 0.78909 0.78960	#/DMAX 0.39800 0.43100 0.44900 0.52200	•			N A
42 ADDITIONAL D. WORD D. 7 12 22 27 27 37 42	PRESSUPE PL 14.836 14.741 14.746 15.061 15.071 14.976	0.98357  PATINS FOR  PL/PO     0.97438     2.97076     0.97109     0.98916     0.98987     0.98357	0.54349 PERMY IMET PL/PTF 0.53641 0.53641 0.57658 0.54658 0.54649 0.54749	PL/PTP 0.77720 0.77461 0.77467 0.78909 0.78960 0.78463	#/DMAX 0.39800 0.49100 0.44900 0.52200 0.52200				
42 ADDITIONAL D. HORD 07 12 22 27 37 42 42	14.976  PRESSUPE  PL 14.836 14.781 14.786 15.061 15.071 14.976 17.245	0.98357  PATINS FOR  PL/PO 0.97438 0.97109 0.98916 0.98982 0.98357 1.0007	0.54349 PERMY IMET PL/PTF 1.52841 0.53641 0.57658 0.54658 0.54694 0.54749 0.7777	PL/PTP 0.77720 0.77461 0.77467 0.78909 0.78960 0.78463	#/DMAX 0.39800 0.49100 0.44900 0.52200 0.52200				
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A2017104AL 0 HORD 12 12 17 17 18 18 18 19 19 19 19 19 19 19 19 19 19	PRESSUPE PL 14.836 14.786 15.061 15.071 14.976 17.245 17.238	0.98357  PATINS FOR  PL/PO     0.97438     2.97076     0.97109     0.98916     0.98357     1.0007  PATINS FAR	0.54349 PERMY IMEY PL/PTF 0.53641 0.53649 0.54658 0.54696 0.54749 0.54749	0.784AT PL/PTP 0.77720 0.77461 0.77467 0.78909 0.78460 0.78460 0.78463 0.74625	#/DMAX 0.39800 0.49100 0.44900 0.52200 0.52200 11.0000				
42 ADDITIONAL D. HORD 97 12 22 27 37 42 42 42 42 42 42 43 44 44 44 44 44 44 44 44 44 44 44 44	PRESSUPE PL 14.836 14.786 15.061 15.071 14.976 17.245 17.238 PPETSUPP PL 15.236 17.236	0.98357  PATINS FOR  PL/PN 0.97438 0.97109 0.98916 0.98982 0.98357 1.0007	0.54349 PERMY IMEY PL/PYF 0.53641 0.53649 0.54658 0.54696 0.56349 0.56349 0.56349 0.56349 0.56349	PL/PTP 0.77720 0.77461 0.77467 0.78909 0.78960 0.78463 0.74625 0.74625 0.74625 0.74625	#/DMAX 0.39800 0.43100 0.44900 0.58600 -1.0000  X/DMAX -1.0000				
42 ADDITIONAL D. HORD 12 22 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PRESSUPE PL 14.836 14.781 14.786 15.061 15.071 14.976 17.238 PPESSUPE PL 15.216 PPESSUPE	0.98357  PATINS FOR  PL/PO     0.97438     0.97076     0.97109     0.98357     1.0007     1.0007     1.0007	0.54349 PERMY IMEY PL/PYF 0.53641 0.53649 0.54658 0.54696 0.56349 0.56349 0.56349 0.56349 0.56349	PL/PTP 0.77720 0.77461 0.77467 0.78909 0.78960 0.78463 0.74625 0.74625 0.74625 0.74625	#/DMAX 0.39800 0.43100 0.44900 0.58600 -1.0000  X/DMAX -1.0000				
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42 ADDITIONAL D. HORD D. 17 37 37 37 37 37 37 37 37 37 37 37 37 37	PRESSUPE PL 14.836 14.781 14.786 15.061 15.071 14.976 17.238 PPESSUPE PL 15.216 PPESSUPE	0.98357  PATINS _ FOR  PL/PO 0.97438 0.97076 0.97109 0.98357 1.0007 1.0007 1.0007 1.0007	0.54349 PERMY IMET PL/PTF 1.53P41 0.53641 0.53641 0.54658 0.54658 0.54649 0.54749 0.64749 0.64749	0.784AT  PL/PTP 0.77720 0.77441 0.77467 0.78909 0.78940 0.78463 0.78463 0.78463 0.78925 0.78925 0.79835	*/DMAX 0.39800 0.49100 0.4900 0.52200 0.58800 -1.0000  **/DMAX -1.0000 1.0000				
A20   T   T   T   T   T   T   T   T   T	14.976  PRESSUPE  PL 14.836 14.781 14.786 15.061 15.071 14.976 17.238  PPT 1927  PL 15.236 17.276  PPFSSUPE  PL 15.231 15.231	0.98357  PATINS FOR  PL/PO     0.97438     0.97076     0.97109     0.98357     1.0007     1.0007     1.0007     1.0007  PATINS 20  PL/PO     1.0003	0.54349 PERMY IMET PL/PTF 1.52841 0.53641 0.53649 0.54694 0.54749 0.54749 0.65762 0.65762 0.65762 0.65762 0.75275	PL/PTP 0.77720 0.77441 0.77467 0.78909 0.78463 0.78463 0.78463 0.7877 0.7977	X/DMAX 0.39800 0.49100 0.44900 0.52200 0.52200 11.0000 -1.0000 X/DMAX -1.0000				
42 ADDITIONAL D MORD 07 12 27 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	14.976  PRESSUPE  PL 14.836 14.786 15.061 15.071 14.976 17.245 17.236  PPESSUPE  PL 15.231 15.231 PPESSUPE	0.98357  PATINS FOR  PL/PU     0.97438     0.97076     0.97109     0.98357     1.0007     1.0007     1.0007     1.0007  PATINS 20  PL/PU     1.0003     1.0003  PATINS 80	0.54349 PERMY IMET PL/PTF 0.53641 0.53649 0.54658 0.54696 0.56349 0.56349 0.56349 0.56349 0.56349 0.56379 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65700 0.65	PL/PTP 0.77720 0.77461 0.77467 0.78909 0.78460 0.78460 0.78460 0.78463 0.74625 0.74625 0.74625 0.74626 0.79729 0.79729 0.79729	X/DMAX 0.39800 0.49100 0.44900 0.52200 0.58000 -1.0000 X/DMAX -1.0000 X/DMAX 0.79300 0.84400				
42 ADDITIONAL DE WORD 12 22 27 37 42 42 42 42 42 47 47 47 47 40 MORD 52 77 ADDITIONAL DE WORD 67 72 ADDITIONAL DE WORD	14.976  PRESSUPE  PL 14.836 14.781 14.786 15.071 14.976 17.235 17.235  PPESSUPE  PL 15.231 15.231 PPESSUPE  PL	9.98357  PATINS _ FOR  PL/PN	0.54349 PERDOY IMET PL/PTF 1.53P41 0.53641 0.53641 0.53659 0.54658 0.54649 0.54349 0.54349 0.54349 0.54349 0.55275 0.65762 0.65762 0.65762 0.65762 0.65762	0.784AT  PL/PTP 0.77720 0.77441 0.77467 0.78909 0.78463 0.78463 0.78463 0.78463 0.78463 0.78629 0.78729  PL/PTP 0.79729 0.79729 0.79729 0.79729	#/DMAX 0.39800 0.43100 0.44900 0.58800 -1.0000  ****  **************************				
42 ADDITIONAL D. MORD 12 22 27 42 42 42 42 42 42 42 42 42 42 42 42 42	14.976  PRESSUPE  PL 14.836 14.786 15.061 15.071 14.976 17.238  PPT3SUPF  PL 15.236 17.276  PPFSSUPE  PL 15.231 15.231 15.231 PPESSUPF  PL 14.746	0.98357  PATINS _ FOR  PL/PN 0.97438 0.97076 0.97109 0.98367 0.98357 1.0007 1.0007 1.0007 1.0007 1.0007 1.0003 1.0003 PATINS _ RD  PL/PN 0.96846	0.54349 PERMY IMET PL/PTF 1.52841 0.53641 0.53659 0.54658 0.54694 0.54694 0.54694 0.54694 0.56769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769 0.65769	PL/PTP 0.77720 0.77441 0.77467 0.78909 0.78463 0.78463 0.78463 0.7877 0.7977 PL/PTP 0.79825 0.79825 0.79826 0.79799 0.79799 0.79799 0.77257	#/DMAX 0.39800 0.49100 0.44900 0.48600 0.52200 0.58800 -1.0700 -1.0000  */DMAX 0.79300 0.84400  */DMAX 0.79300				
ADDITIONAL DISTRICT ADDITIONAL DISTRICT ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL	14.976  PRESSUPE  PL 14.836 14.786 15.061 15.071 14.976 17.236  PPESSUPE  PL 15.236 PPESSUPE  PL 15.231 15.231 PPESSUPE  PL 14.416	9.98357  PATINS _ FOR  PL/PO	0.54349 PERMY IMEY PL/PTF 0.52841 0.53641 0.53658 0.54658 0.54694 0.54694 0.54749 0.55293 PEG SHPOUD I PL/PTF 0.55275 0.55275 DEG SHPOUD I PL/PTF 0.55275 DEG SHPOUD I PL/PTF 0.55275	0.784AT  PL/PTP 0.77720 0.77441 0.77467 0.78909 0.78463 0.78463 0.78463 0.78463 0.78463 0.78629 0.78729  PL/PTP 0.79729 0.79729 0.79729 0.79729	#/DMAX 0.39800 0.43100 0.44900 0.58800 -1.0000  ****  **************************				
ADDITIONAL DISTRICT ADDITIONAL DISTRICT ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL	14.976  PRESSUPE  PL 14.836 14.781 14.786 15.061 15.071 14.976 17.238  PPESSUPE  PL 15.236 17.276  PPESSUPE  PL 15.231 15.231 15.231 PPESSUPF  PL 14.746 14.416  MEASURED	0.98357  PATINS FOR  PL/PO	0.54349 PERMY IMEY PL/PTF 0.52841 0.53641 0.53658 0.54658 0.54694 0.54694 0.54749 0.55293 PEG SHPOUD I PL/PTF 0.55275 0.55275 DEG SHPOUD I PL/PTF 0.55275 DEG SHPOUD I PL/PTF 0.55275	PL/PTP 0.77720 0.77461 0.77467 0.78909 0.78960 0.78660 0.7865 0.79625 0.79625 0.79625 0.79626 0.79709 0.79709 0.79709 0.79709 0.77257 0.77557	#/DMAX 0.39800 0.49100 0.44900 0.48600 0.52200 0.58800 -1.0700 -1.0000  */DMAX 0.79300 0.84400  */DMAX 0.79300	F4 0. 3221268			

454-L FW IS	PRFL 14 f	NARY NATA	26/13/79	CADDELL	RFC 10/24/7	9 05:94:37.909	FAC REGEL	PG" 6036 PDG 1394								
10017 TOUA	1 PRESSURE	PATENS , PRE	MARY PLUG		•											
S WORD	 PL	면/마	PI /PTF	FI /PTP	X/DMAX											
2	14-442	0.94691	0-44949	0.64569	0.72200											
7	16.251	1. 2655	0.50580	0.7265R	0. #2000											
7	16.671	1.0931	0.51887	0.74535	0.91900											
?	16.931	1.1036	0. 52385	0.75250	1.0170			The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon								
	10.431	1.1030	U• 173811	0.7770	1.0170											
APPIT IONA	L PRESSIJPE	PATIOS , FLC	M CAFILLER I	. P.												
0.40k0	թը	PL / PD	PL /PTF	PL /PTP	X/DMAX			•								
2	16.246	1.0652	0.50565	0.72636	0.42200											
7	14.972	0.98165	P. 46599	0.66938	0.67000											
	F BKEZZOKE		W SPLITTEP O													
n word	PI	PL / PO	PL / PTF	PL/PTP	X/DMAX											
7	13-337	0.87448	0.41511	0.59630	0.50800											
2	14-051	1.1435	0.56180	0.80702	0.58300											
2	15.257	1.0003	0.47485	0.68211	3-67000											
THE THEFT	C PRESSURE	FATIOS . COLLAR	CTCP SHECOU													
O WOPD	PL	PL/PO	PL/PTF	PLANTE	X/DMAX											
07	14.837	Q. 972RO	0.56179	0.66374	-1.0000											
12	14-762	0.95789	0.45945	0.65999	-1-0000											
5.5	14.802	9.47051	0.46069	0.66178	-1.0000											
?7	15-072	D. 98821	0.46000	0.67385	-1.0000											
17	15.067	O. 98 788	0.46894	0061367	-1.0000			The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa								
4	14-942	0.97969	0.46505	0.6680	-1.0000											
ADD LT.IQNA	L PRESSURE.	RATIOS ECP	ERODY_LNLET_													
NORD	PL	PL/PD	PL/PTF	PL/PTP	X/DMAX			OR OF								
) 7	14.837	0.97280	0.46178	0.46334	0.39800	**										
12	14.762	0.96789	0.45045	0.65999				<b>₹</b> ₹								
12 22		0.96789			0.43100			PGOO.								
	14.902		0.46069	0.66178	0.44900			⊇ <i>₹</i>								
27	15-072		0.46909	0.67385	0.48600			- <del>2 2</del>								
37	15.067	0.98788	0.46894	0.67362	0.52200			<b>~</b>								
42	14.942	0.97969	0.46505	0.66804	0.58800			~~~								
7 7	15.267	1.0010	0.47516		1-0000			QUA								
								C E								
TO THE	E PREJOUNE:		NOZZLE TLAP					3-								
O ALBO	PL.	PETER	E PL / PTF	PL/PTP	X/DMAX			₹ 55								
5 >	15.257		11-47-16	0.68256	-1.0000											
1	15.267	1.0010	0.47516	0.0455	-1.0000											
IOUIT IONA	L PRESSURE	RATIOS . 20.	DEG SHPCUD L	CCATION												
า พกรก	PŁ	Pt / PN	PL / PTF	Pt /PTP	X/DMAX											
57	15-267	1.2212	9.47516	0.68256	0. 79300			7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 4 7 1 1 1 1								
72	15.267	1.0010	0.47516	0.68256	0.84400											
ANT: TEODE	LIPRESSURE	PATINS L. RO.	DEG_SHPPUD_L	OCATION												
		PL/PN	Pt / PTF	PL/PTP	X/DMAX											
) WORD	PI.	0.96559		_				والمنافعة المنافعة		()* Ab 22A	0.45836	7. F5843	0.79300			
7 WIRD 82	14.777		0.64703	0 44345	0.04400											
82 87	14.392	0.94364 THRUST PARAM	0.44793	0.64345	0.84400			فسنس شده الداليات الماليات								

MASA-LEWIS	. PPFLI4	SHARY DATA	06/13/79	CADDETI	PEC 1077	9 05:35:57.198	FAT 98681	PG# 1334 PPG 1395
>6.70   T   MW	LL PRESSURF	PATINS . PRI	MAPA MING					e ee
EVD HOPO	Pt	ሚ / የባ	PI/PTF	Pt /PTP	X/DMAX		<del></del>	
3?	12.354	0.83743	0.32153	C-46731	J-72200			
37	15.265	0.93763	0.30764	0.57740	0.72000			
47	17.125	1.1192	9.444.00	0.64775	0.91900			
52	17.679	1.1555	0.46055	0.66874	1-0170			
PADDITION	L PRESSIPE	PATTOS . FLO	M COLITACE	i.n.			<del></del>	
AVD WORD	<b>?</b> 1	PL /PR	PL /PTF	PI /PTP	x/DMAX			e anne
62	17.579	1.1695	0.46575	0.67631	0.42200			and the company of the property of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of t
67	13.925	0. 91 005	0.36273	0.52671	0-67900			
NAUL AT LUBK	IL PRESSURE	PATINS . FLO	W SPI ITTEP (	.D.				
AND MUND	Pt	PL / PO	PI /PTF	PL /PTP	X/DMAX			
77	8.7578	0.57237	0.22814	0.33127	9.50800			and the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of th
#?	22.554	1-4740	7.59752	0.85312	0.54300			
. 92	15.295		0.39942_	0.57853	0.67900	·		
	L PPESSUPE	PATITIES & COL	פני נווב איזם					
AVD HOPD	PL	PL/PD	PL/PTF	_DLIPTP	x/DMAX			/
-107	14.899	03-02312	0.38787	0.56321	-1.0000			
-112	4.550	0.95985	0.38657	0.56132	1.0000			· / · · / · · · / · · / · · / · · · / · · · · · · · · · · · · · · · · · · · ·
-172	14.960	<b>7.97116</b>	3000	0.5620#	-1.0000			
-127	15.T30	0.99991	2.39412	5.57279	-1.0000	+ + +		
-137 -142	15.145	0.98979	0.39451	0.572	-1.0000			
-142	15.395	0.98652	0.39321	0,57097	-1.0000			
>voola Tuiñv	L PRESSURE	RATIOS . FOR	ENDOY INLEY					
AVD WORD	PL	PL/PN	PI / PT F	PL /PTP	x/DMAX			a mana anama a mana mana mana mana mana
137	14.890	0.97312	0.38787	0.56321	0.39800		•	
112	14.947	0.96986	9.38657	0.5613?	0.43100			
12?	14.860	0.77116	0.78709	0.56208	<b>3.4490</b> J			
127	15.130	0.99591	0,39412	0.57229	9.4.8690			
137	15.145	0.98979	0.39451	0.57284	9.52200			
142	15.095	0.98652	0.79321	0.57097	0.58800			
462	19.270 15.276			0:57759 0-5777A				
	•						· · · · · · · · · · · · · · · · · · ·	
ALASTE WAI		-						
-1-5 TAU ALBU	Pt 15-270	P[7PI	PI / PTE 0. 10777	PI /PTP 0.57759	X/DMAX -1-0000			
	- 15.275	J. 99824	0.30790		- L 0000	-		
157	L PRESSURE	PATIOS , 20	ը <u>Բ</u> ց_Տ₩Ր <u>ՍԴ_Լ</u>	DCATEON_				
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32	7.5367	0.49454	0.17977	0.26351	0.72200	
37	15.366	1.0477	0.38084	0.55825	0.82000	
47	18.152	1.1911	0.43796	0.63466	J. 91900	
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62	19.377	1.2715	0.46219	U. £7749	0.42200	
67	15.396	0, 99 059	0.36008	0.52783	0.67000	
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77	9.6997	0.63641	0-23134	0.33910	0.50800	
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VD WORD	PL	PL/PD	PL/PTF	PLEPTP	X/DMAX	
107	14.846	201614	0.35612	0.51908	-1.0000	_
112	14.786	0.97024	35269_	O.5169B_	-1.0000	
127	14.476	_0.07754	0.3434	0.51768	-1.0000	<b>32</b>
127	15.221	0.99895	0.25940	52695	-1.0000	
137	17.171	0.99092	0.36020	0.52800	-1.0000	30
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107	14.946	0.97419	0.35412	0.5190#	0_39800	<i>₹₽</i>
112	14.786	0.97024	0.25269	0.51698	2.43100	and a second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control o
122	14.876	0.97156	0.75316	0.51769	0.44900	
12?	15-071	<u>9.</u> 9.8.29.5	0.35949_	0. 52695	2.48699	
137	15.101	0.99092	0.36020	0.52400	0.52200	
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7	14.153	7.92984	0.25762	0.37745	J. 91 900	
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7	12.872	0.84571	0.23377	0.33875	0.50800	والمراور والمنطق المقطر والمراحة المتأسب المراجع والمراجع والمراجع والمراجع والمراجع والمراجع والمراجع والمراجع
<b>?</b>	18.384	1-2078	0.33786	0,48389	0.50300	
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7	19.914	1.7125	0.34609	0.50324	0. #2000	
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D WITH D	PL	PL / PD	PL/PIF			to the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of
97	14,503	0-07440	0.25320	r.37400	-1.0000	
12	14.763	2.97211	2.25651	0.37209	-1-0000	
72	14, 788	344457	0.7340	0.37367	-1-3000	
21	15-04	3.99155	0.26145	0.10013	-1.0300	and the state of the control to the state of the control of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state
31	15.193	7.99518	0.26242	U-341ch	-1.0000	
	15.163	J. 97913	0.26346	0.39310	-1.0000	Application of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of
47						
		PAŢĮOS "FOR	ENDON THEEL	THE RESIDENCE AND ADDRESS OF THE VEHICLE		
WAULT TOUN		PL /PO	bf/bat	PL/PTP	X/MAX	
D MUND PAULTECT	L PRESSURE	PL /PO		PL/PTP 0-27400	X/DMAX 0.35P00	
APOITENNA D HORD OT	PE 14.403		PL/PTF 0.25720			
<u>879] T [RNA</u> D WORD 97 17	PRFS5UPE PL 14.403 14.763	PE /PO 1.97549 1.97777	PL/PTF 0.25720 0.25651	0.27400	0.35800 0.43109	
639]T[NAA D WORD 97 12 22	PE 14.403 14.763 14.763	M /PG 7.97547 7.9777 0.97442	PL/PTF 0.25720 0.25651 0.25654	0.37400 0.37299 0.37362	0.35600 0.43109 9.44909	
63911 [FINA D. WORD 97 17 27 27	PE 14.403 14.763 14.764 15.049	M /PO 9.97549 9.97277 0.97442 9.99155	PL/PTF 0.25720 0.25651 0.25654 0.26146	0.27400 0.37299 0.37362 0.38019	0.35600 0.43100 0.44900 0.44900	
830111048 D WORD 97 17 27 27 37	PE 14.403 14.763 14.764 15.049 15.103	Pt /PG 7,97549 9,97277 0,97462 9,99155 7,99518	PL/PTF D.25720 D.25651 D.25654 D.26146 D.26247	0.27400 0.37299 0.37362 0.38019 0.3868	0.35#00 0.43100 0.44900 0.48600 0.52200	
\$70]T [ANA D WARD 07 17 72 27 27 37	Pt 14.403 14.763 14.763 14.764 15.049 15.103 15.163	M /PG 7, 97 549 8, 97 777 0, 97 442 2, 99 155 5, 94 51 8 7, 94 71	PL/PTF 9.25729 9.25651 0.25654 9.26146 0.26747 9.26746	0.27400 0.37299 0.37347 0.38019 0.38158 0.3810	0.35800 0.43103 0.44900 0.48603 0.52200 2.58803	
839111048 9 MORD 97 12 22 27 37 43	PE 14.403 14.763 14.763 14.769 15.103 15.103	M /PO 0.97549 0.97777 0.97462 0.99155 0.9811 0.98811	PL/PTF 0.25720 0.25651 0.25656 0.26146 0.26246 0.26346	0.27400 0.37299 0.37367 0.30019 0.38168 0.28310	0.35800 0.43100 0.44900 0.48600 0.52200 2.58800	
43911 (048 0 408 0 97 12 27 27 37 42	PE PEFSSURE 14.403 14.763 14.764 15.049 15.103 15.163	M /PO 7,97549 8,97277 0,97442 2,99155 7,90518 7,90713	PL/PTF 9.25729 9.25651 0.25651 0.25654 9.26146 9.26246 9.26247 8.26277	0.27400 0.37299 0.37367 0.3019 0.3819 0.3810 0.28310	0.35#00 0.43100 0.44900 0.48600 0.52200 2.58#00 -1.0000	
A3911 [0MA D MORD 97 12 72 27 37 43	PE 14.403 14.763 14.763 14.769 15.103 15.103 15.103 15.177	M /PO 7.97549 7.97547 7.97462 9.99155 7.99519 7.99713 1.9971	PL/PTF 9.25729 9.25651 0.25656 9.26146 9.26246 9.26346 9.26377 0.26377	0.27400 0.37299 0.37367 0.38019 0.3816 0.28310 0.27347	0.35 P00 0.43103 0.44 900 0.48 603 0.52 200 2.5 8 P03 -1.0000	
ADDIT [ [ ] N   N   D   N   N   D   N   D   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D   N   D	PL #8F\$59#E  PL 14.803 14.763 14.763 14.789 15.103 15.103 15.103 15.118	M /PO 7.97549 7.97777 0.97442 2.99155 7.90718 7.9071 1.9071	PL/PTF 0.25720 0.25651 0.25654 0.26166 0.26267 0.26346 0.26347	0.27400 0.37299 0.37347 0.28019 0.3814 0.28310 0.27317 0.27347	0.35#00 0.43100 2.44900 0.48600 0.52200 2.58#00 -1.0000	
#3911 [04# 0 40# 0 97 17 17 27 27 37 42 42 42 6 40 40 40 40 40 40 40 40 40 40 40 40 40	PE 14.403 14.763 14.763 14.769 15.103 15.103 15.103 15.177	M /PO 7.97549 7.97547 7.97462 9.99155 7.99519 7.99713 1.9971	PL/PTF 9.25729 9.25651 0.25656 9.26146 9.26246 9.26346 9.26377 0.26377	0.27400 0.37299 0.37367 0.38019 0.3816 0.28310 0.27347	0.35 P00 0.43103 0.44 900 0.48 603 0.52 200 2.5 8 P03 -1.0000	
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ATO IT INNA D WORD OT 17 77 77 77 37 47 37 47 50 WORD E2 62 67 67 67 67 67 67 67 67 67 67 67 67 67	PE 14.803 14.763 14.763 14.769 15.103 15.163 15.178 15.178 PE 15.178	M /PO 7.97*49 9.9777 9.97442 9.99155 7.99518 7.99713 1.9991 1.9991 1.9991 1.9991 1.9991	PL/PTF 9.25729 9.25651 9.25651 9.26747 9.26747 9.26747 9.26777 9.26777 9.26777 9.26777	0.27400 0.37299 0.37347 0.38019 0.38168 0.28310 0.27317 0.27347 0.38347 0.38347	0.35#00 0.43100 0.43100 0.44900 0.52200 0.52200 2.58#00 -1.0000 -1.0000	
ATOIT INM D WIRD OT 12 77 12 77 27 37 42 42 42 42 42 44 42 44 44 45 46 46 47 47 47 47 47 47 47 47 47 47 47 47 47	PE 14.403 14.763 14.763 14.764 15.049 15.103 15.163 19:174 19:174 15.175 PE 15.176	M /PO 7.97*49 7.97*47 7.97*47 9.99155 7.9951 1.9971 1.9971 1.9991 1.9091 1.9091 1.9091	PL/PTF  9.25779  0.25651  0.75854  9.26146  0.26746  9.26747  0.26777  0.26777  0.26777  DEC SHEDUD 1  P1/PTF	0.27400 0.37299 0.37347 0.38019 0.38168 0.38310 0.39347 0.38347 0.38347	0.35#00 0.43100 0.44400 0.49600 0.52200 2.5##00 -1.0000 -1.0000 -1.0000	
ADDITIONA D MORD OT 12 72 27 37 42 27 37 42 ADDITIONA D MORD E2 ADDITIONA ON MORD AT	PE 14.803 14.763 14.763 14.769 15.103 15.163 15.178 15.178 PE 15.178	M /PO 7.97*49 9.9777 9.97442 9.99155 7.99518 7.99713 1.9991 1.9991 1.9991 1.9991 1.9991	PL/PTF 9.25729 9.25651 9.25651 9.26747 9.26747 9.26747 9.26777 9.26777 9.26777 9.26777	0.27400 0.37299 0.37347 0.38019 0.38168 0.28310 0.27317 0.27347 0.38347 0.38347	0.35#00 0.43100 0.43100 0.44900 0.52200 0.52200 2.58#00 -1.0000 -1.0000	
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#10111048 D MORD 97 12 22 27 37 42 27 37 42 42 42 42 43 44 45 46 47 47 47 47 47 47 47 47 47 47	PL 14.903 14.763 14.763 14.769 15.103 15.103 15.103 15.177 15.177 15.177 15.177 15.173 17.173 18.PRESSUPE PL 14.6PR 14.303	M /PO 7.97*49 7.97*49 7.97*49 7.97*77 7.97*42 7.99155 7.90518 7.90718 1.0001 1.0001 1.0001 1.0001 PATINS : 20 PL/PN 7.90979 PATINS : RO PL/PN	PL/PTF 9.25729 9.25551 0.25651 0.25656 9.26146 9.26346 9.26346 9.26377 0.26377 0.26377 0.26377 0.26377 0.26363 0.26363 0.26363 0.26363	0.27400 0.37299 0.37347 0.28019 0.38168 0.28310 0.27347 0.38347 0.38347 0.38347 0.38347 0.38335 0.38335	0.35#00 0.43107 2.44909 0.52200 2.58#03 -1.0000 x/DMAX -1.0000 x/DMAX -1.0000 x/DMAX 0.79300 0.44400	

YACA-I FHIS	PRES SH	THPPY DATA	26/13/79	CADDETT	PFC 10/24/79 05:13:2P.588	FAC *X6X1	PGP C034	Run 11 mg 1400	
>eust thet	i parssime	PATIOS . PRI	MAPY PEUG						•
GRUP CAV	PL	PI / n/1	Pt / PT F	PI /PTP	x/DMTx			···	
22	11.349	2. 74 773	0.10716	0.28628	0.72200				
- 7	19.031	1.3132	7.34626	0.50278	7. <b>P2 30</b> 9				
47	14.985	0.98733		0.37801					
			0.26033		0.91900				
" ?	21201	1.4035	0. 37004	0.53774	1.0170				
>633111048	L PRESSURE	PATINS . FLM	W CPLITTEP !	- n-					
AVD WORD	Pl	Pt / PG	PI /PTF	PI /PTP	x/DMAX				
1.2	27.208	1.7927	0.47268	0.68634	0.42200				
47	22.346	1.4723	0.29822	0.56371	0.67000				
					0.67700				
>A701710MA	L PRESSURE	PATTOS . FIO	W SPI ITTEP O	'•n•					
AVD WOPD	Pt	PL/PO	PL /PTF	PL /PTP	x/DMAX				
77	13.435	0.88517	0.23340	0.33890	0.50800				
R2	19.231	1.2671	0.33409	0.48512	0.58300				
92	15-195	1-0012	0.26395	0.38331	2.67002		<del></del>		
24801710M	<del></del>	RATIOS & EJE	<del>(10, sustan</del>						
-	PL								
AVD WORD		PL / PD	PL /PTF		X/DMAX				
107	14.975	0 97679	0.2579	0.3739A	-1.0000				
112	16.775	O. 97332	0.25668 _	0.37271	-1-0000				
122	14.805	0+97547	0.26.720	0.37347	-1.0000				
127	15.265	0.97260	0.26172	0.39003	-1.0000				
								····	
	15.120	9-99623	0.2626#						
-137 -147	15.120 15.180 L PRESSURE	0.99623 1.0002 PATIOS . FOR	0.2626# 0.26372 EBODY_INLET	0.381+2	-1.0000 -1.0000				
-137 -142 >ADDITIONA DROW OV	15-180 L PRESSURE PL	1.0002 PATIOS <u>. FOR</u> FL/PD	0.26372 EBODY JHLET PL/PTF	0.381+2 0.38293 PL/PTP	-1.0000 1.0000 X/DMAX				
-137 -142 >ADDIT IDMA -VN WOPD 107	15.180 L PRESSURE PL 14.825	1.0002 PATIOS FOR (1./PD 0.97679	0.26372 EBDDY _INLET_ PL/PYF 0.25755	0.38293	-1.0000 1.0000				
ADDIT IDMA Vn MOPD	15-180 L PRESSURE PL	1.0002 PATIOS <u>. FOR</u> FL/PD	0.26372 EBDDY _INLET_ PL/PYF 0.25755	0.381-2 0.38293 PL/PTP 0.37398	71.0000 71.0000 X/DHAX 0.39800				
137 142 >ADDIT IDNA: Vn WOPD 107 112	15-180 L PRESSURE PL 14-825 14-775	1.0002 PATIOS FOR (1.70 0.97679 0.97349	0.26372 EBODY LINLET PL/PYF 0.25755 0.25668	0.381-2 0.38293 PL/PTP 0.37398 0.37271	-1.0000 1.0000 X/DMAX 0.39800 0.43100				
137 142 >ADDIT 104A VN MOPD 107 112 122	15-180 L. PRESSURE PL 14-825 14-775 14-805	1.0002 PATIOS FOR GL/PD 0.97679 0.97349 0.97547	0.26372 EBOOY INLET PL/PTF 0.25755 0.25668 0.25720	0.38142 0.38293 PL/PTP 0.3739N 0.37271 0.37247	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900				
>ADDIT 10% Vn MOPD 107 112 122 127	15.180 L PRESSURE PL 14.825 14.775 14.805 15.065	1.0002 RATIOS FOR (1./PD 0.97679 0.97349 0.97547 0.99260	0.26372 EBODY INLET PL/PYF 0.25755 0.25668 0.25720 0.25720	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.38003	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600				
>ADDIT IDMA Vn MOPD 107 112 122 127	15-180 L PRESSURE PL 14-825 14-775 14-805 15-065 15-120	1.0002 PATIOS FOR: (1/PD 0.97679 0.97349 0.97547 0.99260 0.99623	0.26372 EBODY INLET PL/PTF 0.25755 0.25668 0.25720 0.26172 0.26768	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.38003 0.38142	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200				
2137 142 2 ADDIT 10MA: VN MOPD 107 112 122 127 127 142	15.189 L PRESSURE PL 14.825 14.775 14.805 15.965 15.120 15.120	1.0002 RATIOS FOR: (1/PD 0.97679 0.97349 0.97547 0.99260 0.99623 1.0002	0.26372 EBODY LINLET PL/PTF 0.25755 0.25668 0.75770 II.26172 0.26768 0.26372	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.38003 0.38142 0.38293	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.52800				
>ADDITIONA Vn WOPD 107 112 122 127 127 127	15.180 L PRESSURE PL 14.775 14.775 14.805 15.265 15.120 15.190 17.127	1.0002 RATIOS FOR (L/PD 0.97679 0.97349 0.97547 0.99260 0.99623 1.0002	0.26372 EBODY INLET PL/PTF 0.25755 0.25668 0.25720 D.26172 0.26768 0.26372 9.26374	0.38142 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.38003 0.38142 0.38293	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 -1.7000				
137 142 >ADDIT IDMA: VN WOPD 107 112 122 127 127 142	15.180  L PRESSURE  PL 14.825 14.775 14.805 15.065 15.120 15.190 17.197	1.0002 PATIOS FOR: (1/PO	0.26372 EBODY INLET  PL/PTF 0.25755 0.25668 0.25770 0.26172 0.26268 0.26372 0.26372	0.381+2 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.28003 0.38142 0.36293 0.3811+2 0.39291	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.52800				
>ADDITIONAL VN MOPD 107 112 122 127 127 142	PRESSURE PL 14.775 14.775 14.805 15.965 15.120 15.199 17:147 17:147	1.0002  RATIOS . FOR  (1/PD	0.26372 EBODY INLET PL/PYF 0.25755 0.25668 0.26372 0.26768 0.26373 0.26373 0.26374 0.26374	0.38142 0.38293 PL/PTP 0.3739N 0.37271 0.38003 0.38142 0.38293 0.381142	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1:7000				
2 ADDIT IDNA VM MOPD 107 112 127 127 127 147 242 147 242 147 242 147 242 147 242 147 242 147 242 147 244 247 247 247 247 247 247 2	PL 14. #25 14. #25 14. #75 14. #95 15. 120 15. 120 15. 120 15. 120 15. 120 17. 127 12. 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129	1.0002  PATIOS . FOR  (1/PD	0.26372 EBODY INLET PL/PYF 0.25755 0.25668 0.25720 0.26172 0.26268 0.26372 0.26372 0.26374 0.26377	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.38003 0.38142 0.38293 0.3811-2 0.39291	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 2.58800 -1.7000 -1.0000				
137 142  >ADDIT 10MA  VN WOPD 107 112 122 127 142 1-7 142 1-7  WO WOPD 152	PRESSURE PL 14.475 14.775 14.805 15.065 15.120 15.190 15.197 17:197	1.0002  RATIOS FOR:  (1./PD	0.26372 EBODY INLET  PL/PTF 0.25755 0.25668 0.25770 0.26172 0.26268 0.26372 0.26372 0.26374 0.26374	0.38192 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.28003 0.38142 0.36293 0.36142 0.36293	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 2.58800 -1.7070 -1.0000 X/DMAX -1.0000				
137 142  >ADDIT 10MA  VN WOPD 107 112 122 127 142 1-7 142 1-7  WO WOPD 152	PL 14. #25 14. #25 14. #75 14. #95 15. 120 15. 120 15. 120 15. 120 15. 120 17. 127 12. 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129 17. 125 129	1.0002  PATIOS . FOR  (1/PD	0.26372 EBODY INLET PL/PYF 0.25755 0.25668 0.25720 0.26172 0.26268 0.26372 0.26372 0.26374 0.26377	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.38003 0.38142 0.38293 0.3811-2 0.39291	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 2.58800 -1.7000 -1.0000				
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	PL 14.825 14.875 14.805 15.065 15.120 15.190 19.197 19.197 19.199 15.199 15.199	1.0002  RATIOS FOR:  (1./PD	0.26372 EBODY INLET PL/PYF 0.25755 0.25668 0.25720 0.26172 0.26768 0.26379 U.20379 U.20379 U.20379 U.20379 U.20379	0.38193  PL/PTP 0.37398 0.37271 0.37247 0.38003 0.36142 0.36293 0.38119 0.99991	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 2.58800 -1.7070 -1.0000 X/DMAX -1.0000				
>ADDIT IDMA  VN MOPD  107  112  127  127  142  1-7	PL 14.825 14.875 14.805 15.065 15.120 15.190 19.197 19.197 19.199 15.199 15.199	1.0002  PATIOS . FOR:  (1/PD	0.26372 EBODY INLET PL/PYF 0.25755 0.25668 0.25720 0.26172 0.26768 0.26379 U.20379 U.20379 U.20379 U.20379 U.20379	0.38193  PL/PTP 0.37398 0.37271 0.37247 0.38003 0.36142 0.36293 0.38119 0.99991	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 2.58800 -1.7070 -1.0000 X/DMAX -1.0000				
2 ADDIT IDMA  VN MOPD  107  112  127  127  142  142  142  144  VN MOPD  152  157  2600 IT IDMA  VN MOPD	PL 14.775 14.775 15.965 15.129 17.127 19.139 L PRESSURE PL 15.196 L PPESSURE PL	1.0002  RATIOS FOR  (L/PD	0.26372  EBDDY INLET  PL/PTF 0.25755 0.25668 0.25720 0.26172 0.26372 0.26374 0.26377 0.26377 0.26377 0.26377 0.26377	0.38142 0.38293 PL/PTP 0.37398 0.37271 0.38003 0.38142 0.36293 0.38714 0.36293 0.38714 0.36319 0.38319 0.38331	-1.0000 -1.0000 -1.0000  X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 -1.0000  X/DMAX -1.0000 -1.0000				
20017 IDMA  VN MOPD  107  112  127  127  147  147  VN MOPD  152  157  260017 IDMA  VN MOPD  167	PRESSURE PL 14.475 14.775 14.805 15.065 15.120 15.190 17.197 19:199 L PRESSURE PL 15.196	1.0002  PATIOS FOR  (L/PO	0.26372 EBODY INLET PL/PTF 0.25755 0.25668 0.25720 II.26172 0.26268 0.26372 9.28389 C.28389 MUZZLE FLAP PL/PTF 9.26389 DEG SIRCUD L	0.38192 0.38293 PL/PTP 0.37398 0.37271 0.38003 0.38142 0.38293 0.38119 0.99991 PL/PTP 0.38319	-1.0000 -1.0000 -1.0000  X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 -1.0000				
2 ADDIT IDMA  VN MOPD  107  112  127  127  142  127  147  20011 IDMA  VN MOPD  152  257  26011 IDMA  VN MOPD  167  177	PESSURE PL 14.775 14.775 14.775 15.065 15.190 17.197 17:199 L PRESSURE PL 15.196 15.196 PL 15.196 15.197	1.0002  RATIOS FOR  (L/PO	0.26372 EBODY INLET  PL/PTF 0.25755 0.25668 0.25770 II.26172 0.26268 0.26372 7.26389 C.26372 PL/PTF 0.26398 DEG SIRRUD L  PL/PTF 0.26398 0.26407	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.38003 0.38142 0.38293 0.3911 0.39311 0.38319 0.38319 0.38331 0.38331 0.38331	-1.0000 -1.0000 -1.0000  X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 -1.7000 -1.0000  X/DMAX -1.0000 -1.0000				
2 ADDIT IDNA  VN MOPD  107  112  127  127  142  127  147  240  152  157  240  240  240  240  240  240  240  24	PRESSURE  PL 14.425 14.775 14.405 15.265 15.120 15.190 17:107 17:107 17:107  PRESSURE  PL 15.196 15.195 L PRESSURE  PL 15.195 L PRESSURE  PL 15.195 L PRESSURE	1.0002  PATIOS . FOR:  (1/PD	0.26372 EBODY INLET PL/PYF 0.25755 0.25668 0.26372 0.26368 0.26372 0.26368 0.26398 DEG SHRUUL L PL/PYF 0.26398 0.26398	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.28003 0.36142 0.36293 0.3611- 0.99391 PL/PTP 0.36319 0.38311 0.36331 0.36344	-1.0000 -1.0000 -1.0000  X/DMAX 0.39800 0.43100 0.44900 0.58600 0.52200 0.58800 -1.7070 -1.0000  X/DMAX -1.0000 -1.0000  -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
237 242 27 207 112 122 127 142 127 142 127 240 1152 250 260 211 27 260 211 27 260 211 27 260 211 27 260 211 27 260 211 27 260 211 27 260 211 27 260 211 27 260 211 27 260 211 27 260 211 20 20 20 20 20 20 20 20 20 20 20 20 20	PRESSURE PL 14.475 14.475 14.475 14.495 15.196 15.190 15.197 175.197  L PRESSURE PL 15.196 15.196 L PPESSURE PL 15.197 15.197 L PRESSURE PL 15.197 L PRESSURE PL 15.197 L PRESSURE PL 15.197 L PRESSURE PL 15.197 L PRESSURE	1.0002  PATIOS FOR:  (1/PO	0.26372  EBODY INLET  PL/PTF 0.25755 0.25668 0.25720 0.26172 0.26268 0.26372 9.28389 0.26398  DEG SHRTUD L  PL/PTF 0.26398 0.26407  DFG SHPT(M) 1	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.38293 0.38142 0.38293 0.38142 0.38293 0.38319 0.38319 0.38331 0CATION PL/PTP 0.38331 0.38344	-1.0000 1.0000  X/DMAX 0.39800 0.43100 0.49600 0.52200 2.58800 -1.7000  X/DMAX -1.0000 -1.0000  X/DMAY 0.79300 0.94400				
-137 -142 -2 ADDIT IDMA	PL 14.775 14.775 15.065 15.190 17.197 17.197 17.197 17.195 L PRESSURE PL 15.195 L PRESSURE PL 15.195 15.200 L PRESSURE PL 14.715	1.0002  RATIOS FOR  (L/PO	0.26372 EBDDY_INLET. PL/PTF 0.25755 0.25668 0.25770 0.26172 0.26368 0.26372 0.26389 THUZZLE FLATT PL/PTF 0.26389 0.26398 DEG_SIRROUD_L PL/PTF 0.26398 0.26407 DFG_SHRROUD_L PL/PTF 0.26398	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.37247 0.38003 0.36142 0.36293 0.3711 0.36319 0.36319 0.36331 0.36331 0.36331 0.36331 0.36331 0.36331	-1.0000 -1.0000 -1.0000  X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000  X/DMAX -1.0000 -1.0000  Y/OMAY 0.79300 J.94400				
-137 -142	PESSURE PL 14.775 14.775 14.775 15.965 15.120 15.199 17:177 175.199 L PRESSURE PL 15.196 15.196 L PPESSURE PL 15.196 15.200 L PPESSURE PL 14.715 14.420	1.0002  PATIOS FOR:  (1/PO	0.26372 EBODY INLET PL/PYF 0.25755 0.25668 0.25770 0.26172 0.26372 7.26377 0.26377 0.26377 0.26377 0.26397 DEG SHROUD L PL/PYF 0.26398 0.26407 DEG SHROUD 1 PL/PYF 0.26398 0.26407	0.381-2 0.38293 PL/PTP 0.37398 0.37271 0.38293 0.38142 0.38293 0.38142 0.38293 0.38319 0.38319 0.38331 0CATION PL/PTP 0.38331 0.38344	-1.0000 1.0000  X/DMAX 0.39800 0.43100 0.49600 0.52200 2.58800 -1.7000  X/DMAX -1.0000 -1.0000  X/DMAY 0.79300 0.94400				

	PRELIM	HARY DATA	06/13/79	CADDE ! 1	PEF 10/24/79 0*:15:03.359	ere urest	bea cose – bue 1451 Kryl	
SANOTT TONAL	PRFSSUPF	PATIOS , PRI	MAPY PLUG					
מפיוש חע	PI	<b>91</b> / PO	PL /PTF	PI /PTP	X/DMAX			
32	11.316	0.74222	0.20515	0.29677	3.72200		at a	
2.7	18.451	1.2197	0.31450	0.48388	0. #2000			
47	14.186	0.93049	0.25719	0.37204	0.91900			
52	21.260	1.3745	0.38544	0.55756	1-0170			
JAPOT T TOMAL	PPFSSUPF	RATINS , FLN	W SPLITTER I	.n.	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			
WO WORD	PL	PL /PO	PI /PTF	PL /PTP	X/DMAY			
62	26.230	1.7185	0.47499	0.68711	0.42200			
6,7	21.750	1.4273	0.39457	0.57067	3.67900			
JAMOIT TOMAL	PRESSURE	PATIOS . ELO	M COLITTED I	.D.	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s			
NU MUBU	PL	P) /PN	PL / PTF	PL /PTP	x/DMAX		A Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Comp	
77	12.976	0.84456	0.23744	0.33769	0.50890			
<b>A7</b>	18.431	1.2089	0.33414	0.49336	0.58300			
92	15-241	0. 29966	0.27632		0. 6 7 000			
SHOOT BUILD	PRESSURE	P41175 & EJE	CT DR SHEDDO				e a ne na man ann a man e Mark e nghelikhangari na wakin e wa s	
מפחש פעו	PL	PL/20	PL/PTF	Pl /219	X/DMA X	مارسا المحدور والمستوال المارا الما		
197	14.866	0-07509	0.26952	0.38988	1.0000			
112	16-521	0.97214	0-24070	0-38870	-1-0000			
122	14.851	0.97410	0.75.035	0.38048	-1.0000			
127	15.126	2-99714	0.27423	0-39670	-1.00c0			
137	15.191	0.99575	0. 27523	0.3981	-1.0000			
-147	15:231	0.99993	9.27613	0.39945	-1.0000		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	
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107	14.966	0.97509	0. 26952	0.349#8	0.39800	•		
112	14.871	0.97214	0.26#70	0.38870	0.43100			
122	14.851	0.97410	0.26925	0.38948	0.44900			
127	15-126	0. 99214.	0. 27425		0_46600			
	15.141	0.99575	0.27523	0.39#14	0.52200			
137	15.231	0. 99903	0.27613	0.39945	0.58900		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
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142 163 Vn wnwn	15+241 - P4E3311PP P1	9.99989 PATENS : PAN	402246 PERF	PL /PTP	y/DMAX			
142 143 VA MORD 152	15+241 -P42331109 P1 	9.55466 PATIOS : PAN PL/PII T. 9794 6	0.27632 MIZZEE PERF 0.27632	PL /PTP 0.39971	y/DMAX -1.0000			···
142 143 VN MORD 157	P1 15.251 15.261	PATING PAN PATING PAN	0.27632 0.27632	PL/PTP 0.39971 0.39971	y/DMAX			
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>ADDITION	AL PRESSURE	PATINS . PRI	MAPY PEHG			
AVD HOPD	PL	PI /PA	PL /PTF	PL /PTP	Y/DMAX	
32	8.9843	0.59116	0.18966	0.27777	0.72200	
77	14.970	9.98174	0.31497	6.46129	J. 82000	
47	19.564	1-2873	0.41300	0.60487	0.91900	
52	19.949	1.3126	0.42113	0.61677	1.0170	
>ADD IT ION	AL PRESSUPE	PATIOS . FLO	W SPLITTER I	.D.		
NO HOPD	PI	PL/PO	PI / PTF	PI /PTP	X/DMAX	· · · · · · · · · · · · · · · · · · ·
52	21.948	1-4442	0.46334	0.67858	0-42200	
67	17.689	1.1640	0.37343	0.54691	0.67000	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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77	11-060	0-72774	0.23348	0.34195	0.50800 _	
P 2	15.765	1.0373	0.33261	0.48741	0.58300	The second control of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco
92	15.210		0.32109	0.47025	0.67000	
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-1 17	14.46)	9.97770	0=3-370	0.45944	-1.0000	
112	14-805	0.076	0.31254	0_45774_	-1-0000	
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127	15.099	0.99325	9.31866	0.46670	-1.0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
137	15.150	0.99687	0.319A2	0.46	-1.0000	
447	15.205	1.0005	0. 32099	0.47010	-13-0000	e de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della comp
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VO WORD	PL	PL / PO	PL / PTF	PL /PTP	X/DMAX .	
107	14.860	0.97779	0.31379	0.45944	0.39000	•
112	14.805	0.97417	0.31254	0.45774	0.43100	
122	14.835	9.97614	0.31318	0.45866	0.44900	
127	15.095	D. 99325	0.31866	C-46670	0.48600	
137	15.150	0.99687	7.31987	0.46840	0.52200	
142	15.205	1.0905	0.32099	0.47010	0.58900	A CANADA AND A DESCRIPTION OF A SERVICE OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE
153	19.199	<del></del>	0.37077	*******	-1.0000	
147	17,199	2,29983	0-32077	******	-1.0000	
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15?	15_149	0.99983	0.37677	C.46079	-1.0000	
-167	15.195	0.99983	0. 32077	9.4697	-1,0000	en la companya de la companya de la companya de la companya de la companya de la companya de la companya de la
>4º01710W	AL PRESSURE	PATINS 20	DEG SHPRUD 1	GCATION		
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167	15.195	0.97983	0.32077	0.46979	0.79300	
172	15.190	0.99950	0.32067	0.46964	0. 84400	ا الله المستقد الله المستقد الله الله الله الله الله الله الله الل
>4001110N	AL PRESSUPE.	PATIOS . 90	DEG_SHP.CUD_L	DCVITON -		
NU MUBD	PL	PI / PI)	PL/PTF	PL /PTP	X/DMA X	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
187	14.595	0.95970	1.30790	0.45093	0.79300	
187	14.250	0.93765	0.30083	0.44058	0.84400	
SORTION F	ME . C	THPUST PARAM				

	S PRELIM	INARY DATA	06/13/79	CADDELL	REC 10/24/7	9 05:17:58.123	FAC RXAXI PGM CO34 PDG 1403
>40011104	IAL PRESSURE	PATINS . PRI	MAPY PLUG				· · · · · · · · · · · · · · · · · · ·
VI WORK	PL	Pt /PI)	PL / PTF	PL /PTP	X/DMAX		
32	7.5367	0.49610	0.17951	0.26356	0.72200		
27	15. 961	1.0441	0.37779	0.55447	0.72000		ն և հատուս հատուա մայատաբին չուդարարար ընտ հաջարագա
47	18.112	1. 1922	0.43139	0.63337	0.91900		
52	18.497	1.2116	0.43841	0.64368	1.0170		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
MOI TI COA	AL PRESSUPE	RATIOS . FLO	W SPLITTER I	.n.			
NU MUBU	PL	PL/PN	PL / PTF	PL /PTP	X/IMAX		
7	19.357 15.396	1.2742 0.99370	0.46104 0.35956	0.67691 0.52792	0.42200 0.67000		and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th
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/በ ዘግዋብ	P1	የፈ / ዮባ	Pt / PT F	PL /PTP	X/DMAX		
77	9.6837	9.63742	0. 23965	0.33864	0.50800		1 To 1 To 1 Think to the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of
• 7	21.377	1.4971	0.50916	0.74756	U. 5 8300		
2	15.201	1.0006	0.36207	0.53159	0-67000		
40017 Inn	AL-PRESSURE	<del>RATIOS Y CIC</del>	CTTR SHEDON				and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t
O NORD	PL	PL / PO	PL/PTF	PLAPTE	X/DMAX		
107	14.436	Q. 9765R	0.35327	0.51982	-1.0000		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
112	14-776	0.07263	Je 35194 -	9.51672	-1-0000		
122	14.906	0-47561	9-35265	0.51777	-1.0000		•
27	15.051	0.99074	0.354	0.52634	-1.0000		
37	15.086	0. 99304	0.35933	0.42757	-1-00CO		The same of the same of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the same transfer of the sa
المستحدث	15.071	0.99205	0.35897	0.5270	-1.0000		
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				20. 42.72			
/N 4080 107	PL 14.836	PL/PD 0.9765#	PL/PTF 0.35337	PL/PTP 0.51882	X/DMAX 0.39800	<del></del>	OF STREET
17	14.776	0.97763	0.35357	0.51672			一句 ガ
22	14.836	0.97461	0.35265	0.51777	0.43100 0.44900	and the second second	
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.27	15. 351		0.35849	0.52634	0.48600		
42	15.086	0.99205	0.35923	0.52757	0.52200		22
. <del></del>	15.071		0.35897	0.52704	0.58900	post of the same	
47	15.201	1.0776	9.96207	0.93199	-1-0000		
7	19.201	1.0776	76 50 707	0-13154	-1:00m0		은 물
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ID WORD	PL	9/80	TPYF.	PL /PTP	X/DMAX		AGE IS
57 WILE!	15-291	1.0006	0.36207	-0-53159	-1.0000		
9	15.271	1.0006	0.36207	0.53156	1.0000		⊀ დ
		RATIOS . 20	DEG SHPCUD I				The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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· >AOTITINŅ VD WORD	PL	P( /P()		A = 71.41			
- >AODITINN VD WORD 167	PL 15.196	1.0003	0-36195	0.53141	0.79300		
-A00 T TINN ID WORD  67  72	PL 15.196 15.196	1.0003	0-36195 0-36195	0.53141	0.84400		
AODITINN 70 WORD 67 77 ADDITION	PL 15-196 15-196 AL PRESSIME	1.0003 1.0003 RATIOS , RO	9-36195 0-36195 DEG SHRPUD 1	0.53141 NÇATINN	0.84400		•
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27	16.305	1.0667	0.50627	0.72509	0.82000	
47	16.725 .	1-0942	C. 51932	0.74377	0-91900	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
<b>~</b> 2	16.990	1.1050	0.52444	0.75111	1.9170	
NOT T 1004<	AL PRESSIME	RATIOS . FLO	W SPLITTEP 1	.n.		
VO WORD	PL	PL / PO	PL/PTF	PI /PTP	X/DMAX	
62	16.310	1.0671	0.50643	0.72531	J-42200	ALC THE RESIDENCE TO A STATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF
67	15-010	0.99201	0.46606	0.66750	9.67099	
NOTTECCAS	AL PRESSUPE	PATINS . FIR	W SPLITTER F	-0-	The second second is the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the secon	
VO WORD	PL	<b>91 /</b> PO	PL /PTF	P; /PTP	X/DMA X	
77	13.375	0.87502	0.41528	0.59477	2-50800	and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th
92	19.065	1.1819	0.56092	0.80336	G. 58300	
92	15.295	1.0007	0.47491	0.68017	0-67000	
SHOOT TOWN	NE PRESSURE	RATIOS & EJE	CTOR SHPOUR			. The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the
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197	14.860	0-07219	0-56149	0.66083	-1.0000	
112	14.795	0.96 700	1.45938		-1-0000	
122	14.875		0.39070	0.65838	-1-9000	
127	15-090	0.98659	0.44FZ4	67061	-1-0000	and the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of th
137	15.005	0.08757	0.46870	0.6717	-1.0000	
143	14.965	9.97906	9.46466	0.66550	-1:0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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VD WOPD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX	المعارض والمعارض المعارض المعارض المعارض والمعارض
137	14.967	9.97219	0.46140	0.660#3	0.39800	•
112	14.795	0. 96 794	0.45938	0.65794	0.43160	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
177	14.405	0.46859	0.45970	0.65838	0.44900	
127	15. 089	D.98657	0_46824	0.67061	0.48600	
137	15. 395	7. 99757	0.46970	C.67128	0.52200	
147	14-965	0.97906	Q.4646£	0.66550	0.56600	. The companies with the companies with the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of the companies of
157	15.207	1.0007	n, 47471	0.0017 0.07995	-1.0000	
				0.0199-	-1.0000	
	AL PRESSIBLE	RATIOS - PAN				
VP WORD	PL	PL /PI)	PETPIF	PL /PTP	X/DMAX	. We see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the see that the
152	15.295 15.290	1.0007	0.47491 C.47476	0.68017	-1.0000 -1.0000	
		PATINS ± 20				The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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1 f 7 1 7 2	15.295 15.290	1.0000 9.99967	0.47460 0.47445	0.67973 ?.67951	0.79300 0.84400	
	-	RATIOS . PO		-		
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1 P 7	14.759	0.96499	7.45799	9.65593	0.79300	் பது உடை உடங்கள் இருந்தில் இருந்தில் இருந்தில் இருந்தில் இருந்தில் இருந்தில் இருந்தில் இருந்தில் இருந்தில் இர
107	14.400	0. 94 200	0.44712	0-64037	0.74300	
				いってマリンド	V-0-400	and the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contra
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12	15.195	0.99810	2.54919	0.79040	0.72200		
7	15.959	1.0477	0.57542	9.42946	0- 82000		
7	16.145	1.0605	0.58245	0.83980	0.91900		
2	16.235	1.0664	0.58570	0.84448	1.0170		
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32	10.063	0.65983	0.19296	0.32694	0.72200				
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57	19.942	1.3011	0.38050	0.64468	1-0170			and the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street of the street o	
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62	21-372	1.4014	0.40983	0.69438	0.42200	*·= *		and the second second	- ·
67	19.429	1.7093	0.35337	0.59872	0-67000				
>4001 T TONA	L PRESSURE	RATIOS . FLO	W SPLITTER O	.n.					
AVD WORD	PL	PL/PN	PI /PTF	PI /PTP	X/DMAX				ter a ser a service a commander the many a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a service and a s
77	12-103	0.79688	0.23363	D.39584	. 0.50800	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s			and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
82	17.379	1.1395	0.33324	0.56461	0.58300				
92	15.263	1.0008	0.29769	0.49591	0.67000				
	t-PPESSURE	RATEOS & CUE	eter surcus			<b>₩</b> ₩ # 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	and the second of the second	e some anni alla salar anni a a salar alla salar anni a salar a	in the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commenc
AVD WCPD	P	PL/ PO	PL/PTF	_84975	X/DMAX				
-107	14.883	0.07503	0.28540	0.48356	-1.0000				
-112	14-823	0.97190	0.28425	0. 49161	0000			· · · · · · · · · · · · · · · · · · ·	
-122	14-943		8-28454	0.48226	-1-0000				
-127	المالية المالية	0. 99368	0. 28972	0.49047	-1.0000				· · · · · · · · · · · · · · · · · · ·
-1?7	15.163	9.99478	0.29077	11:00366	-1.0000	•			
-445_	15.218	0.99789	0.29183	0.49445	-1-0000	e* :			
MOITICOA⊊.	L_PRESSURE	RATIOS FCE	EBODY THLET						
			m 4075	PL/PTP	X/DMAK				
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GRUP UAN	PL	PL/P0	PL/PTF						desired could be to a second of the second of
107	14.883	0.97593	0.29540	0.48356	0.39800				destroys or allow the common of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common property of the common pr
107 112	14.883 14.823	0.97593 .0.97199	0.29540 0.29425	0.48356 0.48161	0.39800 0.43100				
107 112 127	14.883 14.823 14.843	0.97593 .0.97199 0.97330	0.28540 0.28425 0.28464	0.48356 0.48161 0.48226	0.39800 0.43100 0.44900				
107 112 127 127	14.883 14.823 14.843 15.108	0.97593 0.97199 0.97330 0.99068	0.28540 0.28425 0.28464 0.28572	0.48356 0.48161 0.48226 0.49087	0.39800 0.43100 0.44900 0.48690				
107 112 127 127	14.883 14.823 14.843 15.128 15.163	0.97593 0.97199 0.97330 0.99068 0.9942#	0.25540 0.2555 0.2564 0.2572 0.26572	0.48356 0.48161 0.48226 0.49287 0.49266	0.39800 0.43100 0.44900 0.48600 0.52200				
107 112 127 127 137 142	14.883 14.823 14.843 15.128 15.163 15.219	0.97593 0.97199 0.97330 0.99068	0.25540 0.26425 0.26464 0.26572 0.2077 0.29183	0.48356 0.48161 0.48226 0.49286 0.49266 0.49445	0.39800 0.43100 0.44900 0.48690				
107 112 127 127 137 142	14.883 14.823 14.843 15.128 15.163 15.215	0.97593 0.97199 0.97333 0.99068 0.9942# 0.99789	0.28540 0.28425 0.28464 0.28572 0.29077 0.29183	0.48356 0.48161 0.48226 0.49266 0.49266 0.49445	0.39809 0.43100 0.44900 0.48690 0.52200 0.58809				
107 112 127 127 137 142	14.883 14.823 14.843 15.128 15.163 15.219	0.97593 _0.97199 0.97330 0.99068 0.9942# 0.99789	0.25540 0.26425 0.26464 0.26572 0.2077 0.29183	0.48356 0.48161 0.48226 0.49286 0.49266 0.49445	0.39809 0.43100 0.44900 0.48690 0.52200 0.58809				
107 112 127 127 127 137 142	14.883 14.823 14.843 15.128 15.163 15.219	0.97593 0.97199 0.97333 0.99068 0.9942# 0.99789	0.28540 0.28425 0.28465 0.28972 0.20077 0.20163 0.20270 0.20287	0.48356 0.48161 0.48267 0.49266 0.49266 0.49445 0.49558	0.39809 0.43100 0.44900 0.48690 0.52200 0.58809				
107 112 127 127 137 142 142 143 7AD>S LIGHT	14.883 14.823 14.843 15.108 15.108 15.218 17.229 17.229 1 PRESSURE	0.97593 0.97199 0.97330 0.99068 0.99428 0.99428 0.99789 1.9772 0.29980	0.28540 0.28425 0.28464 0.28572 0.20077 0.20163 0.20273 0.20273 0.20273	0.48356 0.48161 0.48276 0.49276 0.49276 0.4945 0.4945 0.4957	0.39809 0.43100 0.44400 0.44800 0.52203 0.58609 -1.7970 -1.0000				
107 112 127 127 137 142 142 143 7AD>S LIGHT	14.883 14.823 14.843 15.198 15.163 15.219 17.229 17.229	0.97593 0.97199 0.97330 0.97330 0.99068 0.99428 0.99789 1.7777 0.44986	0.28540 0.28425 0.78464 0.28572 0.20077 0.20163 0.20163 0.2079	0.48356 0.48161 0.48276 0.49087 0.49766 0.49445 0.49457 0.49587	0.39809 0.43100 0.44400 0.48690 0.52200 0.58809 -1.7999				
107 112 172 127 127 137 142 143 144 147	14.883 14.823 14.843 15.108 15.108 15.218 17.229 17.229 1 PRESSURE	0.97593 0.97199 0.97330 0.99068 0.99428 0.99428 0.99789 1.9772 0.29980	0.28540 0.28425 0.28464 0.28572 0.20077 0.20163 0.20273 0.20273 0.20273	0.48356 0.48161 0.48276 0.49276 0.49276 0.4945 0.4945 0.4957	0.39809 0.43100 0.44400 0.44800 0.52203 0.58609 -1.7970 -1.0000				
107 112 127 127 137 142 -142 -142 -147 -148 -148 -148 -148 -148 -148 -148 -148	14.883 14.823 14.843 15.108 15.108 15.218 17.249 1 PRESSURE PL 15.253 15.248	0.97593 0.97199 0.97333 0.99068 0.99428 0.99428 0.99789 1.9772 0.9988	0.28540 0.28425 0.28464 0.28572 0.20077 0.20183 0.2737 0.2727 0.2727 0.2727 0.2727 0.2727 0.2727	0.48356 0.48161 0.48276 0.49276 0.49276 0.4945 0.4945 0.4957	0.39809 0.43100 0.44900 0.48690 0.52203 0.58809 -1.7990 -1.0000				
107 112 127 127 137 142 142 147 AND HOPD -152 -157	14.883 14.823 14.843 15.109 15.163 15.219 17.245 1 PRESSUPE	0.97593 0.97199 0.97333 0.99068 0.99428 0.99428 0.99428 0.99428 1.9772 0.9948 2.47103 _ FAN	0.28540 0.28425 0.28465 0.28466 0.28972 0.2017 0.20183 0.2770 0.2787 0.2787 0.2787 0.2787 0.2787	0.48356 0.48161 0.48276 0.49276 0.49276 0.4945 0.4958 0.4958 0.4958	0.39809 0.43100 0.44800 0.48600 0.52203 0.58809 -1.7990 -1.0000				
107 112 127 127 137 142 142 147 2AD9413000 AVD WOPD AVD WOPD	14.883 14.823 14.843 15.138 15.163 15.219 17.249 1 PRESSURE PL PRESSURE	0.97593 0.97199 0.97330 0.99068 0.99428 0.99489 1.9772 0.9986 247122 FAN PLYPO 1.9002 0.9986 RATIOS 20	0.28540 0.28425 0.78464 0.28572 0.20077 0.20163 0.20163 0.20279 0.20287  MOTPLE FLAC PL/PIE 0.29240 DEG SHPNUN 1 PL/PTE	0.48356 0.48161 0.48276 0.49276 0.49276 0.4945 0.8958 0.49558 0.49558 0.49558	0.39809 0.43100 0.44800 0.48600 0.52203 0.58809 -1.7770 -1.0000				
107 112 127 127 137 142 142 147 AND HOPD -152 -157	14.883 14.823 14.843 15.109 15.163 15.219 17.245 1 PRESSUPE	0.97593 0.97199 0.97333 0.99068 0.99428 0.99428 0.99428 0.99428 1.9772 0.9948 2.47103 _ FAN	0.28540 0.28425 0.28465 0.28466 0.28972 0.2017 0.20183 0.2770 0.2787 0.2787 0.2787 0.2787 0.2787	0.48356 0.48161 0.48276 0.49276 0.49276 0.4945 0.4958 0.4958 0.4958	0.39809 0.43100 0.44800 0.48600 0.52203 0.58809 -1.7990 -1.0000				
107 112 127 127 137 142 142 147 AND WIPD -152 -157 >ADDITIONA AVD WIPD 167 172	14.883 14.823 14.843 15.109 15.103 15.219 17.249 17.249 17.249 15.253 15.248 L PRESSUPE	0.97593 0.97199 0.97393 0.99068 0.99428 0.99789 1.9772 0.9986 241123 I FAN 1.9202 0.9986 RATIOS 1 20 Pl /PD 0.99986	0.28540 0.28425 0.28464 0.28972 0.2017 0.20183 0.2770 0.2727 WOPPLE FLAR PL/PIE 0.29250 0.29240 DEG SHPOUD 1 PL/PTE 0.29240 0.29240	0.48356 0.48161 0.48276 0.49276 0.49276 0.4945 0.4945 0.4958 0.4958 0.4958 0.49582 0.49542 0.49542	0.39M07 0.43100 0.44400 0.48400 0.52203 0.58800 -1.77777 -1.0000 X/DMAX -1.0000 -1.0000				
107 112 127 127 127 137 142	14.883 14.823 14.843 15.108 15.108 15.108 15.219 17.249 1 PRESSURE PL 15.253 15.248 L PRESSURE PL 15.248	0.97593 0.97199 0.97393 0.99068 0.99428 0.99789 1.9777 0.2986 241103 1 748 1.2002 0.9986 RATIOS 20 PLANTING 1.90	0.28540 0.28425 0.28464 0.28572 0.20173 0.20173 0.20173 0.20273 0.20273 0.20273 0.202740 0.20240 0.20240 0.20240 0.20240 0.20240	0.48356 0.48161 0.48266 0.49266 0.49266 0.49465 0.49552 0.49552 0.49552 0.49542 0.49542 0.49542	0.39809 0.43100 0.44400 9.48690 0.52203 0.58609 -1.7970 -1.0000 X/DMAX -1.0090 -1.0000				
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107 112 127 127 137 142	14.883 14.823 14.843 15.128 15.128 15.129 17.249 17.249 17.249 15.253 15.258 L PRESSUPE PL 15.248 15.248 L PRESSUPE	0.97593 0.97199 0.97330 0.99068 0.99428 0.99428 0.99489 1.9772 0.9986 RATIOS _ 20 M /PO 0.99986 RATIOS _ 80 PL/PO 0.99986 RATIOS _ 80 PL/PO 0.99560	0.28540 0.28425 0.78464 0.28572 0.20177 0.20173 0.20173 0.20273 0.20273 0.20273 0.202740 0.20240 0.20240 0.20240 0.20240 0.20240 0.20240	0.48356 0.48161 0.48276 0.49276 0.49276 0.4945 0.4945 0.4957 0.4957 0.4957 0.49542 0.49542 0.49542 0.49542 0.49542 0.49542	0.39809 0.43100 0.44400 0.48690 0.52203 0.58609 -1.7970 -1.0000 X/DMAX -1.0090 -1.0000 F/DMAX 0.79300 0.84400				
107 112 127 127 137 142 -442 -442 -442 -442 -447 AVD WOPD 167 172 -2400[T]ONA AVD WOPD 167 172 -4400[T]ONA AVD WOPD 167 172 -4400[T]ONA AVD WOPD 167 172	14.883 14.823 14.843 15.108 15.108 15.128 17.249 1 PRESSUPE PL 15.253 15.248 L PRESSUPE PL 15.248 L PRESSUPE PL 15.248 15.248 15.248	0.97593 0.97199 0.97393 0.99068 0.99428 0.99428 0.99428 0.99428 1.97772 0.99428 1.97772 0.99428 RATIOS 20 PL/PD 0.99986 RATIOS 30 PL/PD 0.99986 RATIOS 30 PL/PD	0.28540 0.28425 0.28425 0.2864 0.28572 0.20183 0.20183 0.20297 0.20287 0.20287 0.20287 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280 0.20280	0.48356 0.48161 0.48276 0.49276 0.49276 0.49445 0.4945 0.49557 0.49557 0.49562 0.49542 0.49542 0.49542 0.49542	0.39809 0.43100 0.44400 0.48490 0.52203 0.58509 -1.7979 -1.0000 X/DMAX -1.0090 -1.0000				

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>42217104	ML PRESSUPE	RATIOS . PP	IMARY PLUG			
AUM UND	et	PL / PN	PI /PTF	PI /PTP	X/PMAX	
32	10.737	0-72621	0.20600	0-29749	9-72200	
27	16.546	1.0943	0.20000	0.45842	0.02000	· • •
47	15-121	0.99457	0.29011	0-41896	0.91900	A Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Comp
<b>~</b> 2	20.979	1.3752	0.40114	0.57930	1.0170	
>APRITION	IAL PRESSION	RATIOS . FLO	W SPI ITTEP 1	.n.		
IVE WORE	PL	PL/PN	PI /PTF	PL /PTP	X/DHAX	
62	24.657	1.6217	0.47306	0.68316	J. 42200	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
67	20.294	i. 3341	0.3#016	0.56200	0.67003	
YOU TEGGA	AL PRESSUPE	PATIOS . FLO	W SPI ITTEP F	n.		
WO WORD	Pl	PL /PO	PL /PTF	PL /PTP	x/OMAX	
77	12.177	2.82291	9.23362	0.33738	0.50000	
82	17.369	1.1418	0.33307	0.48099	J_5#3G0	. At the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in the same in t
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92	15_206		0-29174	0.42131	0.67000	
***********	ME PAF TSUFF	R01103 1 EUR	CT CF SHERWIN			• The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second sec
VD 40RD	PL	PL/PD	PL/PTF	PLANTE	X/DMAX	and the second control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the contro
197	14. R?6	0-87517	0.28649	0.41079	-1.0000	
112	14.797	2. 9725	U. 28369	0.40968	-1_0000	
1??	14.976	D-1044165	0.74607	0.41023	-1.0000	
127	15.021	2.99129	0.29915	0.41757	-1.0000	
137	15:131	0.99522	0. 29030	0.21934	-1.0000	to the term of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of t
	15.191 AL PRESSURF	0.99917 RATINS . FOR	0.29145 ERODY INLET	0.42090	1 0300	
152 >ANDITINA		0.99917 RATINS FFF PL/PN		0.42090 PL/PTP	XAPPOX	
>ANDITINN	AL PRESSUPF	RATINS FOR	EUGOA THEET			
>ADDITANA VD WORD	AL PRESSURF PL 14.926	RATIOS FOR PL/PO 9-97517	PERDOY INLET PL/PTF 0.29445	PL/PTP 0.41079	X/PMAX 0.39800	
>APDIT <u>in</u> y VD WDRD 107 112	AL_PRESSURF PL 14.926 14.787	RATINS _#, FCP PL/PN 0.97517 0.97254	PL / PTF 0. 28445 0. 28369	PL/PTP 0.41079 0.43948	X/DMAX 0.39800 0.43190	*
>ANDITINN VN WORD 107 112 127	AL PRESSURF PL 14. 926 14. 787 14. 806	RATIOS FOR PL/PO 9.97517 9.97254 9.97345	PERODY INLET  PI / PTF  0. 28445  0. 28369  0. 28407	PL/PTP 0.41079 0.49048 0.41023	X/DMAX 0-39800 0-43100 0-44903	
>ADDIT_ION VD WORD 107 112 127 127	PL 14.926 14.787 14.896 15.971	RATINS FCP PL/PN 9. 97517 9. 97254 9. 97385 9. 99128	PERODY INLET PM / PTF 0. 28445 0. 28407 0. 28915	PL/PTP 0.41079 0.4948 0.41023 0.41757	X/DMAX 0-39800 2-43120 0-44903 0-48900	
>ADDITION VD WORD 107 112 127 127	PL 14. 926 14. 926 14. 787 14. 836 15.971 15.131	RATIOS FOR PL/PO 0.97517 0.9754 0.97385 0.99128 0.99522	M / PTF 0. 28445 0. 28369 0. 28915 0. 29030	PL/PTP 0.41079 0.43948 0.41023 0.41757 0.41924	X/DMAX 0-39800 2-43190 0-44903 0-48600 0-52200	
>ADDIT_ION VD WORD 107 112 127 127 127	PL 14-926 14-926 14-787 14-896 15-971 15-131 15-191	RATIOS , FOR PL/PO 0.97517 0.97254 0.97385 0.99128 0.99522 0.90917	PERODY INLET PERODY INLET 0.28445 0.28407 0.28407 0.29030 0.29145	PL/PTP 0.41079 0.41079 0.41023 0.41757 0.41924 0.42090	X/DMAX 0.39800 0.43190 0.44900 0.52200 0.52200	
>ADDIT ION VO WORD 107 112 127 127 127 147	PL 14. 926 14. 926 14. 787 14. 836 15.971 15.131	RATIOS FOR PL/PO 0.97517 0.9754 0.97385 0.99128 0.99522	M / PTF 0. 28445 0. 28369 0. 28915 0. 29030	PL/PTP 0.41079 0.43948 0.41023 0.41757 0.41924	X/DMAX 0-39800 2-43190 0-44903 0-48600 0-52200	
>ADDIT JON VO MORD 107 112 127 127 127 147	PRESSUPF PL 14. 926 14. 787 14. 876 15.071 15.131 15.191 15.276	RATINS FCP PL/PN 7. 97517 7. 97254 7. 97254 7. 97128 7. 99128 7. 99522 7. 9917 1. 00772	M / PTF 0. 28445 0. 28369 0. 28915 0. 29030 0. 29145 0. 29175 0. 29175	PL/PTP 0.41079 0.49948 0.41073 0.41757 0.41924 0.42090 0.62131	X/DMAX 0-39800 2-43120 0-44903 9-48600 0-52200 3-58800 -1-0920	
>ADDIT JON VD WORD 107 112 127 127 147 147	PL 14-926 14-926 14-787 14-876 15-971 15-131 15-191 15-276	PL/PN 9-97517 9-97517 9-97554 9-97385 9-99128 9-99522 0-99917 1-00092 1-00092 RATINS # FAP	M / PTF 0. 28445 0. 28467 0. 28915 0. 2915 0. 2915 0. 2917 0. 29174	PL/PTP 0.41079 0.47047 0.41023 0.41757 0.41924 0.42090 0.42131	X/DMAX 0.39R00 0.43190 0.44903 0.52200 0.52200 0.58R00 -1.0930	
>ADDIT JON VO WORD 107 112 127 127 147 147 147	PRESSUPF PL 14.926 14.787 14.896 15.071 15.131 15.191 15.276 17.276	PL/PN 9-97517 9-97517 9-9754 9-97385 9-99128 9-9952 0-99117 1-0072 RAYINS 1-FAP	M / PTF 0. 28445 0. 28360 0. 28407 0. 28915 0. 29030 0. 20145 0. 79174 0. 7174	PL/PTP 0.41079 0.47048 0.41073 0.41757 0.41924 0.47090 0.42131 0.42171	X/DMAX 0-39R00 0-43190 0-44903 0-58900 0-52200 0-57800 -1-0930 -1-0930	
>ANDITION VN WORD 107 112 127 127 147 147 157 VN WORD 152	PL 14-926 14-926 14-787 14-876 15-971 15-131 15-191 15-276	PL/PN 9-97517 9-97517 9-97554 9-97385 9-99128 9-99522 0-99917 1-00092 1-00092 RATINS # FAP	M / PTF 0. 28445 0. 28467 0. 28915 0. 2915 0. 2915 0. 2917 0. 29174	PL/PTP 0.41079 0.47047 0.41023 0.41757 0.41924 0.42090 0.42131	X/DMAX 0.39R00 0.43190 0.44903 0.52200 0.52200 0.58R00 -1.0930	
>ADDIT JON VO MORD 107 112 127 127 147 147 147 147 147 VO MORD 152	PL 14-926 14-926 14-797 14-896 15-971 15-131 15-191 15-736 19-236	PL/PD 9-97517 9-97517 9-97554 9-97385 9-99128 9-99522 0-90917 1-0092 1-0002 1-0002	M / PTF	PL/PTP 0.41079 0.4704P 0.41073 0.41757 0.41924 0.47090 0.42131 0.42131 0.42131	X/DMAX 0-39800 0-43190 0-44903 0-52200 0-52200 0-52200 0-510930 -1-0930 X/DMAX -1-0000	
>ANDITION  VO WORD  107  112  127  127  147  147  VO WORD  152  >ANDITION	PRESSUPE  14. 926  14. 787  14. 826  15. 071  15. 131  15. 191  15. 276  PRESSUPE  PL  15. 226  AI PRESSUPE	PL/PD 9-97517 9-97517 9-9754 9-97385 9-99128 9-9952 0-9917 1-0772 1-0772 RAVIDS 1-FAP	M / PTF 0. 28445 0. 28369 0. 28467 0. 28915 0. 29030 0. 29145 0. 79175 0. 79175 0. 79174 0. 29174	PL/PTP 0.41079 0.4048 0.41079 0.41073 0.41757 0.41924 0.47090 0.42131 0.42131 0.42131	X/DMAX 0-39800 0-43190 0-44903 0-46900 0-52200 0-52200 0-52200 1-0930 1-0930 X/DMAX -1-0000	
>ANDIT INN VN MNRD 107 112 127 127 127 127 127 127 127 127 12	PL 14-926 14-926 14-797 14-876 15-071 15-131 15-191 15-736 15-276  PL 14-76 15-276 AI PRESSUPE	PL/PN 9-97517 9-97517 9-97254 9-97285 9-99128 9-99522 0-99917 1-0792 RAVINS _ FAP	# / PTF  0. 28445 0. 28467 0. 28467 0. 28915 0. 20130 0. 20145 0. 20145 0. 20145 0. 20174  MNY/IF FLAF 0. 20174 DEG SHPRUM_L PI / PTF	PL/PTP 0.41079 0.41079 0.41073 0.41757 0.41924 0.42090 0.62131 0.42131 0.42131 0.42131	X/DMAX 0.39800 0.43190 0.44903 0.52200 0.52200 0.58900 -1.0930 X/DMAX -1.0000 1.0000	
>ADDIT ION  VD WORD  107  112  127  127  147  147  >ADDIT ION  VD WORD  152  >ADDIT ION  VD WORD  167	PRESSUPE PL 15.276 PRESSUPE PL 15.271 PRESSUPE PL 15.276 PL 15.271	PL/PD 9-97517 9-97517 9-97517 9-97517 9-97517 9-99128 9-99128 9-99522 9-99128 9-99522 9-9917 1-0007 1-0002 1-0002 1-0002 1-0002 1-0002 PATIOS 20 PL/PD 0-99983	M / PTF 0. 28445 0. 28360 0. 28407 0. 28915 0. 2915 0. 2915 0. 79174 0. 79174 0. 79174 0. 79174 0. 79174 0. 79174 0. 79174 0. 79174	PL/PTP 0.41079 0.4704P 0.41073 0.41757 0.41924 0.42090 0.42131 0.42131 0.42131 0.42131 0.42131	X/DMAX 0.39R00 9.43190 0.44903 0.52200 0.52200 0.59R00 -1.0930 1.0930 X/DMAX 0.79300	
>ANDITION VN WORD 107 112 127 127 127 127 127 127 127 127 12	PL 15-236  AL PRESSUPE  PL 15-736  15-736  AL PRESSUPE  PL 15-236  AL PRESSUPE  PL 15-236  PL 15-236	PL/PN 9-97517 9-97254 9-97254 9-9728 9-99128 9-99522 0-99917 1-0792 RATINS _ FAP 9/PD 1-0702 1-0702 1-0702 PATINS _ 20 PL/PN 0-99983 9-99983	# / PTF	PL/PTP 0.41079 0.41079 0.41079 0.41023 0.41757 0.41924 0.42090 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131	X/DMAX 0.39800 0.43190 0.44903 0.52200 0.52200 0.58900 -1.0930 X/DMAX -1.0000 1.0000	
>ANDITION  VN WORD  107  112  127  127  127  127  127  127	PL 15-236  AL PRESSUPE  PL 15-736  15-736  AL PRESSUPE  PL 15-236  AL PRESSUPE  PL 15-236  PL 15-236	PL/PD 9-97517 9-97517 9-97517 9-97517 9-97517 9-99128 9-99128 9-99522 9-99128 9-99522 9-9917 1-0007 1-0002 1-0002 1-0002 1-0002 1-0002 PATIOS 20 PL/PD 0-99983	# / PTF	PL/PTP 0.41079 0.41079 0.41079 0.41023 0.41757 0.41924 0.42090 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131	X/DMAX 0.39R00 9.43190 0.44903 0.52200 0.52200 0.59R00 -1.0930 1.0930 X/DMAX 0.79300	
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>ANDITION  VN WORD  107  112  127  147  147  147  147  >ANDITION  VN WORD  167  177  >ANDITION  VN WORD  VN WORD  VN WORD  VN WORD  VN WORD	PRESSUPE  PL 14.926 14.787 14.876 15.071 15.131 15.191 15.276 15.276  PRESSUPE  PL 15.276  PL 15.201 15.201 AL PRESSUPE	PL/PN 9-97517 9-97514 9-97515 9-97515 9-99128 9-9952 9-9917 1-0002 1-0002 1-0002 1-0002 PATINS 2-PAP PL/PN 0-99983 9-9983 RATIOS 2-RO	M / PTF	PL/PTP 0.41079 0.47049 0.41073 0.41757 0.41924 0.42090 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131 0.42131	X/DMAX 0.39800 0.43190 0.44903 0.52200 0.52200 0.59800 -1.0030 1.0000 1.0000 1.0000 1.0000 0.79300 0.84490	
>ANDITION  VO WORD  107  112  127  127  147  147  147  147  >ANDITION  VO WORD  152  >ANDITION  LC7  177  >ANDITION	PRESSUPE PL 15.236 AL PRESSUPE PL 15.236 AL PRESSUPE PL 15.231 AL PRESSUPE PL 15.231 AL PRESSUPE PL 15.231	PL/PN 9-97517 9-97517 9-97517 9-9752 9-99128 9-99128 9-99127 1-0772 RATINS _ FAP  PL/PN 0-99983 RATINS _ 80 PL/PN	PI / PTF 0. 2915 0. 2915 0. 2915 0. 2915 0. 2915 0. 2915 0. 2915 0. 2917  WMY/IF FLAF 0. 29174 DEG SHPRIM_t PI / PTF 0. 29165 0. 29165 0. 29165 0. 29165 0. 29165 0. 29165 0. 29165 0. 29165	PL/PTP 0-41079 0-41079 0-41079 0-41023 0-41757 0-41924 0-42090 0-62131 0-62131 0-62131 0-62131 0CATION PL/PTP 0-42117 C-42117 C-42117	X/DMAX 0.39800 2.43190 0.44903 0.48900 0.52200 3.58903 -1.0930 X/DMAX 0.79300 X/DMAX 0.79300 X/DMAX 0.79300	
>ANDIT INN  VN WORD  107  112  127  127  147  147  >ANDIT INN  VN WORD  152  >ANDIT INN  VN WORD  167  177  >ANDIT INN  VN WORD  167  177  >ANDIT INN  VN WORD  182	PL 15-236  AL PRESSURE  PL 15-236  15-236  AL PRESSURE  PL 15-236  AL PRESSURE  PL 15-231  AL PRESSURE  PL 15-231  AL PRESSURE  PL 15-231  AL PRESSURE  PL 15-231  AL PRESSURE  PL 15-231  AL PRESSURE  PL 15-231  AL PRESSURE	PL/PN 9-97517 9-97254 9-97254 9-97385 9-99128 9-99522 0-99917 1-0792 RATINS _ FAP 9/PD 1-0702 1-0702 1-0702 PL/PN 0-99983 9-99983 PATINS _ RO PL/PN 0-94773	M / PTF	PL/PTP 0.41079 0.4048 0.41079 0.41079 0.41079 0.41757 0.41924 0.42090 0.42131 0.42131 0.42131 0.42131 0.42131 0.42137 C.42117 C.42117	X/DMAX 0-39800 0-43100 0-44903 0-52200 0-52200 0-57800 -1.0000 1-0000 1-0000 X/DMAX 0-79900 0-84490	

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		へかかを1918 一かじヹオ£ E				C3 SPLIT F	et ne t	EXTEND	FD)									Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria del Maria de la Maria del Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria de la Maria dela Maria de la Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela Maria dela
	FENW SP					SHORT F		DI ITTEI	9									
		21.F 11 PNST	TION			חיים היים ביים ביים ביים ביים ביים ביים ב	ENP								*			
	E JE CT OP	INLET	DPENING			YANGIP.		~					_					
PPG	ME)	PTF/PTP	PFF/PN	PTP/PN	OMEGA	PTS/PTF	COF	CDP	CFI	ETAL É	TAI.INT	CEPL	Ceuš	<b>¢</b> q				
	0.012	1.69	1-91	1 07	0.000	0 540	0.044	0 840	0.0300	0.0300	0.0300	2 9390	0 0630	*****			des regions	Mark Marks, Co. 100 Marks — Mark
	2.012		2.11	1.26										*****				
	0.041	1.67	2.52		0.220									*****		***************************************		
	7.054	1.70	3.12		0.100									*****				the time accompanies of the con-
	).041	1.69	2.76		0.000									*****				
	3.052	1.70	3.61		0.000									*****				
-	0.055	1.70	4.19 4.19		0.000					-				*****				
	2.26Q 0.055	1.70	3.59		מטר אנו									*****				
-	7.752	1.73	3.10		0.270									*****				
	0.949	2.69	2.76		0.000									*****				Minimum of the con-
-	0.019	1.69	2.49		0.000									*****			-	
	0.023	1.69	2-11		0.000									*****				
	J.037_		1.61		0.000									*****				
	3.004	1.79	1.80		0.000									*****				
	0.029	1.46	1.81		0.000									*****		*** *****	menone selection of selections will be	
	2-214	1.43	2.11		0.000									*****				
425	7. 03 7	1.44	2.50	1.74	0.000									*****				
	0.000	1.46	2.76											*****				
	0.052	1-47	1.11		0.000									*****				
	1, 35?	1.44	3.61		0.000									*****				
	0.063	1.45	4.13 4.14		0.000						0.9704			*****				
_	3.055	1.45	3.60		0.000									*****			-	the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
	0.043	1.47	3.10		0.922			-				_		*****				
	0.053	1.46	2.75		0.000									*****				
435	0.035	1.44	2.51		0.000									*****				Term appropriate 1995
	0.331	1.47	2.12		0.000						0.9326							
427	0.719	1.45	1.41	1.25	0.000	0.544	3.064	0+614	0.9243	0.9243	0.5243	3.9243	0.9273	****				Commercial Commercial

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<b>1454-€ F#</b>	S PREITM	PLAPY DATA	06/13/79	CADDELL	RFF 10/24/7	79 20:20:58.548	FAC 9X6X1	PGM CO34	#222 = 3 RPG 140R	^
NOT 11008	AI PRESSIRE	RATTOS . PR	BIJJ9 Y9AMI					-		•
AVD HOPD	PŁ	PL / PO	Pt / PT F	Pt /PTP	X/DMAX					
32	14.509	1.0124	0.55976	0.94561	0-72200					
27	14.689	1.0249	0.56670	0.95732	9. F2000					
47	14-738	1.0284	0.56862	0.96057	0.91900					
52	14.748	1.0291	0.56901	0.96123	1.0170					
>ATOTTION	AL PRESSIRE	RATIOS , FLI	W SPLITTER I	.D.	P TO THE WANTED THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE TANK THE T					
AVD HORD	Pi	PL/PN	PI /PTF	PL /^TP	X/DMAX					
62	14.589	1.0180	0.56285	05081	0.42200					
£ 7	14-514	1.0127	0. 55996	0.94593	0.67000					^
>+70 ET ION	AL PRESSURE	RATIOS . FLI	W SPLITTER F	.n.						
DAUM UAV	PL	PL / PO	PL / PTF	PL /PTP	X/DMAX		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s			
77	12.567	0.87687	0.48483	0.81902	0.50800					
97	16.016	1.1176	0.61793	1.0439	0.58300					-
92	14.299	0.99776	0.55167	0.93194	0-67000					
-ALDOTTION	AL PRESSUPE	####B5 <b>↓ €</b> #I	CTOR SHPOUD							
AVD WORD	PI	PL/PO	PL/PTF	PLIP	X/DMAX					
-107	14.269	2 99567	0.55052	0.92999	-1.0000	*				
112	14.264	0.99333	0.55033	0-92966	-1.0000					
-122	14.264	2-99533	0.55033	0.97966	-1.0000					
-127	14.269	0. 99567	0.55052	0.02999	-1.0000					•
-137	14.249	3.9942R	0.54975	0. 97868	-1-0000					
شلامها الم	14-204	0-99114	0.54801	0.92576	1-0000					
MOI TIOCAC	AL PRESSURE	PATIOS . FO	EBODY INLET				···	·		
AVD WORD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX .					
107	14.269	0.99567	0.55052	0.92999	0.39800		•			
112	14.264	0.99533	0.55033	0.92966	0.43100					
122	14.264	C. 99533	0.55033	0.02966	0.44900					
127	14.269	0.97567	0.55052	Q-92999 _	3-48600					
137	14.249	0.99428	0.54975	0.92669	0.52200					
147	14.204	0.99114	0.54801	0.92576	0.58800	w 10		<del></del>		,•
=1=>	1414		9.59187	03227	-1.0000					
-1 -1	14.304	7 <del>. 94 448</del>	0. 5520A	9.93299	<del>-1.0000</del>					•
	AL PRESSURE	RATIOS FAI	HOZZER FLAR							
AVD WERD	PI	PLTPC	PL/PTF	PL /PTP	X/DMAX			a various above the contract and an accordance and an accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance and accordance accordance and accordance and accordance and accordance and a		
-152	14.304		0.55127	0.93227	-1.0000					
-157	- 14.379	0.99846	<b>1.</b> *5706	0.63250	-1:00C0		en en marken aparte i i i make i a a mili			
>ADDITION	AL.PRESSURE	PATIOS . 20	DEG_SHPOUD_I	DEATION						
AVD HORD	ՐԼ	P( /P1	PL/PTF	PI /PTP	X/DMAX					
1/7	14.304	0.99811	0.55187	0.93227	0. 79300					
177	14.309	0.99846	0.55206	0.03259	0.64400					_
>APD TEOP	AL PRESSURE	PATIOS80	neg sherunjit	DÇATÎDN						<b>_</b> _,
AVD WOPD	PI	<b>የ</b> ኒ/የበ	PI / PTF	Pt /PTP	X/DMAX					
107	13.615	0.95004	0.52528	0.88736	2. 79300					-
187	13.520	0.94342	0.52162	0.88118	0.84400					
SOPTION 5		THRUST PAPAR					•		-	C.
		795.94	STOMA LE 2.7		MF-0.13212		CFM 1.1137757			

ACA-1 FW19	S 98FE <b>14</b> 1	NEPY TATE	06/13/79	CADDELL	PFC 10/24/79 20:37:33.57	ን	PG4 F734	FM233
ATTION	ef batcellat	PATINS . PPI	MAPY PING					
U 4090	Pţ	Pt /PO	PL / PTF	PI /PTP	X/DMAX		·	<del></del>
2	14.920	1.0342	0.49010	0.82372	0.72200			
7	15.499	1.0916	0.51256	0.86146	0~82000			
7	15-643	1.0917	0.51735	0.86951	0.91900			
7	15.629	1.0907	0.51695	C.P6867	1.0170			
ANTITION	M BESÖME	PATTOE . FIC	W SPETTTEP T	.n.	manus de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya del la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya			
0 4090	Pţ	PI / PO	PI / PTF	PL /PTP	X/DMAK			
2	15.239	1.0635	0.50397	0.84703	<b>3.</b> 42200			
7	14.934	1.0477	7.49390	0-93010	3.£7000			
AUDIT TON	AL PRESSURE	PATIOS . FLE	W SPLITTER O	.n.				
ก พกคก	Pŧ	PI /PN	Pt / PTF	PT /PTP	X/DMAX			. At an .
7	12.398	0.86522	9.41901	0.68911	0.50800	,		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
?	16.712	1.1663	0.55268	0.92889	0.58300			
2	14.295	Q. 99694	0. 4724?	0-19402	0.67000			
PSTITION	rf backine	******* * FJF	ETOP SHPOHA					
በ ቀቦም ፲	Pl	የኒ/የባ	PL/PTF	PLIPTO	K/DHAX			
97	14.250	- 8-99450	0.47128	0.7920R	-1.0000			
12	14-250	2. 99450	0:5712°_	D_ 79208	-1-0000			
2.3	14.255	7.99465	0.47144	0.79236	-1.0000			
? 7	14.270	<b>一一7、79590</b>	0.47194	0.70310	-1.0000			
3,7	_14.755	0.99416	0.47111	0.79189	-1.0000			
43	14.205	0.99137	0.46979	9,78958	-1-0000			
VUJET TŪNA	L PRESSIPE	PATENS . FOR	ERPRY_INLET					
u AUBU	Pt	PLVPII	Pt / PTF	PL/PTP	X/DMAX	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	At an address of the second second	· ·
77	14.250	0.99450	0.4712A	0.79208	0.39800	•		
12	14.250	0.99450	0.47128	0.79208	0.43100			
??	14.255	0.99485	0.47144	0.79236	0.44900			-
7	14.270	2. 99590	0.47124	Q. 79319 _	9,48600			
37	14.245	9.99415	9.47111	0.75180	0.52200			
<b>17</b>	1205	0. 99137	C.46979	0.78958	0.58800			
	14.300	0, 49 704	<del></del>		-1.0070			
	14.275	<del></del>		0.79913	<del>-1.0000 -</del>			
		avitor A LAN						
n mubu	P1	DE TOTAL	PILPIF		X/DMAX			
= ,	14.300 14.399	0.9 <del>0797</del> 2.99934	0.47300	0.79513	-1.0000 -1.0000			
		PATINS .1. 20		_				
	Pt	P[/pri	Pt / PT F	PL /PTP	X/DMAX			
n ucen	14.300	). 99799	0.47293	0.79485	0.79300			
	19.300	J. 99 144	0.47275	0.79541				
. 7			11 + 7 1220	J. 1979I	U. 84499			
, 7 77	14.319		DEC 51100115 1	554776W				
f 7 77	14.319	PATTOS : 90	DEG SHPPIIN L	UCTALON				
ጋ ሕርቆሀ	14.319 N PPESSIPE PL	PATTOS ± 90	PI / PT F	PE /PTP	X/DM&X			
67 77 70 WORD 1 WORD	14.319 41 PPESSIPE PL 13.401	PATTOS 2 80 Pt / PO De 97526	94 / PTF 9.44320		X/DM&X 0.79300			
67 72 የባባ <b>፤ፕ [ቦላል</b> ገ ພቦዋበ የግ	14.319 SI PPESSIPE PL 13.401 13.307	PATTOS ± 90	91 / PTF 0=44720 0=44007	PI /PTP				

A L'OUT I D'AR									
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12	14.232	7. 49494	0-39547	0.66212	0.52200				***************************************
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172	14.246	0.99878	0.39700	3.66467	0.74300			•	
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	P1	PI / PO	Pt /PTF	PL /PTP	X/DMAX	
IN WORN	16.010	1.1207	0.35914	0.60982	0.72200	
2		1.7367	0.42819	0.77708	0.82000	
7	19.089		0.43670	0.74153	0.91900	, and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second
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.?	19.094	1.3366	n. 42931	11. 12121	1.0179	
ATTIONAL	PRESSIPE	PATINS . FIR	W SPITTTER 1	.D.		<u>.</u>
กษายา	Pl	PL / PO	PL / PTF	Pt /PTP	X/NMAX	
2	18-629	1.3934	0.41767	0.70922	G.42200	<u> </u>
7	16.749	1.1774	0.37570	0.63795	0.67909	
APPLITIONAL	PRESSUPE	PATINS . FEN	W SPLITTER O	, n,		
ก พกคก	PL	PL / P/3	PL / PTF	PL /PTP	K/DMAX	
		0.73014	0.23397	0.39729	0.50800	the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the co
17 12	10.431	1.0428	0.37417	0.56744	0.58300	
2	14.898		0.31962	D.54273	0.67000	
		PATINS - EJE				
	_			PL/BTP	X/DMAX	
/ቦ <b>ሣ</b> በ₽ባ	PL	PL/P1	PL/PTF			
27	14.184	9-86588	0.31817	0.54925	-1.0000	
.12	14-164	1.99145	11 <i>112</i>	0.53949_	-1-0000	
22	14.174	J_ 2021 4	0. 31 306	0.53987	-1-0000	
27	14-326	0.99567	0.31906	0.56178	-1.0000	
37	-15. ?39	0.99672	0.31940	0.4229-		
سنجا	14.709	0.99463	0.31973	0.54121	-1.0000	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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137	14.194	0.99288	7.31917	0.54025	0.39800	
112	14.164	J. 9914A	0.3177?	0.53949	0.43100	
122	14.174	0.99219	0.21794	0.53947	0.44900	
127	14.224	0.99567	0.31906	0.54178	J. 4860Q	
	14.239	0.93672	0.31940	0.54235	0.52200	
137			0.31 873	0.54121	0.58800	
4 ²	14.209	0.99463	0.314.2	- 0.94°RT	-1.0000	
	14,270	<del> 0, 49952</del>	<del></del>		<del></del>	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
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157 157	14.279	0. 99952	0-37029	7.74547	-1.0000	. The second second second second second second second second second second second second second second second
		PATENS 2 20	DEC CHOURD I	I DE AT INN		
			Pt /PTF	PI /PTP	X/DMAX	
ላሁ ማጣቀብ	Pt	P( /P')	0.32019	0.54368	0.79300	
167	14.274	0.99917		0.5436P	0.44400	
177	14.274	0. 90917	0.32019		U-744UJ	
>479171044	f section	OF t PRITAG	DEC SHELID I	LOCATION		
	Pi	PL /PO	PL /PTF	PI /PTP	X/DMAX	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
Au mus D	13.771	0.9?546	0.29456	0.50357	0.79300	
107		0-92371	<b>9.2960</b> 0	0.50262	J.84400	
yn wnen 187 187 Northe S	13.176	0.92371 THPUTT PAPA	7.29600 METERS	0.50262	₩4400 1PF 7.60297 - 85M 0.0	346 ag7

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SENDITION	AL PRESSIPE	PATIOS . PRI	IMTOA BLUC						
tyn anen	PI	P4 / PG	PI / PT F	PI /PTP	X/DMAX				
32	14.993	1.0473	0.27995	0.64201	0.72200				
17	17.477	1.2177	7.4417A	7.74649	J. • 2000				
47	17.937	1.2459	0.45702	0.76389	0.91933				
5.7	17.448	1.2341	0.4477?	n.75654	1.0170				
>&701 T [ 104	AL PPFSSIPF	PATIOS , FLO	W SPLITTER	1.0.					
AVP HOPP	PL	PL / PN	PL/PTF	PI /PTP	X AMOL X				
62	16.600	1-1595	0.42066	0.71081	3-42200				
67	14.828	1.0358	0.77577	0.63496	0.67000				
POST TOOM	AL PRESSIPE	PATINS . FLE	W SPLITTER	າ. ຄ.					
ያለሁ ለሀይቢ	PĮ	Pt /PO	PI /PYF	PI, /PTP	X/DMAY				
77	9.0732	0.63376	0.22993	0.38852	0.50000				
97	19-174	1.3393	0.48591	0.82106	0.58300				
. 92	14.260	0.99603	0 <u>-</u> 36136 _	0.61060	0.67009				
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AVP MORD	PI	PL / PG	PL/PTF	PL LEJP	X/DMAX				
-107	14.195	99150	0.35971 -		-1.0000				
112	15-190	1.99115	0.35959	0-607£1	-1-0000				
-177	14.210	0.99244	0.36309	0.60846	-1.0000				
-127	14.242_	j. 9949B	0.36097	0.60996	-1.0000				
-117 -142	14.245	9.9949 <i>9</i> 9.99324	0.3609# 0.36034	0.60889	-1.0000 1.0000				
>ADDIT 10M	AL PRESSURE	RATIOS . FOR	ERODY INLET						
DEUM GAV	PL	PL/PO	PL/PTF	PL/PTP	Y/DMAX				
107	14.195	0.99153	0.35971	0.60782	3.39800		•		
112	14.190	0.99115	0.35959	0.60761	0.43100				
177	14.210	0. 99254	0. 36009	0.60846	0.44900				
127	14.245	3.99495	D-36098	O_E0996	2-48600		· · · · · · · · · · · · · · · · · · ·		
127 142	14.745	9,99498	0.36098	0.60996	0.52200				
- <del>192</del>	14.220	0.99324 	0.36024	0.609#9 	0.59800 -1.9000				
157	14.294	0. *****	9.36199	0.01107	-1.0000-				
-> <del>************************************</del>	AL PRESSURE	P#7193_E FAR	* ****						
AVD 4DPD	Pŧ	PL / PI7	PLCPTF	PL /PTP	x/DMAX				
-157	14.284	m. 99777	0.36199	9+61167	-1.0000				
-157	14.784	0.99777	0.36199	0.61167	-1.0000-		, united	العداد براجاليا السد	
יחן דורמיי<	AL PRESSUPE	PATINS 20	DEG SHROUD I	OCATION.					
440 406U	Pt	PI /PN	PL /PTF	Pt /PTP	X/DMAX				
167	14.279	9.99742	0.36186	0.61145	0.79300				
177	14.279	0.99742	0.36186	0.61145	0.84400				and the second second second
>40111104	AL PPESSUPE	RATINS . 40	DEC SHEDUD I	nçatin <u></u>					
TAU AUSE	PL	PL/PN	PI /PTF	PI /PTP	X/DMAX				
142	13.236	0.92457		0.56679	0-79300				
[ P 7	13.221	0.92352		0.56615	0.84403				
		THOUST PARAM							

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SHUP WAL	=	Ud / 1d	M /PTF	Pt /P1P	X/Deax			
Zt.	18.257	1.2770	0.35352	0.60103	0.72200			
	\$41.07 \$4.00	1604.1		0.16347	000100			
. 2	21-126	1.4778	0.40910	1700.00	1.0170			
ANDITIONAL	tal prescipe	BATINS . FLOW	soy (TTFP )	<u>.</u>				
	i				1			
101	22-160	י קיבער	0.624.0	0.72952	0-4-200			
14	£ 2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1.4362	0.3975	0.67595	0.67000			
SANDIT INNAL	IAI PRESSUPE	PATINS . FIFT	J ddill las r	e.		der von der der der der der der der der der der		
2000	ā	20/ 20	Ot /PTE	91 / 919	Y/DMAX		•	į.
7.7	12.132	0.84.661	0.23492	0.39940	0.50800			
92	17,294	1. 21 00 0. 99 73 7	0.47£07 0.27£11	0.5694R 0.46941	0.6 TUO			
Mul 1 iuas	-346-5-340-14	** 1405 * FJECEON	CHBOND CHBOND					
AVD WOPD	14	PL / PO	Pl /PTF	PL/PTP	X / DMAX	!	1	
-107	14.204	0.99353	0.27504	0.46760	-1.0303			
-112	14.199	0.99318	0.27495	0.46711	-1,0000			
-127	14.714	0.99423	0.27524	0.46703	0000*1			
	14.184	£1200°0	7.27466	J. 67F96	-1.0000			
-155	14.159	60160.0	0.27437	0.46645	-1-0000	Service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the service of the servic		***
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AVP WOPT	PL	PL/PC	PL/PTF	PL/PTP	x/DMAx			
101	14.704	0.99353	0.27504	0.44760	0.39803	•		
112	001-71	0.09318	0.27495	0.46744	9,43100			
127	14.214	0.99423	0.27524	0.46793	0-4-4-00			
137	16.194	0.99213	0.27466	9.46694	0.52203			
3 (	14-149	0.99109	9-27637	0.44645	0.5 4600		!	
-1-	14.2.41	4 4000	9.2760	0.47033				
		****	***************************************			1		:
Uaur un		6	. ⋤	91 / 19	Y / DMAY			
	14.249	1.9994.7	0.27769	0.47040	-1,0000	1		•
-143	14.2 %	21005.0	0.27459	0.47077	-1-0000		. 1	i
SAUDIT IONEL	ALI PPECCUPE	PATINS 1 20 C	i Lufiu aris 530	ncation	And the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			
AVD STPD	id	E .	P) / PTF	914/14	x Clastra			
	14.284	0.30912	2.27659	0.47023	0. 79300			•
17.	14.284	21.66.6	0.27459	62645-0	0.84400	!		
I Anni Tinna c	dinstitut iv	PATINS , AN DEG	SHERIN	LUCATION				
daum uA7	14	Pt / Pn	310/1d	91 / 919	x / PMAK	•		:
(4)	13.209	0.93033	0.75755	0.43796	2, 79300			
101		1) C2784	10.75697	0.43671	0.84400			
10000								

	C 08FL 14	ENARY DATA	06/17/70	CADDETT	RFC 10/24/79 20:44:48.177	Pun 23 . FAC RYSKI PGM CO34 PDG 1414
>4ንካተ፣ የጥ	N PRESSURF	PATITS . PRI	MARY PILIG			
<b>งว พกตก</b>	Pl	PL / PO	PI /PTF	PI /PTP	x/DMAX	
32	18.721	1.3106	0.31333	0.53159	0.72200	
77	23.388	1.4372	0.39147	0.66438	9. 42 999	
67	24.611	1.7228	0-41189	0.69880	J. 91900	
 57	24. 361	1- 7054	0.43771	0.69171	1.0170	
ATOITION	AL PRESSURE	PATINS , FLE	W SPLITTER I	. n.		
ID WORD	Pt	Pt /PO	PI /PTF	P1 /PTP	x/DMAX	
52	24.331	1.7033	0.40721	0-69086	0.42200	
57	20.623	1.4437	0.34515	0.58557	0.67000	
APPITION	LL PRESSUPE	PATINS , FLO	W SPLITTEP O	 1. N.		
0 4000	Pt	Pt / Pr)	PL/PTF	PL /PTP	y/DMAX	والمراجع والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد والمستحد وال
/N 4080	13.995			0.39737		
17 17	20.059	0.97 <del>968</del> 1.4042	9.23422 9.33571	0.56956	0.50800 0.58300	e commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of
2	14.249	0.99750	D. 23848	0.55956	0.58300 0.6 7000	
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07	14.139	0.98981		0.4014P	-1.0000	
12	16_116	0. 98606	0-23622		-1-0000	
22	14.119	7.98841	0.23631	0.40051	-1.0000	
27	14.189	-9.99331	0.23747	0.40249	-1.0000	e e l'article de la complete de la magnificación de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la production de la pr
37	14.204	0.99435 0.99540	0.23773	0.45332	-1.0000	
42	-14.219	リップサラサリ	0.23798	0.40374	1.0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
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ADDIT 10N		RATIOS FOR	ERODY .INLET .			
		RATIOS FOR	REBODY JULEY .	PL /PTP	X/DMAX	
NOT TICCY	L. PRESSURE			Pt /PTP 0.40148	X/DMAX 0.39800	
ADDITIONA VD WORD	AL PRESSURE	PL/PO	PL/PTF 0.23664		0.39800	
MOLTICCA	PL 14.139	PL/PG 0.98981	PL/PTF	0.40148		
ADDIT 10N/ /D WOPD   0.7   112	PRESSURE Pt 14.139 14.114	PL/PO 0.98981 0.98806	PL/PTF 0.23664 0.23622	0.40148 0.40077 0.40091	0.39800 0.43100	•
ADDIT 10N/ /D WOPD 107 112	PL 14.139 14.114 14.119	PL/PO 0.98981 0.98806 0.98841	PL/PTF 0-23664 0-23622 0-23631	0.40148 0.40077	0.39800 0.43100 0.44909	
ADDIT ION/ /D WOPD 107 112 127 127	PL 14-139 14-114 14-119 14-159	PL/PO O.98981 O.98806 O.98841 O.99331	PL/PTF 0.23664 9.23622 0.23631 9.23748	0.40148 0.40077 0.40091 0.40299	0.39800 0.43100 0.44909 0.48600 0.52200	
ADDIT IONA 7D WOPD 12 12 27 27 142	PL 14-139 14-114 14-119 14-159 14-204	PL/PO 0.98981 0.98806 0.98841 0.99415 0.99415	PL/PTF 0.23664 9.23622 0.23631 0.23748 0.23773	0.40148 0.40077 0.40091 0.40299 0.40332 0.40374	0.39800 0.43100 0.44909 0.48600	
ADDITIONA TO WORD 07 12 27 27 27 42 53	PL 139 14.119 14.119 14.129 14.219	PL/PG 0.98981 0.98806 0.98841 0.99435 0.99475	PL/PTF 0-23664 9-23622 0-23631 0-23748 0-23777 0-23798	0.40148 0.40077 0.40091 0.40299 0.40332 0.40374	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800	
ADDITION/ O WOPD O7 12 27 27 27 42	PL 139 14-114 14-119 14-189 14-214 14-279 14-279	PL/PG 0.98981 0.98806 0.98841 0.99435 0.99475	PL/PTF 0-23664 9-23622 0-23631 9-23748 0-23777 0-2,798 9-23898	0.40148 0.40077 0.40091 0.40289 0.40332 0.40374	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800	
ADDIT ION/ /D. WIPPD 107 112 127 127 147 147	PL 139 14-114 14-119 14-189 14-214 14-279 14-279	PL/PO 0.98981 0.98806 0.98841 0.99331 0.99475 0.99540 	PL/PTF 0-23664 9-23622 0-23631 9-23748 0-23777 0-2,798 9-23898	0.40148 0.40077 0.40091 0.40289 0.40332 0.40374	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800	
ADDITION  (D. WIPD  107  112  127  127  147  147  149  159  100  100  100  100  100  100  10	PL 14-139 14-114 14-119 14-294 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279	PL/PO 0.98981 0.9886 0.98841 0.99425 0.99425 0.99540 0.9955 PATIOS FAN	PL/PTF 0.23664 0.23622 0.23631 0.23768 0.27777 0.2.798 0.27798 0.27798 0.27798 PL/PTF 0.73898	0.40148 0.40077 0.40091 0.40289 0.40332 0.40374 - 0.40545 0.40545	0.39800 0.43100 0.44909 0.48600 0.52200 0.58800 -1:9090	
ADDIT ION/ //D. WIPPD // 12 // 12 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 // 27 //	PL 139 14-114 14-119 14-159 14-274 14-219 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14	PL/PO 0.98981 0.98806 0.98841 9.99331 0.99475 0.99540 0.99599 PATIOS FAN	PL/PTF 0.23664 9.23622 0.23631 9.23748 0.23777 0.2,798	0.40148 0.40077 0.40091 0.40289 0.40332 0.40374 - 0.40545 0.40545	0.39800 0.43100 0.44907 0.48600 0.52200 0.58000 -1:9090	
ADDITION/ /D WIPD   12   12   12   12   12   12   12   1	PL 139 14.139 14.119 14.139 14.204 14.219 14.279 14.279 14.279 14.279 14.279	PL/PO 0.98981 0.9886 0.98841 0.99425 0.99425 0.99540 0.9955 PATIOS FAN	PL/PTF 0.23664 9.23622 0.23631 9.23748 0.23777 0.2.798 9.23698	0.40148 0.40077 0.40071 0.40299 0.40332 0.40374 -0.40545 0.40545	0.39800 0.43100 0.44909 0.48600 0.52200 0.58800 -1:9090	
ADDITION  (D. HOPD  O7  12  27  27  42  42  42  44  49  ADDITION  (D. HOPD  52  57	PL 139 14.139 14.119 14.139 14.204 14.219 14.279 14.279 14.279 14.279 14.279	PL/PO 0.98981 0.98806 9.98841 9.99331 0.99475 0.99476	PL/PTF 0.23664 9.23622 0.23631 9.23748 0.23777 0.2.798 9.23698	0.40148 0.40077 0.40071 0.40299 0.40332 0.40374 -0.40545 0.40545	0.39800 0.43100 0.44909 0.48600 0.52200 0.58800 -1:9090	
ADOLT IONA (D. WOPD) (7) (12) (7) (12) (7) (27) (27) (27) (27) (27) (27) (27	PL 14-139 14-114 14-119 14-219 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279	PL/PO 0.98981 0.98861 0.99831 0.99435 0.99435 0.99560 0.99560 PATIOS FAN	PL/PTF 0.23664 9.23622 0.23631 9.23748 0.23777 0.2.779 9.23898	0.40148 0.40077 0.40091 0.40289 0.40332 0.40374 - 0.40545 0.40545 0.40545	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 -1:9090 1:0090	
ADDITION/ /D WIPD   12   12   12   12   12   12   12   1	PL 14-139 14-119 14-119 14-294 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279	PL/PO 0.98981 0.98806 9.98841 9.99331 0.99475 0.99476	PL/PTF 0.23664 0.23622 0.23631 0.23748 0.23779 0.2.798 0.23798 0.23898 0.23898 DEG SHPOUN 1	0.40148 0.40077 0.40091 0.40289 0.40332 0.40374 -0.40345 0.40545 0.40545 0.40545	0.39800 0.43100 0.44909 0.48600 0.52200 0.58800 -1:9000 -1:0090	
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ADDIT ION/ /D WOPD /O7 12 // 12 // 12 // 12 // 13 // 14 // 14 // WOPD // WOPD // WOPD // WOPD // WOPD // 17 // WOPD // 17 // WOPD	PL 139 14-114 14-119 14-199 14-274 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279	PL/PO 0.98981 0.98806 0.98861 0.99415 0.99415 0.99459 PATIOS FAN PL/PO 0.99959 RATIOS 20 PL/PO 0.99959 0.99959 0.99959	PL/PTF 0.23664 9.23622 0.23631 9.23768 0.27777 0.2.798 9.23898 PL/PTF 0.23898 DEG SHPNUN 1 M/PTF 0.23898 DEG SHPNUN 1	0.40148 0.40077 0.40091 0.40259 0.40332 0.40774 	0.39800 0.43100 0.44907 0.48600 0.52200 0.58600 -1:9090 -1:0090 X/DMAY -1.0000 -1:0000 -1:0000 0.79300 0.84400	
ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL	PL 14-139 14-114 14-119 14-189 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279	PL/PO 0.98981 0.9886 0.9841 0.99435 0.99455 0.9956 0.9956 PATIOS FAN PL/PO 0.99959 RATIOS 20 PL/PO 0.99959 PATIOS 40 PL/PO	PL/PTF 0.23464 9.23422 0.23631 9.23748 0.27777 0.2.7798 9.23898 PL/PTF 0.23898 DEG SHPOUN 1 PL/PTF 0.23898 DEG SHPOUN 1	0.40148 0.40077 0.40091 D.40289 0.40332 0.40374 - 9:49545 0:49545 PL/PTP 0.40545 0.60945 DCATION PL/PTP 0.40545	0.39800 0.43100 0.44900 0.48600 0.52200 0.58600 -1:9090 -1:9090 X/DMAY -1.0000 -1:0000 -1:0000 -1:0000 X/DMAX 0.79300 0.84400	
ADDIT IONA (D. WINDD) (1) (1) (1) (2) (2) (2) (3) (4) (4) (4) (5) (6) (7) (8) (8) (8) (8) (8) (8) (8) (8) (8) (8	PL 14-139 14-119 14-119 14-294 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279	PL/PO 0.98981 0.98861 0.98861 0.99475 0.99475 0.99560 0.9959 PATIOS 2 PATIOS 3 80 PL/PO 0.99959 0.99959 0.99959 0.99959	PL/PTF 0.23664 9.23622 0.23631 9.23748 0.2777 0.2.779 9.23790	0.40148 0.40077 0.40091 0.40289 0.40332 0.40374 	0.39800 0.43100 0.44900 0.48600 0.52200 0.58600 -1:9090 -1:9090 X/DMAY -1.0000 -1.0000 -1.0000 X/DMAX 0.79300 0.84400	
ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL ADDITIONAL	PL 14-139 14-119 14-139 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279 14-279	PL/PO 0.98981 0.9886 0.9841 0.99435 0.99455 0.9956 0.9956 PATIOS FAN PL/PO 0.99959 RATIOS 20 PL/PO 0.99959 PATIOS 40 PL/PO	PL/PTF 0.23664 9.23622 0.23631 9.23748 0.23779 0.2.798 9.23898 1-M0221E-F1AP PL/PTF 0.23898 0.23898 0.23898 0.23898 0.23898 0.23898 0.23898	0.40148 0.40077 0.40091 D.40289 0.40332 0.40374 - 9:49545 0:49545 PL/PTP 0.40545 0.60945 DCATION PL/PTP 0.40545	0.39800 0.43100 0.44900 0.48600 0.52200 0.58600 -1:9090 -1:9090 X/DMAY -1.0000 -1:0000 -1:0000 -1:0000 X/DMAX 0.79300 0.84400	

MASA-LEWIS	081144	MEPY DATA	06/13/79	CANDETE	REC 10/24/79 20:45:46.516	ENC MARKE	PGM C034	FUN 23
>annitinma	I OPFSSIRE	PATIOS . PPI	ANDA BLUC					
VD WC#D	Pţ	PL/PO	PL /PTF	PI /PTP	X/DMAX			
37	18.714	1.3099	0.31256	0.53121	0.72200			
27	23.472	1.6394	0.29120	0.664 #7	0.72000			
47	24.666	1.7265	0.41197	0.70016	0.91900			
£ 7	74.411	1.7086	0.40771	3.49297	1.0170			
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122	14.135	7.98926	0-23608	0.40124	-1.0000			
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122	14.135	0.98936	0.2360	0.40124	0.44930			
127	14.195	9.99356	0.2370*	0.40294	0.46602			
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97	13.221	0.02434	0.27791	0.50595	<b>).</b> 79300				
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57	17.675	1.235#	0-44703	7.75617	1.0170	
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47	18.743	1.310*	0-47405	0.80148	3.54303	
92	.14.274	0-99404	0-36103	0_62069	0.67000	
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177	14.215	0.99385	0.35951		-1.0000	
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137	15.744	0.99595	0.36027	0.609=1-	-1.0000	
167	14.225	0_99455	0.35976	0.69856	-1:0600	to a complete and a substitution and the control of the proper control of the administration of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of
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197	14.715	0.99385	0.35951	0.60#13	0.39800	•
112	14. ? 35	9- 99316	3- 35926	0.60770	0.43100	
122	14.720	0.09420	0.35964	0.63634	9-44993	
127	1449	D. 99630	0.26040	0.60963	0.48600	
137	14.744	9. 99595	0. 36927	0.50941	0.52700	
142	14.225	9.99455	0.35576	0.69856	0.58800	I proposed the Miller too. More than the second of the contract products of products of the second
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157	14.299	3, 99903	2.36141	0:41123	-1.0000	المعاومين المعاوم والمعارض المعارض
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167	14.289	1. 99939	0.36141	0.61173	0.79300	g garage of the contract of the garage of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the
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37	14.763	1.0334	0.41430	0.69976	0.72233		
77	14.462	1.1492	0.46174	0.77991	g. #2000		
47	16.301	1.1729	0.47126	0.79500	0.91900		
42	16.737	1.1694	0. 46944	0.79261	1.0170		
>ATTITIONA	PRESSUPE	PATTOS . FLO	W SPETTER I	•n•	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	- AMERICAN PROGRAMMENT - SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECURITARIA SECUR	rdf-r-uddish et-udsishidadhudishin et-et-eu-bukutu-dashusu-dashusu-dashusu-dashusu-sanya-sanya-sanya-sanya-
AVP WORD	Pŧ	PL / PO	PL /PTF	PL /PTP	Y/DMAX		
£ 2	15.524	1.0937	9.43542	0.73545	J.42200		
* 7	14. 786	0. 99 72 7	0.49969	0.4449	0.67000		•
SATOLY LONG	L PRESSUPE	PATINS . FEE	W SPLITTER O	• n•	W 1 1 W 22 1 2 W 23 24 W	, we approve view in the second to the second appropriate property of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	
AVO MORO	PL	PL/PO	Pt /PTF	PL /PTP	X/DMAX		
77	6.3633	0.56290	0.22617	0.38201	0.5000		. Nome to be a second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the
<b>#</b> ?	29. 935	1-4574	0. 49754	0.08564	0.58309		•
92	14.271	0.79622	D. 50027	9-67609	2-61993		
Seast Lines.	<del></del>	******* * ***	CTO- 344FUR			e de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la compan	
SAD MUSED	P!	PL / PO	PL/PTF	PLANGE	X/DMAX		و د د د میده هدید ره ایم داشد . این می
-107	14.221	9-99274	0. 39AA7	0.67372	-1.0000		
-112	14,216	9.99233	C. 35973	0-67365	-1.0000		
-122	14.211	0.44704	3.90859	0.67325	-1.0000		
-12"	15-241	3, 99413	0. 20043	0.67467	-1.0000		
-137	14.746	0.9744#	0.30057	0.67899	-1.G090		the strong of the strong magnetic control of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of the strong of
-147	14.221	1). 99274	0.39887	0.67372	-1-0000		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
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TAU HUBD	Pŧ	P[ /PO	PI /PTF	P( /PTP	X/IMAX		
107	14.221	0.99274	0.39687	0.67372	J. 3 9 0 0 3	•	
112	14.216	0.99239	0.30873	0.67348	0.43100	no species of	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
127	14.711	7. 99204	O" Sawed	0.47325	0.44900		
127	14.241	7,09413	9.39943		0.42600		
127	14.246	7.994-8	9.39957	0.67400	0.52203		
147	14.721	3. 99274	0.29697	0.67372	0.5MR00		•
-462			<del></del>		-1.2022		
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AVP WORD	Pl	Pron	PL/PTF	01 /PTP	#/DMAX		
-167	14.796	9.99727	3.47769	0.67£79	-1.0000		
-157	14.286	1.99727	9.40949	0.87674	-1.3000		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
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AVD WOPD	Pŧ	Pt /PD	PI / PTF	21 / PTP	X/D4AX		
167	14.291	7,99767	9.49983	0.67703	J. 79300		
172	14.291	0.09762	0.40083	*******	0-64400		
Sampt Innat	PRESSURE	RATINS + *0	DEG SHADIM 1	OCATION	g - Commission - gar conta qua variante que contra en en contra compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña de la compaña		
AVD WORD	ol	91 / PO	PI /PTF	רן /פוף	<b>ХДРИДХ</b>		
107	13.777	0.92498	0.37129	0.62717	0.79300		
Įpi	13.292	0.92164	0.37031	0.62547	J. 84400		_
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41-01 679.7		£38.33					

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		66. 51	1.0333	0.49340	0.82766	0-72200			
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15-203	> ADD IT IN		PATINS .	Ş	ċ				
		ā	8	7107 10	0.070	7			
		15,203	1,0615	0.503.80	0.85027	0-62200			
### UPPD PRINCE   1.1677   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4151   0.4	14	14.919	1.0410	0.49404	Q#FFA.0	3.67000			
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S . TERSIDED THOUST DADANTIEDS				0.44012	0.74279	3. 64409			

	VASA-I FWI	l2 bb£f[w	THARY DATA	06/13/79	CABRETT	REC 10/24/	79 :20:56:42.013	FAC 9YAX1	PGM C034	RUN23
	>47711100	IAL PRESSURE	RATIOS . PRI	IMAPY PLUG						• · · · · · · · · · · · · · · · · · · ·
	AND HUBD	PŁ	PI /PO	PL /PTF	PI /PTP	X/DHAX		<del></del>		
	32	14.451	1.0299	0.55884	0.95270	0. 72200				
	37	14.610	1. 2211	0.56502	0.96323	J.#2009				•
	47	14-640	1.0232	0. 56618	0.96521	0.91900				
_	52	14.655	1.0242	0.56675	0.96620	1.0170				
() ~	>AUT TEODAC	IAL PPESSURE	RATIOS , FLO	W SPLITTER	, n.					-
_	AVD HOPD	PL	PL /PO	PL/PTF	PL /PTP	X/DMAX				to the same that is a company
(	62	14.491	. 1.0127	0. 56038	0.95534	0.42200				
^	57	14.436	1.0089	0.55926	0.95172	0.67006				
1, -	>AODIT MA	IAL PRESSIME	PATIOS . FLO	W SPLITTER I	·. n.					
	AVP HORD	PL	PJ / PO	PL/PTF	PL /PTP	X/DMAX				
	77	12.539	0.87630	0. 454 90	0.92665	0.50800				
	87	15.948	1.1146	9.61675	1.0514	U. 58300				
-	92	14.286	0.99840	0.55247	0.94184	0.67000			· · · · · · · · · · · · · · · · · · ·	
		<del>IAL PRESSURE</del>	******* <u>* Ed</u>	CTOP SHPPUS						
N -	AVD HOPD	PL	PL/PO	PL/PTF	PLZPTP T	X/DMAX				
28	-197	14.201	0.99666	7.55151	0.94029	-1.0000				
_	-112	14-256	0-99631	0.55131	0.93987	-1.0000				
_	-122	14.256	0.99631	0.55131	0.93987	-1.0000				
J	-127	14.266	0.99701	0.44170	0.94053	-1,0000				
	-137	14.241	0. 99526	0-55073	0.03888	-1.0000				
	»14?	14.191	0.99109	0.54842	0.43463	-1.0000				
_	>400 FT FCR	AL PRESSURE	SATINS . FM	ENDY IM ET						
	AVD WORD	, PL	PL/PO	PL/PTF	PL /PTP	X/DMAX		. ~	·	
	107	14.261	0. 99666	0.55151	0.94020	J.39800		•		
	117	14.256	0. 99631	0.55131	0.93987	0.43100			<del></del>	
	122	14.256	9.99631	0.55131	0.03087	0.44900				
-	127	14. 266	0.99701	<u> </u>	0-94053	3.48600				
	137 142	14.241	0.99526	0.55073	0.93688	0.52200				
	-152	14.181	0.9910# 	0.54842 0.55286	0.93493 	0.58800 				
	-1-1		<del></del>			1.0000	· •			
-	->+ 10.1 T 100	WE PRESSURE		-NO7725 FLAT	·		<b>.</b>			
	AVD WITED	PL	- PLAND	PL /PTF		X/DMAX				
	-152	14.296	0. 99910		0.94250	-1.0000				
	-157	15.294	0.99910	0. 552 PM	0.94250	-1.0000				
-	אחן דן פראל	ML PRESSUPE	RATIOS . 20	DEG SHROUD L	OCATION					
_	MANA GAV	PL	PL/PO	m /PTF	PL /PTP	x/DMAX				
	167	14.296	0.93910	0.55286	0.94250	0.79300			·	
	172	14.296	0.99910	0.55286	0.94250	0.84400				
		IAL PRESSUPE	PATINS 1 80	DEG_SHPMIN_I	OCATION					· · · · · · · · · · · · · · · · · · ·
-	AVN WOPN	PL	PL / PO	PL/PTF	PL /PTP	X /PMAX				
•	187	13.612	0.95131	0.52641	0-89742	0.79300				
	187	13.507	0.94398	0. *2736	0.89050	0.44400				
_			THRIST PAPAP		•			· — ——-		
	{F-7} 270.	.37 F1C	277.01	STOWA 1 C 2.5	1914 FT/	MF 0.42777	DCF 6.033799	CE4 0.0030854		

	NASA-I FWIS	PARELY	INAPY PATA	06/17/79	CADDELL	4+6 10/24/14	21:02:58.096	FAC RY6K1	PGP CQ34	RDG 1422
,	PANUL ALGUA	PRESSURE	RATIOS . PPI	MARY PLUG						
4	งก พกกก	PL	pj /pn	PL/PTF	PL /PTP	X/DYAX				
3	32	18.242	1.2765	0.35344	0.59940	0.72200				
	17	27.129	1.4086	0.39001	0.66141	0. #2000				
	47	21.762	1.4879	0-41196	0.69865	J. 91 900				
	52	21.127	1.4784	0.42935	6.69422	1.0170				The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
	··· · · · · · · · · · · · · · · · · ·									
,	PAPRITE T ECIC. A.C.	. PRF22178F	RATIOS . FIG	W SPLITTER I		= :		The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa		
	AU MUNU	PL	PL/PN	PL/PTF	PL /PTP	X/DMAX		•		
	62	22-161	1.5508	0.42938	0.72812	0.42200				
5	57	20.488	1.4337	D. 39697	0.67322	0.67000				
)	AD TITLEDA	PRESSURE	RATIOS . FLO							
AV	VD WORD	PL	PL/PD	PL /PTF	PL /PTP	X/DHAX			<del></del>	
7	77	12-160	0.85091	0.23560	0.39956	J.50800				
	92	17.323	1.2122	0. 33564	0.56921	0.58300				
9	92	14.247	0.99699	0.27605	0.46815	0.67000				
-	ADDIT HIME	PRESSURE	RATTOS E JE	CTOR SINCUO	to effect offer a real management of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the sec					
. AV	VD WORD	7	PL/PD	PL/PTF	PL ZEXP	X/DMAX				
	107	14-197	0.99350	9-27508-		-1.0000				
	112	14-177	0. 12.210	4.27469	0-46585	-1-0030				
	12?	14-187	0,99290	0.27489	0.46618	-1.0000				
	27	14.202	0.99384	0.27714	0.46667	-1.0000				
		-14.177	0.99210	0.27469	0-46585	-1.0000			· · · · · · · · · · · · · · · · · · ·	
۱- الد		14. 157	0. 99070 RATIOS . FOR	0-27431	0.46529	-1.0000				
۱- لز ۲ <u>۰</u>	ADDITIONAL ORD	PRESSURE	0. 99070 .RATIOS FOR PL/PD	0.27431 ERCOY_IMLET PL/PTF	Q.46529	-1-0000 X/DMAX				
ا- لا ۸۷	ADDITIONAL D WORD	PRESSURE PL 14.197	0. 99070 .RATIOS FCR PL/PO 0. 99350	0.27431 ERCOY INLET PL/PTF 0.27508	PL/PTP 0.4651	X/DMAX 3, 39800		•		
-1 -1 	ADDITIONAL VD WORD . 107	PRESSURE 14.197 14.177	0.99070 RATIOS - FOR PL/PO 0.99350 0.99310	0.27431	PL/PTP0.46515	-1.0000 X/DMAX 3.39800 0.43100				
-1 -2 -2 -4 1 1	ADDITIONAL D WDPD	PRESSURE PL	0.99070  RATIOS . FOR  PL/PO 0.99350 0.99210 0.99280	9.27431 FRODY_IMLET PL/PTF 0.27508 0.27569 0.27489	PL/PTP 0.4651 0.4651 0.46585 0.46618	-1.0000 X/DMAX 3.39800 0.43100 0.44%00		•		
-1 -1 -2 -2 -4 -1 -1	ADDITIONAL D WORD 107 112 127	PRESSURE PL 14-197 14-197 14-197 14-202	0.99070 RATIOS FOR PL/PO 0.99350 0.99210 0.99280 2.99384	9.27431 FRIDY IMLET PL/PTF 0.27509 0.27569 0.27469 0.27518	PL/PTP 0.4661 0.4658 0.46618 0.46618	-1.0000 X/DMAX 3.39800 0.43100 0.44900 0.48603		•		
-1 -1 	ADDITIONAL /D WORD	PRESSURE PL 14.197 14.197 14.197 14.197 14.197 14.197	0.99070 RATIOS . FOR PL/PO	9.27431 PL/PTF 9.27508 9.27569 0.27569 0.27518 9.27469	PL/PTP 0.4651 0.4658 0.46618 0.4667 0.46585	-1-0000 X/DMAX 3-39800 0-43100 0-44800 0-48603 0-52200		•		
-1 -2 	ADDITIONAL VD MORD . 107 112 127 127 142	PRESSURE PL 14.197 14.197 14.197 14.197 14.197 14.197 14.197	0.99070 RATIOS . FOR PL/PO 0.99350 0.99210 0.99280 2.99384 0.99210 0.99070	9.27431 PL/PTF 0.27508 0.27569 0.27469 0.27518 0.27469 0.27431	PL/PTP 0.46515 0.46618 0.46667 0.46515 0.46519	-1.0000 X/DMAX 3.39800 0.43100 0.44800 0.48600 0.52200 0.58800		•		
-1 -2 -2 -3 -4 -1 -1 -1 -1	ADDITIONAL /D WDPD 107 112 127 127 127	PRESSURE PL 14-197 14-177 14-197 14-202 14-177 14-157 14-277	0.99070 RATIOS . FOR PL/PO 0.99350 0.99210 0.99280 2.99384 0.99210 0.99070	9.27431 PL/PTF 0.27508 0.27508 0.27508 0.27489 0.27518 0.2769 0.27431 0.27469	PL/PTP 0.46651 0.46515 0.46618 0.46667 0.46519 0.46519 0.46519	-1.0000 X/DMAX 3.39800 0.43100 0.44%00 0.52200 0.58800 -1.7000		•		
-1 -2 -2 -3 -4 -1 -1 -1 -1	ADDITIONAL VD MORD . 107 112 127 127 142	PRESSURE PL 14.197 14.197 14.197 14.197 14.197 14.197 14.197	0.99070 RATIOS . FOR PL/PO 0.99350 0.99210 0.99280 2.99384 0.99210 0.99070	9.27431 PL/PTF 0.27508 0.27569 0.27469 0.27518 0.27469 0.27431	PL/PTP 0.46515 0.46618 0.46667 0.46515 0.46519	-1.0000 X/DMAX 3.39800 0.43100 0.44800 0.48600 0.52200 0.58800				
-1 -2 -2 -4 -1 -1 -1 -1	ADDITIONAL /D MDRD 197 112 127 127 137 142	PRESSURE PL 14-197 14-197 14-197 14-197 14-197 14-202 14-177 14-157 14-272	0.99070 RATIOS . FOR PL/PO 0.99350 0.99210 0.99280 2.99384 0.99210 0.99070	9.27431 PL/PTF 9.27508 9.27569 0.27569 0.27518 9.2769 0.27469 0.27431 9.2763	PL/PTP 0.4651 0.4658 0.46618 0.4667 0.46585 0.46519 0.46519	-1.0000 X/DMAX 3.39800 0.43100 0.44%00 0.52200 0.58800 -1.7000		•		
-1 -1 -2 -2 -1 -1 -1 -1 -1 -1	ADDITIONAL D MORD 197 112 127 127 147 147 147	PRESSURE PL 14-197 15-177 14-197 15-202 14-177 15-202 14-177 15-277 15-277 15-277	0.99070 RATIOS . FOR PL/PO	9.27431 PL/PTF 0.27508 0.27569 0.27569 0.27489 0.27518 0.27469 0.27469 0.27469 0.27469 0.27469	PL/PTP 0.4661 0.46505 0.46505 0.46505 0.46505 0.46505 0.46509	-1.0000 X/DMAX 3.39800 0.43100 0.48603 0.52200 0.58800 -1.9000		•		
-1 -1 -1 -1 -1 -1 -1 -1	PADDITIONAL /D MORD 107 112 127 127 142 142 143 143 144 147 147 147 147 147 147 147	PRESSURE PL 14-197 14-197 14-197 14-197 14-202 14-177 14-157 14-277 14-277	0.99070  RATIOS . FOR PL/PO	9.27431 PL/PTF 9.27508 9.27569 9.27549 9.27518 9.27469 9.27463 9.27463 9.27463 9.27463 9.27463	PL/PTP 0.46651 0.46651 0.46585 0.46618 0.46585 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519 0.46519	-1.0000 X/DMAX 3.39800 0.43100 0.44900 0.52200 0.58800 -1.9000 **/DMAY -1.0000		•		
-1 -1 -1 -1 -1 -1 -1 -1	ADDITIONAL D MORD 197 112 127 127 147 147 147	PRESSURE PL 14-197 15-177 14-197 15-202 14-177 15-202 14-177 15-277 15-277 15-277	0.99070 RATIOS . FOR PL/PO	9.27431 PL/PTF 0.27508 0.27569 0.27569 0.27489 0.27518 0.27469 0.27469 0.27469 0.27469 0.27469	PL/PTP 0.4661 0.46505 0.46505 0.46505 0.46505 0.46505 0.46509	-1.0000 X/DMAX 3.39800 0.43100 0.48603 0.52200 0.58800 -1.9000		•		
-1 -1 1 1 1 1 -1 -1 -1	PADDITIONAL (D WORD 107 112 127 127 147 147 147 147 147 147 147 14	PL 14-197 14-197 14-197 14-197 14-197 14-197 14-157 14-272 PRP33URP	0.99070  RATIOS . FOR PL/PO	9.27431  FRIDY IMLET  PL/PTF 0.2750R 0.2750R 0.2751R 0.2769 0.27431 0.2763 0.27631 0.27632 0.27633 0.27633	PL/PTP 0.46519 0.46518 0.46518 0.46519 0.46519 0.46519 0.46519 0.46913 0.46913 0.46913	-1.0000 X/DMAX 3.39800 0.43100 0.44900 0.52200 0.58800 -1.9000 **/DMAY -1.0000				
AV AV AV AV AV AV AV AV AV AV AV AV AV A	PADDITIONAL  (D MORD	PL 14-197 14-197 14-197 14-197 14-197 14-202 14-177 14-157 14-277 14-277 14-277 14-277 14-277	0.99070  RATIOS . FOR PL/PO	9.27431  FRODY IMLET  PL/PTF 0.27508 0.27508 0.27518 0.2769 0.27518 0.2769 0.2769 0.2769 0.27693 0.27693 0.27653 0.27653 0.27653	PL/PTP	-1.0000 X/DMAX 3.39800 0.43100 0.44%00 0.52200 0.52200 0.52200 -1.0000 -1.0000 -1.0000 -1.0000		•		
-1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -	PADDITIONAL (D WORD ) 107 112 127 127 142 142 142 152 167 167 160 167 160 160 160 160 160 160 160 160 160 160	PL 14-197 14-197 14-197 14-197 14-197 14-197 14-197 14-197 14-197 14-272 PRESSURE PL 14-277 14-277	0.99070 RATIOS . FOR PL/PO 0.99350 0.99210 0.99280 0.99210 0.99070 7.99909 0.99074 RATIOS . FAM PL/PO 0.99074 PATIOS . 20 PL/PO 0.99909	9.27431  FRODY IMLET  PL/PTF 0.2750R 0.2750R 0.2751R 0.2769 0.27431 0.2763 0.27631 0.27633 0.27633 0.27653  DEG SHROHO 1  PL/PTF 0.27663	PL/PTP 0.46651 0.46585 0.46518 0.46517 0.46519 0.46519 0.46519 0.46913 0.46913 0.46913	-1.0000 X/DMAX 3.39800 0.43100 0.44%00 0.52200 0.58800 -1.7000 -1.0000 -1.0000 -1.0000 X/DMAX 0.79300				
-1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -	PADDITIONAL  (D MORD	PL 14-197 14-197 14-197 14-197 14-197 14-202 14-177 14-157 14-277 14-277 14-277 14-277 14-277	0.99070  RATIOS . FOR PL/PO	9.27431  FRODY IMLET  PL/PTF 0.27508 0.27508 0.27518 0.2769 0.27518 0.2769 0.2769 0.2769 0.27693 0.27693 0.27653 0.27653 0.27653	PL/PTP 0.46651 0.46585 0.46518 0.46517 0.46519 0.46519 0.46519 0.46913 0.46913 0.46913	-1.0000 X/DMAX 3.39800 0.43100 0.44%00 0.52200 0.52200 0.52200 -1.0000 -1.0000 -1.0000 -1.0000				
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	0.56207	0.95317	9-42200			
ATINE CO	0. <5956	0.94801	0.67000			
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<b>~</b>		a	X/DMAX	- <del>-</del> -		The second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of th
PL / PO	PL/PTF	PI /PTP				
9-87549	0.48576	0.02376	0.5000	* ~ ~ * * * * * * * * * * * * * * * * *		
1.1132	0.61771	1.0475	0-59300			
2.99656	9.55299	0.93778_	0.67000			
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PL/PO	. PL/PTF	PLAPTE	X/DHAX			
0.99482	7. 55203	0.93614	-1-0000			
7-99613	7-55164	0.93548	-1-0000	_		
2-99413	2.55164	0.03548	-1.0000			
0.99552	0. ***	0.93679	-1.0000			
2-99343	2-55125	9.93483	-1.0000			<del></del>
0.98995	0.54937	0.031	-1.0000			
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ATIOS . FOR	REPORT INLEY					
PL/PG	PL/PTF	PL/PTP	X/DHAX			
9.99482	9.55203	0.93614	0.39809		•	
2.99413	0.55164	0.0354#	0-43100			
0.99413	0.55164	0.93548	0.44900			
2.99552	2. 55241	0.93679	0-48699			
0. 99363	0.55125	0.93483	0.52200			· · · · · · · · · · · · · · · · · · ·
0.48995	0.54932	0.9315	0-58807			
0.79701	0.77377	0.4-010	1.9000	1		
2. 99728	7. 17738	0.03003	-1.0000			
ATTIVS & PAN	THE STREET					
	- PLIPTE	PL/PTP	Y/OMAX			
7, 99 761	9-55357	0.93876	-1.0000			
J. 99726	0.55338	93843	-1.0000			
	DEG SHARUR LI					
PL/PN 0.99724	PL/PTF	Pt /PTP	X/OHAX		·	
	0.55338 0.55319	0.43843	0.79300			
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	0.52672	0.89377	9- 79300			
7.44922	0.52728	0.48568	0-84400			
0.94171				•	- · · · · · · · · · · · · · · · · · · ·	
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VACA-L FUIS	00 EF 14	14684 UT.4	34/13/79	rennf11	MEC 19/24/79	21:10:48.122	FAC ANAMI	PGM C034	RUN 23
SAPORT FORA	PPFSSIME	PATINS . PRI	MANY PLUG						
rAu Mulbu	PL	PL / PG	PL/PTF	PL /PTP	X/DMAX				
32	14.599	1.0198	3.56384	0.92405	0.72200				
77	15.222	1.2633	7.59792	0. 25476	3. 82000				
47	15.352	1.0724	0.59293	0.86658	3.91900		4		
<b>5</b> ?	15.337	1.0713	0.59736	0.84574	1.0170				
>ANDITIONA	F BEEZEIBE	PATINS . FLE	W SPLITTER I	.n.					
IND MUBD	PL	PL/PD	PL /PTF	PI /PTP	X /DMA X		****		
62	15.948	1.0511	0.58115	0-84940	0.42200				
67	14.759	1.0322	0.57000	0.03307	0.67000		and the second state of the second state of the second		
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TAU MUBD	PL	PL/PN	PL /PTF	PI /PTP	x/DMAX				
77	12.698	9.88062	0.48694	0.71167	0.50800				
P2	16. 346	1.1200	0.61972	0.93573	0.58700				
.92	14.279	0.99745	0-55150	0_83603	0_6 700J				<del></del>
SHROLL BUILD	PRESSURF	RATIOS & EJE	CYCR. SHEGO			Marine page 11 and 12 and 12 and 12	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s		
VO WORD.	Pl	<b>PL/</b> Pa	.PL/PTF _		. X/DMAX				
107	14.254	9.99571	0.55054	0.40462	-1.0000				
112	14.254	0.99511	J.55056.	D. 80462	-1-0200	<del></del>			
122	14.254	0-94471	N755054	0.89462	-1.0000				
127	14.264	0.99641	0.55092	0.00510	-1.0000	<del></del>			
1??	14.244	7.97501	0.55015	0. MY406	-1.0000				
مستعدد	14.209	2.99257	0. 54889	0.0208	1.0000	mana ya amandari ilay a ilah ilah ilah ilah	· · · · · · · · · · · · · · · · · · ·		
SMOLTLEGRAC	L PRESSUPE	RATIOS . FCR	EDIDY INLEY	<del></del>			······································		
VO HOPD	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX .				
107	14.254	0.99571	0. 55054	0.80462	0.39A00		•		
112	14.254	0.99571	. 0.55054	0.83462	0.43100				
127	14.254	2 <b>. 9</b> 9571	0.55054	0.00462	0.44900				
127	_14.264		0.55992_	0.89518	0-4860-)				
127	14.244	0.99501	0.55015	0.80496	0.52200				
142	14.209	Q 9925?	0.54880	0.60206	0.58800				
197	14.294		<del>0.9</del> 9199		1.7000				
	14.24					and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th	· · · · · · · · · · · · · · · · · · ·		
		: <del>247103 . y _ £9</del> 4							
AD MUMD	PL	PE/AC	PL/PTE		X/DMAX				
157	14.299	0.99815	0-55189	0.20659	-1.0000				
157	14,289-	7. 94815	0.44180	0.0650	-1.0000				
PMOITICOTK	PRESSUPE	PATINS . 20	DEG SHPOVO 1	DCATECH				<del></del>	<del></del>
Aŭ AŭbD	PL	PL/PR	PL/PYF	Pt /PTP	X/DMAX	a y same	yr i'r awn i mae awnaig y mae'r den gellan a		<del></del>
167	14.294	7.00850	0.55204	0.0687	<b>0. 79</b> 300				
172	14.289	0.99815	0.55189	0.70659	0.84400	•	Color Copum (B) of Allestina we group. (B) (2.1)		
SATOIT IONA	L.PRESSURE	gatins	DEG SHRYUQ.1	PCATLON				<del></del>	
מפחש קע	PL	የኒ/ቀባ	PL/PTF	PI /PTP	X/DMAY		a nika nimin dinika kacamatan dan menjadi sebagai nimban menjadi sebagai nimban menjadi sebagai nimban menjadi		
187	13.546	0.94627	0.52317	9.76467	9.79300				
187	17.451	0.93959	0.51941	0.75927	0.84400				an an indian service service and service
		THPHST PAPAN	E TEDS						
>001108 5    F-01 721,81			STOWA IF 1.5		PF-0.079060	<b>ቦናዞ በ. ሳንያ</b> ዋለብ	CF4 0.0032047		

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32	14.310	0. 99891	0.47287	0.67498	3.72200					
7	15.900	1.1099	0.52543	0. 75000	9. 82000					
7	16.254	1.1346	0.53712	0.76669	0.91900					
?	16,254	1.1346	0.53712	0.76669	1-0170					
ADDITION	LI PRESSIRE	RATIOS . FLE	W SPLITTEP I	-0-						
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U MUND	PL	PL/PF:	PI /PTF	PI /PTP	X/DMAX					
2	15.636	1.0594	0.51571	0.73612	J. 42200		The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa		-	
:7	14. 534	1.0146	0.48028	0.64556	3.67909					
ADDITION	AL PRESSUPE	PATTOS . FLO	W SPLITTER O	.P.						
D WINED	PL	PL/PO	PL/PTF	PE /PTP	X/DMAX		pr			
7	12.395	9.86525	0.40960	0.56466	3.50800		A or nine way - to hake which his departs with			
7	16.693	1.1653	0.55167	0.79739	J.58300		· ·-	- "-		
2	14.275	0.97648	0.47172	0.63233					<del></del>	
addition.	IE-PRESSIRE	PATENS + EJE	CTCF SHFOUR				a springer in the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the community of the commu			
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07	14.235	0.95 360	0.47040 -		~1.0000					
12	14.240	0.97704	0-47055_	0.67169	-1.0000		•			
72	14.235	0.99369	7-47040	0.67145	-1.0000	<del></del>				
27	14.255	0.99508	0.4710	0.67239	-1.0000					
37	14.230	0.99324	0.47023	0.07122	-1.0000					
49	-14.199	0.99091	0.46409	0.66957	1.0000					
	PL	PATIOS . FOR	PI /PTF	PL /PTP	x/DMAY					
n worn		PL/P1)		ri/rir	~ / U""~ ~					
n word . 07	14.235	7. 99369	0-47040	0.67145	0.39800		•			
07							•			
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07 1? 2? 27 27 37 42	14.235 14.240 14.235 15.255 14.230 14.195	0.99369 0.99404 0.99369 0.99508 0.99334 0.99391	0.47040 9.47056 0.47049 9.47106 0.47023 0.46908	0.67145 0.67149 0.67145 0.67239 0.67122 0.66957	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800		•			
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07 12 27 27 37 42 42 42 42 42 42 43 40 40 40 40 40 40 40 40 40 40 40 40 40	PL 14.299 14.299 14.299 14.195 14.299 14.299 14.299 14.299 14.299 14.299 14.299	0.99369 0.99404 0.99369 0.99308 0.99334 0.99901 0.99717 0.99752 PATIOS 20 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PA	0.47040 9.47056 0.47040 9.47105 0.46908 9.47709 0.47201 0.47205 0.47221 DEG SIPPUIN 1 PL/PYF 0.47221 0.47221 DEG SIPPUIN 1	0.67145 0.67169 0.67145 0.67129 0.67122 0.66957 9.67366 0.67366 0.67366 0.67366 0.67366 0.67404 0.67404 0.67404 0.67404	0.39800 0.43100 0.44400 0.52200 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 X/DMAX 0.79300 0.84400					
07 12 27 27 37 42 47 47 40 40 40 40 40 40 40 40 40 40 40 40 40	14.235 14.240 14.735 15.255 14.230 14.195 14.290 14.290 14.290 14.290 14.290 14.290 14.390 14.390	0.99369 0.99404 0.99369 0.99369 0.99334 0.99001 0.99717 0.99717 0.99752 PATIOS 20 M / PO 0.93627 0.93627 0.93627	0. 47040 9. 47056 0. 47040 9. 47106 0. 47023 0. 46909 9. 4720 0. 4721 0. 47221 DEG SHPRIM 1 PL/PYE 0. 47221 0. 47221 DEG SHPRIM 1 PL/PYE 0. 47221 0. 47221 0. 47221 0. 47275	0.67145 0.67169 0.67169 0.67122 0.66957 0.67380 0.67380 0.67380 0.67380 0.67404 0.67404 0.67404	0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 X/DMAX 0.79300 0.84400					
07 12 27 27 37 42 47 47 40 40 40 40 40 40 40 40 40 40 40 40 40	14.235 14.240 14.245 15.255 14.237 14.195 14.295 14.293 14.795 14.293 14.290 14.290 14.290 14.393 13.309 PEASIRED	0.99369 0.99404 0.99369 0.99360 0.99334 0.99934 0.999712 0.99772 0.99772 0.99772 0.99772 PATIOS 20 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.99752 PATIOS 50 PL/PO 0.997626 7.997626 7.997626	0. 47040 9. 47056 0. 47040 9. 47106 0. 47023 0. 46909 9. 4720 0. 4721 0. 47221 DEG SHPRIM 1 9L/PYE 0. 47221 0. 47221 0. 47221 0. 47221 0. 47221 0. 47221 0. 47221	0.67145 0.67169 0.67169 0.67122 0.66957 0.673404 PI/PTP 0.67340 PL/PTP 0.67404 0.67404  PL/PTP 0.673265 0.62771	0.39800 0.43100 0.44400 0.52200 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 X/DMAX 0.79300 0.84400	Dem 0.974-6831	(F4 2_035799			

	< PRF1 [4	THARY DATA	06/13/79	CANDELL	PEC 10/24/79 71:14:18.680	FAT AVEX!	PSP CO34 PRG 1426
>ACC T FOR	AL PPESSIPE	PATIOS , PRI	MARY PLUG			•	and the second second
חאט מא	<b>Pl.</b>	PI /PI	M_/PTF	PL /PTP	X/DMAX		
?2	13.249	0.92629	0.27089	0.53275	3.72200		
77						-	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t
	15.273	1.1166	0.4471?	0.64278	0-82000		
67	17.350	1.2128	J. 48567	0.69763	0. 91 900		and a crawn with a constant specimen of the constant of
52	17.459	1.2705	0.44974	0.79764	1.0170		
		RATEOS . FLO	W SPI ITTEP	r.D.			
9804 84	PL	PL /PI1	PI /PTF	PL /PTP	x/nmax		والمراجع والمستوان والمستوان والمستوان والمستوان والمستوان والمستوان والمستوان والمستوان والمستوان والمستوان والمستوان
62	16.421	1.1759	0-47087	0-67637	0-42200		
67	13.249	0.92629	0.37089	0.53275	0.67000		
NOT TECOM	AL PRESSUPE	PATINS . FLO	W SPLITTEP (	n. n.			
VO WOPD	PL	9L/9Ĥ	PL/PTF	PL /PTP	X/DPAX		
77	8-0592	0.56330	0. 22560	0.32496	0.50800		
#2	20.751	1.4506	0.58089	0.#3441	0.56300		
92	14.252	0_97630	0.39 <b>836</b>	0.57307	0.67000		<del></del>
20017100	AL-PRESSUPE	RATIOS V ESC	EFC SHACUS				
VO WORD	N.	PL/PO.	PL/PTF	914099	X/BMAX		
197	14.197	0.99266	0.39742-	0.57087	-1-0000		
112	14,177	0.99107	-0.39686	0.57007	-1.0000		
122	14.192	2,9871	7-99728	0.57067	-1-0000		
127	14.212	0.99386	3.3479R	0-57167	-1.0090		
137	14.272	0.99281	0.39756	0.57107	1.0000	·	en en en en en en en en en en en en en e
	14.192	0.99211	0.39728	0.57067	-1.9000		
142			. 9833120	227,20.			
>ADDIT 10M	AL PRESSURE	RATIOS . FOR	ESCOY INLEY				
>ÁDDITION VO WORD	AL PRESSURE	RATIOS . FOR	PL/PTF	PL/PTP	X/DMAX		
>ÁDDITION VD WORD 177	PL 14.197	RATIOS . FOR PL/PD 0. 99746	PL/PTF 0.39742	PL/PTP 0.57087	X/DMAX 0.39900	•	
>ADDITION  VO WORD  177  112	PL 14.197 14.177	PL/PD 0. 99746 0. 99 107	PL/PTF 0.39742 0.39666	PL/PTP 0.57087 0.57007	X/DMAX 0.39800 3.43100	•	
>ADDIT TONK VD WORD 177 112 127	PL 14.197 14.197 14.177 14.192	PATIOS . FOR PL/PD 0. 99746 0. 99107 0. 99211	PL/PTF 0-39742 0-39656 0-39778	PL/PTP 0.57087 0.57007 0.57067	X/DMAX 0.39800 3.43100 0.44900		
>ADDITION  VO WORD  177  112	PL 14.197 14.177	PL/PD 0. 99746 0. 99 107	PL/PTF 0.39742 0.39666	PL/PTP 0.57087 0.57007	X/DMAX 0.39800 3.43100		
>ADDIT 1090 VD WORD 177 112 122 127	PL 14.197 14.197 14.177 14.172 14.217	PL/PD 0. 99746 0. 99107 0. 99211 0. 99386 0. 99281	PL/PTF 0-39742 0-39676 0-39778 0-39778	PL/PTP 0-57007 0-57007 0-57067 0-57167	X/DMAX 0.39800 3.43100 0.44900	•	
>ADDIT TONG VO WORD 177 112 122 127 127 127 142	PL 14.197 14.197 14.177 14.172 14.217 14.217 14.272 14.192	PL/PD 0.99746 0.99107 0.99211 0.99386	PL/PTF 0.39742 0.39666 0.39778	PL/PTP 0.57087 0.57007 0.57067 0.57167	X/DMAX 0-39800 3-43100 0-44900	•	
>ADDIT TONU VO WORD 197 112 122 127 127 142 142	PL 14-197 14-197 14-177 14-192 14-217 14-272 14-192 14-192	PL/PD 0, 99246 0, 99107 0, 99211 0, 99286 0, 99281 0, 99211	PL/PTF 0-30742 0-39676 0-36778 0-39778 0-29756 0-39728 0-39728	PL/PTP 0-57007 0-57007 0-57067 0-57167 0-57197 0-57067	X/DMAX 0.39800 3.43100 0.44400 0.52200 0.52200 0.58800	•	
>ADDIT.ROM VD WORD 197 112 127 127 137 142 127	PL 14-197 14-197 14-177 14-177 14-192 14-217 14-272 14-192 14-272	PL/PD 0.99746 0.99717 0.99211 0.99211 0.99211 0.79211 0.79709	PL/PTF 0.39742 0.396-0 0.39790 0.39790 0.39790 0.39720 0.39720	PL/PTP 0.57007 0.57007 0.57067 0.57167 0.57107 0.57067	X/DMAX 0.39800 3.43100 0.44800 0.52200 0.58800		
>ADDIT NOW  VD WORD  177  112  127  137  142  142  142  142	PL 14.197 14.197 14.197 14.192 14.217 14.217 14.272 14.192 14.277 14.272	PL/PD 0. 99746 0. 99107 0. 99211 0. 99211 0. 99211 0. 99211 0. 79211 0. 797167	PL/PTF 0-30742 0-39676 0-36778 0-39778 0-39778 0-39778 0-39778 0-39778	PL/PTP 0-57007 0-57007 0-57067 0-57167 0-57167 0-57107 0-57067	X/DMAX 0.39800 3.43100 0.44900 0.52200 0.52200 0.58800 -1:0008		
>ADDIT NOW  VD WORD  177  112  127  137  142  127  147  ***CONTROL OF THE PROPERTY OF WORD  ***CONTROL OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE	PL 14-197 14-197 14-197 14-192 14-217 14-272 14-192 14-277 14-272	PL/PD 0. 99246 0. 99210 0. 99211 0. 99286 0. 99211 0. 99386 0. 99281 0. 79211 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 79286 0. 792	PL/PTF 0-30742 0-39742 0-39756 0-39756 0-39756 0-39756 0-39756	PL/PTP 0.57007 0.57007 0.57067 0.57167 0.57167 0.57167 0.57067 0.57068	X/DMAX 0-39800 3-43100 0-44400 0-58600 0-52200 0-58600 -1-0000 -1-0000		
DÁDDIT ROM  VO WORD  177  112  127  127  137  142  127  127  WORD  WORD  157	PL 14-197 14-197 14-177 14-177 14-217 14-217 14-272 14-192 14-277 PL PRESSUPE	PL/PD 0. 99746 0. 99746 0. 99707 0. 99211 0. 99386 0. 99211 0. 79211 0. 79709 7. 79709 PA 1103 y CAN	PL/PTF 0.30742 0.30742 0.30742 0.30770 0.30770 0.30770 0.30770 0.30770 0.30770 0.30770	PL/PTP 0.57007 0.57007 0.57067 0.57167 0.57107 0.57067 0.57579 0.57579	X/DMAX 0.39800 3.43100 0.44400 0.52200 0.58800 -1.0000 -1.0000		
DÁDDIT ROM  VO WORD  177  112  127  137  142  142  142  147  MODEL ROM  VD WORD  142	PL 14-197 14-197 14-197 14-192 14-217 14-272 14-192 14-277 14-272	PL/PD 0. 99246 0. 99210 0. 99211 0. 99286 0. 99281 0. 99281 0. 99281 0. 99281 0. 99281 0. 99281 0. 99281	PL/PTF 0-30742 0-39742 0-39756 0-39756 0-39756 0-39756 0-39756	PL/PTP 0.57007 0.57007 0.57067 0.57167 0.57167 0.57167 0.57067 0.57068	X/DMAX 0-39800 3-43100 0-44400 0-58600 0-52200 0-58600 -1-0000 -1-0000		
PÁDDIT MONO 177 112 127 137 142 127 142 127 142 127 142 127 142 127 127 127 127 127 127 127 127 127 12	PL 14-197 14-197 14-197 14-192 14-217 14-272 14-192 14-197 14-277 14-272 PL 14-277 16-277	PL/PD 0. 99746 0. 99746 0. 99707 0. 99211 0. 99386 0. 99211 0. 79211 0. 79709 7. 79709 PA 1103 y CAN	PL/PTF 0-30742 0-30742 0-30778 0-30778 0-39798 0-39756 0-39758 0-39791 0-39791	PL/PTP 0.57007 0.57007 0.57067 0.57167 0.57167 0.57067 0.57067 0.57288	X/DMAX 0.39800 3.43100 0.44400 0.52200 0.58800 -1.0000 -1.0000		
VADDIT NOW  VALUE OF THE PROPERTY OF WORD  107  112  127  137  142  142  142  142  144  VALUE OF THE PROPERTY OF WORD  142  145  ADDIT ION	PL 14-197 14-197 14-197 14-217 14-217 14-272 14-192 14-277 15-272 PL 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-277 14-	PL/PD 0. 99746 0. 99746 0. 99711 0. 99386 0. 99281 0. 99281 0. 79211 0. 79769 PA 1103 * FAN PL/PB 0. 99404 0. 99769 RA 1105 * 20	PL/PTF 0.30742 0.30742 0.30742 0.30770 0.30770 0.39720 0.39720 0.39720 0.39721 PL/PTF 0.30951 DEG SHPPIN L	PL/PTP 0.57007 0.57007 0.57067 0.57167 0.57167 0.57388 PL/PTP 0.57408 0.57388	X/DMAX 0.39800 3.43100 0.44400 0.52200 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000		
>ADDIT 10M  VD WORD  177  112  127  137  142  142  142  142  142  142  142  14	PL 14.197 14.197 14.197 14.192 14.217 14.217 14.272 14.277 14.277 14.277 14.277 14.277	PL/PD 0. 99246 9. 99107 0. 99211 0. 99286 0. 99281 0. 99281 0. 79211 0. 79767 PATIOS FAM PL/PS 0. 99409 0. 99769 RATIOS 20	PL/PTF 0.30742 0.30742 0.39778 0.39778 0.39778 0.39778 0.39778 0.39778 0.39778 0.39778 0.39778 0.39791	PL/PTP 0-57007 0-57007 0-57067 0-57167 0-57167 0-57167 0-57167 0-57067 0-57067 0-57067 0-57067	X/DMAX 0.39800 3.43100 0.44900 0.52200 0.52200 0.58800 -1:0000 -1:0000 -1:0000		
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>ADDIT 10M  VD WORD  177  112  127  137  142  142  142  142  142  142  142  14	PL 14.277 14.272 14.277 14.272 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277 14.277	PL/PD 0. 99746 9. 99107 0. 99211 0. 99211 0. 99211 0. 99211 0. 99211 0. 99211 0. 99769 PATIOS - FAM PL/PS 0. 99769 RATIOS - 20 PL/PT 0. 99764 9. 99804 PATIOS - 80 PL/PT 0. 92849 0. 92829	PL/PTF 0-30742 0-30742 0-30778 0-32778 0-32778 0-39778 0-39778 0-39779  PL/PTF 0-39944 0-3995  PL/PTF 0-39947 0-39965  PFG SHRIGIN L PL/PTF 0-37728 0-37172	PL/PTP 0.57007 0.57007 0.57007 0.57107 0.57167 0.57167 0.57200 0.57200 PL/PTP 0.67400 0.57300 PL/PTP 0.57300 PL/PTP 0.57300 PL/PTP 0.57300 PL/PTP	X/DMAX 0.39800 3.43100 0.44400 0.58600 0.52200 0.58600 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 X/DMAX 0.79300 0.84400		
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4454-EFW1 <b>5</b>	pertin	IMARY DATA	<b>3</b> +/13/79	CADDELL	REC 10/24/79	71:19:56.097	FAS GHANT	PG# C034	RUNDS	· -
AND IT IONA	1 046551386	PATINS , PP1	MAPY PLUG					at a second		
In Morb	PL.	PI /P(1	PI /PTF	PL/PTP	X/DMAX					
2	13.765	2.96234	0.34673	0.50002	U. 72200					
7	16.697	1.1673	0.42301	7.61714	J.#2000		• -			*
7	18-333	1.2017	0.46444	0.67767	2.91900					
?	14.417	1.2976	9.46659	0.68077	1.0170					
APPIT IONA	PRESSIPF	RATERS . FLC	W SPEETFE !	,n,	teriproduktionen in den <u>anne produktionen in den produktionen in den produktionen in den produktionen in den p</u>					
9 WORD	PL	PL/PO	PL/PTF	PI /PTP	H/DMAH			and the same and the same	to the second second second	
.2	18.348	1.2927	0.46482	0.67519	0.42200			and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property and the same property		
.7	14.409	1.0973	9.36503	0.53258	0.67000					
APPIT TONA	PRESSIME	RATIOS . FLO	W SPLITTER C	n. n.						
D WORD	PL	PL / PO	PL/PTF	PL /PTP	X/PMAX					
7	9.0961	0.63522	0.23019	0-33595	0.50000				-	
2	19-331	1.3305	0.48213	0.70343	2.58303					
2	14.249	0.99615	0.36090	0-52669	0.67000					
10017 10WA	t-PRESSUPF	<del>natins y Car</del>	CTO SIFE							
D WIND	PL	PL/PG	PL/PTF	21.437	X/DHAX	يسوارا بدامان بيسانستوس			-	
07	14.199	Qa 99 28 7	0.35972	0.52484	-1.0000					
12	14-194	2.99102	25 35 924	0.52429	-1-0000					
22	14.194	2-90277	0.36959	0.52466	-1.0000					
27 37	14.236	2.99511	0.36060	0.57851	-1.0000	# ##			<del></del>	
32	14.224	), 99546 ), 99441	0.36973 0.36935	0.52576	-1.0000 -1.0000					
A 2017 [ONA	L PRESSURE	RATIOS . FOR	EATHY IMET							
D WCRD	PL	PL/PN	PL /PTF	PL/PTP	XAMAX					
07	14.199	0.99267	0.35972	0.52484	0.39800	a 1988 - Article September - Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committee Committ				
12	14-174	0.99162	0. 35934	0.52429	0.43100					
72	14.194	0.99232	0.35949	0.52466	0.44900					
27	15.235	0.99511	0.36060	0.52613	0.49600					
77	14.239	1.99546	0.26073	0.52631	0.52200					
42	14.224	0.99441	0.36035	0.52576	0.58800					
<del></del>	14,767	7: 99755	0.36149	0.9797	-1.0000					
<del>5}</del>		0x94755	9 <del>1 36149</del>							
		-471 <del>05 F</del> AN	MUSTER FINE						····	
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n ween	PL	PO								
M WORD	PL 14.269	10 97755	0-36149	0.52742	-1.0000		The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa			
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N WORD 57 57 479111044	PL 14.769	0. 99755 0. 99755 PAYIOS . 20	0.36149 0.36149 DFG SIPPOUD (	0.52742 - 0.5 <u>274</u> 2 ncating	-1.0000 -1.0000				1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	
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70 WORD (57 57 (470) T T TOMA (7) WORD (67	PL 14.769	0. 99755 0. 99755 PAYIOS . 20	0.36149 0.36149 DFG SIPPOUD (	0.52742 - 0.5 <u>274</u> 2 ncating	-1.0000 -1.0000					
n unen 57 57 470fffnga n unen 67	PL 14.269 14.789 1 PRESSUPE PL 14.274 14.269	0. 99755 0. 99755 PATIOS . 20 PL/PO 0. 99700 0. 99755	0.36149 0.36144 0FG SHPOUD U PL/PTF 0.36161 0.36149	0.52742 0.52742 NCATION PI /PTP 0.52760 0.52742	-1.0000 -1.0000 */DMAX 0.79300					
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N WORD 57 ATRITIONAL D WORD 67 72 ATRITIONAL D WORD	PL 14.269 14.789 1 PRESSUPE PL 14.274 14.269 PRESSUPE PL	0. 97755 0. 99755 PATIOS . 20 PL/PO 0. 99700 0. 99755 RATIOS . 80 PL/PO	0.36149 0.36144 DFG SHPRUD E PL/PTF 0.36161 0.36149 DFG SHPRUD E PL/PTF	0.52742 0.52742 OCATION PI /PTP 0.52760 0.52742 OCATION PL /PTP	-1.0000 -1.0000 #/DMAX 0.79300 0.84400					
70 HORD 157 57 47911100 10 HORD 67	PL 14.269 14.769 1 PRESSUPE PL 14.274 14.269 1 PRESSUPE	0. 99755 0. 99755 PATINS . 20 PL/PN 0. 99700 0. 99755 RATINS . 80	0.36149 0.36144 OFG SHPRID ( PL/PTF 0.36161 0.36149 DEG SHRRID (	0.52742 0-52762 <u>NCATION</u> PI /PTP 0.52760 0.52742 <u>NCATION</u>	-1.0000 -1.0000 x/DMAX 0.79300 0.84400					

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VR WORD 32 37 47 52 >ADD[T]INA[	PL 14.796 18.713 20.206 19.990	PATICS . PRI PL/PC 1.0341 1.3090 1.4133 1.3976	PL/PTF 0.33266 0.42109 0.45463	Pt /PTP 3.48805	X/DMAX			. • • • • • • • • • • • • • • • • • • •	RNG 1428
22 37 57 52 400 [T](MA)	14.796 18.713 20.204 19.990	1.0341 1.3090 1.4133	0.33266 0.42109	PL /PTP 3.48895					
97 67 52 >400 [T]ONAL	18.713 20.204 19.990	1.0341 1.3090 1.4133	0.42109						
7 52 •400 [ T ] (1)A1	20.204	1.4133			J.72200				
SADDETERNAL	19,990		0.45463	0.61778	J. #2007				
SAUDITIONAL		1. 3976		0.66793	3-91900			and the same of the same of the	
	PRESSIME		0.44958	0.65950	1.0170				
to Hobo		RATIOS . FLE	W SPLITTER I	.n.					
A 13 MITHURS (1.4)	PL	PL /PO	PL /PTF	PL/PTP	X/DMAX				
52	20.563	1.4284	0.46271	0.67885	0-42200			···	
47	16.614	1.1621	0.37384	0.54947	0.67000				
ANDITIONAL	PRESSURE	RATIOS . FLO	W SPLITTER O	. n.					
	ય	PI /PN	PL/PTF	PL/PTP	X/DMAX				
77	13.414	0.72846	0.23433	0.34380	0.50800				
<b>92</b>	[4. A53	1.0390	0.33423	0-49036	J-5#300				
92	14.240	0. 99610 _	0. 32042	0.47010	0.67000	<del></del>			
A TOTT TOTAL	PRESSURE	RPT103 8 EJE	CTCP SHROUT	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -					
VE WORD	7	PL/PO .	PL/PTF	PLANT	X/DMAX				
197	14.170	0.99121	0.31885	0.46780	-1.0000				
112	<u> 14.145</u>	D-98947		BP884-0					
122	14.169	2-94051	0.31763	0.46747	-1.6000				
127	14.225	2, 99505	0.0000	0-46961	-1.0000		·		
! ? ?	14,250	0.99679	0.32065	0.47043	-1.0000				
المعسية	14.225	0.99505	0.32009	0.48961	-1,0000				
ADDITIONAL	PRESSURE	RATIOS FOR	ESCOY IN ET						
	PL	. PL/PG	PL/PTF	"L/PIP	X/DMAX			·	
197	14-170	0.99121	0.31985	0.46780	0.39000				
112	14.145	0.98957	. 9.31829	0-46698 .	0.43100				
127	14.160	0.99051	0.31463	0.46747	0.44900				
L27	14.225	0.99505	0.32009	0-4696:	Q_48600	<del></del>			
137 142	14.257	0,99679	0.32065	0.47043	0.52200				
[45]	14.225 14.289	5. 99505	0.32009 7.32009	0.46961	0.54000			· <del></del>	
90	14.279		0. 52110	7.47109	-1.0000	·			
MEGET TOYAL	PRESSURE.	***********	MERCLE PLAN						
	2	M-180	PL/PTF	PL/PTP	X/DMAX .				
52	14.265	1. 99784	0.27099	0.47093	-1.0000				
152.	14.270	J. 99A19	0.32110	0-47100	-1.0000				
JAMOT TICHAL	PRESSUPE	RATIOS . 20	DEG_SHROUD_I	UČATIUM					
IN MUNER I	PL	PL/PR	PL/PTF	Pt /PTP	X/DMAX				
147	14.270	0.99819	0.32110	0.47109	0.79300				
172	14.265	0.09784	0.32099	9.47093	9. 84400				
ADDIT LONGE	PRESSURE.	# PTEN <u>S</u> <u># 90</u> .	DEG SIPOUN 1	OCATION					
in Auto i	PL	PL/PO	M_/PTF	PE /PTP	X/DMAX				
8,7	13.372	0.93434	9. 30090	0.44145	0.79300				
97	13.347	0.93364	0.30034	0.4063	0.84400				- commence and companies commercial com-
POTTON S .		THPHST PAPAM							

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VASA-L FW IS	PRFL 14	INSPY DATA	06/13/79	CADDFII	MEC 10/24/	/79 21:22:39.720	FAC RYSKI	PGM C034	RBG 2429	
SAPPLE FORMS	PPESSIPE	PATINS . PRI	MAPY PLUG							
VD WOPD	PL	PL /PO	PL /PTF	PL /PTP	Y/DMAX				<del></del>	_
32	11.413	0.79881	0.22138	0.31970	0.72200		منهما ومنتهوهات المااد والمتالية		contracting agreement of the agreement agreement is	
77	20 <u>+</u> 200	1.4130	0. 391 P4	0.565#5	0.42000					
47	22.987	1.6089	0.44551	J.£4393	9. 71 700					
52	22.798	1.5957	9.44223	9.63R62	1.0170					
JAMOE TECHA	PRESSURE	PATIOS . FLO	W SPI STTER S	. n.						
VP WOPD	PL	PL/PN	M./PTF	PI /PTP	X/DMAX	n man i				-
62	24.837	1.7384	0.48180	0.69576	9-42299					
67	21.541	1.5077	0.41786	0.60342	0.67000					-
SAPRIT FRINAL	PRESSURE	PATIOS . FLO	W SPLITTER C	- D.	·					
		•	• •		w 40m 4 w	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	· SPR 4 Francis of Appellion (Apple of Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Company and Com			
	PL	PL/PN	PI_/PTF	PI /PTP	X/IMAX					
77	12.126	0.64873	9. 23522	_ D. 33969	0.50 <b>00</b> 0	year a company again manda.	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
#? 92	17.263	1.2083	9.33486	0.48357	0.58300					
92	_14.231	0.29606	0.27605_	Ue:7507	0.67000					_
PESTATOM	PRESENCE	AATING . EUF	CTOR SIMPLIA		سنسند	·		Barrier Commission of the straight commission of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight of the straight	الوراقي الإياد المعادلين والماري <mark>ي ويس</mark> اد الماريي	
AU MUND	7	PL/PO	PL/PTF	PLAPTP	X/DHAX					_
107	14-14	0.98978	0-27431	0.39613	-1.0000					_
112	16,126	0-9873-		0,39571	-1-0000					
122	14.136	0. 4f 943	- 0.27421	0.39599	-1.0000					
127	15-196	0.99292	0.27914_	0.39739	-1.0000					
137	14.166	0. 99152	0.27479	8-396P?	-1.0000					
442	14.176	0.99222	0. 27499	0.39710	-1.0000	A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
24221TIONAL	PRESSUPE	PATIOS . FOR	EBODY INLET							
AU MUND	PL	PL/PO	PL/PTF	PL/PTP	XAMOX					
107	14.141	0. 98978	0.27431	2.39613	0.39700					-
112	14.126	0.98873	9. 27492	0.39571	0.43160					
127	14-136	0.48443	0.27421	0.39599	0.44900					
127	15.176	0.99292	0.27510	0.39734	0.48600					
137	14.166	0.99152	9.27479	9.39692	0.52200					,
142	14.176	0.99227	0.27490	0,39710	0.58800					
1-5	-14.PRB	7, 99 990	110 270 73	0 9907	-1:0000	<b>-</b>				
<del></del>	14.501	<del></del>		0,3340						4
-403[5]-me		90 1195 FAN					,			
AU ALIES	PL	- AL/PO	9 /PIF	PI TPTP	X/OMAX					
15?	14.256	0.99840	0.27672	0,39942	-1-0000	na 100 a				
ië	_14+261	0.99815	2.27863	C.3904#	-1.0000					
	PRESSIME	RATIOS . 20	NEG SHPPUN I	OCATION			,			
	PL	PL/PN	PL/PTF	PL /PTP	X/DHAX					
167	14.261	0.99915	0.27663	0.3994#	0.79300					
177	14.761	0.99815	0.27663	0.3994#	0. 84400		. Harring angles	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		-
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AU AUBU	PL	PL/PN	PI /PTF	PL /PTP	X/DMAX					
18?	13.519	0.94614	0.76221	0.37866	0.79300					
1#7	17.488	3.94464	0.26163	0.37782	0.84400					
> 111111115		THPIIST PAPAM	FTFOS							
F-01 1024.7			STONA IT 2.6	***	WF 0.31711	P[<250.0 M20	CF4 0.0079694			

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ONDITIONAL MORD F	Pt 1129 23.443 20.126 25.937 PRESSIME Pt 27.568 21.469 PRESSIME Pt 13.868 19.942 14.112 14.077 14.107	#L/PO 0.78351 1.6416 1.8295 1.0142  RAYIOS , FLO #L/PO 1.9305 1.5047  RATIOS , FLO #L/PO 9.97250 1.3495 0.99625  RAYIOS , Edd #L/PO 9.97627 1.996822 9.99677	M /PTF 0.18962 0.39739 0.44277 0.43905 W SPLITTFP PL/PTF 0.46720 0.36417 W SPLITTER ( PL/PTF 0.23536 0.33629 0.26111	PL /PTP 6-67749 0-52888	X/DMAX 0.72200 0.92000 0.91900 1.0170 X/DMAX 0.42200 0.67000 X/BMAX 0.50000 0.50300 0.A7090					
ODITIONAL OWNED FOR THE PROPERTY SOUTH	1199 23.443 20.126 25.937 PRESSIME 27.568 21.469 PRESSIME 13.868. 19.442 14.227 PRESSIME	0.78351 1.6416 1.8295 1.8142 RAYINS . FLO PL/PD 1.9305 1.5047 RAYINS . FLO PL/PO 9.97250 1.3495 0.99625 RAYINS . EM	0.18962 0.39739 0.44277 0.43905 W SPLITTEP PL/PTF 0.44720 0.36417 W SPLITTER ( PL/PTF 9.23536 0.33629 9.26111 CTCP SHROW	0.27497 0.57612 0.64206 0.63667 i.n. PL/PTP G.67749 0.52808 i.n. PL/PTP .0.34130 0.48763 .0.48763	0.72200 0.82000 0.91900 1.0170 */DMAK 0.42200 0.67000 */BMAX 0.50000 0.50000 0.67000					
ODITIONAL OWNED FOR THE PROPERTY SOUTH	1199 23.443 20.126 25.937 PRESSIME 27.568 21.469 PRESSIME 13.868. 19.442 14.227 PRESSIME	0.78351 1.6416 1.8295 1.8142 RAYINS . FLO PL/PD 1.9305 1.5047 RAYINS . FLO PL/PO 9.97250 1.3495 0.99625 RAYINS . EM	0.18962 0.39739 0.44277 0.43905 W SPLITTEP PL/PTF 0.44720 0.36417 W SPLITTER ( PL/PTF 9.23536 0.33629 9.26111 CTCP SHROW	0.27497 0.57612 0.64206 0.63667 i.n. PL/PTP G.67749 0.52808 i.n. PL/PTP .0.34130 0.48763 .0.48763	0.72200 0.82000 0.91900 1.0170 */DMAK 0.42200 0.67000 */BMAX 0.50000 0.50000 0.67000					
ODITIONAL MORD F	2u.126 25.937 PRESSIME 27.568 21.469 PRESSIME 13.888 19.442 16.227 PRESSURE 14.112 16.077 14.107	1.8295 1.8142 RATIOS , FLO PL/PO 1.9305 1.5047 RATIOS , FLO PL/PO 9.97250 1.3495 0.99425 RATIOS , ESE PL/PO 9.98822	0.44277 0.43405 W SPLITTEP PL/PTF 0.46720 0.36417 W SPLITTER ( PL/PTF 0.23536 0.33629 0.26111 CTTP SHROWS PL/PTF 0.23216	0.64206 0.63667 i.n. Pt /PTP G.67749 0.52808 0.n. Pt /PTP -0.34130 0.48763 -0.34963	U-91900 1-0170 Y/DMAX 0-42200 0-67000 X/BMAX 0-50000 0-67000 0-67000					
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O MORD P	PL 27.568 21.409 PRESSIME 13.888 19.442 14.227 PRESSIME 14.117 14.077	PL/PN 1.9305 1.5047 RATIOS , FLO PL/PO 9.97250 1.3495 0.99425 RATIOS V CAL PL/PD 9.94822 0.946577	PL/PTF 0.46720 0.36417 W SPLITTER ( PL/PTF 0.23536 0.33629 0.26111 CTTP SHROW PL/PTF 0.23216	PL/PTP G-67749 G-528GR N-N- PL/PTP G-34130 G-48763 R-34963	0.42200 0.67000 X/BMAX 0.50000 0.50300 0.67000					
O MORD P	27.568 21.469 PRESSIME 13.888 19.442 14.227 PRESSURE 14.112 14.077	1.9305 1.5047 RATIOS , FLO PL/PO 9.97250 1.3995 0.99425 RATIOS , CAL PL/PO 9.98822 0.994577	0.46720 0.36417 H SPLITTER ( PL/PTF 0.23534 0.33629 0.26111 CTCP SHROW PL/PTF 0.23216	G.67749 Q.528QR I.D. PL/PTP 	0.42200 0.67000 X/BMAX 0.50000 0.50300 0.67000					
ON TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TOWAL  SOUTH TO	27.568 21.469 PRESSIME 13.888 19.442 14.227 PRESSURE 14.112 14.077	1.9305 1.5047 RATIOS , FLO PL/PO 9.97250 1.3995 0.99425 RATIOS , CAL PL/PO 9.98822 0.994577	0.46720 0.36417 H SPLITTER ( PL/PTF 0.23534 0.33629 0.26111 CTCP SHROW PL/PTF 0.23216	G.67749 Q.528QR I.D. PL/PTP 	X/BMAX 0.50000 0.50000 0.47000					
NORD F	21.469 PRESSIME 13.868 19.942 14.227 PRESSURE 14.112 14.077	1.5047 RATIOS , FLO PL/PO 9.97250 1.3495 0.99425 RATIOS , Edi PL/PO 9.96822 0.94577	0.36417  M SPLITTER ( PL/PTF 0.23536 0.33629 0.26111 CTCP SHROLD PL/PTF 0.23216	0.52808 1.0. PL/PTP 0.34130 0.48763 0.34963	X/BMAX 0.50000 0.50000 0.47000					
WORD P	13.888. 19.442 14.227. PRESSURE 14.112 14.077. 14.107	R./PO 9-97250 1.3495 0-99425 RATIOS V CAL PL/PO 9-98822 D-94577	PL/PTF 0-23536 0-33629 0-26111	PL/PTP 0.34130 0.48763 0.34963	0.50000 0.50300 0.67000		\			
MORD 7	13.868. 19.442 16.227. PRC 35URC 14.112 16.077. 14.107	9.97250 1.3495 0.99425 RATIOS V CAL PL/PD 0.94822 0.94577	0.23536 0.33629 0.26111 erer siness PL/PTF 0.23916	0.34130 0.48763 0.34963	0.50000 0.50300 0.67000					
MORD 7	13.868. 19.442 16.227. PRC 35URC 14.112 16.077. 14.107	9.97250 1.3495 0.99425 RATIOS V CAL PL/PD 0.94822 0.94577	0.23536 0.33629 0.26111 erer siness PL/PTF 0.23916	0.34130 0.48763 0.34963	0.50000 0.50300 0.67000					
001710HAL HORD 77 2.2.77	19.442 16.227 PRC 32482 14.112 16.077 14.107	1.3995 0.99625 RATIOS V CAL PL/PO 0.96822 0.96577	0.33624 0.26111 ero ameno PL/PTF 0.23916	0.48763 0.34963	0.50300 0.67000 X/DMAX					
001710HAL HORD 7	14.227 PRE 19URE 14.112 16.077 14.107	0.99625 RATIOS V EXE PL/PO 9.98822 DESESTE	0.26111 CTCF 3HROW PL/PTF 0.23216	9.34963 PLDW	0.67090 X/DMAX					
WORD 7	14.117 16.077 14.107	PL/PD 1.98822 0:98577	PL/PTF 0.23916							
2	14.112 16.077 14.107	9. 98822	0-23216							
2	14.112 16.077 14.107	9. 98822	0-23216							
2	14-107	98577								
7		1 00 77		4.34595	-1.0000					
		4 Table 144 1	Q.2300A	0.34669	-1.6000					
_	14. 202	J. 99450	0:24049	0.34902	-1.0000					
·	14.277	0.99625	0. 24111	0.34963	-1.9000					
3	14.277	0.99974.	0.24195	0.36086	-1.0000			·		
POIT IONAL	PRESSURE	RATIOS FOR	EBODY LINLET.							
unen #	PL .	PL / PO	PL/PTF	PI /PTP	I/MAI					
							•			
		). 94787	9.23908	0.34669						
7	14-202	0.99450	0.24069	0-34902	J-4 0500					
7	14.227	0.99625	0.74111	0.34963	9 <b>.52200</b>					
2	14.277	J. <del>9</del> 9974	D. 24195	0.35046	9.58000					
•	14:202	46 25 154			1:0090					
<del>*</del>	14.257	<del></del>		9.35037	1.0000					
0402 TO 18	PRESSURE	PAT103_1_FAC	HOLITE-FLM						<del></del>	
MUSD P	1	PLLED.	_PL/87F	PLIPTP	X/DMAX					
	14.262	4.44170	0.24170	0.35049	-1.0000					
	14.257	0.99835	0.24100	0.35037	-1,0000		·			
ODIT TOMAL	PRESSURE	RATIOS . 20	DEG SHERUD I	DEATICM		······································		······	<del></del>	
-	ય	PL/PO	PL /PTF	PI /PTP	X/DMAX					
7	14.257	0.99835	0.74162	0.35037	0. 79300					
2	14.262	9. <del>99</del> 870	0.24170	9.35049	0.84400					
DDIT IONAL	PRESSURE	RATIOS . 90	DEG_SHRPUD_I	DCATION						
		PL/PO	PL/PTF	PL/PTP	x/OHAX		·			
		0.97285	0.23544	0.34142	0.79300					
	13.414	2.96761		0.33058	0.84400					
77104 5 .				1914 FTS	PF 0.67523 DSM 0.34	9359 EF# 6.	.1370733			
	POIT IONAL WORD I 7 2 2 7 7 2 WORD I 7 7 7 00 II IONAL WORD I 7 2 00 III IONAL WORD I 7 2 00 III IONAL	### PRESSURE  #### PRESSURE  #### 14-112 2	### PL PL/PD  7 14-112 0.98822  2 14-377 0.98577  2 14-107 0.98577  7 14-202 0.99550  7 14-227 0.99625  7 14-227 0.99625  2 14-277 3.99979  14-227 0.99625  2 14-277 3.99979  7 14-287 0.99935  #################################	## PT   PL/PD   PL/PTF   14.112   0.94822   0.23916   2.23916   2.23916   2.23917   0.23957   0.23957   0.23957   0.23957   0.23957   0.23957   0.23957   0.23957   0.23957   0.23957   0.24069   0.24069   0.24069   0.24069   0.24069   0.24069   0.24069   0.24069   0.24069   0.24069   0.24069   0.24069   0.24069   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.24170   0.	### PRESSURE RATIOS . FOREBODY INLET  #### PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP PL/PTP P	DOIT IONAL PRESSURE RATIOS	DOIT IONAL PRESSURE RATIOS . FORERODY INLET  WORD PL	DOIT IONAL PRESSURE RATIOS FOREBODY LINET  WORD PL PL/PD PL/PTF PL/PTP X/DRAX  7 14-112 0.98577 0.23957 0.34681 0.39800 2 14-107 0.98577 0.23957 0.34595 0.43180 2 14-107 0.98577 0.23957 0.34589 0.44400 7 14-227 0.99450 0.24069 0.34669 0.44400 7 14-227 0.99455 0.75111 0.34963 0.52200 2 14-277 0.9974 0.24195 0.25964 0.58000 2 14-277 0.9979 0.24197 0.3964 0.58000 2 14-277 0.9979 0.24197 0.35040 0.3000 2 14-257 0.99035 0.26162 0.35037 -1:0000  WHORD PL PRESSURE PATIOS 2. FOR HOLELE FLAD  WHORD PL PL/PD PL/PTP N/DWAX 0.35049 -1:0000  ODIT INMAL PRESSURE RATIOS 2. 0. DFG. SHROUD LOCATION  WHORD PL PL/PD PL/PTP PL/PTP X/DWAX 0.35037 0.79300 2 14-257 0.99835 0.24162 0.35037 0.79300 2 14-262 0.99870 0.26170 0.35049 0.84400  ODIT INMAL PRESSURE RATIOS 2. 0. DFG. SHROUD LOCATION  WHORD PL PL/PD PL/PTP PL/PTP X/DWAX 0.84400 2 13-93 0.97285 0.23170 0.35049 0.84400  ODIT INMAL PRESSURE RATIOS 2. 0. DFG. 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WF	Pŧ	PL /PO	PI /PTF	PL /PTP	¥708AX	
7	14.268	0.99774	3.32200	0.47418	0.79300	
2	14.268	0. 99774	0.32200	0.47418	0.84400	والمراقب المراقب المورث والمستخدم والمستخدم والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والمراقب والم
70 IT ION	AL PRESSURE	PATTINS	ute sierno t	OCATION		
AU&D	PL	Pį/PO	PL /PTF	PL/PTP	x/DMAX	
2	13.370	0.93496	0.30174	0.44434	0.79300	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
7	13.335	0.93252	0.30095	0.44318	0.84400	
PT [ ] M S		THRUST PAPAR				
า) ควา	20 546	700_78	STOPP IF 3.2	412 674	PF 0.17425	PSP 0.744205 CFW 9.0938384

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FAT REAT

CARRETT

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HASE-LEWIS

PRFLIMINARY DATA

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NAS	4-1 FW 15	buil In	IMARY DATA	06/13/79	CADDETT	RFC 10/24/79 21:30:49.4	33 FAC 88681	PGM CO34	RUN 23
>6.	O ET IONAL	PPFSSIME	RETINS . PPI	MAPY PING			*		
AUD	พกคก	PĮ	n( / #/)	PL / MY F	DI /PTP	X/DHAX			
32	W(12-11	13.714	0.95947	0.34496	0.53816	0.72200			
27		14.571	1.1593	0.42153	0.61401	u. 82000			
47		18.241	1.2762	0.46401	0.67589	0.91900			
62		18.350	1.2838	0.46680	0. A 7905	1.0170			
>40	DITIONAL	PRESSURE	RATTOS , FLO	W SPEETTEP I	•n•	- 275 ; - He within though the Million region ( Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and August Manifestary and Augu			
AUP	พกคุก	PL	PL /P/)	PL /PTF	PL /PTP	X/DMAX	s will a to a reflex supples. Here a	rescourse (Pagachillaneae neur Maria servindaga), e como recordo o servinda	ge at this manage spirit, the additional magnification in additional spirits and spirits a text
62		18.275	1.2786	0.46490	0.67718	0.42200			
67		14. 347	1.0738	0.36407	0.53143	0.67000			,
>41	TITIONAL	PRESSURE	PATINS , FIR	W SPLITTER C	.n.				
AVD	MUBD	Pl	PL /PG	Pt /PTF	PL /PTP	X/DMAX	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa		an annual derivatives, and the appropriate property and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
77		9-1958	0.64337	0.23393	0.34074	0.50800			The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s
82		19.218	1-3445	0.48886	0.71709	0.58300			
92		14-243	0.99645	0.36231	0.52175_	<u>u_67000</u>			
-	91719MA	PRESSURE	441196 v E46	CTOP SHPOUD		The second second second second second	e i a an mar an ann an an an an an an an an an an an		**************************************
AVD	MORD	T-	PL/PG	PL/PTF	PLERTY	X/0MAX			
-101		14.183	D. 99276	0.36039	0.52553	-1-0000			
		14-179	0.99191	2.36066	0.52534	-1-0000			
-127		14.183	2-4-226	0-36070	0.52552	-1.0000			
-127		14.223-	0. 99505	9.36177	0.52701	-1.0000		·	
-137		14.723	0.99505	0.36183	0.32701	-1.0000			
تهلت		14.203	. 0.99366	0.36129	0.52627	1_0000			
>A1	JAMOLTIC	PRESSURE	RATIOS . FCR	ERODY INLET					
AVD	HURD	PL	PL/P0	PL/PTF .	PL/PTP	X/DMAX.	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t	pathology the party of the control of the party of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of	ngang, American phagasana makana dhay a .
107		14.187	0.99226	0.36079	0.52553	0.39800	•		
112		14-178	0.99191	9-36066 .	0.52534	J.43100			
127		14.183	0. 99326	0.36079	0.52553	0_44900			
12?		.14-223	0.99505	0.36180	0.52701_	0.48600			
127		14.223	0.99505	0.36180	0.52701	0.52200			
142		14.793	0. 99366	0.36129	0.52627	0.58800			
-1-4 -1-4		******	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		0:52868	-1.0000 -1.0000			
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		PL	PLZPO		PL/PTP	x/max			
-147				0.362A1	0.52848	-1.0000	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s		
-151	_	14.267	9, 99819		De52867	-1.0000			
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AVE	MUPD	Pt	PL/PO	PL/PYF	PL /PTP	x/max	. at a second second second second second		
167		14.262	0.99784	0.362P1	0.52848	J. 79300			
173		14.267	9-99619	0.36294	0.52967	0.84400	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		appalar sam, filmanasis as aga atap algas filipida del appalationne di les aprilationne del la compansión de l
>A5	DIT.IONAL	PRESSURE	RATIOS 80	DEG_SHROUD_L	OCATION				5
		PL	ቦኒ / PI)	PI /PTF	PI /PTP	X/DHAX	, more than the specimentary of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments of the speciments o	gare a magnitude pagner strategist was a ville	
182		13.305	0.930A7	0. 33846	0.49301	0. 79300			
187		13.290	0.92982	0.33808	0.49246	0.#4409			

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<b>งก พกจ</b> ก	PL	PT / PO	PL /PTF	PI /PTP	Y/DMAY					
32	13-255	3.92699	0.36992	0.53367	0-72200					
37	15.944	1.1150	0.44454	0.44190	0-62000					
47	17.333	1.2119	9.48363	0.65772	0.91900					
<b>-</b> 2	17.455	1.7207	0.48711	0.70774	1-0170					
APPIT INNA	PRESSIPE	PATINS . FLO	W SPEETFF	.0.						
VO WORD	PL	PI /PI	PL /PTF	PI /PTP	X/PMAK	4.5			e de la primario del Arib de deservolución del este como la	
62	16-911	1.1757	0.46916	C. 67684	9-42200					
67	13.260	0.92734	9. 37006	0.53387	0.67000					
APPRITTORA	PRESSURE	RATIOS . FLO	W SPLITTED I	'. D.						
VO WOPD	Pt	PL /PO	PI /PTF	PI /PTP	4/DMAX				-	
77	6.1362	0.56900	9-22706	0.32757	0.50800					
R2	29.581	1.4393	0.57437	0.82862	0.58309					
92	14-258	0-99711	2.39790	0-5.7403	0-67000					
10017 INNA	L PRESSURE	<del>8475-y-E</del> t	CTCP SHACUP	<del></del>						
YO WORD	76-	PL/P0	PL/PTF	PLANTE	X/DPAX					
197	14.198	0.99292	0.39625	0.57162	-1.0000					
112	14.193	7-90197	-0.395PL	0.57102	-1-0000					
127	14.193	0-99787	D.39581	7.57172	-1-9000					
127	14.218	0.99432	0.39679	0.57243	-1.0000					
	15.198	0.99292	0. 39623	0.57162	-1-0000		•			
152	14-199	0.99292	0.39623	0.57162	-1.0000					
PAUDITICAN	PRESSURE	PATIOS . FCP	ENDON IMPLEA							
AG MUMB	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX					
197	14.198	0.99292	0.39623	9.57162	0.39800		•			
112	14-183	0.99187	0.39581	0.57102	J-43107					
127	14.153	0.99187	0.39581	0.57102	0.44960					
127	14.219	0. 99 432	0.29679	<u> </u>	0-48600	· · · · · · · · · · · · · · · · · · ·				
127	14.199	9-99292	9.39623	0.57162	J. 522 <b>0</b> 0					
142	14.198	0. 99292	0.39623	0.57162	0-58800					
	14:279	7.99780 7.99815	<del></del>		-1-0000					
_		847103Fat	_							
AL RUND			PL/PTF							
yr: ₩(1721) [47	14.268-	PL/PN	0.39818	PI /PTP 0.57444	X/D#AX				<del></del>	
L57	14.273	n. 99915	7.39832	0.57464	-1.0000 -1.0000					
>4001T_[@ <b>9</b> 41		PATIOS 20	DEG SHRAUA 1							
Au Mubb	Pt	PI / PO	PL/PTF	PL /PTP	X/DMAX					
167	14.273	2.99415	0.39#32	0.57464	0.79300	· · · · · · · · · · · · · · · · · · ·				
72	14.273	0.99815	0.39437	0.57464	J. 64400		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			
APPIT TOMAL	PRESSIPE	PATINS, , RO	NEG SHRPUN 1	PEATION						
	Pl	PL / PO	PI / PTF	PI /PTP	X/DMAX					
182	13.300	7. 93013	C-37117		7-79300					
176 197	13.760	7. 93013	7.37776	C.53548						
		THPUST PARAM		C.533P7	. 7, 84400					
	FIC	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s								

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AU MUBU	Pt	PI / PI?	PI /PTF	of /PTP	TAPA						_
32	14.276	0.99757	0.47154	0-67444	9.72290						
37	15.876	1.1094	0.52449	0.75004	0.82000		•		*** *** * **	***************************************	
67	16.275	1.1334	2.53592	0.76652	2. 91900						
<b>~</b> 2	14.239	1.1341	0.57604	C.75675	1.3170						
> 4 7 7 7 7 7 7 10 44	al pressire	PATIOS . FIG	W SPI ITTEP	I.D.			_				
UN WORD	P1	<b>ም</b> ( /ምበ	PI /PTF	PL /PTP	x/fmax						
62	15.557	1.0071	0.51386	0.73496	J.42200		and the second of the second of the second of				
47	14.486	1.0122	3.47846	0.68433	3-67000	~					
WOITEGAL	L PRESSURF	PATINS . FLO	W SPI 177ER 1	.n.			<del></del>				
40 40PD	PI	Pt /P0	M /PTF	PI /PTP	Y/DMAX						
17	12-407	0-86693	0_40979	0.58612	0.50800						
A2	16.799	1.1738	0.55485	0.79360	0.58300						
92	16-271	0.99722	0.47138	0-67621	0.47000						
M201710W	<del>N. PRESSURS.</del>	- <del> </del>	CTO SIMBLE			Name and Associated States of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Co					
-	Please	PL/PD	PL/PTF	PLANTE	X/DMAX					<del></del>	
197	14.235	0.99478	0.47023	0.67256	-1.0000						
112	16-236	200478	1.47023	D-67256	-1.0000						
122	14.236	2-49471	0.47923	0.67256	-1.0000						
127	14.256	0.99617	0.0000	0.67350	-1.0000			·			
137	75. 731	0. 99443	0.47006	0.67232	-1.0000						
	14.197										
المستحكا		0.99199	9.46 <b>89</b> L	0.67068	-1.9000	e i u u u managara samagara					
5433111 <u>04</u> 4	IL PRESSURE	PATIOSEOP	ERODY INLEY								
AU MUNU SEJJIIJAN	IL PRESSURE	PATIOS FOR	ERCOY IMLET	PL/PTP	.X/DMAX						-
<u>PEDDITION</u> VD WORD 197	PL 14.236	PATIOS_+_EOP PL/PO 0.99478	PL/PTF 0.47023	PL/PTP 0.67256	X/DMAX 0.39R00						-
<u>&gt;£99171996</u> VD WORD 197 112	PL 14-236 14-236	PATIOS FOP PL/PO 0. 99478 2.99478	PL/PTF 0.47023 0.47023	PL/PTP 0.67256 0.67256	X/DMAX 0.39800 0.43120						-
>£99171996 VD WORD 197 112 17?	PL 14.236 14.236 14.236	PATIOS - FOP PL/PO 0.99478 2.99478 0.59478	PL/PTF 0.47023 0.47023 0.47023	PL/PTP 0-67256 0-67256 0-67256	X/DMAX 0.39800 0.43199 0.44900		•				
2622111236 VD WORD 137 112 127 127	PL 14.236 14.236 14.236 14.236	PATIOS . FOP M./PO O. 99478 2. 99478 O. 59478 O. 59417	PL/PTF 0.47023 0.47023 0.47023 0.47023	PL/PTP 0.67256 0.67256 0.67256 0.67256	X/DMAX 0.39800 0.43199 0.44900 0.46800						-
020017109M VD WORD 107 112 127 127	PL 14.236 14.236 14.236 14.236 14.236	PATIOS . FOP PL/PO O. 99478 O. 99478 O. 99478 O. 99417 O. 99443	PL/PT= 0.47023 0.47023 0.47023 0.47023 0.47023 0.47006	PL/PTP 0.67256 0.67256 0.67256 0.67250 0.67232	X/DMAX 0.39R00 0.43100 0.44800 0.52200		•				
2279171096 vn worn 197 112 127 127 137	PL 14.236 14.236 14.236 14.236 14.236 14.231 14.197	PATIOS FOP PL/PO O. 99478 2. 99478 O. 59478 99417 O. 99443 O. 99199	PL/PT 0.47023 0.47023 0.47023 0.47023 0.47023 0.47026 0.46891	PL/PTP 0.67256 0.67256 0.67256 0.67256 0.67232 0.67232	X/DMAX 0.39000 0.43199 0.44900 0.4660 0.52200 0.58800						-
227	PL 14.236 14.236 14.236 14.236 14.236	PATIOS . FOP PL/PO O. 99478 O. 99478 O. 99478 O. 99417 O. 99443	PL/PT= 0.47023 0.47023 0.47023 0.47023 0.47023 0.47006	PL/PTP 0.67256 0.67256 0.67256 0.67250 0.67232	X/DMAX 0.39R00 0.43100 0.44800 0.52200		•				
2200171090 10 WORD 107 112 127 127 137 42 159	PL 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.290	PATIOS FOP PL/PO O. 99478 2.99478 O. 99478 O. 99473 O. 99443 O. 99199 2.99070	PL/PT 9. 47023 0. 47023 0. 47023 0. 47023 0. 47009 0. 46891 7. 47107	PL/PTP 0.67256 0.67256 0.67256 0.67256 0.67232 0.67068	X/DMAX 0.34400 0.43120 0.44900 0.52200 0.52200 0.58800						
VD WORD 197 112 127 127 137 142 142	PL 14.236 14.236 14.236 14.236 14.256 14.231 14.197 14.290 14.290	PATIOS EOP PL/PO 0. 99478 2.99478 0.99478 0.99478 0.99478 0.9917 0.9919 2.99870 2.99870	PL/PT 0. 47023 0. 47023 0. 47023 0. 47023 0. 47004 0. 46891 0. 46891 0. 47107 0. 47107 0. 47107	PL/PTP 0.67256 0.67256 0.67256 0.67250 0.67232 0.67068 7.87491	X/DMAN 0.34R00 0.43190 0.44490 0.52200 0.58800 0.58800						
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VD WOWD 197 112 127 127 127 127 137 142 159	PL 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.299 14.299	PATIOS EOP PL/PO 0. 99478 2.99478 0.99478 0.99478 0.99478 0.9917 0.9919 2.99870 2.99870	PL/PT 0. 47023 0. 47023 0. 47023 0. 47023 0. 47004 0. 46891 0. 46891 0. 47107 0. 47107 0. 47107	PL/PTP 0.67256 0.67256 0.67256 0.67256 0.67232 0.67068 7.87491 0.67491	X/DMAX 0.39808 0.43109 0.44800 0.52200 0.58800 -1.7008 -21008 X/DMAX -1.0000						
VD WORD 107 112 127 127 137 142 142 142 143 144 147 147 147 147 147 147 147 147 147	PL 14.236 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.290 PL 14.290 PL 14.296	PATIOS FOP  PL/PO 0. 99478 2.99478 0.99478 0.99478 0.99478 0.99479 2.9979 2.9979 2.9979 2.9979 2.9979	PL/PTF 0. 47023 0. 47023 0. 47023 0. 47023 0. 47023 0. 47029 0. 47006 0. 46891 0. 47107 PL/PTF 0. 47187 0. 47187	PL/PTP 0.67256 0.67256 0.67256 0.67250 0.67232 0.67068 7.07091 0.67491 0.67491 0.67491	X/DMAX 0.39R00 0.43190 0.44900 0.52200 0.58000 1.77000						
VD WORD 197 197 122 127 137 142 147 147 147 149 159 159 169 169	PL 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.290 14.290 14.290 14.290 14.296 15.296	PATIOS . FOP  PL/PO 0. 99478 2.99478 0.59478 0.99617 0.99617 0.99617 0.99617 0.99617 0.99199 2.99076 2.99076 2.99076 0.99076 0.99076 PATIOS . 20	PL/PTF 0.47023 0.47023 0.47023 0.47023 0.47006 0.46891 0.47107 PL/PTF 0.47187 0.47187	PL/PTP 0.67256 0.67256 0.67256 0.67256 0.67232 0.67068 0.67291 0.67491 0.67491 0.67491	X/DMAX 0.39R00 0.43100 0.44800 0.52200 0.58800 1.7000 1.7000 1.0000						
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VD WORD 107 112 127 137 142 142 142 157 VD WORD 157 VD WORD 167	PL 14.236 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.290 PL 14.290 PL 14.296 PL 14.296 PL 14.296	PATIOS FOP  PL/PO 0. 99478 2.99478 0.99478 0.99478 0.99478 0.99479 2.99872 PATIOS FAM PO 0: 99826  PATIOS 20 PL/PO 0. 99826	PL/PTF 0.47023 0.47023 0.47023 0.47023 0.47023 0.47006 0.46291 0.47007 PL/PTF 0.47187  PL/PTF 0.47187	PL/PTP 0.67756 0.67256 0.67256 0.67250 0.67232 0.67232 0.67232 0.67232 0.67491 0.67491 0.67491	X/DMAX 0.34R00 0.43190 0.44490 0.52200 0.52200 0.58800 -1.77700 -1.77700 -1.0000 -1.0000						
VD WORD 197 197 197 197 197 197 199 199 199 199	PL 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.290 14.290 PL 14.290 14.290 PL 14.296 14.296 14.296	PATIOS EOP  PL/PO 0. 99478 2.99478 0.99478 0.99417 0.49443 0.99199 2.99070 2.99070 PATIOS EOP PL/PO 0.99826 PATIOS 20 PL/PO	PL/PTF  0. 47023 0. 47023 0. 47023 0. 47026 0. 47026 0. 47026 0. 47027 0. 47187 0. 47187 0. 47187 0. 47187	PL/PTP 0.67256 0.67256 0.67256 0.67256 0.67232 0.67068 7:07041 0:07491 0:67491 0:67491	X/DMAN 0.39800 0.43100 0.44900 0.52200 0.5800 0.5800 -1.7000 -1.0000 -1.0000						
VD WORD 197 197 112 127 137 142 147 147 147 157 VD WOPD 167 167	PL 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.290 14.290 14.296 14.296 14.296 14.296	PATIOS FOP  PL/PO 0. 99478 2.99478 0.99478 0.99478 0.99478 0.99479 2.99872 PATIOS FAM PO 0: 99826  PATIOS 20 PL/PO 0. 99826	PL/PTF 0. 47023 0. 47023 0. 47023 0. 47026 0. 47006 0. 46891 0. 47187 0. 47187 0. 47187 0. 47187	PL/PTP 0.67256 0.67256 0.67256 0.67256 0.67252 0.67068 7:07091 0.67491 0.67491 0.67491 0.67491	X/DMAX 0.34R00 0.43190 0.44490 0.52200 0.52200 0.58800 -1.77700 -1.77700 -1.0000 -1.0000						
VD WORD 197 197 112 127 137 142 147 147 147 157 VD WOPD 167 167	PL 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.290 14.290 14.296 14.296 14.296 14.296	PATIOS FOP  PL/PO 0. 99478 2.99478 0.99478 0.99478 0.99617 0.99199 2.99776 2.99776 0.99826  PATIOS 20 PL/PO 0.99826 0.99826	PL/PTF 0. 47023 0. 47023 0. 47023 0. 47026 0. 47006 0. 46891 0. 47187 0. 47187 0. 47187 0. 47187	PL/PTP 0.67256 0.67256 0.67256 0.67256 0.67252 0.67068 7:07091 0.67491 0.67491 0.67491 0.67491	X/DMAX 0.39R00 0.43199 0.44900 0.52200 0.58000 1.7000 120000 1.7000 1.0000 1.0000 1.0000						
VO WORD 107 112 127 137 142 142 157 26017 1046 VO WORD 157 26017 1046 VO WORD 167 172	PL 14.236 14.236 14.236 14.236 14.236 14.236 14.231 14.197 14.290 PL 14.296 14.296 PL PRESSURE	PATIOS FOP  PL/PO 0. 99478 2.99478 0.99478 0.99478 0.99478 0.99478 0.99479 2.99702 PATIOS FAM 0.99199 0.99702 PATIOS ZO PL/PO 0.99826 PATIOS ZO PL/PO 0.99826 PATIOS ZO PL/PO 0.99826 PATIOS RO PATIOS RO PATIOS RO PATIOS RO PATIOS RO PATIOS RO PATIOS RO PATIOS RO PATIOS RO PATIOS RO	PL/PTF  0.47023 0.47023 0.47023 0.47023 0.47023 0.47006 0.46291 0.47107  PL/PTF 0.47187 0.47187 0.47187 0.47187 0.47187 0.47187 0.47187	PL/PTP 0.67756 0.67256 0.67256 0.67256 0.67250 0.67232 0.67068 0.67068 0.67068 0.67491 0.67491 0.67491 0.67491 0.67491	X/DMAX 0.39R00 0.43190 0.44490 0.52200 0.58800 1.7900 119000 119000 1.0000 X/DMAX 0.79300 0.84490						
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2	14.557	1.0160	0.56023	0.81152	J. 72200					
3 <del>7</del>	15.225	1.0626	0.58594	0.84776	0.82000			and the same and the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract		
67	15.365	1.0723	0.59131	0-25654	3.91900					
52	15.760	1.0729	7.59112	0.85626	1.0170		* 19 max			
	غربيب مامورت النالية مستقاله ، م <u>يمين .</u> .				1.01/0					
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AU MUMU	PL	P) / P1)	PL/PTF	PL/PTP	X/DMAX					
2	15.036	1.0494	9-57865	0.93820	0.42200					
7	14.717	1.0271	0.56677	0. #2741	0.67000	• • • • • • • • • • • • • • • • • • • •	** ***********************************		the second district the second second second second second second second second second second second second se	
PETT TON	AL PRESSIPE	PATINS , FLI	TW SPLITTER	7. D.						
משחש מע	PL	PL/PO	PL/PTF	PI /PTP	X/NMAX	بهدانه والمرادات				
77	12.613	0. 88026	9-49540	0.70312	0.50800					
7	16.083	1.1224	0.41894	0.89656	0.50300		· · · · · · · · · · · · · · · · · · ·			,
2	14.273	0.99614	9.54930	0.79560	2.67000	······································				
	<del>at parssure</del>	<del>*************************************</del>	tere surnun							
D HOPP	PL	. PL/PO.	PL/PTF.	PLANTE	X/DMAX					
07	14.243	99405	0-54814	0. 79401	-1.0000					
112	14.243	2.99402	7.55014	0.79401	-1.0000					
122	14. 239	0.44373	0.44.795	0.79373	-1-0000	<del></del>			<del></del>	
127		2.99474	0.54853	79457						
	14.252				1.0000	The second second second second				
137	14.233	0.99335	9.54776	4.10	-1.0000					
سسمه	14, 203	9. 99127		0.79179	-130000					
MOTTION	AL PRESSURE	RATIOS . FOR	ERTTY INLEY	<del></del>				·		
IN WARD	PL	PL/PN	PI /PTF	PL/PTP	X/DMAX					
107	14.243	0.99405	2.54814	0.79401	0.39800			·		
112	14.243	0.99405	0.54814	0.79401	J. 43100		•			
127	14.239	0.99370	03 54795	0.79373	2.44902	· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·		
27	14.253	<u></u>	0.54 <u>953</u>	<u> </u>	0,48600		<del></del>			
137	14.233	2,79335	9.54776	0.79346	0.52200					
47	14.203	2.99127	0.54661	0,79179	D. 5 8800					
\&\$			7.94987	0,79651	-1-0000					
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/D 4080			MARKET SET SET	PI /PTP						
	PL	7-77-18	0.54987		XAMONY					<b></b>
152	14.280			0.79651	-1,0000					
L57	14. 2AR	J. 997] 9	7,64987	0.79651	-1.0000					
MUITIOCE	AL_PRESSURE	PATTINS 20	UEC SHOUNT	DEATION						
מפחצ מו	PL	PL/PR	PI /PTF	PL /PTP	Y/DMAX					
	14.283	0.996#3	0.54668	0.79623	0.79300					
167	14.293	0.99683	0.54969	0.79673	0.84400					
167 172		PATINS . PO	DEG SHPOUD L	CCATION					····	
172	AL PPESSURF									
172 •409 [T ] <b>0%</b>	AL PPESSURE. Pi	PL / PO	PI /PTF	PL /PTP	X/DMVX					
172	PI	PL / PO 0 - 94 360	PI /PTF 0-52032		X/DMAX 079300				· ,	
i72 Maattinn Yn unpn i•2	PI 13,520	7. 94 3KD	0.52032	0.75371	0.79300	· · . • • · · · · · · · · · · · · · · ·	e a company array on assume transference of the con-	in allemants the large absorption and the site of the site of	er agent og en en en en en en en en en en en en en	
172 >ADD [T [MN VM WMPN 192 187	PI 13.520 13.416		0.52032 0.51629			V VIII A MARKET ON A TAK THE MICH				

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		COPOLTI	ONS			TAKEDE												
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	2.937	1.45	1.31		0.000						0.9631				-			
-	0.008				0.030						0.9622							
440	0.021	1.69	2-11	1.25	0.000	0.471	0.968	1.091	0.9556	0.9556	0.9556	0.9556	0.9594	*****				
	9-927		2.50								0.9322				• •		_	
	0.043		3.11 3.60		0.000						0.9332 0.9436							•
	0.00		4.20		0.000						0.9452							Many order is the second
445	2-057	1.70	4.19	2.47	0.000	0.241	0.969	0-981	0.9456	0.9456	0.9456	.0.9556	0.9475.	-				
	1.054		3.61		9.000						0.9431							
	0.054		3.10 2.76		0.000						) 0.929 <u>1</u>   0.9288						* *	<b>→</b> → ·-
	3.952		2.76								0.9291							
	0.027		2.49		0.900						0.9377							
	0 <u>052</u>		<u>2.12</u> 1.79		0.000						0.9558							<del></del>
	9.051			1.63							0.4301							
454	0.041	1.70	3.59	2-11	0.000						0.9425							
	0.023				9.000						0.9557							\$
	0.031	1.43	2.12 2.51		0.000						0.9536 L.D.9358							
	0.047		2.76		0.000						0.9323							
	0-0-1		3.11		0.000						0.9361				·			
	0.062		3.60 4.18		0.000						0.9439 0.9459							
	0.055		7.17		0.000						0.9458							
	0.050		3.60		0.000						0.9435							
	9.041		3-11		0.000						0.9328							
	9.045		2.76 2.51		0.300						7 <b>0.</b> 5328 1 0.9378				**			S
467	0.006	1.43	2-11	1.47	0.000	0.470	0.966	1,023	0.9571	0.9571	0,9571	0.9571	0.9610	*****				a 1.
	2.019	• • • •	1.01		0.000						0.9573							
	<u>7.359</u> 0.364		1.91 2.10		0.000						<u>_0.9120</u> 0.9265							
	0.366		2.50		0.000						0.915R							and meaning again to the
472	0.371	1.70	2.76	1.62	0.000	0.362	0.968	0.990	0.9106	0.9106	0.9117	0.9117	0.9147	*****				
-	9.372		3.11		0.077						0.9122							•
	0.769		3.61 3.97		0.000						0.9320 0.9348							
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76 0.354	1.71	3.07		0.000						0.9356	0.9356	0.9375	*****		•		
77 0-365	1.71	3.61	2.11	0-002	0-278	9.963	2.266	Q- 9360	9-9369	0-9367	9-2367	8.2362	*****				
	1.71			0.200						0.9142							
	1.70			0, 022						0.9124							
#0 7.362	1.70	2.51		0.000						0.9151							
MI 0,363		. 2-11_		0,000						0.9237							
42 9.361 82 9.358	1.70	1.82		0.000						0.9103							
84 0.367	1.43			0.000						0.9783							
	1.47		1.77							0.9205							
	1.48		1.86							0.9206						en i Mercander i s	2 · · · · <del>· · ·</del> · · ·
M7 0.360	1-44	3,12	2.11	0.000	0.319	0.968	0.979	0.9179	0,9179	0.9187	0-9197	0.4213	*****				
88 0.364	1.45		2.49							7-9366							
689 <u>0. 366</u>	1.46		2.67							0.9376							
9 9.364	1.46		2-68							0.9412							
91 0,367	1.45		2,44	0,000						0.9425							-
	1.48		1.07							0.9724							
- 7	1.46			0.000						0.9193							
95 0.358	1.43			0.000						0.5319							
	1.45	1.61	1.25	0.100	0.556	3.965	1.006	0. 9295	0.9295	0.9315	0.9315	0.9348	*****				
	1.45			0.000						0.9245							
98 0.354	1.70	1.92	1.07	0. 723	0. 553	0.965	1.037	0.9115	0.9115	0.7138	0.4178	0.9150	*****				
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22 37 57 52 50 67 52 67 54 67 77 77 77 72 92	12.868 13.417 14.277 14.441 PRESSUPE 13.687 13.093 PRESSURE 12.064 15.570	0.90009 0.97345 0.99869 1.0136 RATERS , FLO M /PR 0.95738 0.91580 PATERS , FLO PL /PR 0.84383 1.0891 2.99860	0.49673 0.5721 0.55109 0.55938 W SPLITTED T PL/PTE 0.50540 W SPLITTED C PL/PTE 0.46569 0.60102	Q.72254 Q.70144 C.82163 Q.81369 .n. P1 /PTP Q.76954 Q.73516 .n. PL/PTP Q.67739	9.72200 0.82000 0.91900 1.0170 x/nmax 0.42200 0.67000					
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ADDITIONAL  ADDITIONAL  ADDITIONAL  ADDITIONAL  ADDITIONAL	14-277 14-491 PRESSUPE 13-607 13-093 PRESSURE 12-064 15-570	0.99869 1.0136 RATIOS , FLO M /PO 0.95738 J.91590 RATIOS , FLO PL/PO 0.84383 1.0991 2.99860	9.55109 7.55938 W SPLITTEP T P1/PTF 9.52834 0.50540 W SPLITTEP C PL/PTF 9.46569 0.60102	C.#2163 0.#1369 .n. PI /PTP 0.76954 0.73516 .n. PL/PTP 0.67739	0.91900 1.0170 */DMAX 0.42200 0.67000					
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ADDITIONAL	13.607 13.093 PRESSURE 12.064 15.570	M /PO 0.95738 J.91590 PATEOS , FLO PL/PO 0.84383 1.0991 J.99860	P1 /PTF 9.52834 0.50540 W SPLITTEP C PL/PTF 9.46569 0.60102	PI /PTP 0.76954 0.73516 .n. PL/PTP 0.67739	0.42200 0.67000					
SE SE SE SE SE SE SE SE SE SE SE SE SE S	13.687 13.093 PRESSURE 12.064 15.570	0.95738 J.91590 PATENS , FLO PL/PN 0.84383 1.0891 2.99860	9.52834 0.50540 M SPLITTEP C PL/PTF 0.46569 0.60102	0.76954 0.73516 .n. PL/PTP 0.67739	0.42200 0.67000					
ANDER IONAL	13.093 PRESSURE 12.064 15.570	0.91590 PATEOS - FLO PL/PD 0.84383 1.0991 2.99860	0.50540 W SPLITTEP C PL/PTF 0.46569 0.60102	0.73516 .n. PL/PTP Q.67739	3.67000 #/DMAX					
PARTET TONAL  OF WHERE  OF PARTET TONAL  ADDLESONAL	PRESSURE 12.064 15.570 14.277	PATENS , FLO PL/PN 0.84383 1.0891 2.99860	PL/PTF 0.46569 0.60102	PL/PTP 0.67739	Y/DMAX					t minimum in the
70 4990 P 77 92 92 94301710941	12.064 15.570 14.277	M /PN 0.84383 1.0991 2.99860	PL/PTF 0.46569 0.60102	PL/PTP 0.67739						
ADDLESOMAL	12-064 15-570 14-277	0.44383 1.0991 2.99860	0-46569	0.67739						* ****
77 92 92 PADDLEHOMAL	12-064 15-570 14-277	1.0991 2.99860	0.60102	0.67739						
ADDLI IONAL	15.570 15.277	1.0991 2.99860	0.60102		0.50000			-		
ADDLE IONAL	14.277		0.55100	0.87425	0.58300					
	DESCURE.	847105 FAF		0.50163	0.67009					
	_		CTCD SIMOUR							
D MURD	1	FL/PD	PL/PTF	PLOTE	X/DHAX					
	14.232	0.99546	0.54936	0.79910	-1.0000	and the second control of the paper of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the second control of the s				
	14.222	3.99476	4.097	0.79654	-1.0000					
22	14.222	0-90475	0	0.79854	-1.0070					
	14.227	0.99511	0.54917	29892	-1,0000					
	44.142	0. 99 196	0. 54743	0. 79470	-1.0000					
52	14.057	0.94323	0.54261	0.76929	1.77999					
ANDITIONAL	PPESSIRE	RATIOS . FOP	ENCOY IN ET							
ID WORD P	PL .	PL/PG	PL/PTF	PL/PTP	X/04AX					
	14.272	0. 99546	0.54036	0.79910	0.39800		•			
	14.222	0.99476	0.54897	0.79854	3,43100					
22	14.222	0.99476	0.54897	0.79854	0.44900					
27	14.227	0-99511	_0.54917_	0.79882	0.48600					
	14.192	7.90106	0.54743	0.79639	7.52200					
	14-057	9.98323	0.54261	0.78929	0.58800					
	14,343	<del></del>	<del></del>	<del></del>	-1:0000					
				484.35.38.	- 60 0000					
		PATENCE EAN	MOZZLE ELAB							<del></del>
ID HUBD BI		77.400	- Report	PI /PTP	X/DMAX					
	15.282	7, 99895	4-4430	0.50191	-1.0000			•		
,	14.292	7.99895	0.55129	1	-1.0000			ilia -a simulatako musika 1997 -ariiliako (h. 1991)		
TOWNET TOWNS	PRESSIME	PATINS . 20 !	NEG SHPMUN L	OCATIO:				<u> </u>		
ID MUSEU BI		2/27	PI / PTF	PL/PTP	X/DMAX		a standard or compression			
	14.787	2, 99895	7.54129	0.90191	0.79300					
172	14.292	7,99895	0.55129	9.89191	O. 84400					
ADDITIONAL	PRESSIPE	PATIOS 40 (	neg s <del>iprun</del> i	ucatton						
n warn p		PE / PFI	M /PTF	PL /PTP	ZAMON F	_				
107	13.697	0.95808	0.52973	0.76910	0.79300					
187	13.412	0.95214 THRIST PARAM	7. 52545	0.76433	0. 84400			- we	and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th	

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VASA-LEWIS	PPFLIMI	NERT DATA	06/13/79	CARPETT	PEC 10/24/7	79 27:30:50.912	FAC AKAKE	PG# 1934	RUN24	
ልባባያ T ያቦባል!	PRESSUPE	PATENS . PPE	MAPY PLUG					. accept	y nagan na y amin'ny sara anana	
ID WERD	Pt -	<b>የ[ / P</b> ቦ	Pt /PTF	PL /PTP	Y/DMAX			<del></del>		
32	13.533	0.94588	0.52309	0.88505	0.72200					
17	13.033	J. 97392	0.53 454	0.91119	0.82000					
67	14-102	0.98569	0.54511	0.92230	0. 91 900					
52	14.197	0.99232	0.54878	0.07841	1.0170					
ADD IT TONAL	PRESSURE	PATINS , FLE	W SPI ITTER I	.n.						
n was	PL	የኒ/ቀበ	PL /PTF	PL/PTP	Y/DMAY					
52	13.710	0. 95 880	0. 53024	0.89714	0.42200					
7	13.578	0.94902	0.52483	0.89799	0.67000					
AND IT INNA	PPESSUPE	PATENS . FLO	W SPLITTEP F	`. n.						
rn wnen	PI	PL / PO	PL / PTF	P1 /PTP	X/NMAX					~ -
77	12.119	0.84704	. 0.46843	0.79257	0.50800					
	15.671	1.0904	0.60304	1.0293	0.58300			······································		
92	14.277	0.99791	0-55187	0.93374	0.57000					
								-		
AODITIONAL	PRESSURE	PATIOS . EJE	CTOP-SH-BUD							
D WORD	AL.	PL/PO	PL/PTF	PLAPTIF	X/DMAX					
197	14.252	0.99617	0.55000	0.93211	-1.0000					
112	16.237	799512		9-53112	-1-9000					
127	14.232	0.44477	9 55013	0.930PO	-1.0000					
127	14.252	0.99547	0.55051	0.93145	-1.0000					
137	14.062	0.99232 0.99290	0.54878 0.54356	0.91969	-1.0000 -1.0000					
152				06 71 76 7						
		RATIOS . FOR					•			
OSON CV	PL	PL/PO	PL/PTF	PL/PTP	X/DMAX					
107	14.252	0.99617	0.55090	0.93211	0.39800		•			
112	14.237	0.99512	0- 55032	0.93112	0.43100					
172	14-232	0.99477	0.55013	0.93040	0.44900					
127 137	14242 14.197	<u>0.99547</u> 0.99232	0.54878	<u>0</u> _93145 0_92851	0 <u>-48600</u> 2-52200		·······			
42	14.762	0.98290	0.54356	0.91569	0.58800					
52	14.702			0.76767						
£2	14-247									<u></u>
TADITION!	- POESCUPE	*** <del>**********************************</del>	-W-221							
n when	PL	PL/PD		PL/PTP	x/DMAX					
5.7	14.292	7. 941146	0.55744	0.93472	-1.0000					
57	14.787	0.99861	0.55225	0.93439	-1.0000	• • • • • • • • • • • • • • • • • • • •				
	L.PPESSURE	PATIOS . 20	nes sippun l	ULATION				<u> </u>		
ID WORD	PI	ሚ/ምብ	M \use	ol /PTP	X/DMAX				_	
167	14.292	0. 99996	7.55244	0.03472	0.79300					
72	14.292	6. 99896	0. 55244	0.53472	0.84400					
AND TECHA	PRESSIME	PATINS . PO	DEG SIMPUN_L	CCATION				*		
rn ween	PĮ	PL / PO	PL /PTF	PI /PTP	X/DMAX					
LA2	13.683	0,45635	0.52888	0.49485	0.79300					
			0.52599		0-84400					
P7	13.608	0.95112	11-2/244	0.88995	ひょうサランス・					

		<b>8854 I</b> W		0	cappet	nec 10434470	**********			RUN24	
	-I FWIS	_	[HARY DATA   PATIOS   PRI	76/17/79	Capueli	KFC 10/24/14	27: 17: 34. 700	FAC 9x6v1	PG4 C034	97G 1448	
AVD M	ukl	PL	Pt /PD	PI /PTF	PI /PTP	X/RMAX					•
32		12.558	0.87833	0.41706	0.70303 0.77234	0 <b>.</b> 72200 0. 82000		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o			
37		17.807	0.9649 <i>2</i> 0.99530	0.45814 0.47260	0.79665	0.91900					
47 57		14.242 14.496	1.0124	7.49377	0.A1035	1.0170			·		
>#07	IT IONAL		PATINS . FLE	W SPILITTER I	- 0-						
					-				resident and the second second	processing and released and pure money readings.	
AVD M	(1m)	PL	PL / PG	PL /PTF	PI /PTP	X/D9AX					
62		13.452	0.94013	0.44641	0.75250	J.42200					• • •
67		12.708	0.58811	0.42170	0.71046	0.67000					
>477	11 IUAT	PPESSIPE	PATINS . FLO	M SPLITTER C	.0.						•
AVO W	(Let)	PL	ML / PN	PL /PTF	PL /P TP	K/DMAY		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of the Commence of th	
77		11.719	0. 51897	0.38897	0-65552	0.50000					
92		16.499	1.1531	0. 54 753	0.92295	0.58300					
92_		14.272	0.99739	0.47359	0.79823	0.67800					
_>400	<del>17 PMAL</del>	<del>or regure</del>	*******	CTOR SHROUD				and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t	Marin Allen andre at the second and the second		
					21 /2 32						
W CVA	ORD .	14.272	~L/P0	PL/PTF 0.47194	el com	X/DMAX		· · · · · · · · · · · · · · · · · · ·	······································		
-107		14.212	0.99390	- 37161	0.79554	-1.0000 -1.0000		-			-
<u>-112</u> -122		14.207	0.90305	- 47144	0.79470	-1.0000	······································				
-127		14.222	0.99390	0.41	0, 79554	-1.0000					
-137		14.187	0.99006	0.47011	3.77744	-1.0000					
-147_		14. 327	0. 98029	0.46547	0.78464	-170000					
>400	I T IOMAL	PRESSUPE	PATINS . FINE	FROOY INLET							
AVD W						~ /0m A 7					_
107	THE CO	PL 14.222	PL /PD 2.99390	PL /PYF 2.47194	PI /PTP 0.79554	X/DMAX 0.39800	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o				
112		14.212	0. 99320	0.47161	0.79498	0.43100					
122	•	14.207	0.99285	0.47144	0.79470	0.44900			<del></del>	<del></del>	•
127		14.222	0.99390	0-47194	0-79554	0.58600					_
137		14.167	0. 99006	0.47011	0.79246	0.52200		······································			
142		14.027	2.98229	0.46547	9.78464	0.56900					
ــققهـ		-14-242			-0.79680-						
-147-				<del></del>		-1-0000-				<del></del>	
- <del> </del>	<del>t s lowit</del>	vaccinac	AATING _ EAR	MOTTLE FLAS							
- AVD W	nen	rl	AL/PR	-	PLIPTP	x/DMAX					
-152		14.282	0. 99809	0.47393	0.79889	-1.0000					
-157		16.292	0, 99500	3.47103	0.79889	-1.0000					
•	T TOWAL	PRESSURE	PATINS . 20								
AVD W	nP fi	PL	PL/PR	PI /PTF	PI /PTP	X/DMAX					
167		14.292	2.99879	0.47393	0.79889	0.79300					
, 177		14.297	) <b>.</b> 99844	0.47409	0.79017	0.94400		According to the confidence of the	a unique minimigge como i a la determinação com son reporte temporar.		
_ >879	ET FONAL	PRESSURE	PATIOS . 40	DEG SHPOUD L	OCATION						
A WAU A	ጥምብ	Pl	PL /PO	PI /PTF	PI /PTP	X/DMAX					
182		13.602	7.953E L	0.45139	7.76055	0.79300					
197		13.507	0. 94307	0.44823	9.75557	0,84403				na i wasan wasan wasan wa	
			THRUST PAPAN								
16-31	477.44	FIC	479.47	CICMA IF 1.2	398 FT1	IPF-1, 7467K	ns# 0.31259A	LEM 0.0033830			

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>^03[7][04	AL PRESSIPE	PATIOS . PRI	MARY PLUG				received the second		
Au NuaD	Pl	PI / PO	PL/PTF	PI /PTP	X/DMAX				
32 .	5.9745	J. 41782	0.16731	0.28284	0.72200				
•	12.501	0.89522	0.35847	0.60601	3. 92000				
47	14.319	1.0014	0.40099	0.67790	J. 91900				
52	14.864	1.0395	0.41624	0.70367	1.0170				
MODIFICA		PATIOS . FLO	W SMITTER I						
					45500 6				
NU MUND	PL	PL /PI	PL/PTF	PL /PTP	Y/IMAX				
62 67	14.324 11.492	1.0018 0.80369	0.40113 0.3216?	0.67814 0.54405	0.4220 <u>0</u> 0.67 <b>00</b> 0		agent our comments of the comment		The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th
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10 40R0	PL	PL / PO	PI./PTF	PL/PTP	X/DMAX				
77	8.2790	0.57410	0.22988	0.38863	0.50800				ay and annual reports Militer relationships and a second
12	19.967	1.3964	0.55916	0.94579	3.58300				
2	14.244	0-99617	0.39859	0_67435_	0-67000				
<del>2001719</del> 4	ME-PRESSURE	++1105 y Est	STER SHROWS				. And the book is the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the		
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07	14.100	0. 99303	0.39762	0.67227	-1.0000				
12	14.189	D-40233	39735	0.47175	-1,0000				
22	14.194	0.901-4	0.39721	0.67151	-1.0000				
27	14.199	0.99303	2. 19263	0.67222	-1.0000				
37	11884	7.98919	0. 39609	0.06962	-1.0000				
42	14.039	0.98185	0.39316	0.66400	-1-0000				
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CROW O	PL	PL/PD	PL/PIF	PL/PTP	X/DPAX	n gamen a suma y garan i a i an			
07	14-199	0.99303	0.39763	0.67227	0.39007		•		
12	14-189	0.99233	0.39735	0.67175	0.43100	a a la companie de alam			
.22	14.194	0.99198	0.70721	0.67151	0-44908				
27	14-199	0.99303	2_39763	0.67222	0.586G0				
.37	14.144	0.98919	0.39609	0.66962	0-52200				
42	14.239	0.99105	0.39316	0.46466	0.58800				<del></del>
47					<del></del>				
	•	#4710GF4				·			
10 MORD	PL 740	4.40	7+38959	PL /PTP 0.67553	x/DMAX -1.0000		, the company was a second		
57	14.269	0.99722	0.39531	U.B. 1993					
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47	14.264	0.99757	0.39945	0.67530	·). 79300				
72	14.254	0.99757	0.39945	0.67539	0_84400		-		
ADDIT TON	AL PRESSURE	PATIOS . SO	DEG SHPOUD (	nratina					
O WOPD	PL	PL/PD	PI /OTF	PL /PTP	X/DMAX				
#2	17.550	0.94762	0.37945	0.64148	0. 79300			. <del></del>	
•	13.395	7.93679	0.37511	0.63415	J.84400				
97	19.400								

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משריף מי	PL	PL/PD	PL /PTF	PL /PTP	X/DMAX				
2	7. 7976	0-54554	0-17547	0-29755	0-72200				
7	13.167	0. 92116	7. 29629	0.50742	0.02000				
7	10.333	3.72299	0.23252	0.39428	0.91900				
2	15.495	1-0778	9.34667	J.58785	1.0170				and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
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n HUB i	<b>ુ</b>	PI /PO	PL / PTF	PI /PTP	X/NMAX			e	er grade entertremental and a consider
2	17.993	1.2589	0.42491	0.68661	U.42200				
7	14.981	1.0461	0.33711	0.57164	0.67000			The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	
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1 .	10.652	0.74527	9.23972	9.40648	0.50000				The decision of the second second second second second second second second second second second second second
2	14.946	1.0456	0.33632	0.57030	0.58300				
2	14.231	0. 99563	2. 32024	0.54304	0-67000	****	· · · · · · · · · · · · · · · · · · ·		
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7	14.171	2.29144	0.31.000	0.54075	-1.0000				
2	14-156	7.25.73	7.31256_	0.54018	-1.0000				· · · · · · · · · · · · · · · · · · ·
27	14.151	0.04374	11:31-265	0.53999	-1.0090				
27	14212	0.99179	0.21901	0.54094	-1.0000	and the transfer of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same o			
37	14.136	0. 99899	0.31011	U- RADO	1.0000				
٠	14,391	0.98514	0.31687	0.53732	32-1036				عداد بينيونينيوناك كالويييونين عاد
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AUNU .	PL	PL/PT	PI /PTF	PL/PTP	X/RHAX				
7	14.171	0.99144	0. 31 890	0.54075	0.39800		•		
2	14.156	0.99039	0. 31 856	0.54718	9.43100				
??	14.151	7.99004	0.31845	0.53999	J-44900				
??	14.176	0.99179	0-31901	0.54094	0.48600				
17	14.136	7.95599	7.31811	0.53941	2.52203				
•2	14.781	J. 98514	9.316P7	0.53732	3-58900				
52	14.254			0,54300_					
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esti lui		BATTITE FAR	-HPPTAE-FLAP						
HOPB	PL	- Trees		PL/PTP	X/DMAY				
	14-256		II. WOOL	0.56399	-1.0000				
37	14.761	0.99773	9.32092	0.40014	-1.9000	THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT THE COLUMN TWO IS NOT			
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HUBL	PL	PL/PO	PL/PTF	PL/PTP	X/MAX				
67	14-256	0. <del>99</del> 738	0.32081	0.54399	0.79300				
72	14.256	7.99738	0.32081	0.54399	J. 84400			ago, consistent or the energy processor, in the 4-1990	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
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		ŋ <b>.</b> 93 <b>9</b> 6 9	0.30225	0.51253	0.79300				
ስ <b>ህብቃ</b> [ስ ቃን ቃን	13.431	ე. 93 <b>9</b> 6 9 ე. 9246 6	0.30225 9.29742	0.51253 0.50433	0.793 <b>00</b> 0.84400				

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32	A.6613	2.62699	0.14849	J-28653	0.72200			
37								10 ▼MIL 10 10 10 10 10 10 10 10 10 10 10 10 10
	14.748	1.0476	0.24077	0.49450	) <b>.</b> 47003			
<b>.</b> 7	12.764	0.90156	0.25024	0.42557	0. 51 500		-	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
52	15.447	1-0926	0.30049	0.51102	1-0170			
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62	20.717	1.4519	0. 40300	0.68537	0.42200			a i i grande programme in the communication of the programme are not the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the communication of the
57	17.376	1.1967	0.37216	0.56490	0.67000			
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VD WORD	71	PL/PD	PL/PTF	PLEATE	X/DHAX			
107	14-143	2-99129	0.27512	U. 46789	-1.0000			
		77827						
112	16-133	0.570.9	27493 .	0.46756	-1-0000			
122	14.128	7.990	0-42483	0.44779	-1.0000			
27	14.153	100101	9.27531	0.46655	-1.0000			
137	Livery	J. 98917	0.77454	0.465	1.0000			
142	14.363	0,94540	0.27356	0.46524	-1-0000			
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97	14-143	0.99120	0.27512	0.46789	0.39800		•	· · · · · · · · · · · · · · · · · · ·
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AVD WITTED         PL 4337         0.64114         0.15754         0.24720           37         16.092         1.1278         0.24724         0.24720           47         16.092         1.1278         0.24673         0.24720           47         16.092         1.1278         0.24673         0.3078           47         16.092         1.1278         0.24673         0.3078           47         16.092         1.1278         0.24673         0.3078           47         16.092         1.1278         0.24673         0.3078           57         12.46         0.90024         0.24673         0.3078           62         23.86         1.3056         0.31111         0.3278           57         18.212         1.3056         0.31111         0.3278           57         18.212         1.3056         0.31111         0.3278           57         18.212         1.213         0.3147         0.3178           57         18.213         0.2392         0.4803           57         18.213         0.2392         0.4803           57         18.213         0.2392         0.4803           57         18.213         0.29	######################################			
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1.5137   0.66114   0.15754     1.5144   1.0517   0.25672     1.5144   0.90024   0.21443     1.5144   0.90024   0.21443     1.5144   0.90024   0.21423     1.5144   0.90034   0.21423     1.5144   0.90034   0.21423     1.5144   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423     1.5145   0.90034   0.21423	2502 22 22 222 222			
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14.324   1.0039   0.23322   20.137   1.4113   0.33429   0.23323   1.4113   0.33429   0.23323   0.33429   0.23323   0.33429   0.23323   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429   0.23429	23			
	E22   E22565   E12			
14,214   0,99619   0,23129     14,214   0,99619   0,23129     14,115   1,99619   0,23525     14,115   1,99619   0,23525     14,115   0,99619   0,23555     14,115   0,99619   0,23557     14,115   0,99619   0,23577     14,115   0,99619   0,23577     14,115   0,99619   0,23577     14,115   0,99691   0,23577     14,115   0,99691   0,23577     14,115   0,99691   0,23577     14,125   0,99691   0,23577     14,125   0,99691   0,23577     14,125   0,99691   0,23577     14,125   0,99691   0,23577     14,244   0,99694   0,23577     14,244   0,99697   0,23577     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23778     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,244   0,99697   0,23788     14,1000   0,99697   0,23788     14,1000   0,99697   0,23788     14,1000   0,99697   0,23788     14,1000   0,99697   0,23788     14,1000   0,99697   0,23788     14,1000   0,99697   0,23788     14,1000   0,99697   0,23788     14,1000   0,99697   0,23788     14,1000   0,99697   0,99697     14,1000   0,99697   0,99697     14,1000   0,99697   0,99697     14,1000   0,99697   0,99697     14,1000   0,99697   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697     14,1000   0,99697				
14.115   4.48919   0.23523   14.115   2.44819   0.23523   14.110   0.34619   0.235423   14.110   0.34619   0.235423   14.113   0.36604   0.235403   0.235423   14.275   0.36604   0.235473   14.115   0.36604   0.235473   14.115   0.36604   0.235473   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.235673   14.110   0.39611   0.2357673   14.110   0.39611   0.2357673   14.110   0.39611   0.2377673   14.110   0.29611   0.2377673   14.110   0.29611   0.2377673   14.110   0.29611   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977673   0.2977773   0.2977773   0.2977773   0.2977773   0.2977773   0.2977773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.297773   0.29				
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77	14.236	0.99762	0-23786	0.40347	0.50000					
82	29.195	1.408R	3.33590	0.56977	0.54300					
92	14.216	D-99622	0.23752	0.40299	0.67000					
->+66F4164	HE-PRESSUPE	RATIOS: v-Ect	<del>c19-34000</del>				er en red <b>e</b> o re <del>desir symptotis de la redesir de</del>			
AVD WOPD	2	PL/PD	PL/PYF.	PLANT	X/DMAX					
-107	14.117	99922	C-23585	0.40007	-1.6000	The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa				
-112	16.112	0. 95 501		0-39993	-1-0000					
-122	14-112	0.98347	17283577	0.39993	-1.0000					
-127	14.146	0.99132	0.23635	40092	-1.0000					
-137	16-997	0.99782	0.23552	0.37950	-1.00%)			· · · · · · · · · · · · · · · · · · ·		
-142	14.072	0.98607	0-23510	0.39800	1-0000					
	N. PPESSUPE	RATIOS . ECR	EBCOY IMET							
NOT TEGGOS					Y / DMAY	<del> </del>				
SADDITION	PL	PL / PO	PL/PTF	PL/PTP	E/DMAX					
AVD YORD	PL 14.117	PL /PD 0.99922	PL/PTF 0.23585	0.49037	0.39000	/ · · · · · · · · · · · · · · · · · · ·				- * ***
AVD YORD 107 112	PL 14.117 14.112	Pt /PD 0.99972 0.98867	PL/PTF 0.23585 0.23577	0.49097 0.39993	0.39000 0.43100					
AVD YORD 107 112 122	PL 14.117 14.112 14.112	Pt /PD 0. 99977 0. 9987 0. 9987	PL/PTF 0.23585 0.23577 0.23577	0.49097 0.39993 0.39993	0.39800 0.43100 0.44900					· * * ** · · ·
APD TONE  APD TONE  107  112  122  127	PL 14.117 14.112 14.112 14.146	PL/PD 0.98922 9.98867 9.9987 2.99132	PL/PTF 0.73565 0.23577 0.23577 9.23635	0.49097 0.39993 0.39993 0.49092	0.39800 0.43100 0.44900 9.48600					- M 100 - 1
>ADDIT ION  AVD YORD  107  112  122  127  177	PL 14.117 14.112 14.112 14.146 14.397	PL/PD 0.98922 9.98867 9.9987 9.99132 0.98782	PL/PTF 0.73585 0.23577 0.23577 9.23635 0.23552	0.49097 0.39993 0.39993 0.49092 0.39950	0.39000 0.43100 0.44900 0.44900 0.52200		•			2 - 35 SM3 - 4
AVD YORD 107 112 122 127 127 142	PL 14.117 14.112 14.112 15.146 14.397	PL/PD 0.94972 9.94807 9.94877 9.9132 0.96782 0.98607	PL/PTF 0-23595 0-23577 0-23577 9-23635 0-23552 0-23510	0.49027 0.39993 0.39993 0.49092 0.39950 0.39980	0.39003 0.43100 0.44900 0.52200 0.52200 0.58800					3 3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
AVD YORD 107 112 122 127 127 142	PL 14.117 14.112 14.112 14.146 14.397 14.372	Pt /PO 0-94972 9-94867 0-94977 2-99132 0-9607 0-98607	PL/PTF 0.73565 0.23577 0.23577 9.23635 0.27552 0.23510	0.49097 0.39993 0.39993 0.39993 0.39950 0.39980	0.3900 0.43100 0.44900 0.52200 0.52200 0.52200					
AVD YORD 107 112 122 127 177 142	PL 14.117 14.112 14.112 14.146 14.397 14.372	PL/PD 0.98972 9.96867 9.99867 9.99132 0.96782 0.98607	PL/PTF 0.73585 0.23577 0.23577 0.23577 0.23535 0.27552 0.23510 0.23011	0.49097 0.29992 0.29992 0.39990 0.39950 0.39950 0.49300	0.39003 0.43100 0.44900 0.52200 0.52200 0.58800		•			- 10 100
>ADDITION: AVD YORD 107 112 122 127 1-7 1-42 157	PL 16.117 16.112 16.112 16.166 16.397 16.372 16.251	Pt /PO 0. 98972 9. 98887 9. 9987 9. 99132 0. 98687 9. 98687 9. 98687	PL/PTF 0.73565 0.23577 0.23577 9.23635 0.23552 0.23510 0.23510 0.23511	0.49097 0.29992 0.39993 9.49092 0.39950 0.39950	0.39803 0.43100 0.44903 0.52200 0.52200 0.52200 0.58800					
AND 1T ION  AVD YORD  107  112  122  127  1-7  142  1-57	PL 14.117 14.112 14.112 14.146 14.397 14.372 14.751 14.251	PL/PD 0.99972 9.9687 9.9987 9.99132 0.98782 0.9867 9.9967	PL/PTF 0.73585 0.23577 0.23577 9.23635 0.27552 0.23510 7.23611	0.49027 0.29992 0.29992 0.39950 0.39950 0.39950 0.49344 0.49344	0.39A03 0.43100 0.44900 0.44900 0.52200 0.58800 2x0000					4 64 4-
AND STORM AVD YORD 107 112 122 127 137 142 1-7 1457 -157 AND STORM	PL 16.117 16.112 16.112 16.166 16.397 16.372 16.251	Pt /PO 0. 98972 9. 98887 9. 9987 9. 99132 0. 98687 9. 98687 9. 98687	PL/PTF 0.73565 0.23577 0.23577 9.23635 0.23552 0.23510 0.23510 0.23511	0.49097 0.29992 0.39993 9.49092 0.39950 0.39950	0.39809 0.43100 0.44909 0.44603 0.52200 0.58800 -1.9990 -1.9990					
AVD YORD 107 112 122 127 1-7 142 147 149 149 149 149 149 149 149 149 149 149	PL 16.117 16.112 16.112 16.166 16.397 16.372 16.751 16.251 PL 16.251	PL/PD 0.98972 9.9887 0.9987 1.99132 0.98607 0.98607 0.99607 0.99607	PL/PTF 0.73585 0.23577 0.23577 9.23635 0.27552 0.23510 0.23611 0.23611	0.40027 0.29992 0.29992 0.39950 0.39950 0.39980 0.49369 0.49369	0.39A03 0.43100 0.44900 0.44900 0.52200 0.58800 2x0000					
AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND STORE AND ST	PL 14.117 14.112 14.112 14.116 14.397 14.372 14.372 14.371 14.251 14.251 14.251 14.251	PL/PO 0.98972 2.96867 2.99182 0.9677 2.99182 0.98607 2.99607 2.99607 2.99667 2.99667 RATIOS 20	PL/PTF 0.73585 0.23577 0.23577 0.23535 0.23510 0.23510 0.23511 0.23611 0.23611 0.23611 0.23611	0.49027 0.29932 0.29932 0.39950 0.39950 0.39980 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360	0.39M03 0.43100 0.43100 0.44603 0.52200 0.58800 1.0000 1.0000 1.0000					
>ADDITION AVD YORD 107 112 122 127 1-7 142 157	PL 14.117 14.112 14.112 14.116 14.397 14.372 14.251 14.251 14.251 14.251 NL PRESSURE	PI /PO 0. 98972 9. 9687 9. 99877 9. 99132 0. 98607 9. 99607 9. 99607 7. 97677 0. 99867 RATIOS 2. 20 PI /PO	PL/PTF  0.23577 0.23577 0.23577 0.23635 0.27552 0.23510 0.23611 0.23611 0.23611 DEG. SHROUD 1 PL/PTF	0.40027 0.29992 0.39992 0.39950 0.39950 0.39950 0.49360 0.49360 0.40369 0.40369 0.40369	0.39809 0.45100 0.44909 0.44909 0.52200 0.58800 -1:0000 -2:0000 X/DMAX -1.9000					
AVD YORD 107 112 122 127 1-7 142 147 149 147 AVD YORD AVD YORD AVD YORD AVD YORD AVD YORD AVD YORD AVD YORD 157 >ADDITION	PL 14.117 14.112 14.112 14.116 14.097 14.072 14.251 14.251 14.251 14.251 RL PRESSURE PL 14.746	PI /PO 0. 98972 9. 9887 9. 9987 9. 99132 0. 98607 9. 99607 9. 99607 9. 9967 RATIOS 20 PI /PO 0. 99832	PL/PTF 0.73585 0.23577 0.23577 0.23577 0.23510 0.23510 0.23511 0.23011 0.23011 0.23011 0.23011 0.23011 0.23011	0.40027 0.29992 0.39993 0.49092 0.39950 0.39980 0.49300 0.40300 0.40300 0.40300 0.40300 0.40300 0.40300	0.39809 0.42100 0.44490 0.44603 0.52200 0.58800 1.0000 1.0000 1.0000					
>ADDITION AVD YORD 107 112 122 127 1-7 142 157	PL 14.117 14.112 14.112 14.116 14.397 14.372 14.251 14.251 14.251 14.251 NL PRESSURE	PI /PO 0. 98972 9. 9687 9. 99877 9. 99132 0. 98607 9. 99607 9. 99607 7. 97677 0. 99867 RATIOS 2. 20 PI /PO	PL/PTF  0.23577 0.23577 0.23577 0.23635 0.27552 0.23510 0.23611 0.23611 0.23611 DEG. SHROUD 1 PL/PTF	0.40027 0.29992 0.39992 0.39950 0.39950 0.39950 0.49360 0.49360 0.40369 0.40369 0.40369	0.39809 0.45100 0.44909 0.44909 0.52200 0.58800 -1:0000 -2:0000 X/DMAX -1.9000					
>ADDITION AVD YORD 107 112 122 127 1-7 1-42 1-7	PL 14.117 14.112 14.112 14.112 14.116 14.097 14.072 14.751 14.251 14.251 14.251 14.251 14.251	PI /PO 0. 98972 9. 9887 9. 9987 9. 99132 0. 98607 9. 99607 9. 99607 9. 9967 RATIOS 20 PI /PO 0. 99832	PL/PTF 0.23585 0.23577 0.23577 0.23577 0.23510 0.23510 0.23511 0.23611 0.23611 PEG_SHBOUD_1 PI_/PTF 0.23802 0.23811	0.40027 0.29992 0.29992 0.39950 0.39950 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360 0.49360	0.39809 0.42100 0.44490 0.44603 0.52200 0.58800 1.0000 1.0000 1.0000					
AND STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED STEED ST	PL 14.117 14.112 14.112 14.116 14.097 14.072 14.075 14.075 14.075 14.075 14.075 14.075 14.075 14.075 14.075 14.075 14.075 14.075  PL 14.075 14.075 14.075  PL 14.075 14.075  PL 14.075 14.075  PL 14.075 14.075  PL 14.075  PL 14.075  PL 14.075  PL 14.075  PRESSURE	PL/PD 0.98972 0.96867 0.99887 0.99872 0.98607 0.99607 0.99667 0.99667 RATIOS 20 PL/PD 0.99867 PATIOS 20 PL/PD 0.99867	PL/PTF 0.73585 0.23577 0.23577 0.23577 0.23510 0.2552 0.23510 0.25611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611	0.40027 0.29992 0.39993 0.39950 0.39950 0.39980 0.40349 0.40349 0.40389 0.40389 0.40389 0.40389	0.39809 0.43100 0.44400 0.44603 0.52200 0.58800 -1:8800 X/DMAX -1.9000 -1.0000 X/DMAX 0.79300 0.84400					
AND STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREE	PL 14.117 14.112 14.112 14.112 14.116 14.097 14.072 14.751 14.251 14.251 14.251 14.251  NL PRESSURE PL 14.746 14.251  PRESSURE PL 13.427	PL/PD 0.98972 2.9687 2.99132 0.9667 2.99132 0.9667 2.9967 2.9967 RATIOS CPN PL/PD 0.9967 PATIOS 20 PL/PD 0.9967 PATIOS 80 PL/PD 2.94091	PL/PTF	0.40027 0.29992 0.39992 0.39950 0.39980 0.49389 0.40389 0.40389 0.40389 0.40389 0.40389 0.40389	0.39 MO9 0.43100 0.44400 0.44603 0.52200 0.58800 -218800 -218800 -10000 -10000 -10000 0.84400					
>ADDITION AVD YORD 107 112 122 127 1-7 142 157	PL 14.117 14.112 14.112 14.112 14.112 14.197 14.372 14.251 14.251 14.251 14.251 14.251 14.251 14.251 14.251 14.251 14.251 14.251 14.251 14.251 14.251 14.251	PL/PD 0.98972 0.96867 0.99887 0.99872 0.98607 0.99607 0.99667 0.99667 RATIOS 20 PL/PD 0.99867 PATIOS 20 PL/PD 0.99867	PL/PTF 0.73585 0.23577 0.23577 0.23577 0.23577 0.23510 0.23510 0.23511 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23611 0.23612 0.23611 0.23612 0.23611	0.40027 0.29992 0.39993 0.39950 0.39950 0.39980 0.40349 0.40349 0.40389 0.40389 0.40389 0.40389	0.39809 0.43100 0.44400 0.44603 0.52200 0.58800 -1:8800 X/DMAX -1.9000 -1.0000 X/DMAX 0.79300 0.84400					

VASA-E FW	r Prejim	INAFY DATA	06/13/79	CADDETT	PFC 10/24/	/79 /2:44:43.654	FAC 946#1	PG4 C034	PNG 1446
>APPITION	INE PRESSIME	RATIOS . PRI	MARY PLUG						and the set of the context of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of the settlement of
מאראי מעם	PL	M /PO	PL /PTF	PI /PTP	X/DMAX				<del></del>
32	8.6575	0.60649	0-16815	0.28644	0.72200			Ween and	
37	14.794	1.0364	0. 29733	0.48947	9-82000				
47	12.935	0.90409	0.25065	0.42699	J. 91 907				
5?	15,458	1.0839	0.70024	0.41145	1.0170				
>ADD TT IDA	AL PRESSIME	RATIOS . FLO	W SPLITTEP I	i.n.	··········				
AVD WORD	PL	PL /PN	PL / PTF	PI /PTP	X/DMAX				- pro ter allegation a since the against an existing our space
42	23.708	1.4507	0.40223	7.62514	J. 42200				
67	17.132	1.2001	0.33274	0.56682	3.67003				
>A00 [7 [00A<	AL PRESSURF	RATIOS . FLO	W SPLITTER I	·. n.					
04Uh UA	Pt	PL /PO	PL/PTF	PL /PTP	X/DMAX	Care and an order of the same of the		. ***	
77	12.326	. 0.86347	0.23940	0.40781	U. 50800				
92	17.312	1-2127	0.33627	0.57277	0.58300			*	
. 92	14.224	0.9964#	0.27627	0_470£2	0-67000				
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-122	14.129	0,98987	0-54473	0.46749	-1.0000				
-127	14.154	7.99150	0.27491	0-46831	-1,0000			· —————	
-137	14:114	0.98878	3.27414	0.44660	-1.0000				
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16.247 0.56773 0.32148 0.54730 1.0000  ADDITIONAL DESCRIPE ACTION FAM MCZZAS 5448  IN WIRD PL PLAND MAPPY PL/PTP X/DMAX  52 16.247 0.59773 0.32148 0.54720 -1.0000  52 16.247 0.99773 0.32148 0.59790 -1.0000  ADDITIONAL PRESSURE RATIOS 20 DEG SIPPUD INCATION  IN WIRD PL PL/PT PL/PTP X/DMAX  57 14.247 0.99773 0.32148 0.54729 0.79380  72 14.252 0.99800 0.22159 0.54735 0.84400  *********************************		14-769	0.98515	0.31742	0.54030	3.59860			
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WIRD   PL   PL/PT   PL/PTP   X/DMAX   S2   16.247   S. 90148   O. 90772   O. 32148   O. 90772   O. 32148   O. 90772   O. 32148   O. 90772   O. 32148   O. 90772   O. 32148   O. 90772   O. 32148   O. 90772   O. 32148   O. 90773   O. 32148   O. 90773   O. 32148   O. 90773   O. 32148   O. 90773   O. 32148   O. 90773   O. 32148   O. 90773   O. 32148   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 90773   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O. 907743   O		16.247	0.69773	0.33144	G,54738		general and the second		
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72 14.252 0.99505 0.32159 0.54735 0.84400  *771TIPMAL PRESSURE RATIOS . 80 DEG SERCUD INCATION  0 WIRD PI PL/PD PI/PTP X/DMAX  87 13.403 0.93864 0.37243 0.51474 0.79300  87 13.184 0.97375 0.79749 0.50624 0.86400			PL/PP					مساعرتها سياسا المامات	
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22	6.9959	2.47652	0.17242	0.29226	2. 72200						
37	17.935	0.75638	0.27370	7.46303	0.82000						
47	13.997	0. 96656	0.34975	0.59284	0.91900						
² 2	14.461	1.2403	9.27644	G. 63A10	1.0170					· · · · · · · · · · · · · · · · · · ·	• • •
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AU RUBU	Pt	PL/PN	PL/PTF	PI /PTP	X/DMAX						
62	15.993	1.1117	0.40225	0.68184	3-42200		المستسدد بالمالية				
47	13.143	0.92285	0.33393	0.56604	3.67000						
MULTICE .	AT PRESSURE	PATINS , FLO	W SPLITTER P	·. n.							
VA WAPA	PL	PL / PO	M /PTF	PL /PTP	X/DMAX	- · · · · · · · · · · · · · · · · · · ·					<del>-</del>
77	9.3409	0.65389	0.23661	0.40107	0.50800						
9 Z	13.353	0.93474	0. 23 723	0.57333	0.56300	· · · · · · · · · · · · · · · · · · ·					
92	14.227	2.99593	2.36037	0.61086	0.67000						
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/D WERD	14.167	PL/PO Q. 99173	-PL/PTF	0-69829	X/DMAX						
12	19.157	3-9103	25962_	9-69786	-1.0000						
2?	14.152	0.0406	0.35646	0.60764	-1-0000						
27	14.172	0. 99208	0. 33000	0.60850	-1.0000						
77		0.99929	0-25797	60678	-1.0000						
المنافعة أ	14.047	0.95334	0.35592	0.6031	-1.0000						
FULL LUNG	<u>al pressure</u>	RATIOS . FOR	FRODY INLET								
n woma	PL	PL/PN	PL/PTF	PL/PTP	x/OMAX						
/n שחשח   37	PL 14.167	PL/PN 0.99173	PL/PTF 0.35886	9.60029	0.39800						
70 4000 27 .12	PL 14.167 14.157	PL/PN 0.49173 6.34103	PL/PTF 0.35886 0.35860	0.60029 0.40786	0.39800 0.43100		•				
77 12 27	PL 14.167 14.157 14.152	PL /PN 0.49173 C. 34103 0.49068	PL/PTF 9.35886 9.35869 0.35849	0.60829 0.40746 0.60764	0.39800 0.43100 0.44903						
n wnen 97 12 22 27	PL 14.167 14.157 14.152 14,172	PL/PN 0.99173 (.39103 0.99068 2.99208	PL/PTF 9.35886 9.25869 0.35849 0,35898	0.60029 0.40746 0.60744 0.60050	0.39600 0.43100 0.44900 0.48600						
70 4000 27 12 12 127 127	PL 16.167 16.157 16.152 16,172 14,132	PL/Pn 0.49173 (.34103 0.49068 2.99208 0.48929	PL/PTF 9.35886 9.35869 0.35849 0.35898	0.60829 0.40786 0.60784 0.60850 0.60678	0.39600 0.43100 0.44600 0.52200						
7n un#n 197 122 129 127 137	Pt 14.167 14.157 14.152 14.172 14.132 14.347	PL/PN 0.49173 C.39103 0.49068 2.99208 0.48924 0.48334	PL/PTF 0.35886 0.35860 0.35849 0.35898 0.35797 0.35582	0.60029 0.60746 0.60744 0.60850 0.60678 0.60314	0.39800 0.43109 0.44909 0.48600 0.5220C 0.58800		•				
70 100 100 100 100 100 100 100 100 100 1	Pt 16.167 16.157 16.152 14.172 14.132 14.247	PL/PN 0.99173 C.79103 0.99068 2.99208 0.98929 0.98334	PL/PTF 9.35886 9.35869 0.35849 0.35898 0.35797 9.35582	0.60829 0.40786 0.60784 0.60850 0.60678 0.60314	0.39800 0.43109 0.44909 0.48690 0.5220C 0.58800						
7n unpn 97 112 22 27 37 42	Pt 14-167 14-157 14-152 14-152 14-132 14-347 14-242 14-242	PL/PN 0.49173 C.39103 0.49068 2.9926 0.48924 0.4834 0.48978	PL/PTF 9.35886 9.25869 0.35849 0.35898 0.35797 9.35582 7.36777	9.60829 0.60746 0.60744 0.60859 0.60878 0.60314 0.01170	0.39800 0.43109 0.44909 0.48600 0.5220C 0.58800						
n unpn 07 12 22 27 37 42	Pt 14-167 14-157 14-157 14-152 14-172 14-132 14-347 14-242 14-742	PL/PN 0.99173 C.79103 0.99068 2.99208 0.98929 0.98334	PL/PTF 9.35886 9.35869 0.35849 0.35898 0.35797 9.35582 7.26777	9.60929 0.60746 0.60746 0.60850 C.6067R 0.60314 0.01150	0.39000 0.43109 0.44407 0.48690 0.52200 0.58800 1.0000						
70 unpn 27 12 22 27 27 37 42 42	Pt 14-167 14-157 14-152 14-172 14-132 14-347 14-242 14-242	PL/PR 0.99173 C.34103 0.99068 2.99208 0.98929 0.98334 0.99393 0.99399	PL/PTF 9.35886 9.35869 0.35849 0.35898 0.35797 9.35582 9.20777	9.60829 0.60746 0.60744 0.60859 0.60878 0.60314 0.61170	0.39600 0.43109 0.44909 0.52200 0.52200 0.58800 -1.0000						
(n wn#n 197 112 27 27 27 137 142 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	Pt 14-167 14-157 14-152 14-172 14-132 14-247 14-242 14-242 M. companies	PL/PN 0.99173 C.39103 0.99068 2.99206 0.98929 0.9834 0.9834 0.9999	PL/PTF 9.35886 9.25869 0.35849 9.35898 0.35797 9.35582 7.2077 10.20077	9.60829 0.60746 0.60746 0.60859 0.60878 0.60314 0.91170 0.91170	0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 -1.0000						
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/n unpn   127   112   127   27   27   47   47   47   47   47   47   47   4	Pt 14.167 14.157 14.157 14.152 14.172 14.132 14.247 14.249 14.742 14.742 14.742 14.742	PL/PN 0.99173 C.39103 0.99068 2.99206 0.98929 0.9834 0.9834 0.9999	91/PTF 9.35886 9.35869 0.35849 0.35898 0.35582 9.35582 9.35582 9.36977 0.36075	9.60929 0.60746 0.60744 0.60859 C.6067R 0.60314 0.01150 Pt/PTP 0.61150	0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 -1.0000						
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(n unpn )7 112 27 27 27 47 42 42 53 63 63 65 65 65 67 67	Pt 14.167 14.157 14.157 14.152 14.172 14.172 14.247 14.242 14.242 At pressure	PL/PN 0. 99173 C. 79103 0. 99068 2. 99209 0. 98929 0. 98334 9. 9909 0. 98999 0. 98999 0. 98999 0. 98999	PL/PTF 9.35886 9.25869 0.35849 9.35898 9.35582 9.35582 9.36973 0.26073 0.36075 DEG SIMMUN I	9.60829 0.60746 0.60746 0.60859 C.60678 0.60314 0.01170 0.01170 0.01170	0.39800 0.43109 0.44909 0.52200 0.52200 0.52800 1.0000 1.0000 1.0000						
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32	6. 7862	0.47534	3-17244	0.29147	0.72200			
7	10.769	7.75432	3.27365	7.46757	0. 92000			
67	13.431	3.96880	0.35145	0.59405	0.91900			
; ,	14.979	1.0416	0.37785	0.63866	1.0170	• •		a marriage
400 I T TOM		MATIOS , FIR						
D MUBU	PL	PL/PD	PL/PTF	PI /PTP	x/nmax			
52	15.884	1-1126	0-40361	0.68220	0.42200			
57	13.157	J. 92157	0.7347?	0.56509	0-67000			
4771 T [ [ [ ]	AL PRESSUPE	PATIOS . FLO	W SPI ITTEP O	.n.				
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7	9-3301	0-65143	0.23632	0.39944	0.50800			
12	13.486	J. 94466	0.34270	0.57924	0.50300			
2	14.226	0.99643	0.36148	0.61099	0-67000			
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D WOPD.	16 176	PL/PD	PL/PTE	0.60885	-1.0000			· · · · · · · · · · · · · · · · · · ·
07	14.176	9. 99293	n. 36021 -					
12	<u> </u>	0.991	25502	0.60020	-1.0020		· · · · · · · · · · · · · · · · · · ·	
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42	14.256	0.98384	0.35691	0.60327				
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D HPRD		PL/PD 0.99293	PL/PTF 0.36021	0.60485	0.39800			
ID HPRD	PL .	PL/PG	PL/PTF					
D HPRD	PL 14-176	PL/PD 0.99293	PL/PTF 0.36021	0.60485	0.39800			
10 HPRD 107 12	PL 14-176 14-161	PL/PG 0.99293 0.99188	PL/PTF 0.36021 0.35983	0.60485	0.39800 C.43100		20	
7D WPRD 107 112 127 127	PL 14-176 14-161 14-156 14-176 14-136	PL/PD 0.99293 0.99188 0.99153	PL/PTF 0.36021 0.35983 0.35970 0.36021 0.35019	0.60985 0.60820 0.60799	0.39800 G.43100 J.44900	-	3 20	
10 MPRD 07 12 22 21 27	PL 14.176 14.161 14.156 14.176 14.136 14.346	PL/PG 0.99293 0.99189 0.99183 0.99293 0.99384	PL/PTF 0.36021 0.35983 0.35983 0.36021 0.36021 0.35691	0.60985 0.60820 0.60799 0.60885 0.60713	0.39800 C.53100 0.44900 0.5800 0.52200 0.5800		3 20	
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07 HPRD 07 12 27 27 27 42	PL 14.176 14.161 14.156 14.176 14.136 14.346	PL/PG 0.99293 0.99189 0.99183 0.99293 0.99384	PL/PTF 0.36021 0.35983 0.35983 0.36021 0.36021 0.35691	0.60985 0.60820 0.60799 0.60885 0.60713	0.39800 C.53100 0.44900 0.5800 0.52200 0.5800		3 20	
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32	5.7769	0.47762	3.19993	0.32002	0.72200					
77	12.498	7. 69743	0.25587	0.60111	0.82000			•		
67	14-131	3.99761	3.39635	0.66897	J. 91 900					
57	14.736	1.029#	0.4179A	0.69758	1.0173					
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52	14.311	1.0002	0.49109	9.67749	3.42203					
67	11.474	0.60193	0.37157	0.54318	0.47000					
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yn ynen.	PL	PI /PO	PL /PTF	PL /PTP	X/DMAY	<del></del>			**************************************	
77	8.2114	7-57388	0.23013	9.38872	0.50000			-		
<b>P</b> 2	27. 739	1.4005	0.56161	0.94862	0.58300					
2	15-256	2. 97563	0.39927	0.67441	0.61000		·····			
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107	14.191	0.99179	0.39773	0.67161	-1.0000					
112	15.191	0.00110	39745_	0_67134	0000					
177	14.176	7-20-27-5	70-19731	9.67119	-1.0000					
127	14-191	7.99179	0,30773	0.67171	-1.0000				and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
137	14:166	0 <b>.</b> 94865	7. 39647	0.63964	1.0000					
162	14.721	0.97993	0.39297	Q.66377	-1,0000	<u></u>				
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YN HORN ,	PL	PL/PO	PL/PTF	PL/PTP	X/D4AX					
107	14-191	9. 97179	0.39773	0.67141	0.39800		•			
112	14-191	0.99110	0.39745	0,67134	2.43190					
122	14.176	7. <del>99</del> 075	0.39731	0.67110	9.44400					
127	_15-191	0. 99179	0. 29 773	0.67191	0.49600					
137	14.146	0.98865	9.39647	0.6696#	0.52200					
4?   <del>  42  </del>	14.921 14.981	0. 97993	0.39297	0.66377	9.58900,					
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152	14.261	H. 99668	0. 79964	0.67512	-1.0000	to age of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the				,
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167	14.266	0.99703	0. 29983	0.67536	0.79300					
172	14.241	7.97664	7.79969	0.67512	J. 84403			www.s		· <b>-</b>
JAPOTT IONAL	PRESSIME	#ATJ05_#_90	DEG SHRPUD, I	OCATION						
		PI / PI	PE / PTF	PI /PTP	X/IMAX					
Vባ ቁርዌቡ	PL		1 1 1 1 1 1 1 1	1						
VO WORD 1#2	13.552	2. 94712	J. 37981	0.64155	0.79300					
VO WORD 1#2 1#7	13.552		).37981 9.37619	0.64155	0.79300 0.84400					

4626-1 FWI	5	PARY DATA	36/13/79	CADDETT	PFC 10/24/7	9 22:57:00-122	FAT REARI	PG# 1034	PNO 1451	
>40017 f04	ML PRESSIBE	PATIOS , PRI	MAPY PIUG					·	ina a mandananananan a menembah menembah penembah menembah menembah sebagai an	
n unen	•	PL/P1	PL /PTF	PL /PTP	X/NMAX			<del></del>		
		0-87893	2-41547	0.70013	9. 72200					
32	12.557								the second of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the con	
7	13.795	0.96563	0.45645	0.7691	0.92000					
.7	14.230	0.99604	0.47083	0.79341	0.91900		man, in a second second second		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
2	14.497	1.0135	0.47909	0.80733	1.0170					
ADDIT HOW	AL PRESSIME	PATINS . FLO	W SPLITTER I	· D.						
n unen	<b>P1</b> .	PL/PO	PL / PTF	PL /PTP	X/DMAX	*		Landarie Land Gapting Co.		
7 -	13.476	0.94326	0.44588	0.75136	0.42200					
7	12.717	0.49012	9.42076	0.77994	0.67000					
Annit inu	AL PRESSIPE	PATINS . FLO	W SPLITTER P	·. n.						
n ween		es / e-7	PL/PTF	PI /PTP	7 /DMA 7		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	grammed train and with the second		
ማ <b>ሣቦ</b> ዋበ	PI.	PL/PF			X/DMAX					
7	. 11-653	0. 81 566	0.38556	0.64972	0.50000					
2	16.407	1.1481	0.54270	0.91451	0.54300					
2	14.269	0.99814	0-67122	0.79508	J-67000				<del></del>	
<u> 20017 104</u>	PL PRESSURE	RAT103- V- £4£	eren-sincus-			per ver a comparement particle (1988)				- <del></del> -
D MC+D		PL/PO	PL/PTF	PLANTE	X/DPAX					
07	14.215	0.99490	0.47032	2. 79257	-1.0000					,,,,,,,
12	16.200	0.97394	9.56985	0_79174	-1.0000					
22	14.202	0.00396	7046984	0.79174	-1.0000			·····		
				V-17[17						
27	14.215	0.99499	0.47933	0-79257	-1.0000	· · · · · · · · · · · · · · · · · · ·				
37		0.99079	0.46835	0.77079	-1.0000					
				0-76115						
32	14-019	0. 98066	0.46356	00.011	-1:0000	- 1				
		RATIOS . FOR					·			
MOLT 1.C.C.A	AL PRESSIRE	RATIOS . FOR	ERCOY IMLET	· · · · · · · · · · · · · · · · · · ·						
	AL PRESSURE	RATIOS . FOR	PL/PTF	PL /P TP	X/DMAX					
A <u>991110M</u> N 40PD 97	AL PRESSURE PL 14.215	PL/PO 0.99499	PL/PTF 0.47033	PL /PTP 0.79257	X/DMA X 0.39800		•			
A <u>991710M</u> N WOPD 07 1 <i>2</i>	PL 14.215 14.209	PL/PO 0.99499 0.99394	PL/PTF 0.47033 0.46984	PL /PTP 0.79257 0.79174	X/DMAX 0.39800 0.43100					
A <u>PDITION</u> D WOPD D7 12 22	PL 14-215 14-200 14-200	PATIOS - FOR PL/PO 0.99499 0.99394 0.99394	PL/PTF 0.47033 0.46984 0.46984	PL /PTP 0.79257 0.79174 0.79174	X/DMAX 0.39900 0.43160 0.44900					
ADDITION O WOPD O7 12 22	PL 14-215 14-209 14-299 15-215	PL/PD 0.99499 0.99394 0.99394 0.99499	PL/PTF 0.47033 0.46984 0.46984	PL /PTP 0.79257 0.79174 0.79174 0.79257	X/DMAX 0.39800 0.43100 0.44900 0.48600		•			
ADDITION O WOPD O7 12 22 27 37	PL 14-215 14-209 14-209 14-209 14-215 14-15	PL/PD D. 99499 D. 99394 D. 99492 D. 99479	PL/PTF 0.47032 0.46984 0.46983 0.46783	PL /PTP 0.79257 0.79174 0.79175 0.79257 0.78523	R/DMAX 0.39800 0.43100 0.44800 0.52200		•			
ADDITION  N WOPD  12 22 27 37	PL 14-215 14-209 14-279 14-279 14-155 14-15	RATIOS . FOR PL/PO 0.99499 0.99394 0.99494 0.99699 0.9966	PL/PTF 0.47032 0.46984 0.47033 0.46983 0.46983 0.46835 0.46256	PL /PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800		*			
A9DITION  O WCPD  12  27  27  47	PL 14-215 14-209 14-279 14-215 14-155 14-919	PL/PD 0.49499 0.99394 0.99394 0.9959 0.99675 0.98066	PL/PTF 0.47033 0.46984 0.46984 0.47033 0.46356 0.47033	PL/PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115	X/DMAX 0.39800 0.43160 0.44900 0.52200 0.58800		•			
A991110M D WCPD 07 12 22 27 37 42	PL 14-215 14-209 14-279 14-279 14-155 14-15	RATIOS . FOR PL/PO 0.99499 0.99394 0.99494 0.99699 0.9966	PL/PTF 0.47032 0.46984 0.47033 0.46983 0.46983 0.46835 0.46256	PL /PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800					
A921110W D WCPD 07 12 22 27 27 42	PL 14-215 14-209 14-279 14-155 14-155 14-157 14-275	PL/PD 0.49499 0.99394 0.99394 0.9959 0.99675 0.98066	PL/PTF 0.47032 0.46984 0.46984 0.46983 0.4635 0.4635 0.4635	PL/PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115	X/DMAX 0.39800 0.43160 0.44900 0.52200 0.58800					
A021110N 0 WOPD 17 12 22 27 37 42	PL 14-215 14-209 14-279 14-155 14-155 14-157 14-275	RATIOS . FOR PL/PO O. 99499 O. 99394 O. 99499 O. 99675 O. 99066 O. 99075	PL/PTF 0.47032 0.46984 0.46984 0.46983 0.4635 0.4635 0.4635	PL/PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115	X/DMAX 0.39800 0.43160 0.44900 0.52200 0.58800		•			
A921110N 0 WOPD 07 12 22 27 37 42 42 42 42 42 42 42 43 44 47 47 48 49 49 40 40 40 40 40 40 40 40 40 40	PL 14.215 14.209 14.209 14.209 14.215 14.155 14.019 14.275	PL/PD 0.99499 0.99394 0.99394 0.99499 0.99679 0.99679	PL/PTF 0.47933 0.46984 0.46984 0.46983 0.4635 0.46356 0.4723	PL/PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115 0.79257	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58000 1.9000		*			
ADDITION O WOPD O7 12 22 27 37 42 42 42 42 42 42 53 0 WOPD 52	PL 14-215 14-215 14-209 14-299 14-295 14-155 14-155 14-157 14-275	PL/PD 0.99499 0.99394 0.99394 0.99499 0.99679 0.99679	PL/PTF 0.47033 0.46904 0.46904 0.47033 0.46903 0.46905 0.47033 0.46905	PL /PTP 0.79257 0.79174 0.79174 0.79257 0.7823 0.78115	X/DMAX 0.39800 0.43160 0.44900 0.52200 0.58800 1.58800					
A021110N D WOPD D T 12 22 27 37 42 42 42 42 42 43 44 45 46 47 47 48 48 48 48 48 48 48 48 48 48	PL 14-215 14-209 14-279 14-275 14-155 14-155 14-275 14-275 14-275 14-275 14-275 14-275 14-275 14-275	PL/PD 0.99499 0.99394 0.99394 0.99492 0.9966 0.9966 0.99075	PL/PTF 0.47933 0.46984 0.46984 0.47933 0.46835 0.46356 0.47231	PL/PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115 0.79521 0.79591 0.79591	X/DMAX 0.39800 0.43100 0.48400 0.52200 0.58600 1.9000 1.9000		•			
A 2217 LOND D WOPD D 7 12 22 27 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 14.215 14.209 14.279 14.155 14.155 14.019 14.275 14.275 14.275 14.275	PATIOS . FOR PL/PO	PL/PTF 0.47932 0.46984 0.46984 0.46933 0.46835 0.46835 0.46356 0.47232 0.47232 DEG SIPCUD 1	PL/PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115 0.79591 0.79591 0.79591	X/DMAX 0.39800 0.43100 0.48400 0.52200 0.58800 1.9800 1.9800 1.9800 1.9800 1.9800		•			
A921110N  0 WOPD  07  12  22  27  37  42  42  42  42  42  42  42  42  42  4	PL 14-215 14-209 14-209 14-279 14-15 14-15 14-17 14-275 14-275 41 PRESSUPE	RATIOS . FOR PL/PO 0.94499 0.99394 0.99394 0.99595 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.99079 0.9	PL/PTF 0.47933 0.46984 0.46984 0.47933 0.46835 0.46356 0.47231 DEG SHETUD 1	PL/PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.78115 0.79591 0.79591 0.79591	X/DMAX 0.39800 0.43160 0.44900 0.52260 0.58800 1.9800 1.9800 X/DMAX					
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APPLITION  NOPD  OT  12  22  27  37  42  42  42  42  42  42  42  42  42  4	PL 14-215 14-209 14-279 14-155 14-155 14-157 14-157 14-277 AL PRESSURE PL 14-275 14-275 AL PRESSURE PL	PATIOS . FOR PL/PD 0.99394 0.99394 0.99495 0.9966 9.99918 PATIOS . 20 PATIOS . 20 PATIOS . 20 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS . 30 PATIOS .	PL/PTF 0.47933 0.46984 0.46984 0.46983 0.46356 0.46256 0.47231 DEG SHPTUD 1 PL/PTF	PL/PTP 0.79257 0.79174 0.79174 0.79257 0.78523 0.76115 0.79523 0.776115 0.79501 0.79501 0.79501 0.79501 0.79501 0.79501 0.79501	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.9000 1.9000 X/DMAX 0.79300 0.84400					

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VI WILED	PI	PI / PTI	PI / PT F	PL /PTP	×/max				
32	6. 9170	9.47711	2.17230	0.29129	0-72200				
32 37	10.029	0.75646	0.27319	0.46279	J. #2000		and the secondary was an ex-		ere or a commonwealing amount of
67	13.729	0.96090	0.34702	0.58787	0.91900				
• <i>•</i> • • • • • • • • • • • • • • • • •	14.813	1.0367	0.37102	0.63426	1.0170		e por de la late de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de la companie de l		
MULT LUUK	AL PRESSUPE	PATIOS , FIG	M SPLITTER I	• n•					
40P0	Pŧ	PI. / PO	PL /PTF	PL /PTP	Y /DMAX				
62	15.936	1.1153	0.40279	0.68235	3.42200				
67	13.220	0. 97526	0.33415	0.56606	0.67000				
>A77 [ T [ [ N	AL PRESSURE	RATIOS . FLO	W SPLITTER O	.n.			······································		<u> </u>
AU MUBU	PL'	PL / PO	PL/PTF	PL/PTP	X/DMAX		The second second	*** ****	rentere entrementation de la company
77	9.2950	0-65055	0.23494		0.50200				-
12	13.395	0. 93749	0.33856	0.57355	0.58300				
2	14,224	0.99550	0-35951	E0904-0	0.67000				<del></del>
H22[[100	AL PRESSUPE	<del>*************************************</del>	e <del>rer sunnus</del>	<del></del>		era ar a la eree	-		-
080W CV	PL	PL/PO	PL/PTF	PL/PIP	X/DMAX				
107	14.164	0. 99130	2.35900-	C.60647	-1.0000				
112	14-156	0.97060	0-5174	0.62626	-1-0000				
172	14.159	0.99094	2-35787	0.60625	-1.0000		······	<del></del>	
127	14.179	99235	0.35838	0.69711	-1.0000				
37	14.4	2.99951	7. 156 99	0.00476	-1.0700	a company of the company of the company			
192	14.059	0.98397	0.35535	0.60166	-1.0000				
>/DDITICM	AL PRESSURE	RATIO:FOP	ERODY INLEI						
VD 40PD	PL	PL/P0	PI /PTF	PL/PTP	X/DMAX				
107	14.164	0.99130	0.35800	0.40647	0.39800		•		
112	14-154	0.99060	0.35774	0.60604	0.43100				
122	14.159	0. 99095	0.35787	0.69625	0-44900				
	14.179	0-99235	0.35838	0.60711	0.48600				
127	14.124	0.99851	0.35699	0.63476	0.52200				
		0. 93397	0-35535	0.60198	0.58800				
37				0.000				·	
37 142	14.059								
37 142 53	14-959		30000	C+00*0*	-110000-	· · · · · · · · · · · · · · · · · · ·			
137 142 153	14.059		30000	•					
42 42 67 48217 IDN	14.059 14.244 14.244 4L PRESSURE	74 1192 + 1 41	- 4055F- 1145	C:00****	-1.0000-				
27 42 42 42 42 42 42 42 43 43 43 43 43 43 43 43 43 43 43 43 43	14.059 14.059 14.244 4L PRESSURE	7, 290,00 7, 290,00 PATISE & FAI	30000	PL/PTP	X/DMAX				
137 142 153 157 167 169 170 409 D	14.059 14.244 14.244 4L PRESSURE	74 1192 + 1 41	- 902215 FL42	C:00****	-1.0000-				
197 142 153 10 40P D 157	14.059 14.044 14.244 41. FRESSURE PL 14.244	7, 796, 19 7, 796, 19 0, 596, 19	0179302 HOFFLE FLAS M1-94702	PL/PTP	X/DMAX -1.0000				
42 42 42 42 42 42 42 42 42 42 42 42 42 4	14.059 14.744 16.244 14.244 14.244 AL. PRESSURE	7, 705 P 7, 705 P 7, 705 P 0, 096 P PATIOS 20	0.36002 DEG_SIPPLID_L	CLATICA.	X/DMAX -1.0000 -1,0000				
127 142 143 147 147 147 147 147 147 147 147 147 147	14.059 14.244 4L PRESSURE 14.244 14.244 AL PRESSURE	7. 79649 0. 49649 0. 49649 PATIOS 20.	MODEL SLAS MODEL SLAS MARY MARY MARY MARY MARY MARY MARY MARY	PL/PTP  0.60cm9  0.00cm9  CCATICM  PL/PTP	X/DMAX -1.0000 -1.0000				
2217 10N VD 40P D (57 157 ADDIT 10N VD 40PD	14.059 14.044 14.244 14.244 AL. PRESSURE Pt 14.244	7, 79689 0, 99689 0, 99689 PATIOS 20 PL/PD 0,99689	0.36002 DEG_SHPDUD_L PI_/PTF 0.36002	PL/PTP G. 60989 CCATICM PL/PTP G. 60989	X/DMAX -1.0000 -1.0000				
APOST ION  APOST ION  APOST ION  APOST ION  APOST ION  APOST ION  APOST ION  APOST ION	14.259 14.244 14.244 14.244 AL. PRESSURE Pt 14.244 14.244	7.90549 0.90649 PATIOS 20 PL/PN 0.99649 0.99649	0.36002 DEG_SIPPLID_L PI /PYF 0.36002 0.36002	PL/PTP 6.60089 0.00089 CCATICM PL/PTP G.60089 0.60089	X/DMAX -1.0000 -1.0000				
APOST ION  APOST ION  APOST ION  APOST ION  APOST ION  APOST ION  APOST ION  APOST ION	14.259 14.244 14.244 14.244 AL. PRESSURE Pt 14.244 14.244	7.90549 0.90649 PATIOS 20 PL/PN 0.99649 0.99649	0.36002 DEG_SHPDUD_L PI_/PTF 0.36002	PL/PTP 6.60089 0.00089 CCATICM PL/PTP G.60089 0.60089	X/DMAX -1.0000 -1.0000				
ABOUT ION ABOUT ION ABOUT ION ABOUT ION ABOUT ION ABOUT ION	14.059 14.244 14.244 14.244 AL. PRESSURE Pt 14.244 AL. PPESSUPE Pt	7. 193 L 1 97 7. 193 L 1 97 7. 193 P 7.	######################################	PL/PTP (I. 6 OCR9 U.BYPE CCATICM PL/PTP G. 6 OPP9 O. 6 OPP9 CCATION PL/PTP	X/DMAX -1.0000 -1.0000 X/DMAX 9.79300 0.84400				
VD 40PD 157 157 >A991TION VD 40PD 167 172 >AB91TION VD 40PD	14.059 14.244 14.244 14.244 AL. PRESSURE PL 14.244 AL. PRESSURE PL 14.244 AL. PPESSUPE PL 13.400	7. 70649 7. 70649 7. 70649 7. 70649 PATIOS 20 PL/PN 7. 99649 7. 002 DEG_SHPCUD_L PI_/PYF 0.36002 0.36002 DEG_SHPCUD_L PI_/PYF 0.36002 DEG_SHPCUD_L PI_/PYF 0.73869	PL/PTP (I.E.OCA9 U.B. PL/PTP G.E.OSP9 0.60989 CCATION	X/DMAX -1.0000 -1.0000 -1.0000 X/DMAX 9.79300 0.84400					
127 142 142 142 142 142 142 142 142 142 142	14.059 14.244 14.244 14.244 14.244 14.244 AL. PRESSURE PL 14.244 AL. PRESSURE PL 13.400 13.100	7. 193 L 1 97 7. 193 L 1 97 7. 193 P 7.	######################################	PL/PTP (I. 6 OCR9 U.BYPE CCATICM PL/PTP G. 6 OPP9 O. 6 OPP9 CCATION PL/PTP	X/DMAX -1.0000 -1.0000 X/DMAX 9.79300 0.84400				

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NASA-I FWIS	S DRELIMI	НАРУ ПАТА	06/13/79	CARDELL	PEC 10/24/79	23:02:46.769	FAC RYGHE	PGM C034	RUN24 PMG 1454
>AND IT INNA	AL PRESSIPE	PATINS . FFI	MAPY PLUG		•				
YN WORD	PL	PI /PP	PI /PTF	PL /PTP	X/DMAX	***************************************			
32	8.6184	0.60380 -	3.16829	0.28657	J. 72200		*		
37	15.212	1.0657	0.29704	0.50582	J-#2000				
47	12.767	0.89442	0.24929	-0.42651	J.91900	-	-		
52	15.417	1.0801	0.30194	0.51267	1.0170				
APPI TI COAC	IL PRESSURE	RATIOS . FLO	W SPLITTER I	. n.					
VD WOPD	PL	PL / PO	PL/PTF	PL/PTP	×/DPA¥			*	•
62	20.616	1.4643	O. 40255	0.68549	0.42200				
67	17.088	1.1972	0.33367	0.56820	3.67000				••
>AND IT IONA	IL PRESSIPE	PATINS . FLO	W SPLITTER F	·. n.					
VP WORD	PL	PL/PO	PL / PTF	PL /PTP	X/DMAX				• · · •
77	12.173	0.85282	0.23769	0.40476	0-50800				
<b>#2</b>	17.143	1.2010	0. 334 75	0.57003	2.58300		• •		
97	14.209	0.99547	0.27746	0.47247	0.67000				
>20017 CH	H- PRESSURE	RATIOS: y=E30	CTOP SINCE						
VD. WORD	7	PL/P0	PL/PTF	_MATE	X/DNAX				
107	14.136	7.99023	0.22547	0.46990	-1.0000	***			· · · · · · · · · · · · · · · · · · ·
i 12	14-129	0-90053	0.27580	0.46965	-1.0000				
122	14-114	Quantile 3	0.27560	0.46932	-1.0000				
127	14-156	0.99093	0.27014	0.47031	-1.0000				
137	19.099	0.98778	0.27531	0-46992	-1.0000				* * *
نكا	14-054	Q. 98463	Q. 27543	0.46732	-1.0000				
SADD I T IONA	n percupr	RATIOS . FOR	FARRY IMET						
VD_WORD	PL	PL/PO	PL/PTF	PL/PTP .	X/DMAX				
107 112	14.134	0.99023	0.27599	0.46998	0.39#00				
122	14-124	0_96953	0.27500 .	0.46965	0.43100				
127	14.114	7.98883	0.27560	9.46932	J. 44900				
127	14.144	0.99093 2.99778	0 <u>-27619</u> 2-27531	0.47031	0.48600				
142	14-054	0.99483	0.27443 _	0.468P2	0.52200				
145	140999	Va 79703	V427473 .	0.46732	0.58800				
1-1	14.244	7,99792	9.27714	0,47585	-1.0000		in the second of the second		
ADDLT LOW									
	21	-		PL/PTP	X/QMAX				
Att Milks	14.239	7. 90 757	0.32004	0.47346	-1-0000		19		
		0.99792		0:43343	-1.0000				
157	16.744								
157 157	16.744	RATIOS . 20	DEG SHPPUD L	OCATION					
157 157 >AP21110NA	PRESSIPE		<u>DEG SHPPUD L</u>	OCATION PL/PTP	x/DMAX				
157 157 >ADDITIONA VO WORD	PRESSIPE	RATIOS . 20			x/DMAX 0.79300				
157 157 24021110NA VN WORD 167	LE PRESSIPE	PATIOS . 20 PL/PO 0. 99757	PJ /PTF	PL /PTP					
157 157 >ADDITIONA VD WORD 167 172	PL 14,239 14,239	M / Pn 0. 99757 0. 99757	PJ /PTF 0-27804 0-27804	Pt /PTP 0.47346 0.47346	0.79300				
157 157 2ADDITIONA VD WORD 167 172 2ADDITIONA	PL 14.239 14.239 14.239	MATIOS . 20 M./PO O. 99757 O. 99757 RATIOS . RO	PI /PTF 0.27804 0.27894 DEG SHPCUD I	PL /PTP 0.47346 0.47346 ncat inh	0.79300 0.84400				
157 >ADDITIONA VD HORD 167 172 >ADDITIONA VD HORD	PL 14.239 14.239 14.239	MATIOS . 20 M./PO 0.99757 0.99757 RATIOS . RO M./PO	PL/PTF 0.27804 0.27804 0.27804 0EG SHPCUD L	PL /PTP 0.47346 0.47346 ncat inn Pl /PTP	0.79300 0.84400 X/DMAX			-	
VP MORD 167 172 <u>&gt;ADDITIONA</u> VD MORD 182	PL 14.239 14.239 14.239 14.239 14.239 11. PRESSIRE PL 13.479	PATIOS . 20 PL/PD 0. 99757 0. 99757 PATIOS . RO PL/PD 0. 94373	PL /PTF 0.27804 0.27804 DEG SHPCUD L PL /PTF 0.26303	PL /PTP 0.47346 0.47346 OCATION PL /PTP 0.44791	0.79300 0.84400 x/nmax 0.79300				
157 >ADDITIONA VO HORD 167 172 >ADDITIONA VO HORD 182 187	PRESSIPE PL 14.239 14.239 11. PRESSIPE PL 13.472 13.244	M/PN 0.99757 0.99757 0.99757 RATIOS . RO PI/PN 0.94373 0.92799	PL /PTF 0.27804 0.27804 DEG SHPFUD L PL /PTF 0.26303 0.25865	PL /PTP 0.47346 0.47346 ncat inn Pl /PTP	0.79300 0.84400 X/DMAX			-	
157 >ADDITIONA VO HORD 167 172 >ADDITIONA VO HORD 182 187	PRESSIPE PL 14.239 14.239 11. PRESSIRE PL 13.477 13.2-4 , MEASUPED	M/PO 0.99757 0.99757 0.99757 RATIOS . RO M/PO 0.94373 0.92799 THRUST PAPAR	PL /PTF 0.27804 0.27804 DEG SHPFUD L PL /PTF 0.26303 0.25865	PI /PTP 0.47346 0.47346 0.647346 0.64701 0.44701	0.79300 0.84400 x/nmax 0.79300	05m C- 3A1 303			

MASS-I FUIS	PRF1 14	THARY HAYA	96/13/79	CANNETT	RFC 10/24/79	23:05:24.396	FAC RESE	PG# 1934	RUN24
APD1*1094	PRESSUPE	PATINS . PPI	MARY PLUG						
מפחי חעי	PI	PL /PO	M /PYF	PL /PTP	X/DMAX	······································			-
32	12.898	0.90213	0.49967	0.72329	o. 72200				
37	13.571	0.97369	0.53931	0.78066	0.82000				
47	14.270	2, 99913	9.55294	9.40026	0.91900				
57	14.497	1.012	0. 56094	0.41201	1.0170				
>ANDITIMA	PRESSIME	RATIOS . FLO	W SPLITTER I	. P.		Market Company of F 1987 11 11 11 14 14 15	AND THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON O	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	
AVD WORD	PL	Pt / Pri	PL /PTF	PL /PTP	X /DMA X				
62	13.726	Q. 96 00A	9.53177	0.76975	0.42200				
47	13.132	0.91854	0.50876	0.73444	9. £ 7000				•
AMPLTICCAC	PRESSIME	PATINS . FLO	W SPLITTED O	'. n.	44-2	and deligram or recommend or the deligration of appropri	allitati aliinta geggggg geriyeyin tigil (Mill aga - i iyeyi iyan		
AVD WORD	PL	PL/PO	PL /PTF	PL /PTP	X/DHAX				
77	12,034	0. 84173		0.67486	0.50800				
47	15.483	1.0929	Q,46622 Q.59582	0.86876	0.58300				
92	14.265	9.99773	0.55265	0.7995#	0.67999				
		<del>-047105 <u>y f</u>of</del>							
AYD WORD	71	PL/PO	PL/PTF	PLAN	X/DMAX			ř	
-107	14.223	2. 99499	9- 35110	0.79774	-1.0000				
-115	14.220	77-00-664	-75-5091	0.79746	<u>-1-0000</u>				
-172	14-210	2-203	0.55052	0.79690	-1.0000				
-127	14.230	0. 99534	0.54936	0.7902	-1.0000 -1.0000				
-137	100	0.90144		0.79522					
-137 - <u>162</u>	14.046	0.00242	0.54414	O. PARCE	-1.0000				
152	14.946		0.54414			·			
>4001110MA	14.046 L PRESSUPE	PATINS . FOR	0.54414 ERONY INLEY	0.74366	-1.0000				
>6001TIONA	14.046 L PRESSUPE PL	PATINS . FOR	0.54414 ERODY THEFT PL/PTF	PL/PTP	-1.0000	-		·	
>ANDITIONA AVD WORD 107	14.046 L PRESSUPE PL 14.225	PATINS , FOR	0.54414 EROOW IMLET PL/PTF 0.55110	0.70366 PL/PTP 0.79774	x/DMAX 0.39900	-	• •		
>4001710MA AVD WORD 107 112	14.046 1 PRESSUPE PL 14.225 14.220	PATERS . FOR PL/PR 9.99499 0.99464	0.54414 EROOW IMLET PL/PTF 0.55110 0.55091	PL/PTP 0.79774 0.79746	7/DMAK 0-34806 0-43100				. 4.4
>400171094 AVD WORD 107 112 122	14.046 L PRESSUPE PL 14.225 14.220 14.210	n, 98242  PATENS FOR  PL/PN 9, 99499 0, 99464 0, 99394	0.54414 EROW IM FT PL/PTF 0.55110 0.55091 0.55052	PL/PTP 0.79774 0.79746 0.79690	x/DMAX 0.37806 0.43100 0.44980				
>400[T]094 AVD WORD 107 112 122 127	14.046 1 PRESSUPE Pt 14.225 14.220 14.210 14.230	PATINS . FOR PL/PN 9, 49449 0, 49446 0, 93394 0, 94534	0,54414 FEROIN IM FT PL /PTF 0.55110 0.55091 0.55052 0.55130	PL/PTP 0.79774 0.7976 0.79690 0.79690	*/DMAX 0.39800 0.43100 0.44900 9.48400	-			
>4001710MA AVD WORD 107 112 127 137	PRFSSUPE PL 14.225 14.220 14.210 14.210 14.730 14.180	PATINS . FOR PL/PN 9. 99499 0. 99464 0. 99394 0. 99534 2. 99184	0,54414 PERODY 1MET PL/PTF 0,55110 0,55051 0,55052 0,55130 0,54936	PL/PTP 0.79774 0.79764 0.79690 0.79902 0.79922	*/DMAX 0.39800 0.43100 0.44900 0.48400 0.52200				
>ANNITIONA AYD WORD 107 112 122 127 137 142	14-046 PRESSUPE Pt 14-225 14-220 14-210 14-230 14-180 14-046	PATINS . FOR PL/PN 9.99499 0.99464 0.99394 0.98536 7.99536 0.98536	0,54414 EROOW IMET PL/PTF 0,55110 0,55091 0,55052 0,55130 0,54936 0,54414	PL /PTP 0.79774 0.79746 0.796.90 0.796.92 0.796.22 0.78766	*/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800	-	·		
>4001710MA AVD WORD 107 112 127 137	PRFSSUPE PL 14.225 14.220 14.210 14.210 14.730 14.180	PATINS . FOR PL/PN 9. 99499 0. 99464 0. 99394 0. 99534 2. 99184	0,54414 PERODY 1MET PL/PTF 0,55110 0,55051 0,55052 0,55130 0,54936	PL/PTP 0.79774 0.79764 0.79690 0.79902 0.79922	*/DMAX 0.39800 0.43100 0.44900 0.48400 0.52200				
142   >ANDITIONA   AVD WORD   107   112   122   127   137   142	PRESSUPE PL 14.225 14.220 14.210 14.210 14.180 14.046	PATINS FOR PL/PN 0.99499 0.99464 0.99394 0.99534 0.99534 0.99534 0.99534	0,54414 PEROTW IMET PL /PTF 0.55110 0.55051 0.55052 0.54936 0.54414 0.77922	PL/PTP 0.79774 0.79746 0.79690 0.79690 0.79622 0.78766 0.79652	*/DMAX 0.39800 0.43100 0.44900 0.52200 0.52800 -1.0000		-		
>ANDITIONA AVD WORD 107 112 122 127 137 142 142	PRESSUPE  PL 14-225 14-220 14-210 14-730 14-180 14-046 14-790 14-779	PATINS . FOR PL/PN 0.99499 0.99464 0.99394 0.99534 0.99534 0.99534 0.99534 0.99534 0.99534	0,54414 PEROOW IMLEY PL /PTF 0.55110 0.55091 0.55092 0.54936 0.54936 0.54414 0.9932	PL/PTP 0.79774 0.79774 0.79690 0.79690 0.79622 0.78722 0.787652 0.80052	-1.0000 x/DMAX 0.39800 0.43100 0.44980 0.52200 0.52200 0.58000 -1.0000				
>ANDITIONA AVD WORD 107 112 127 127 137 147 142 153 AVD WORD	PL 14.225 14.225 14.220 14.210 14.210 14.210 14.100 14.046 14.200	0.98262 PATINS : FOR PL/PN 9.99499 0.99466 0.99396 0.99436 0.99436 0.99786 0.99787	0,54414 PEROTW IMET PL /PTF 2,55110 0,55091 0,55052 0,55130 0,54936 0,54414 0,99304 PROTECTION	PL/PTP 0.79774 0.7974 0.79402 0.79402 0.79402 0.79402 0.79402 0.78402	1.0000 X/DMAX 0.39000 0.43100 0.44900 0.52200 0.52200 0.52200 -1.0000		•		
>ANDITIONA AVD WORD 107 112 122 127 137 142 142	PL 14.225 14.225 14.220 14.210 14.230 14.180 14.046 14.230 PL 14.280	PATINS . FOR PL/PN 0.99499 0.99464 0.99394 0.99534 0.99534 0.99534 0.99534 0.99534 0.99534	0,54414 PEROOW IMLEY PL /PTF 0.55110 0.55091 0.55092 0.54936 0.54936 0.54414 0.9932	PL/PTP 0.79774 0.79774 0.79690 0.79690 0.79622 0.78722 0.787652 0.80052	-1.0000 x/DMAX 0.39800 0.43100 0.44980 0.52200 0.52200 0.58000 -1.0000		•		
>ANDITIONA AVD WORD 107 112 122 127 137 142 -142 -152 AVD WORD -152	PRESSUPE  PL 14.225 14.220 14.210 14.230 14.180 14.046 14.790 14.280 14.280	PATINS : FOR PL/PN 2: 99499 0: 99464 0: 99394 0: 99536 2: 99184 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0: 99749 0:	0,54414 PEROTO IMET PL/PTF 2,55112 0,55091 0,55052 0,55130 0,54936 0,54414 0,7932 0,5932 0,5932 0,5936 0,54414 0,7932 0,55304	PL/PTP 0.79774 0.7974 0.79690 0.79620 0.7962 0.7862 0.78652 0.80054	-1.0000 X/DMAX 0.39800 0.43100 0.44980 0.52200 0.53200 -1.0000 -1.0000				
AVN WORD 142 142 142 142 142 142 142 142 142 142	PL 14.225 14.220 14.220 14.210 14.230 14.180 14.046 14.775 PL 14.280 14.275 L PRESSUPF	0. 98242  PATENS . FOR  PL /PN	0,54414 PEROOW IME FY PL /PTF 0.55110 0.55091 0.55052 0.55130 0.54936 0.54414 0.99922 0.2004 PEROOM IME FY D. 1000000000000000000000000000000000000	PL/PTP 0.79774 0.79746 0.79690 0.79692 0.78766 0.78082 0.80094	-1.0000 X/DMAX 0.39000 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000				
>ANDITIONA AVD WORD 107 112 122 127 137 142 142 142 152 AVD WORD 157 >ADDITIONA AVD WORD	PL 14.225 14.225 14.220 14.210 14.230 14.180 14.180 14.280 14.280 14.280 14.280 14.275 L PRESSUPF	0.98242  PATINS FOR  PL/PN 0.99499 0.99464 0.99394 0.99534 0.99734 0.99734 0.99749 0.99749 0.99749 0.99749 0.99749	0,54414 PEROOW IMET PL/PTF 2,55110 0,55052 0,55130 0,54936 0,54936 0,54414 0,9932 0,59304 PEROOM PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF PROOF	PL/PTP 0.79774 0.79774 0.79746 0.79690 0.79692 0.78766 0.79052 0.78766 0.79052 0.78766 0.79052 0.78767	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 X/DMAX				
>ANDITIONA AVD WORD 107 112 122 127 137 142 -152	PRESSUPE  14.225 14.220 14.210 14.230 14.180 14.046 14.790 14.280 14.275 L PRESSUPE  PL 14.280	0.98242  PATINS : FOR  PL/PN	0,54414 PEROTO IMET PL/PTF 0,55110 0,55052 0,55130 0,54936 0,54936 0,54414 0,7932 0,55304 PEROTO IMET	PL/PTP 0.79774 0.7974 0.7974 0.79690 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962	-1.0000 X/DMAX 0.39800 0.43100 0.44980 0.52200 0.52200 0.58000 -1.0000 -1.0000 X/DMAX 0.79300				
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>ANDITIONA  AVD WORD  107  112  122  127  137  142  -152  AVD WORD  -152  >ADDITIONA  AVD WORD  167  177  >ADDITIONA	PL 14.225 14.220 14.210 14.730 14.140 14.775 L PRESSUPE PL 14.240 14.275	0.98262  PATINS : FOR  PL/PN	0,54414 PENON IMET  PL/PTF 0,55110 0,55052 0,55130 0,54936 0,54936 0,54936 0,54936 0,54936 0,54936 0,54936 0,54936 0,55320 0,55324 0,55323 0,55324 DEG SHPDHD 1	PL/PTP 0.79774 0.7974 0.7974 0.79690 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962 0.7962	*/DMAX 0.39808 0.43100 0.44980 0.52280 0.58800 -1.9900 -1.9900 **/DMAX -1.0000 **/DMAX 0.79300 0.84400				
>ANDITIONA AVD MORD 107 112 122 127 137 142 142 142 152 AVD MORD 167 177 >ANDITIONA AVD MORD	PL 14.225 14.220 14.210 14.220 14.210 14.230 14.180 14.046 14.280 14.275 L PRESSUPE PL 14.240 14.270 L PRESSUPE	0. 98242  PATENS . FOR  PL/PN	0,54414 PEROOW IMET PL/PTF 0.55110 0.55091 0.55092 0.54936 0.54436 0.54414 0.99920 0.2000 0.54936 0.54414 0.99920 0.2000 0.54936 0.54936 0.54936 0.54936 0.54936 0.54936 0.54936 0.54936 0.54936 0.54936 0.54936 0.54936 0.54936 0.55323 0.55323 0.55323	PL /PTP 0.79774 0.79774 0.79776 0.797902 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702	-1.0000 X/DMAX 0.39000 0.49100 0.44900 0.52200 0.52200 -1.0000 -1.0000 X/DMAX 0.79300 0.79300 0.79400				
>ANDITIONA AVD WORD 107 112 122 127 137 142 142 153 AVD WORD 167 177 >ANDITIONA AVD WORD 187	PL 14.225 14.220 14.210 14.220 14.210 14.730 14.180 14.280 14.275 1 PRESSUPE PL 14.280 14.270 1 PRESSUPE PL 14.270 1 PRESSUPE PL 14.270	0.98242  PATINS FOR  PL/PN 0.99499 0.99464 0.99394 0.99534 0.99734 0.99734 0.99747 0.99747 0.99747 0.99747 0.99747 0.99747 0.99747 0.99747 0.99747	0,54414 PEROOW IMLET PL/PTF 2,55110 0,55052 0,55130 0,54936 0,54414 0,9992* 0,**** 0,**** 0,**** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,*** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,** 0,* 0,	PL/PTP 0.79774 0.79774 0.79774 0.79746 0.79690 0.79902 0.79702 0.78766 0.79092 0.80092 0.80092 0.80092 0.80092 0.80092 0.90092 0.80092 0.90092 0.90092	-1.0000 X/DMAK 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 X/DMAK 0.79300 X/DMAK 0.79300				
>ANDITIONA AVD WORD 107 112 122 127 137 142 -142 -152	PL 14.225 14.220 14.220 14.210 14.230 14.180 14.046 14.790 14.280 14.280 14.275 L PRESSUPF PL 14.290 14.270 L PRESSUPF PL 14.270 L PRESSUPF	0. 98242  PATENS . FOR  PL/PN	0,54414 PEROOW IME FY PL /PTF	PL /PTP 0.79774 0.79774 0.79776 0.797902 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702 0.79702	-1.0000 X/DMAX 0.39000 0.49100 0.44900 0.52200 0.52200 -1.0000 -1.0000 X/DMAX 0.79300 0.79300 0.79400				

MACA-LEWIC	PPFt 141	HARY DATA	96/13/79	CAPPELL	PEC 10/24/	79 23:38:59.586	FAC SHOTE	PC# C034	RUN24
IAPPITICEAC	PRESSIPE	PATINS . PRI	MARY PLUG						
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32	10.225	J. 71890	0.33941	0.4% 07	0.72200				
37	13.560	9.94783	7.44759	0. 640 96	3. #2300				
47	14.433	1.0059	0.47633	0.68215	0.91500				
52	14.778	1. 7337	0.49779	0.69847	1.0170				
>APOITIONAL	<b>POCSSIPE</b>	PATINS , FLO	W SPLITTEP I	.P.			merementari territoria de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della composición della c		and the second sections with the last of
VO WORD	PL	PL/PN	PL /PTF	PI /PTP	Y/DHAX				
62	14.648	1.0299_	0.47683	0.68285	0.42200				
67	11.977	0.43721	0.39528	0-56607	0.67000				
>ADDITIONAL	PRESSURF	PATTOS . FLO	W SPLITTEP P	.n.					
VD WORD	PL	PL/PR	PL/PTF	PL /PTP	X/DPAX				
	11.551	0.80685	0.38094	0.54554	0.50000				
P2			0.54156	0.77556	0.58300	-			
92	16.410 14.244	1.1470 0.99563	9-47907	0.67312 _	0.58300 0.67000				
>AQQ17109AL	-PPE33KPE-	<del>7+1195 - 5+</del>	<del>( Tan_2#06¥2)</del>			and the second second			
VD HOPD	_	eL/e0	_PL/PTE	PL/232	X/DNAX				
	14.100								*
107		0.99214	0.46962	0.47092	-1.0000				
112	14-184	99145	-56209	0-67035					
127	14.174	0.99	0.46777	0.66988	-1.0000				
127	14.139	3. 99179	0046826	C-67059	-1.0000		An and an		
177	-14-134	3.98796	0.466	0.66799	-1.0000				
152	.13.974	Q_97679	0.46118	0.04044					
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>ADDITIONAL	PRESSUPE	RATIOS . FOP	EDODA INTEA						
		PATIOS . FOP		PL/PTP	X/UMAX				
VO WOED	PL	PL/PD	. PL/PTF				•		~-
VO WOPD	PL 14.194	PL/PD	PL/PTF	0.67092	J. 3 9809		•		*-
VD WOPD 107 112	PL 14.194 14.194	PL/PD 0.99214 0.99145	PL/PTF 0.46842 0.46809	0.670#2 0.67035	J. 3 9809 0.43109	· · · · · · · · · · · · · · · · · · ·	•		
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VD WOPD	PL 14.194 14.184 14.174 14.179	PL/PD 0.99214 0.99145 0.99075 0.99075	PL/PTF 0.46842 0.46809 0.46777 0.46826	0.67092 0.67035 0.6698P 0.67059	0.43107 0.43107 0.44900 0.58600		•		
VD WOPD	PL 14.194 14.184 14.174 14.139	PL/PD 0.99214 0.99145 0.99075 0.99079 0.99796	PL/PTF 0.46842 0.46809 0.46777 0.46826 0.46645	0.67092 0.67035 0.6698P 0.67059 0.66799	0.43109 0.43109 0.44900 0.48600 0.52200		•		
VD WOPD 107 112 177 127 137 142	PL 14.194 14.184 14.174 14.139 14.134 13.974	PL/PD 0.99214 0.99145 0.99075 0.99179 0.97796	PL/PTF 0.46842 0.46809 0.46709 0.46826 0.46645	0.67092 9.67035 0.6698P 0.67059 0.66799	0.39809 0.43109 0.44900 0.48600 0.52200 0.58800		•		
VD WOPD 107 112 177 127 137 142	PL 14.194 14.184 14.174 14.199	PL/PD 0.99214 0.99145 0.99075 0.99079 0.99796	PL/PTF 0.46842 0.46809 0.46777 0.46826 0.46645	0.67092 0.67035 0.6698P 0.67059 0.66799	0.43109 0.43109 0.44900 0.48600 0.52200				-
VD WOPD 107 112 172 127 137 142 137	PL 14.194 14.194 14.186 14.174 14.199 14.134 13.974 14.279	PL/PD 0.99214 0.99145 0.99175 0.99179 0.97679 0.97679	PL/PTF 0.46842 0.46809 0.46777 0.46826 0.46645 0.46119	0.67082 0.67035 0.66988 0.67059 0.66799 0.65044	0.39807 0.43107 0.44900 0.48600 0.58800				-
VO WOPD 107 112 172 127 127 137 142 142	PL 14.194 14.194 14.174 14.174 14.139 14.134 13.974 14.779	PL/PD 0.99214 0.99145 0.99175 0.99179 0.977679 0.97679	PL/PTF 9.46842 0.46809 0.46777 0.46826 0.4615 0.46119	0.670#2 9.67035 0.669#P 9.67059 0.67049 0.65044	0.39809 0.43109 0.44900 0.52200 0.58000 1.9000				
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VD WOPD 107 112 127 127 127 127 142 147 147 VD WOPD 157 >ADDITIONAL	PL 14.194 14.194 14.174 14.174 14.134 13.974 14.779 14.779 PRESSIPE	PL/PD 0.99214 0.99145 0.99145 0.99179 0.9179 0.97679 0.97669 0.97668 PATIOS 20	PL/PTF 0.46842 0.46809 0.46777 0.46826 0.46645 0.46119 0.47937 0.47937 0.47057	0.67082 0.67035 0.6698P 0.67059 0.66799 0.66044 0.67389 PL/PTP 0.67389 0.67799	U. 3 9807 Q. 43107 Q. 44900 Q. 58000 -1.7070 1.7070 X/QMAR -1.0000 -1.0000				-
VO WOPD 107 112 177 127 137 142 142 147 147 240 147 240 240 240 240 240 240 240 240 240 240	PL 14.194 14.194 14.174 14.174 14.134 13.974 14.259 PRESSURE PL 14.259 PRESSURE	PL/PD 0.99214 0.99145 0.99175 0.99179 0.97679 0.97679 0.97668 VAVIUS VAN PL/VO 0.99668 PATINS 20 PL/PD	PL/PTF 9.46842 0.46809 0.46777 9.46826 0.46645 0.46619 9.44997 0.47977 0.47977 0.47057	0.67082 9.67035 9.66989 9.66799 9.66799 9.66044 9.67389 PL/PTP	U.39809 0.43109 0.44900 0.52200 0.58800 1.7080 1.7080 1.7080 1.7080 1.0000				
VO WOPD  107  112  177  127  137  142  142  147  147  240  157  >ANGITIONAL  VO WOPD  167	PL 14.194 14.194 14.174 14.174 14.139 14.134 13.974 14.259 PRESSIPE PL 14.259	PL/PD 0.99214 0.99145 0.99175 0.99179 0.97579 0.97579 0.97668 PATINS . FAN PATINS . 20 PL/PD 0.99668	PL/PTF 9.46842 0.46809 0.46777 0.46826 0.46645 0.46119 0.47057 0.47057 DEG SHROUD 1	0.67072 0.67035 0.6698P 0.67059 0.667049 0.65044 0.07249 0.67389 0.67389	U.39809 Q.43109 Q.44900 Q.58600 127000 127000 127000 127000 127000 127000 127000 127000 127000				
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VD WOPD 107 112 127 127 127 127 142 147 147 200 157 >ADDITIONAL VD WOPD 167 172	PL 14.194 14.194 14.174 14.174 14.134 13.974 14.259 PRESSIRE PL 14.259 PRESSIRE PL 14.259	PL/PD 0.99214 0.99145 0.99175 0.99179 0.97579 0.97579 0.97668 PATINS . FAN PATINS . 20 PL/PD 0.99668	PL/PTF 0.46842 0.46809 0.46777 0.46826 0.46645 0.46119 0.47057  DEG SHROUD 1 PL/PTF 0.47057 0.47073	0.67082 0.67035 0.6698P 0.66799 0.66799 0.66944 0.67389 PL/PTP 0.67389 0.67799 0.67389 0.67799	U.39809 Q.43109 Q.44900 Q.58600 127000 127000 127000 127000 127000 127000 127000 127000 127000				
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>#0011100	HAE PRESSUME	PATENS . PPE	MANY PHUG				
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32	6.5564	0.45915	0.18296	0.76349	0.72700		
37	C.9717	0.69487	0.27685	<b>6.34</b> 63€	0.42000		
47	14.179	2.99294	3-39565	0.5704	0.91900		
57	15.271	1.0667	3-42503	C-61305	1.0170		
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6.2	16.759		7.46763	0.47450	0.42209		
67	13-021	0.41187	9.36335	0.5240#	0.67000		
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77	0.2842	0.56015	0.23117	0.33343	0.50800		
82	19.961	1.3979	0.55700	0.40340	0.5A300	•	
<u>%</u> 2	14.229	0. 99643	0. 39704	0.57269	9.67000		
Munistan	<del>14</del>	***** <del>*******</del>	<del>eten surau</del> n	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t			
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	14.176	0.09759			-1.0000		
-112 -122	14.154	0.2017	C. 39495	0.57008 0.56967			
-127		7.99259	3.3-561		-1.0000		
-137	14.175	0.98910	0.39412	0.57044	-1.0000	And the second of the second	4 W + 2
	14.719	0.98176	0.39120	0.5642	-1.0000		
-152		-10 -4 E . D	7037EE9	A 3 3 de Sign	-1-0600	ti mini ti sali ve i i i imalio di i	
ADD TT COAC	ML PRESSURE	PATINS . FIP	ERMOY INLEY				
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	Pt 14,174 14,164			0.57048	0.39800 3.43103	•	
107	14.174	0. 99259	0. 30541			•	7 m . m
107 112	14.174 14.164 14.154	0.99259	0.39523	0.57000	0.43100 0.44400		, , , , , , , , , , , , , , , , , , ,
107 112 122	14.174	0.99259	0.39561 0.39573 0.39465	0.57000	0,43100		
107 112 122 127 137 142	14.174 14.166 14.156 16.174 14.126 14.019	0.99259 0.99189 0.99119 0.99259 0.98910 0.98176	0.39541 0.39523 0.39464 0.39451 0.39412 0.39120	0.5700P 0.56967 0.5704B 0.56847 0.56425	0.43100 0.44400 0.48600 0.52200 0.58800		
107 112 122 127 137 142	14,174 14,164 14,154 16,174 14,126 14,019	0.94259 9.99189 0.99119 0.9959 9.98919 0.98176	0.39541 0.39523 0.39523 0.39664 0.39651 0.39612 0.39120	0.57000 0.56967 0.57940 0.56847 0.56425	0.43100 0.44400 0.48600 0.52200 0.52200		
107 112 122 127 137 142	14,174 14,166 14,156 14,156 14,126 14,126 14,019	0.94259 7.99189 0.99119 7.99259 7.98917 3.98176	0.39561 0.39523 0.39458 0.39451 0.39412 0.30120	0.5700P 0.56967 0.5704B 0.56847 0.56425	0.43100 0.44400 0.48600 0.52200 0.58800	• • • • • • • • • • • • • • • • • • • •	
107 112 122 127 137 142	14,174 14,164 14,154 16,174 14,126 14,019	0.94259 0.99189 0.99189 0.9919 0.9810 0.9810 0.9817	0.39541 0.39523 0.39523 0.39664 0.39651 0.39612 0.39120	0.5700e 0.56967 0.57049 0.56967 0.56475 0.7349	0.43100 0.44400 0.48600 0.52200 0.52200	•	
107 112 122 127 137 142 142 142 142 144 144 144 144 144 144	14,174 14,166 14,156 16,174 14,126 14,019 14,244 14,244 14,244	0.94259 0.99189 0.99189 0.99259 0.98910 0.98716 0.97764	0, 39561 0, 39573 0, 39466 0, 39451 0, 39412 0, 30120 0, 34763	0.5700P 0.56967 0.5706P 0.56847 0.56475 0.7349	3.43103 3.44400 0.48400 0.52200 0.52200 0.52200 -1.0000	· · · · · · · · · · · · · · · · · · ·	
107 112 127 127 137 142 127 127 142 127 127 127 127 127	14,174 14,166 14,156 16,176 16,126 16,019 16,249 16,249	0.94259 7.99189 0.99119 0.99259 7.98917 3.98176 7.997781	0,34561 0,34573 0,39466 0,39412 0,39120 0,34763	0.5700P 0.56967 0.5704P 0.56847 0.56475 0.7349	3.43103 3.44400 0.48600 0.52200 0.58800 -1.0000 x/8MAX -1.0000		
107 112 122 127 137 142 142 142 142 144 144 144 144 144 144	14,174 14,166 14,156 16,174 14,126 14,019 14,244 14,244 14,244	0.94259 0.99189 0.99189 0.99259 0.98910 0.98716 0.97764	0, 39561 0, 39573 0, 39466 0, 39451 0, 39412 0, 30120 0, 34763	0.5700P 0.56967 0.5706P 0.56847 0.56475 0.7349	3.43103 3.44400 0.48400 0.52200 0.52200 0.52200 -1.0000		
107 112 127 127 137 147 147 147 147 147 147 147 147 147 14	14.174 14.166 14.156 14.156 14.126 14.019 14.249	0.94259 7.99189 0.99119 0.99259 7.98917 3.98176 7.997781	0.39561 0.39573 0.39565 0.39412 0.39120 0.391763	0.5700P 0.56967 0.57069 0.56967 0.56475 0.56475 0.57369 PL/PTP 0.57329 0.57329	3.43103 3.44400 0.48600 0.52200 0.58800 -1.0000 x/8MAX -1.0000	•	
107 112 127 127 137 147 147 147 147 147 147 147 147 147 14	14.174 14.166 14.156 14.156 14.126 14.019 14.249	0.99259 0.99189 0.99189 0.99259 0.98910 0.9810 0.97784 0.97784 0.97784 0.97784 0.99783	0.39561 0.39573 0.39565 0.39412 0.39120 0.391763	0.5700P 0.56967 0.57069 0.56967 0.56475 0.56475 0.57369 PL/PTP 0.57329 0.57329	3.43103 3.44400 0.48600 0.52200 0.58800 -1.8800 */#MAX -1.0000		
107 112 127 127 147 142 -197 -197 -197 -197 -197 -197 -197 -197	14,174 14,166 14,156 16,176 16,126 16,019 16,249 18,249 PL 14,266 15,249	0.94259 7.99189 0.99119 7.99259 7.98917 3.98176 7.99784 7.99784 3.99783 PATINS , 20	0, 34561 0, 34573 0, 39468 0, 39412 0, 30120 0, 34763 0, 34763 0, 34763 0, 34763 0, 34763	0.5700P 0.56967 0.57049 0.56847 0.56475 0.7349 PL/PTP 0.57329 0.57329	3.43103 3.44400 0.48600 0.52200 0.58800 -1.0000 x/8MAX -1.0000	• • • • • • • • • • • • • • • • • • •	
107 112 127 127 137 142 127 127 142 127 127 127 127 127 127 127 127 127 12	14,174 14,166 14,156 16,174 14,126 14,019 14,249 14,249 PL 14,266 15,249	0.99259 0.99189 0.99189 0.99259 0.98910 0.98170 0.99176 0.99784 0.99784 0.99783 PATINS . 20	0.39561 0.39573 0.39466 0.39412 0.39120 0.39763 0.39763 0.39763 0.39763 0.39763	0.5700P 0.56967 0.57069 0.56947 0.56425 0.27349 PL/PTP 0.57349 PL/PTP	3.43103 3.44400 0.48600 0.52200 0.52200 0.52200 -1.0000 -1.0000 -1.0000	• • • • • • • • • • • • • • • • • • •	
107 112 127 127 137 142 137 142 137 142 137 142 137 142 137 143 143 144 145 147 147 147 147 147 147 147 147 147 147	#4.174 14.166 14.156 14.156 16.176 14.126 14.019 14.246 14.246 14.246	0.99259 0.99189 0.99189 0.99259 0.98910 0.98910 0.99784 0.99784 0.99783 PATINS . 20	0.39561 0.39573 0.39468 0.39412 0.39120 0.39763 0.39763 0.39760 0.65 CHROUN 1	0.5700P 0.56967 0.57049 0.56847 0.56475 0.27349 PL/PTP 0.57329 0.57329 0.57329 0.57329	3.43103 3.44400 0.48600 0.52200 0.52200 0.52200 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 127 127 137 147 147 147 147 147 157 20015000 AVD MORD 157 20015100	#4.174 14.166 14.156 14.156 14.126 14.126 14.299 14.249 ML PRESSIME PL 14.246 ML PRESSIME	0.99259 0.99189 0.99189 0.9919 0.9819 0.9819 0.97784 0.97784 0.97784 0.99783 PATINS . 20 PL/PN 0.99784 PATINS . 80	0.34561 0.39523 0.39626 0.39612 0.30120 0.30120 0.34763 0.34763 0.34763 0.34763 0.34760 0.39760 0.39766	0.5700P 0.56967 0.5706P 0.56847 0.56847 0.7369 0.7369 PL/PTP 0.57329 0.57329 0.57329 0.57329	3,43103 3,44400 0,44400 0,52200 0,52200 0,58800 1,0000 1,0000 1,0000 1,0000 1,0000 0,84430		
107 112 127 127 137 142 -127 -127 -127 -127 -127 -127 -127 -12	14,174 14,166 14,156 14,174 14,126 14,019 14,240 14,246 15,249 ML PRESSIME PL 14,244 ML PRESSIME	0.99259 0.99189 0.99189 0.9919 0.98919 0.98919 0.98718 0.99784 0.99783 PATINS . 20 8L/PN 0.99784 PATINS . 80 8L/PN	0.39561 0.39523 0.39626 0.39612 0.30120 0.39763 0.39763 0.39763 0.39760 0.39760 0.39766 0.39766	0.5700P 0.56967 0.5706P 0.56847 0.56425 0.7349 PL/PTP 0.57329 0.57329 0.57349 0.57329 0.57329	3.43103 3.44400 0.48600 0.52200 0.52200 0.58800 10000 -1.0000 1.0000 1.0000 1.0000 0.84430		
107 112 127 127 137 142 127 147 142 127 2000000000000000000000000000000000	#4.174 14.166 14.156 14.156 14.126 14.019 14.240 14.246 15.249  ML PRESSIME PL 14.244  ML PRESSIME PL 14.244  ML PRESSIME	0.99259 0.99189 0.99189 0.99189 0.99170 0.99170 0.99170 0.99784 0.99783 0.99783 0.99784 0.99784 0.99784 0.99784 0.99784 0.99784 0.99784 0.99784	0.39561 0.39573 0.39468 0.39412 0.39412 0.39120 0.39763 0.39763 0.39760 0.39760 0.39760 0.39760 0.39760	0.5700P 0.56487 0.57049 0.5647 0.56475 0.57349 0.57349 0.57349 0.57349 0.57370 0.57370 0.57370 0.57370	3.43100 3.44400 0.48600 0.52200 0.58800 1.0000 -1.0000 1.0000 1.0000 1.0000 0.79300 0.84430		
107 112 127 127 137 147 147 147 147 147 147 20015 100 AVD WORD 167 172 20015 100 AVD WORD 167 172 20015 100 AVD WORD 167 172 187	#4.174 14.166 14.156 14.156 14.126 14.019 14.246 14.246 14.246  ###################################	0.99259 0.99189 0.99189 0.9919 0.98919 0.98919 0.98718 0.99784 0.99783 PATINS . 20 8L/PN 0.99784 PATINS . 80 8L/PN	0.39561 0.39523 0.39525 0.39412 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.30120 0.3012	0.5700P 0.56967 0.5706P 0.56847 0.56425 0.7349 PL/PTP 0.57329 0.57329 0.57349 0.57329 0.57329	3.43103 3.44400 0.48600 0.52200 0.52200 0.58800 10000 -1.0000 1.0000 1.0000 1.0000 0.84430		

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Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   Variable   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	4EC 10/24/79 23:11:19.2	K/IMAT 0.72200 0.72200 0.91900 1.0170		и /гман 0-422 <b>8</b> 0 0-6 700 <b>0</b>		M / UN A V 0 - 5 0000 0 - 4 a 100	0.67089		K/D*AK	-1.00 <b>00</b> -1.00 <b>0</b> 0	-1.0000	1-0000		X APPAK	0.49100	0.44403	0.52200	0600-1		x /DMA x -1.0000	-1.0000	и / Doda и 0., 7 4 3 0 0 0. л 4 4 0 0	AA OA MARKAT YANKA AA AA AA AA AA AA AA AA AA AA AA AA A
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PRESCRIPE RATIOS . PPIN  7.4343	36/13/70 HAFY PLUG	0.18851 0.7416 0.32567 9.34691	SPL IVTER		SM ITTER	0.23732 0.34073	9-3605	E	N. P. C.	27.50	0.35473	0.35819	EAMON IMET	PL/PTF	0.35470	0.35920	0.35419	ALL THE	TOTAL STATE	2195		i	
# # # # # # # # # # # # # # # # # # #	Ē.	9,75727 0,75727 0,89535 1,0587	•	28	PATINS . FLM	94,/m0 2,65952 7,94115	0.99602	West of Guises	77.m	1000	0.90218	0.98438		54/16	0.99078	0.99218	0. 98414 0. 98414		THE PARTY	Core C	9742	0742 9742 9742	
44 CA-1 FUIS  5 27  5 37  5 47  5 47  5 47  5 47  5 47  5 47  5 47  5 62  6 62  6 7  5 87  107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107  1107	E	7-4343 10-408 12-839 15-254	PRESSIDE	18.306 14.396	PRESCIME	9.3562 9.3562 13.433	15.216	1		14.1%	16.13. 14.21.	15.02	PRESSIPE	4	14.14	14.136	14.121		THICK CARE	14.236	<u>"</u>		Berssibe

,	S PPFLIM	ENAPY DATA	06/13/79	CADDETI	PFC 10/24/79	23:13:33.696	FAF RYGYL	PG# (034	RUN24
**************************************	AL PRESSURE	RATIOS , PRI	MARY PLUG						
VO WOPD	PI	PI /PA	PL /PTF	PL /PTP	X/IMAX		to considerational state desperant the made makes an expression of		
37	8,7417	0.61237	0, 19677	0.28852	9-72299				
37	13.894	0.97329	0.31274	0.45857	0.62000				
.7	11.148	0. 78006	7-25094	0.36795	0.91900				
, <u></u>						·			
	15.611	1.0936	0. 35139	0.51523	1.0170				
ANDIT ION	AL PRESSUPE	PATIOS , FIF	W SPLITTER I	. ft.					
O WOPD	PL	PL/PD	PL / PTF	PL /PTP	x /DMA x				
52	. 20-616.	.1.5442	9.46495	0-4 9042	J-42200				
Ĩ	16.619	1.1642	0.37406	0.54850	2.67003				
POTTION	AL PRESSURF	PATENS , FLO	W SPI ITTER O	1. N.				er en en en en en en en en en en en en en	Marine and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the s
D WORD	PL	P( / PI)	PI /PTF	PL /PTP	x/DMA*				
77	10.669	0.74739	0.24015	0.35213	0.50800				
2									
2	14.987	1.0499	0.33734	0.49464	0.58300				
<u> </u>	14.223	7.99636	0.32016	0.46944	0.67000				
<b>PUDITION</b>	NE PRESSURE	PATION_Y.E.OF	<del>c sep- criucino-</del>						
D HUND	7	PL / PN	PL/PTF	91/277	X/DMAX				
07	14.143	0.99147	0. 31 758	0.46713	-1.0000				* 1 1
12	14.143	2.90022		0.46670	-1.0000				
72	14.138	7. 99042	A 31 P25					·	
		11.99217	0. 31 661	0.46664	-1.0000				
	14.163	11.7721	A TENT	0.46746	-1.0670				
		A 8607*	A 314A4						
37	140871	0.99977	0.31602	0.46621	-1.0500				
27 37 62		0.99977 0.98622	0,31699	0.46466	-1.0500	and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th			-
37 <b>5</b> 2	14.979		0, 31699						•
37 52 ADD LT FORM	14.979 AL PRESSUPE	D. 98622 PATIOS , FOR	0,31690 FRODY THLFT	0.4646	20000				
37 42 AND LT FINA	14.079	0.98622 PATENS , FRM FL/PN	0, 31690 FRODY IMLET PI /PTF	0.464AF	X/BMAX				
37 42 ADD LT FONA D 40RO 37	14.979 14.979 14.979 14.153	0.98622 PATIOS , FOP PL/PO 0.99147	0, 31690 FRODY INLFT PI /PTF 0.31859	0.464AF PI /PTP 0.46713	X/RMAX 0.39800				
37 42 AOD LT FONA O WORD O7 12	14.079 14.079 14.079 14.153 14.143	0.98622 PATIOS , FOP FL/PO 0.99147 0.99077	0, 31690 FRODY IMLET M /PTF 0.31859 0.31836	P1 /PTP 0.46713 0.46890	X/BMAX 0.39800 0.43100		· ·		
37 42 A0D LT FONA 0 40R0 37 12 22	14.079 AL PRESSUPE PL 14.153 14.143 14.139	0.98622 PATIOS : FOP PL/PO 0.99147 0.99077 0.99042	0, 31690 FRODY [MLFT M /PTF 0.31858 0.31836 0.31825	0.464AF PI /PTP 0.46713 0.46680 0.46664	X/BMAX 0.39800 0.43100 0.44900				
37 42 400 LT FONU 0 WORD 07 12 22 27	PRESSUPE  14.079  PL  14.153  14.143  14.138  14.163	0.98622 PAYINS , FNP PL/PN 0.99147 0.99077 0.99042 0.99217	0, 31699 FRODY IMLET M /PTF 0.31859 0.31825 0.31825 0.31821	0.4646f P1 /P YP 0.46712 0.46664 0.46746	X/BMAX 0.39800 0.43100 0.44900 0.48600				
37 42 ADD LY FONA D WORD 37 17 22 27	14.079 14.079 AL PRESSUPE PL 14.153 14.143 14.163 14.163 14.163	0.98622 PAYIOS : FOP PL/PO 0.99147 0.99077 0.99042 0.99217 0.98972	0, 31699 FRODY IMLET M /PTF 0.31858 0.31836 0.31825 0.31881 0.31802	P1 /PTP 0.46712 0.46664 0.46746 0.46621	X/BMAX 0.39800 0.43100 0.44900 0.52200				
37 42 AODITION O WORD O7 17 12 22 27 37	PL 14.153 14.143 14.138 14.163 14.128 14.079	0.98622 PATIOS : FOP FL/PO 0.99147 0.99077 0.99042 0.99217 0.98972 0.98627	0, 31690 FRODY IMLET M /PTF 0.31859 0.31825 0.31881 0.31802 0.31690	PI /PTP 0.46713 0.46680 0.4664 0.46746 0.46621 0.46466	X/RMAX 0.39800 0.43100 0.44900 0.52200 0.52200	-			
37 42 AND LT JONA O MORO 37 17 12 22 27 37 42	PL 14.153 14.143 14.143 14.163 14.163 14.163 14.1079	0.98622 PATIOS . FOP PL/PO 0.99147 0.99077 0.99042 0.99217 0.9872 0.98622 0.99011	0, 31699  FRODY IMLET  PI /PTF 0.31859 0.31825 0.31825 0.31802 0.31609 0.31609	P1 /PTP 0.46712 0.46664 0.46746 0.46621	X/BMAX 0.39800 0.43100 0.44900 0.52200				
37 42 40 40 51 10 10 10 10 10 10 10 10 10 10 10 10 10	PL 14.153 14.143 14.138 14.163 14.128 14.079	0.98622 PATIOS : FOP FL/PO 0.99147 0.99077 0.99042 0.99217 0.98972 0.98627	0, 31690 FRODY IMLET M /PTF 0.31859 0.31825 0.31881 0.31802 0.31690	PI /PTP 0.46713 0.46680 0.4664 0.46746 0.46621 0.46466	X/RMAX 0.39800 0.43100 0.44900 0.52200 0.52200				-
37 A0017 IONA O 4080 37 12 22 27 37 42 57	PL 14.153 14.143 14.163 14.163 14.128 14.079 14.246	0.98622 PATIOS . FOP PL/PO 0.99147 0.99077 0.99042 0.99217 0.9872 0.98622 0.99011	0, 31699  FRODY IMLET  PI /PTF 0.31858 0.31836 0.31825 0.31881 0.31802 0.31699 0.22072	0.4646f P1 /P TP 0.46712 0.46680 0.46664 0.46621 0.46621 0.46466	X/RMAX 0.39800 0.43100 0.44900 0.52700 0.58800				
37 42 A001T (ON) O HORO 37 12 22 27 37 42 42 42 42	PL 14.153 14.143 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163	0.98622  PATIOS : FOP  PL/PO 0.99147 0.99042 0.99217 0.9872 0.9872 0.98622 0.9911 0.9871	0, 31699  FRODY IMLET  PI /PTF 0.31859 0.31825 0.31825 0.31802 0.31802 0.31609 0.22072 0.22072	0.4646f P1 /P TP 0.46712 0.46680 0.46664 0.46746 0.46621 0.46466 0.47076	X/RMAX 0.39800 0.43100 0.44900 0.48600 0.52700 0.58800 -1.0000				-
37 42 ADD 17 JONA D MORD 17 17 22 27 37 47 47 57	14.079 14.079 14.173 14.143 14.163 14.163 14.163 14.079 14.289	0.98622  PAYINS : FNP  PL/PN 0.99147 0.99077 0.99042 0.99217 0.98972 0.98627 0.98627 0.98611 PATING : FNN	0, 31699  FRODY IMLET  M /PTF 0.31859 0.31825 0.31825 0.31802 0.31802 0.31802 0.31802 0.31802	0.464Af PI /P TP 0.46712 0.46680 0.46664 0.46746 0.46621 0.46466 0.47777 0.47076	X/RMAX 0.39800 0.43100 0.44900 0.52700 0.58800 -1.0000				
37 42 A0011 IONA O HORD 37 12 27 37 42 47 40011 IONA D HOPD 52	PL 14.153 14.143 14.138 14.138 14.128 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.248 14.079 14.248 14.079 14.248 14.248 14.079 14.248 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.248 14.079 14.248 14.248 14.079 14.248 14.079 14.248 14.248 14.079 14.248 14.079 14.248 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.079 14.248 14.248 14.079 14.248 14.248 14.079 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248	0.98622  PAYINS : FNP  PL/PN 0.99147 0.99077 0.99027 0.98972 0.98972 0.98622 0.99011 0.99011 PAYING : FNP	0, 31690  FRODY IMLET  PI /PTF 0.31859 0.31876 0.31871 0.31871 0.31872 0.31690 0.22072 0.27077  ROZZIP PLAP	0.46467 P1 /PTP 0.46713 0.46680 0.46644 0.46746 0.46621 0.46466 0.47076 0.47076	X/RMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000				
37 42 AND IT IONA O WORD 37 12 22 27 37 42 42 42 42 57 AND IT IONA D WORD 52 57	PI 14.245 14.245 14.128 14.163 14.163 14.163 14.163 14.163 14.163 14.079 14.240 14.079	0.98622  PATIOS , FOP  PL/PO 0.99147 0.99077 0.99042 0.99217 0.98972 0.98627 0.98627 0.98627 0.98627 0.98627 0.98627	0, 31699  FRODY IMET  PI /PTF 0.31859 0.31825 0.31825 0.31802 0.31609 0.22072 0.22072 0.22072 0.32072	0.4646f  P1 /P TP     0.46712     0.46664     0.46746     0.46621     0.46621     0.46466     0.47076     0.47076  P1 /P TP     0.47026	X/RMAX 0.39800 0.43100 0.44900 0.52700 0.58800 -1.0000				
37 42 AND IT IONA O WORD 37 12 22 27 37 42 42 42 42 57 AND IT IONA D WORD 52 57	PI 14.245 14.245 14.128 14.163 14.163 14.163 14.163 14.163 14.163 14.079 14.240 14.079	0.98622  PAYINS : FNP  PL/PN 0.99147 0.99077 0.99027 0.98972 0.98972 0.98622 0.99011 0.99011 PAYING : FNP	0, 31699  FRODY IMET  PI /PTF 0.31859 0.31825 0.31825 0.31802 0.31609 0.22072 0.22072 0.22072 0.32072	0.4646f  P1 /P TP     0.46712     0.46664     0.46746     0.46621     0.46621     0.46466     0.47076     0.47076  P1 /P TP     0.47026	X/RMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000				
37 42 AOD LY TONA O WORD 37 12 22 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 14.179 14.079 14.179 14.173 14.143 14.143 14.163 14.163 14.163 14.079 14.249 14.249 14.246 14.246	0.98622  PATIOS , FOP  PL/PO 0.99147 0.99077 0.99042 0.99217 0.98972 0.98627 0.98627 0.98627 0.98627 0.98627 0.98627	0, 31699  FRODY IMET  PI /PTF 0.31859 0.31825 0.31825 0.31802 0.31609 0.22072 0.22072 0.22072 0.32072	0.4646f  P1 /P TP     0.46712     0.46664     0.46746     0.46621     0.46621     0.46466     0.47076     0.47076  P1 /P TP     0.47026	X/RMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000				
37 42 AODITIONA O MORO 37 12 22 27 37 42 42 52 57 AODITIONA D MORD	PL 14.173 14.173 14.143 14.138 14.138 14.128 14.079 14.248 14.079 14.248 14.079	0.98622  PATIOS , FOP  PL/PO 0.99147 0.99077 0.99042 0.99217 0.98622 0.98622 0.98612 0.98611 0.99011 PATIOS , FON	0, 31699  FRODY IMLET  PI /PTF 0.31834 0.31825 0.31881 0.31802 0.31609 0.22072 0.22072 0.32072 0.32072	0.46467 P1 /PTP 0.46713 0.46680 0.46664 0.46621 0.46621 0.46466 0.47076 P1 /PTP 0.47026 0.47026	X/RMAX 0.39800 0.43100 0.44900 0.52700 0.52700 0.58800 -1.0000 -1.0000				
37 42 A001T IONA O WORD 37 12 22 27 37 42 42 42 52 57 A001T IONA D WORD E 7	PL 14.179 14.079 14.179 14.173 14.143 14.143 14.163 14.163 14.163 14.079 14.249 14.249 14.246 14.246	0.98622  PATIOS , FOP  PL/PO	0, 31699  FRODY IMLET  PI /PTF 0.31859 0.31825 0.31825 0.31801 0.31699 0.22072 0.22072 0.32072 0.32072 0.32072	0.4646f  P1 /PTP 0.46712 0.46680 0.46664 0.46746 0.46621 0.46621 0.47076  P1 /PTP 0.47026 0.47026 0.47026	X/RMAX 0.39800 0.49100 0.44900 0.52700 0.58800 -1.0000 -1.0000				
37 42 AODITIONA O MORD 37 12 22 27 37 42 52 57 AODITIONA D MORD 52 57	PL 14.153 14.143 14.143 14.163 14.128 14.079 14.244 14.079 14.244 14.245 14.246 14.246 14.246 14.246	0.98622  PATIOS , FOP  PL/PO	0, 31699  FRODY IMLET  PI /PTF 0.31859 0.31825 0.31825 0.31807 0.31807 0.31807 0.32072 0.32072 0.32072  PI /PTF 0.32072 0.32072	0.4646f P1 /PTP 0.46713 0.46680 0.46684 0.46746 0.46621 0.46666 0.47076 P1 /PTP 0.47026 P1 /PTP 0.47026 0.47026	X/RMAX 0.39800 0.49100 0.44900 0.52700 0.57000 -1.0000 -1.0000 -1.0000				
37 42 A001TION 0 WORD 37 17 27 27 37 42 57 A001TION 0 WORD 52 57 A001TION	PL 14.153 14.143 14.143 14.163 14.128 14.079 14.229 14.249 14.248 14.246 AL PRESSUPE PL 14.246 AL PRESSUPE	0.98622  PATIOS , FOP  PL/PO 0.99147 0.99077 0.99042 0.99217 0.98972 0.98622 0.99217 0.98622 0.99217 0.98622 0.99217 0.98622 0.99217 0.98622 0.99211 PATIOS , 20  PL/PO 0.99811 PATIOS , 80	0, 31699  FRODY IMLET  PI /PTF 0.31859 0.31825 0.31802 0.31609 0.32072 WF771F PLAP 0.32072 0.32072 DFG SHROUD 1	PI /PYP 0.46712 0.46670 0.46664 0.46746 0.46621 0.46621 0.46666 0.47076 0.47076 0.47026 0.47026 0.47026 0.47026 0.47026	X/RMAX 0.39800 0.43100 0.44900 0.52700 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
37 42 A001TION  0 WORD 37 17 72 27 37 42 57 A001TION  0 WORD  0 WORD	PL 14.153 14.153 14.143 14.138 14.163 14.128 14.079 14.248 14.079 14.248 14.079 14.248 14.246 AL PPESSURE PL 14.248 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSURE PL 14.248 AL PRESSU	0.98622  PATIOS , FOP  PL/PO 0.99147 0.99077 0.99042 0.99217 0.98622 0.98612 0.98611 0.99811 0.99811 0.99811 PATIOS , 20  PL/PO 7.99846 0.99811 PATIOS , 80	0, 31699  FRODY IMLET  PI /PTF 0.31859 0.31825 0.31881 0.31802 0.31609 0.22072 0.32072 0.32072 0.32072 DEG SHENUN II  PI /PTF 0.72083 0.32072 DEG SHENUN II	0.46467 PI /PTP 0.46713 0.46680 0.46664 0.46661 0.46661 0.46466 0.47076 PI /PTP 0.47026 0.47026 0.47026 0.47026 0.47026 0.47026 0.47026	X/RMAX 0.39800 0.43100 0.44900 0.52700 0.52700 1.0000 1.0000 1.0000 1.0000 X/DMAX C.79300 0.84400				
37 42 A001TION 0 40R0 07 12 72 27 37 42 52 57 A001TION 0 40R0 67 72 A001TION	PL 14.153 14.143 14.143 14.163 14.128 14.079 14.244 14.079 14.244 14.245 14.246 14.246 14.246 14.246 14.246 14.246 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248 14.248	0.98622  PATIOS , FOP  PL/PO 0.99147 0.99072 0.99022 0.99217 0.98622 0.99217 0.98622 0.99217 0.98622 0.99217 0.98622 0.99217 0.98622 0.99211  PATIOS , 20  PL/PO 7.90846 0.99811  PATIOS , 80  PL/PO 7.90846 0.99811  PATIOS , 80	0, 31699  FRODY IMLET  PI /PTF 0.31859 0.31825 0.31825 0.31802 0.31809 0.2072 0.32072 0.32072  PI /PTF 0.32072  DEG SHPOUD 1  PI /PTF 0.30252	0.4646F PI /PTP 0.46713 0.46680 0.46684 0.46621 0.46682 0.47026 0.47026 0.47026 PI /PTP 0.47343 0.47026 0.47026 0.47026	X/RMAX 0.39800 0.43100 0.44900 0.52700 0.57800 -1.0000 -1.0000 -1.0000 X/DMAX 0.79300 0.79300				
37 42 A001TION D WORD 37 12 72 73 37 42 57 A001TION D WORD 67 72 A001TION O WORD P2 P7	PL 14.153 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163 14.163	0.98622  PATIOS , FOP  PL/PO 0.99147 0.99077 0.99042 0.99217 0.98622 0.98612 0.98611 0.99811 0.99811 0.99811 PATIOS , 20  PL/PO 7.99846 0.99811 PATIOS , 80	0, 31699  FRODY IMLET  PI /PTF 0.31859 0.31825 0.31825 0.31802 0.31690 0.22072 0.32072  MCZTIP PLAP 0.32072  DEG SHENUN II  PI /PTF 0.30252 0.30252 0.30252 0.29735	0.46467 PI /PTP 0.46713 0.46680 0.46664 0.46661 0.46661 0.46466 0.47076 PI /PTP 0.47026 0.47026 0.47026 0.47026 0.47026 0.47026 0.47026	X/RMAX 0.39800 0.43100 0.44900 0.52700 0.52700 1.0000 1.0000 1.0000 1.0000 X/DMAX C.79300 0.84400				

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1,731   3,0822   0,19015   0,2745   0,7220     1,731   1,2745   0,1917   0,4755   0,4755     1,731   1,2745   0,7741   0,7749   0,4755   0,4755     1,182   0,9910   0,2759   0,3914   1,0170     1,184   0,9910   0,4755   0,4755   0,4750     1,185   0,9910   0,4755   0,4755   0,4750     1,185   0,9910   0,4755   0,4755   0,4750     1,185   0,9910   0,4755   0,4755   0,4750     1,180   0,9910   0,4755   0,4755   0,5700     1,180   0,9910   0,4755   0,4755   0,5700     1,181   0,9910   0,7777   0,3910   0,5700     1,181   0,9910   0,7777   0,3910   0,4750     1,181   0,9910   0,7777   0,3910   0,3910     1,181   0,9910   0,7777   0,3910   0,4100     1,181   0,9910   0,7777   0,3910   0,4100     1,181   0,9910   0,7777   0,3910   0,4100     1,181   0,9910   0,7777   0,3910   0,4100     1,181   0,9910   0,7777   0,3910   0,5700     1,181   0,9910   0,7777   0,3910   0,5700     1,181   0,9910   0,7777   0,3910   0,5700     1,181   0,9910   0,7777   0,3910   0,5700     1,181   0,9910   0,7777   0,3910   0,5700     1,181   0,9910   0,7777   0,3910   0,7777   0,3910     1,181   0,9910   0,7777   0,3910   0,7777   0,3910     1,181   0,9910   0,7777   0,3910   0,7777   0,3910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,3910   0,7910     1,181   0,9910   0,7777   0,7910     1,181   0,9910   0,7777   0,7910     1,191   0,9910   0,7777   0,7910     1,190   0,9910   0,7777   0,7910     1,190   0,9910   0,7910   0,7910   0,7910     1,190   0,9910   0,7910   0,7910   0,7910     1,190   0,9910   0,7910   0,7910   0,7910     1,190   0,9910   0,7910   0,7910   0,7910     1,190   0,9910   0,7910   0,7910   0,7910     1,190   0,9910   0,	17.21 17.21 17.21 17.21 17.21 14.17 24.26 57 14.17 24.26 67 24.26 67 24.26 67 24.26 67 19.50 19.50 17.52 17.53		Pt /DTF						
17.729   2.6622   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0.7720   0	47 17.21 47 14.17 557 14.17 557 14.17 557 14.17 557 14.17 557 14.17 557 14.17 557 14.17 557 14.20			0707 70	W ACRES W				
13.721   1.7344   0.73457   0.44276   0.45200     13.402   0.49340   0.77559   0.4946   1.0110     14.171   0.49340   0.77559   0.4946   1.0110     14.171   0.49340   0.77559   0.4946   0.4000     11.400   1.3650   0.4777   0.5449   0.4700     12.202   1.3650   0.4777   0.4449   0.4000     12.203   0.4777   0.4777   0.4449   0.4000     13.204   1.3650   0.4777   0.4449   0.4000     13.205   1.3650   0.4777   0.4449   0.4000     13.205   1.3650   0.4777   0.4449   0.4000     13.206   1.3650   0.4777   0.4449   0.4000     13.206   1.3650   0.4777   0.4449   0.4000     14.131   0.4970   0.4777   0.4440   0.4440     14.131   0.4970   0.4777   0.4440   0.4440     14.131   0.4970   0.4777   0.4440   0.4440     14.131   0.4970   0.4777   0.4440   0.4440     14.131   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440   0.4440     14.201   0.4970   0.4777   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440   0.4440	47 17.21 47 13.89 52 14.17 NVD WIPD PI 62 24.26 64 19.50 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54.00 54		7 1065	0.27456	0-72200				
13.497   0.4734   0.2705   0.3864   0.9190	47 13.89 57 14.17 54.17 54.18 62 24.26 65 24.26 67 19.50 54.17 54.20 77 12.20		41764.0	0.48269	J. 82000				
	57 14.17  >ANDITIONAL PRESS  WD WIRD PI 24.26  67 24.26  57 19.50  WD WIRD PL 22.20  77 17.25		27055	0.38CA3	0.0100				
	>Annitinual PRESS  NO WIRD PI 24-26  62 24-26  67 19-50  >Annitinual PRESS  WI WIRD PI 22-20  77 17-25		0.27599	n. 39746	1.0170				
	A CONTROL OF 1 19, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 10, 50 1								
19, 265   17, 709   17, 777   0,5449  0,67000   19, 500   1, 1669   0,3777   0,5449  0,67000   19, 500   1, 1669   0,3777   0,5449  0,57000   1, 1669   0,3777   0,5449  0,57000   1, 1669   0,3777   0,5449  0,57000   1, 10000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000	62 24-26 67 19-50 57 19-50 54701710NAL PRESS VD WORD PL 17 17 17-25	• 6:11.4	21.11.14	•					
1, 265   1, 2009   0, 37977   0, 54491   0, 67000	67 19,26 67 19,50 >Annitinal PRESS WD WIRD PL 77 12,28	04 / PG	PL/PTF	01 / b Tb	X/DMAX				
19,100   1.1069   0.31977   0.5463   0.67000     10,225   1.2002   0.31975   0.14976   0.50000     10,225   1.2002   0.31975   0.4931   0.51300     10,236   1.2002   0.31975   0.4931   0.51300     10,236   1.2002   0.31975   0.49310   0.51300     10,113   0.49000   0.2745   0.3957   1.0000     10,113   0.49000   0.2745   0.3957   1.0000     10,113   0.49000   0.2745   0.3957   1.0000     10,114   0.49170   0.2745   0.3957   1.0000     10,114   0.49170   0.2745   0.3957   1.0000     11,114   0.49170   0.2745   0.3957   0.3960     11,114   0.49170   0.2745   0.3977   0.3978   0.49100     11,114   0.49170   0.2745   0.3978   0.4910     11,114   0.49170   0.2745   0.3978   0.49100     11,114   0.49170   0.2745   0.3978   0.4900     11,114   0.49170   0.2745   0.3978   0.3948   0.3948     11,114   0.49170   0.2745   0.3948   0.3948   0.3948     11,114   0.49170   0.2745   0.3948   0.3948   0.3948     11,114   0.49170   0.2745   0.3948   0.3948   0.3948     11,114   0.49170   0.2747   0.3948   0.3948   0.3948   0.3948     11,114   0.49170   0.2777   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3948   0.3	67 19.50 >ADDITIONAL PRESS NO WORD PL 77 12.20		0-47256	0.68055	0.42200	:			
### PRESSURE PATINS , FICH SPITTER P.D.  ##################################	SANDITIONAL PRESS NO WORD PL T7 12.20		0.37977	16995-0	0.6 7000				
12.265   2.66117   0.23926   0.3445   0.50000     12.265   2.66117   0.23926   0.3445   0.50000     12.265   2.66117   0.23926   0.3445   0.50000     12.265   1.6202   0.23224   0.34624   0.43100     14.126   1.9202   0.23224   0.34624   0.24020     14.111   0.9000   0.27224   0.39527   1.0000     14.111   0.9000   0.27224   0.39527   1.0000     14.111   0.9000   0.27224   0.39527   1.0000     14.111   0.9000   0.27224   0.39527   0.39620   0.43100     14.111   0.9000   0.27224   0.39527   0.43100     14.111   0.9000   0.27224   0.39527   0.43100     14.111   0.9000   0.27224   0.39527   0.43100     14.111   0.9000   0.27224   0.39527   0.43100     14.111   0.9000   0.27224   0.39527   0.43100     14.111   0.9000   0.27224   0.39527   0.43100     14.241   0.9000   0.27725   0.39527   0.43100     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.241   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39527   0.4900     14.250   0.9000   0.27725   0.39000     14.250   0.90000   0.27725   0.39000     14.250   0.90000   0.27725   0.39000     14.250   0.90000   0.27725   0.39000     14.250   0.90000   0.27725   0.39000     14.2	17 WORD PL 12.28	PATINS	SPI ITTER	D.					
12,225				1					
1,206   1,200   0,2754   0,2834   0,5830		_	7.771	0 344.54	X/MAX				
14,206			0.33505	0.46341	0.58300				
	-		0.27667	0-39844	0.67000				
14.13	Actual Property		I		1				
				\					
14.114	400		PL/PTF		K/DMAX		:		•
		<i>!</i>		0.39634	-1-0000				
				0.39578	-1.0000				
14.052   0.94816   0.27454   0.37544   -1.0000     14.052   0.94801   0.27556   0.39411   1.0000     14.111   0.9950   0.27427   0.39534   0.39500     14.111   0.9950   0.27427   0.39576   0.43600     14.111   0.99810   0.27541   0.39576   0.45000     14.052   0.99810   0.27541   0.39576   0.55200     14.052   0.99810   0.27554   0.39576   0.55200     14.052   0.99810   0.27554   0.39576   0.55200     14.052   0.99810   0.27756   0.3941   0.58000     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.241   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281   0.99810   0.27726   0.39942   0.84400     14.281		\	73.20	29966	0000-1-				
14.052   0.294501   0.27366   0.39411   1.0000   14.131   0.90960   0.27422   0.39534   0.39600   14.111   0.90960   0.27422   0.39534   0.39600   14.111   0.90960   0.27422   0.39534   0.43100   14.111   0.90951   0.27422   0.39534   0.43100   14.141   0.99531   0.27434   0.39534   0.451000   14.007   0.99614   0.2744   0.39534   0.39536   0.52200   14.007   0.99614   0.2744   0.39534   0.39630   0.2744   0.39630   0.2744   0.39630   0.27735   0.39647   1.0000   14.241   0.99630   0.27735   0.39647   1.0000   14.241   0.99630   0.27735   0.39647   0.39647   0.39640   14.241   0.99630   0.27735   0.39642   0.39640   14.241   0.99630   0.27735   0.39642   0.39640   14.241   0.99630   0.27735   0.39642   0.39640   14.241   0.99630   0.27735   0.39642   0.39640   14.241   0.99630   0.27735   0.39647   0.39641   0.29640   13.503   13.503   0.94410   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.37671   0.3767	1		0.27454	-	-1-0000		***************************************		
	\		0.27366	0.39411	0000			1	******
					,				
#IPD PL   PL/PD   PL/PD   PL/PT   PL/PTP   L/DMAK   L/131   0.990%0 0.27422   0.39634   0.39634   0.39630   14.116   0.99955   0.49100   14.116   0.99955   0.27467   0.39574   0.49100   0.49100   14.111   0.99813   0.27454   0.39574   0.49800   14.007   14.007   0.99814   0.27454   0.39574   0.59610   0.52200   0.52200   0.52200   0.27454   0.39673   0.5941   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59610   0.59	1	PATIDS	. !						
14,   18	d Oduh			PL/PTP	X/DMAX				
14.116			0-27522	0.39634	0.39800		•		
14.141	!		0.27402	0.39592	00164-0				
14,097			0.27484	0.39578	000 77 0				
14,052			0.27656	0.39536	0.52200				
14.24		:	0.27366	0.39411	0.56800				:
14.24			1	2000	1			•	: !
			0.27735	2006-0	1:0000	; ; ; ;	**************	***	
14.24	this land store		L						
14.241	3000				,,,,,,,				
		1	V	7,39967	-1-0000		:		
			0.27735		-1-0000				
PI									
PL 14.736 0.99795 0.77726 0.3992P 14.236 0.99795 0.27735 0.39942  INMAL PRESSUPE RATIOS 8 00 DEG SHRNUM LOCATION  PL PN PL PL PN PL PT PT PT PT PT PT PT PT PT PT PT PT PT	_1_	RATIOS , 29	CHOLID	CATIFN					
14.236 0.99795 0.27726 0.39928 14.241 0.99830 0.27735 0.39942  NNAL PRESSUPE RATIOS 8 80 DEG SHRNUM LOFATION PL PL/PN PL/PN PL/PN PL/PTP N 13.503 0.94.47 0.2677 0.37871 13.283 0.9' 114 0.2677 0.3254 5 WEASINGM THRIST PARAMETERS	۵		PL/PTF	el /PTP	X/DMAX				
14.241 14.9830 0.27737 0.54942  INMAL PRESSUPE RATIOS 8 80 DEG SHRNUM LOFATION  PL/PN P1/PT P1/PTP N  13.503 0.46.7 0.25797 0.37871  13.283 0.9' 114 0.25470 0.3254  5. WEASIDED THRIST PARAMETERS			0.27726	0.39926	J. 79300				
PL PRESSUPE RATIOS 8 80 DEG SHRNUM LOCATION PL/PN PL/PN PL/PN PL/PN R 13-503 0-94-714 0-26-77 0-37871 5 MFASIBED THRUST PARAMETERS			0.2777	24665.0	0.82400	,			!
PL 094043 0,26.97 0,37871 13,503 0,94043 0,26.97 0,26.71 0,25.75 0,37875 5, WFASIBED THRUST PARAMETERS	3	RATIOS , 80	SHRUIN	CATION					
13.503 0.96.53 0.26.797 0.37871 13.283 0.9 114 0.25870 0.37255 5 WEASTRED THRUST PARAMETERS		64/14	Pt / BTE	01/970	X/DMAX				
13.283 0.9 114 0.25870 0.5255 5 MEASIMEN THRUST PARAMETERS			0.26797	0.37671	0.79300				
S . WELSIDED THRUST PARAMETERS			0.25870	0.51255	0.84400				
	TION 5.		ETFPS	1					

	VASA-1 FW19	RFL [m	IMARY DATA	06/13/79	FADDF11	PEC 10/24/	79 73:17:06.326	FAC SEGEL	PSM C034	RUN 24 PRG 1461
OR PHOR OF THE STANDARD	PADDITION	N PPESSUPE	PATINS . PPI	MARY PLUG						
	AVD HORD	PI	PL / PO	PI /PTF	PL /PTP	X /DMAX				
	32	10.901	0.76501	0.10317	0.26641	0.72200				
3 3	37	16.375	1.1442	0.27796	0.39847	0.82000				
	5.7	16.944	1-1790		0.4147	0.91900				
_ ^_	52	17.394	0.86977	0.29824	0.302##	1.0170				
<b>₽</b>	24	27.2.7.4	<b>QQ</b> 1 <b>Q</b> 1.11	301 7 1 7	•••					
	NOT TERRAC	LL PRESSUPE	PATING . FER	M SPI ITTEP I	I.n.				the comments with the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments of the comments	
	AVD WORD	PI	PL /PN	PL /PTF	PI /PTP	X/DMAX				
· ·	62	27.715	1.9449	0.46567	0.67730	0.42200				
rg.	67	21.72R	1.5247	0.36507	0.53099	3.67000				
	>AUDIT TON	N PRESSUPE	PATIOS . FLO	W SPITTER O	D_ 0_	·				
		, man time taken a page and					× + -			
	TAU MUND	<b>*</b> I	PL/PN	Pt /PTF	PL /PTP	x/DMAX				
	. 77	14-170	0.99434	Q+23A09	0.34629	0.50800				
	82	20.017	1.4747	0.33632	0.48917	0.58300				
-	92	14,195	0.99613	0,23850	0.34690	0.67000				
	- AMOUTION	E PRESSURE	<del>Lattis T. en</del>				ryn war i r			
323	AVO WORD	PI	PL / PO	PL /PTF	PLEBRO	X/DMAX				
ü	-137	14.105	2 98 98 2	0.73690	0.34470	/-1-0000	and the second section is a second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the se			
	-112	14.095	0. 949]	0.21693	0.34446	-1.0000				
-	-127	14.790	2-24977	77-23674	0.34434	-1-0000				
	-127	14.125	7.99122	0.23733	0.34519	-1-0000				
	-137	14.090	0. 99877	0.23474	0.	-1-0000	· · · · · · ·		•	•
	-152	14.055	0.79632	0.73616	0.34248	0000				
			RATIOS . FOR							
_	Sector I I I I I I I I I I I I I I I I I I I									
-			PL / PI?	PL/PT C	PL/PTP	X/DMAX		4		
_	AVD_WOPD	P.L.						•		
_	107	14-195	0.94942	0.23699	0-34470	0.39800				
_	107 112	14-105	0.98982 9.99912	9.23683	0.34446	0.43100		englase case a laboration of the con-		
	107 112 172	14.195 14.995 14.990	0.99982 9.99912 0.99877	0.23683 0.23674	0.34446	0.43100				ayan <del>andari</del> ya a <b>a a a</b>
_	107 112 122 122	14-125 14-295 14-290 16-125	0.94982 9.94912 9.94877 0.99122	0.23683 0.23674 0.23733	0.34446 0.34434 0.34519	0.43100 0.44900 0.48600				
-	107 112 122 127 137	14.195 14.995 14.990 14.125 14.999	0.98982 9.99912 9.99877 0.99122 9.99877	9.23683 0.23674 0.23733 9.23674	0.34446 0.34434 0.34519 0.34434	0.43100 0.44900 0.48600 0.52200				
-	107 112 127 127 137 147	14.195 14.995 14.990 16.125 14.999 14.955	0.98982 9.99912 0.99877 0.99122 0.99637	9.23683 0.23674 0.23733 9.23674 0.23616	0.34446 0.34434 0.34519 0.34424 0.34748	0.43100 0.44900 0.48600 0.52200 0.58800				
-	107 112 122 122 127 137 142	14.105 14.095 14.090 16.125 14.090 14.055	0.98982 9.99912 0.99877 0.99122 0.99877 0.99632	7.23683 0.23674 0.23733 7.23674 0.23616	0.34446 0.34434 0.34519 0.34424 0.34748	0.43100 0.44900 0.48600 0.58800				
	107 112 127 127 137 147	14.195 14.995 14.990 16.125 14.999 14.955	0.98982 9.99912 0.99877 0.99122 0.99637	9.23683 0.23674 0.23733 9.23674 0.23616	0.34446 0.34434 0.34519 0.34424 0.34748	0.43100 0.44900 0.48600 0.52200 0.58800				
	107 112 127 127 137 142 =147	14.125 14.295 14.290 16.125 14.093 14.055	0.98982 9.99912 0.99877 0.99122 0.99877 0.99632	9. 23683 0. 23674 0. 23733 9. 23674 0. 23616 9. 2317	0.34446 0.34434 0.34519 0.34424 0.34748 0.24787	0.43100 0.44900 0.48600 0.58800				
-	107 112 127 127 137 142 =147	14.125 14.295 14.290 16.125 14.093 14.055	0.9892 9.9992 0.99877 0.99122 0.99877 0.99632 0.77873 7.90928	9. 736 83 0. 736 74 0. 23 733 9. 23 674 0. 23 674 0. 23 616 70. 23 717 9. 73 926	0.34446 0.34634 0.34519 0.34624 0.34748 0.34748	0.43100 0.44900 0.48600 0.52200 0.58800				
-	107 112 172 127 137 142 117	14-125 14-290 14-290 15-125 14-290 14-25 14-25 14-25 14-25 14-25 14-25	0.98982 9.98912 0.98877 0.99122 0.98877 0.98632 0.98632 0.98632	9. 23683 0. 23674 0. 23733 9. 23674 0. 23616 9. 2317	0.34446 0.34634 0.34519 0.34624 0.34748 0.34748 0.24767 7.54677	0.43100 0.44900 0.48600 0.52200 0.58800 1.0000				
-	107 112 122 127 137 142 117 147	14-125 14-290 14-125 14-090 14-125 14-090 14-055 14-25 14-25	0.98982 9.99912 0.99877 0.99122 0.9957 0.98632 0.7787 7.90928	9. 736 83 0. 736 74 0. 23733 9. 23676 0. 23616 10. 2217 17. 23926	0.34446 0.34634 0.34519 0.34624 0.34748 0.34748	0.43100 0.44900 0.48600 0.52200 0.58800				
-	107 112 127 127 137 142 117 117 117 117 117 117 117 117	14.105 14.105 14.109 14.125 14.000 14.005 14.005 14.005 14.005 14.005 14.005 14.005	0.98982 9.99912 0.99877 0.99122 0.99577 0.99632 0.77873 7.90928 0.77873	9. 73683 0. 73674 0. 23733 9. 23674 0. 23616 9. 7377 9. 73926	0.34446 0.34634 0.34519 0.34624 0.34748 0.34748 0.34747 0.34787 0.34787	0.43100 0.44900 9.48600 0.52200 0.58800 1.0000 X/DMAX -1.0000				
-	107 112 127 127 137 142 147 147 147 147 147 147 147 147 147 147	14.105 14.095 14.095 14.090 14.055 14.097 14.055 14.797 18.797 18.797 14.235 16.240	0.98982 9.99912 0.99877 0.99122 0.98632 0.77873 7.90928 0.77873 7.90928 0.77873 9.99928	9. 23683 0. 23674 0. 23733 9. 23674 0. 23616 9. 12717 9. 23928 HAPPLE PLAN 0. 2-17 9. 23926 DEG SHROUD L	0.34446 0.34434 0.34519 0.34424 0.3448 0.24787 0.34787 0.34787 0.34787	0.43100 0.44900 0.48600 0.52200 0.58800 1.0000 1.0000 X/DMAX -1.0000				
-	107 112 127 127 137 142 147 147 147 147 147 147 147 217 217 217 217 217 217 217 217 217 21	14-105 14-195 14-090 15-125 14-090 14-055 14-075 14-235 14-235 14-240 14-235 14-240	0.98982 0.98912 0.98877 0.98877 0.98632 0.77873 7.90928 PATINS . 20 PL/PD	9. 73683 0. 73674 0. 23733 9. 23674 0. 23616 9. 7317 9. 73928 9. 73928 0. 73926 DEG SHROUN L	0.34446 0.34434 0.34514 0.34424 0.34749 0.34749 0.34747 0.34747 0.34747	0.43100 0.44900 0.48600 0.58800 1.0000 1.0000 X/DMAX -1.0000				
-	107 112 127 127 137 142 127 137 142 127 157 2400111000  AVD MORD -1*2 -157 >AODITION  AVD MORD 167	14-105 14-095 14-090 14-125 14-090 14-095 14-095 14-297 14-295 14-295 14-295 14-295	0.98982 9.9912 0.99122 0.99122 0.99637 0.98632 0.99928 0.99928 0.99928 0.99928 0.99928 0.99928 0.99928	9. 73683 0. 73674 0. 23733 9. 23674 0. 23616 9. 73928 99716 PLAY 0. 23926 DEG SHROUP L	0.34446 0.34514 0.34514 0.34748 0.34748 0.34747 0.34787 0.34787 0.34787	3.43100 9.44900 9.48600 0.58800 1.0000 1.0000 X/DMAX -1.0000 -1.0000				
-	107 112 127 137 142 147 147 147 147 147 147 147 147 147 147	14.105 14.095 14.095 14.090 14.125 14.090 14.055 14.235 14.235 16.240 14.235 14.235 14.235	0.98982 9.9912 0.99127 0.99127 0.99632 0.7783 7.99928 PATINS . 20 PL/PN 0.99893 0.99893	0.23674 0.23674 0.23733 0.23674 0.23616 0.23616 0.2317 0.23926 DEG SHROUN L	0.34446 0.34434 0.344519 0.34424 0.34748 0.24707 0.34787 0.34787 0.34787 0.34787	0.43100 0.44900 0.48600 0.58800 1.0000 1.0000 X/DMAX -1.0000				
- -	107 112 127 127 137 142 142 142 142 142 142 142 142 142 142	14-105 14-095 14-090 14-125 14-090 14-095 14-095 14-297 14-295 14-295 14-235 14-235 14-235	0.98982 9.99912 0.999122 0.99637 0.99632 0.99632 0.99928 PATINS . 20 PL/PN 0.99893 0.99893 0.99893 RATINS . 80	9. 23683 0. 23674 0. 23733 9. 23674 0. 23616 9. 12717 9. 23926 DEG SHROUN 1 PL/PTF 0. 23917 9. 23917 9. 23917	0.34446 0.34634 0.34619 0.34626 0.34748 0.24787 0.34787 0.34787 0.34787 0.34787 0.34787 0.34787	3,43100 0,44900 9,48600 0,58800 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000				
-	107 112 127 127 137 142 142 142 147 147 147 2177 240012 1040 AVD WOPD 167 172 >ADDIT 1040 AVD WOPD	14-105 14-095 14-090 15-125 14-090 14-055 14-095 14-055 14-235 14-235 14-235 14-235 14-235	0.98982 9.9912 9.9912 9.99122 9.9832 0.9832 0.99328 PATINS - 20 PL/PN 0.99893 9.99928 PATINS - 20 PL/PN 0.99893 9.99993 RATINS - 80	9.23683 0.23674 0.23733 9.23674 0.23616 9.12717 9.23926 HOPPLE PLAN 0.23926 DEG SHROUD L PL/PTF 0.23917 0.23917 0.23917	0.34446 0.34634 0.34634 0.34624 0.34748 0.24767 0.34787 0.34787 0.34787 0.34787 0.34787	3,43100 0,44900 9,48600 3,52200 0,58800 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000				
-	107 112 127 127 137 142 147 147 147 147 147 147 147 147 147 147	14.105 14.095 14.095 14.090 14.065 14.065 14.797 18.797 18.797 18.797 18.235 16.240 14.235 14.235 14.235 14.235	0.98982 9.9912 9.9917 0.99127 0.99632 0.777 0.99632 0.777 0.99632 0.777 0.99632 0.777 0.99632 0.777 0.99632 0.777 0.99632 0.99703 0.99928 PATINS . 20 PL/PN 0.99893 0.99893 RATINS . 80 PL/PN 0.93555	0.23674 0.23674 0.23674 0.23616 0.23616 0.23616 0.23616 0.23616 0.23926 DEG SHROUN L PL/PTF 0.23917 0.23917 0.23917 0.23917 0.23917 0.23917	0.34446 0.34434 0.34519 0.34424 0.34748 0.24767 0.34787 0.34787 0.34787 0.34787 0.34787 0.34787	3.43100 0.44900 0.48600 0.52200 0.58600 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
	107 112 127 127 137 142 147 147 147 147 147 147 147 147 147 147	14.105 14.095 14.090 14.125 14.090 14.065 14.075 14.235 14.235 14.235 14.235 14.235 14.235 14.235	0.98982 9.9912 9.9912 9.99122 9.9832 0.9832 0.99328 PATINS - 20 PL/PN 0.99893 9.99928 PATINS - 20 PL/PN 0.99893 9.99993 RATINS - 80	9.23683 0.23674 0.23733 0.23674 0.23616 0.23616 0.23717 0.23926 DEG SHROUN 1 PL/PTF 0.23917 0.23917 0.23917 0.23917 0.23917 0.23917 0.23917	0.34446 0.34634 0.34634 0.34624 0.34748 0.24767 0.34787 0.34787 0.34787 0.34787 0.34787	3,43100 0,44900 9,48600 3,52200 0,58800 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000 1,0000				

VACA-LEW!	2 batflm	IMARY DATA	06/13/79	CADNETI	REC 10/24/	79 23:17:44.424	FAC 9X6Y1	PG4 C034	RUN24
>400111004	LI PPFSSIMF	PATINS . PPI	MARY PLIIG						
NU AUSD	PI	PI / PT	PI /PTF	PL /PTP	X/DMAX	and the same of			*
32	10-892	0.76410	0.19298	0.26593	0.72200				
27	16. 298	1. 1433	0-27340	0.35792	0.92000				
47	16.936	1.1981	2.25453	0.41359	3. 91 900				
57	12.373	0.96803	0.20787	0.39210	1.0170				
>POOLT TONK	IL PRESSUPE	PATINS . FER	W SPESTTEP S	. n.	washin ee waxayaan waxaa ahaa	er vetteterienne i van in steam anders in de			
VP WOPS	Pt	PI /PI	P1 / PTF	PL /PTP	x/P#AX				
52	27.796	_ 1.9437	9-46547	0.67647	) <b>.</b> 422 <b>00</b>				
67	21.717	1.5235	0.36485	0.53024	J.67000				
>ADDIT FON	LL PPESSUPE	PATIOS . FLO	W SPLITTEP D	ı. n.			- <del> </del>		
מפחש מע	PL	PI /PI	PL /PTF	PI /PTP	X/DMAY		•	<del>-</del>	
77	14-174	0.99433		0.35606	0.50000				
R2 ~	20.007	1.4036	0.33612	0.48849	0.5 F 300				
02	14.234	0. 97643	0. 23862	0.34679	0.67000				
**************************************	E PRESSURT	-41173 IL 60	CT CO SHANNE						
VD WORD.	PL	PL/PD	PL/PTF	PLEE	X/PMAX.	rant comp.			
107	14.104	0.98943	7.27696	0.34435	-1.0000				
112	14,094	0. 98973	0623674	0.34411	-1-0000				
122	14.084	0.98865	75-23661	0.34387	-1-0600				
127	14.129	0.99118	0.23736	0,34496	-1.0000				
137	14.019	0.9993#	0. 73669	0.38960	-1.0000				
1.62	15,049	0,94558	0.23602	0.34301	-1-0000				
>ADDITIONA	AL PRESSURE	RATIOS . FCR	ERPOY INLET						
	IL PRESSURE	RATIOS . FOR		PI /9TP	Y/RMAY				
VO HORD	PL	PLZPD	PL/PIF	PL/PTP	X/5MAX				
¥n ⊌nRĐ	PL 14.104	PL/PD	PL/PIF	0.34435	0.39#00		•		
VP WORD	PL 14.104 14.094	PL/PD 0.98943 0.98873	PL/PIF	0.34435 0.34411	0.39400 0.43100				
VN WNRD 107 11? 12?	PL 14.104 14.094 14.384	PL/PD 9.98943 0.98673 0.99803	PL/PIF 0.73694 0.23678 0.23661	0.34435 0.34411 0.34287	0.39400 0.43100 0.44900		•		
VP WORD 107 11? 12? 127	PL 14.104 14.094 14.384 14.129	PL/PD 9.98943 9.98873 0.99803 0.99118	PL/PIF	0.34435 0.34411 0.34287 0.34496	0.39400 0.43100 0.44900 0.48600		•		
Vn WNRD 107 11? 12? 127	PL 14.104 14.094 14.384 14.129 14.089	PL/PD 9.98943 0.98673 0.99803	PL/PIF 0.73694 0.23678 0.23661	0.34435 0.34411 0.34287	0.39400 0.43100 0.44900		•		
Vn WNRD 107 11? 12? 127 127	PL 14.104 14.095 14.384 14.129 14.089	PL/PD 0.9843 0.98673 0.99803 0.9918 0.9918	PL/PIF 0.73694 0.23678 0.23661 0.23736 0.23669 0.73602	0.34435 0.34411 0.34287 0.24496 0.34399 0.34301	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800		•		
VN WNRD 107 11? 12? 12? 127 142	PL 14.104 14.094 14.384 14.129 14.089	PL/PD 9.98943 9.98873 0.99803 0.99118 2.99838	PL/PIF 0.73694 0.23678 0.23661 0.23736 0.23669	0.34435 0.34411 0.34287 0.34496 0.34399	0.39#00 0.43100 0.44*00 0.48690 0.52200				
Vn WNRD 107 11? 11? 12? 12? 137 142	P1 14.104 14.094 14.384 14.129 14.089 14.089 14.049	PL/PD 0.98943 0.98873 0.99803 0.99118 1.99838 0.99558	PL/PIF 0.73694 0.23678 0.23661 0.23736 0.23669 0.73602 0.23617	0.34435 0.34411 0.34287 0.34496 0.34390 0.34390 0.34301 0.54772	0.39#00 0.43100 0.44*00 0.58#00 0.58#00				
Vn WNRD 107 117 122 127 127 142 142 142 142 147 147 Vn WNPD	P1 14.104 14.094 14.384 14.129 14.089 14.049 14.233	PL/PO 9.9843 9.98673 0.99803 0.99118 9.99838 0.99559 9.99559	PL/PIF 0.73694 0.23678 0.27661 0.23736 0.23669 0.73602 0.23617	0.34435 0.34411 0.34287 0.34496 0.34399 0.34301 0.24772 0.24772	0.39400 0.43100 0.44400 0.48600 0.52200 0.58800 1.0000		•		
Vn WNRD 107 11? 12? 12? 127 142 142 142 142 142 142 142 143 Vn WNPD	P1 14.104 14.094 14.384 14.129 14.089 14.089 14.089 14.233	PL/PD 9.9843 9.9873 0.99803 0.99118 9.9959 0.9959	PL/PIF 0.73694 0.23678 0.23661 0.23736 0.23669 0.73602 0.2369 0.73602	0.34435 0.34411 0.34287 0.34496 0.34390 0.34301 0.24772 0.24772	0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 7/0MAY -1.0000				
Vn WNRD 107 117 122 127 127 142 142 142 142 147 147 Vn WNPD	P1 14.104 14.094 14.384 14.129 14.089 14.049 14.233	PL/PO 9.9843 9.98673 0.99803 0.99118 9.99838 0.99559 9.99559	PL/PIF 0.73694 0.23678 0.27661 0.23736 0.23669 0.73602 0.23617	0.34435 0.34411 0.34287 0.34496 0.34399 0.34301 0.24772 0.24772	0.39400 0.43100 0.44400 0.48600 0.52200 0.58800 1.0000				
Vn WNRD 107 11? 12? 12? 12? 142 142 142 142 143 143 144 144 144 147 147 147 147 147 147 147	PL 14.104 14.094 14.364 14.129 14.089 14.049 14.233 14.233 14.233	PL/PD 9.9843 9.9873 0.99803 0.99118 9.9959 0.9959	PL/PIF 0.23694 0.23678 0.27661 0.23736 0.23669 0.23602 0.23612 0.23912 0.23912	0.34435 0.34411 0.34287 0.24496 0.34390 0.34301 0.24772 PL/PTP 0.24752 0.34752	0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 7/0MAY -1.0000				
Vn WNRD 107 112 122 127 127 142 127 142 142 142 142 142 143 144 147 147 147 147 147 147 147	P1 14.104 14.094 14.364 14.129 14.089 14.089 14.089 14.233 14.233 14.233 A1 PRESSURE	PL/PD 9.98943 9.98673 0.99803 0.99116 9.99839 0.9953 0.99853 0.99853 0.99853	PL/PTF 0.73694 0.23678 0.23661 0.23736 0.23665 0.73602 0.23917 0.23917 0.27917 0.27917 0.27917 0.27917	0.34435 0.34411 0.34287 0.34496 0.34390 0.34390 0.34390 0.24772 0.24772 0.24772	0.39#00 0.43100 0.44900 0.52200 0.58000 1.0000 1.0000 7/0MAW -1.0000				
Vn WNRD 107 11? 12? 12? 127 137 142 142 142 152 200 152 200 200 200 200 200 200 200 200 200 2	P1 14.104 14.094 14.364 14.129 14.089 14.089 14.089 14.233 14.233 AL PRESSURE	PL/PO 9. 9843 9. 98873 0. 99803 0. 99118 1. 99839 0. 93559 0. 93559 0. 9373 7. 99853 PATENS 20 PL/PO 0. 99888	PL/PTF 0.23678 0.23678 0.23736 0.23669 0.23602 0.23602 0.23912 0.23912 0.21912 0.21912 0.23912 0.23912 0.23912	0.34435 0.34411 0.34287 0.24496 0.34399 0.34301 0.24772 PL/PTP 0.34752 0.24772 OCATION PL/PTP 0.24764	0.39#00 0.43100 0.44*00 0.48600 0.52200 0.58#00 1.0000 1.0000 1.0000 1.0000				
Vn WNRD 107 11? 12? 12? 127 137 142 142 142 152 200 152 200 200 200 200 200 200 200 200 200 2	P1 14.104 14.094 14.364 14.129 14.089 14.089 14.089 14.233 14.233 14.233 A1 PRESSURE	PL/PD 9.98943 9.98673 0.99803 0.99116 9.99839 0.9953 0.99853 0.99853 0.99853	PL/PTF 0.73694 0.23678 0.23661 0.23736 0.23665 0.73602 0.23917 0.23917 0.27917 0.27917 0.27917 0.27917	0.34435 0.34411 0.34287 0.34496 0.34390 0.34390 0.34390 0.24772 0.24772 0.24772	0.39#00 0.43100 0.44900 0.52200 0.58000 1.0000 1.0000 7/0MAW -1.0000				
Vn WNRD 107 117 127 127 127 127 142 127 Vn WNPD 157 >ANDITION	P1 14.104 14.094 14.364 15.129 14.089 14.049 14.233 14.233 14.233 14.233	PL/PO 9. 9843 9. 98873 0. 99803 0. 99118 1. 99839 0. 93559 0. 93559 0. 9373 7. 99853 PATENS 20 PL/PO 0. 99888	PL/PIF 0.73694 0.23678 0.23661 0.23736 0.23668 0.73602 0.23669 0.73602 0.23917 0.23917 0.23912 DEG SHPRHIP 1 PL/PTF 0.23912 0.23912	0.34435 0.34411 0.34287 0.34496 0.34390 0.34301 0.24772 0.24772 0.24772 0.24772 0.24772 0.24764 0.34764 0.34762	0.39#00 0.43100 0.44*00 0.48600 0.52200 0.58#00 1.0000 1.0000 1.0000 1.0000				
Vn WNRD 107 117 122 127 127 142 127 142 157 200111000 167 177 200111000	P1 14.104 14.094 14.094 14.084 14.129 14.089 14.089 14.089 14.233 14.233 AL PRESSURE P1 14.238 14.233 AL PRESSURE	PL/PD 9.9843 9.98673 0.99803 0.99118 9.99838 0.99559 0.99833 0.99853 0.99853 0.99853 0.99853 0.99853 0.99853 0.99853	PL/PIF 0.73694 0.23678 0.23661 0.23736 0.23669 0.73602 9.23917 0.23917 0.23912 0.23912 0.23912 0.23912 0.23912 0.23912 0.23912 0.23912 0.23912	0.34435 0.34411 0.34287 0.34496 0.34399 0.34301 0.24772 0.24772 0.24772 0.24772 0.24772 0.24772 0.24772 0.24774 0.34722 0.34722	0.39#00 0.43100 0.44*00 0.48600 0.52200 0.58#00 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
Vn WNRD 107 11? 12? 12? 127 142 197 142 157 2001111000 Vn WNPD 16? 172 2001111000 Vn WNPD 182	P1 14.104 14.094 14.364 14.129 14.089 14.089 14.089 14.089 14.233 14.233 14.233 14.233 14.233 14.233 14.233 14.233 14.233	PL/PD	PL/PIF 0.73694 0.23678 0.23661 0.23736 0.23668 0.73602 0.23692 0.23912 0.23912 0.23912 DEG SHPOUP 1 PL/PTF 0.23912 DEG SHPOUP 1 PL/PTF 0.23912 DEG SHPOUP 1 PL/PTF 0.23912 DEG SHPOUP 1	0.34435 0.34411 0.34287 0.34496 0.34390 0.34301 0.24772 0.34772 0.34772 0.34772 0.34772 0.34772 0.34772 0.34772 0.34772 0.34772	0.39800 0.43109 0.44900 0.48600 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
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		-112	14-136	3.99002	7.31.72	0.46680	-1.0000	
		-122	14.131	0.04967	0.31460	0.46663	-1-0000	
		-127	سلفله ا	0,99177	0, 31929	0.46762	-1.0070	•
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		112	14-136	0. 99022	0.31872	0.46680	0.43100	
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1.132	DIT INVAL	00.00 0.99 8 ATTOS	ا تنطيعه ما الأسالات	0.52015 0.52107 0.7102 0.51637	-1.0000			
	OIT INNA	0.99 0.98 0.98	البطيعيدات	0.57107				
14,028   0,99789   0,35784   0,74924   -1,0000     14,028   0,99230   0,3553   0,51637   -1,0000     14,137   0,99696   0,3587   0,52014   0,4900     14,137   0,99696   0,3583   0,52014   0,4900     14,137   0,99696   0,3583   0,52014   0,4900     14,137   0,99696   0,3583   0,52014   0,4900     14,137   0,99696   0,3583   0,51690   0,51690     14,137   0,99697   0,3997   0,51690   0,51690     14,237   0,99607   0,3607   0,51690   0,51690     14,232   0,99607   0,3607   0,52383   0,4990     14,232   0,99607   0,3607   0,52383   0,4400     14,237   0,99607   0,3607   0,52383   0,4990     14,237   0,99607   0,3607   0,52383   0,4490     14,237   0,99607   0,3607   0,52383   0,4490     14,237   0,99607   0,3907   0,4976   0,4930     13,279   0,99607   0,3907   0,4976   0,4930     13,279   0,99607   0,3907   0,4976   0,4930     13,279   0,99607   0,3907   0,4976   0,4976   0,4930     13,279   0,99607   0,3907   0,4976   0,4976   0,4976   0,4976     13,279   0,99607   0,3997   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,4976   0,49	OIT INVAL	0.96 0.98 PATIOS	40. No. 1 (	0.51637	-1.000			
14,026	DIT INNAL	0.9A	<b>4</b> 000	0.51631	-1.000	1		
### ### ##############################	DIT INNAL	PATIOS	1 1		0000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	
14.147		1			/			
14.147	To CAUP		PL/PTF	M /PTP	X/DMAX			
14,137	7	0.99069	0.35657	0.52070	0.3 9.400	•	٠.	
14, 132	1	0.9899P	0.35731	0.52034	1		•	
14.108		0. 00 130 0. 00 130	0.35419	51025-0	0.44400			
14.329		0.98789	0.35756	0.41924	0.52200			
1		0.98230	0.34453	0.51630	0.58800	,		
######################################		1.99067	3.006.0	446.26.26	0000-1			
######################################		ABA a of	216.45.90	0.373	popper	: : : : :		
H4.232         P. 1000         L. 0000           14.232         7.99662         0.70972         0.52383         -1.0000           14.232         9.99662         0.36072         0.77583         -1.0000           10.732         0.99662         0.36072         0.77583         -1.0000           11.237         0.99662         0.36072         0.52383         0.74400           11.237         0.99662         0.36072         0.52383         0.44400           10.737         0.99662         0.36072         0.52383         0.44400           11.237         0.99662         0.35072         0.52383         0.44400           10.738         0.99662         0.35072         0.52383         0.44400           11.237         0.99662         0.35072         0.40798         x/DMAX           11.237         0.9266         0.33656         0.40798         0.79300           13.279         0.91206         0.33011         0.47938         0.86400	Stant fund sacismu	des à Sulation	4					
14,232				25 / 10 TO	244072			
	_	1. Waleb		0.523R3	-1-0990		-	ž k
		9.99662	D. 36072	0.57383	,			
WNP9 PI M1/PG PI/PFF PI/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D PE/PFP D		RATIOS , 20	UI ONUMS 931	CATION				
14,232 0,99662 0,36072 0,52383 14,232 0,99662 0,36072 0,52383 114,232 0,99662 0,36072 0,52383 111,0141 PRESSURE PATINS , MO DEG SHPOUD INTATION 13,279 0,97989 0,33656 0,48875 13,025 0,91206 0,33911 0,47938	000							
14,237		0.59662	9-36972	0.52383	A / DM A A 0 - 74300	•		
DOITINGAL PRESSURE PATINS , NO DEG SHPNIND INTEXTING MIPPE X 13,279 0,429FF 0,33656 0,33656 0,4793F	•	0.99662	0.15372	0.52363	0.84400			
ыпрп рі регреп верет верет в 13,279 0,290м 0,33456 0,4м75 7 13,225 0,91206 0,33011 0,4793м	اب	PATINS . MO	SHOULD	ration.				
7 13,279 0,92988 0,33656 0,4874 7 13,225 0,91206 0,33011 0,47938	u dua	Ca/ 14	P1 / PT F	914/14	X / DMAX			
13,325 0,91206 0,33011 0,47938	· .	0.42988	n. 3345K	0.44874	0. 79300			
	2 1011	0.91206	11686.0	0.47938	0.84400			
S THANKET THREET PARTY	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	THEFT PART			20000			

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1454-1 EN1	S PRFLIMI	HARY DATA	06/13/79	CADDELL	PEC 10/74/7	9 23:72:52.119	FAF 946X1	PG4 (334	PUN 24 PDG 1466
>47017104	AL PPESSIPE	PATINS , PPI	MAPY PLUG						
VD WORD	O(	PL / PO	PL / PTF	PL /PTP	X/DMA X				
32	6.5399	0.45604	0.18202	0.26212	0-72209				
17	9.8449	J. 68964	0.27527	0.39641	0.#2000				
47	14.161	0-99205	0.39596	0.57921	0. 91 <del>90</del> 0				
57 	15.239	1.9675	0.47490	0.61360	1.0170				
>ARRET IRA	IAL PRESSUPE	PATINS , FIN	W SPI ITTEP I	- D-				,	
AL MUBU	PL	PL /PN	PI / PTF	PL/PTP	X/IMAX			•	
£2	16.765	1.1745	. 0.46877.	0.67506	0.42200				•
67	13.099	0. 91 759	0.36624	0.52742	0.67000				
NOT TECOM	AL PRESSURF	PATIOS , FLO	W SPLITTER O	- 0-					
AU NUBD	PL	PL /PG	PL/PTF	PI /PTP	X/OMAX	÷ * · · ·			
	8.2076	2-57496	0.22949	0.33058	0.50000	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1			-
82	19.938	1.3946	0.55663	0.00160	0.58300				
92	14.236	0.99728	0.29005	0.57322	Q-67000				· · · · · · · · · · · · · · · · · · ·
STUDIT SOA	ME PRESSURE	RATIOS IL PAR	COUNTY STORY						
VD WOPD	71	PL/PD	PL/PTE	PLONE	X/DHAX	er e saar e e e			
107	14-171	0.99343	0.39651	0.57101	-1.0000				
117	14-166	0. 99239	39610	0-57041	-1.0000			· · · · · · · · · · · · · · · · · · ·	
122	14-161	0.90294	0.30596	0.57021	-1.0000				
127	14-121	0.99343	0.3969	9.57101	-1.0000	-		*	
1?7 1 <u>52</u>	14.017	0. 98959 9. 98199	0.3949 <i>6</i> 0.39191	0.56438	-1.0000 1.0000				
		RATIOS . FOP					e <del>e</del> n emen	* •	
VO WORD	PL	የL/የበ	PL/PTF	PL/PTP	X/DMAX				
107	14.181	J. 99343	0. 39651	0.571.01	0.39800		τ .		• •
112	14,166	7, 99 239	0.39613	0.57041	0.43100				
122	14.161	0.99204	0.39596	0.57021	0.44900		• • • • • • •		-
127	14-161	0.99343	0.39651	0.57101	0.48600				
137	14.126	0.98959	0.3949P	0.56880	0.52200				
142	14,017	2, 95190	0.39191	0.56438	0.58800				
1-7	14.241	36 9903?		0. 91309	-12:0000				
<del> </del>	14.251	*******	<del>()  </del>	0.97365	-1,0000	*			-
<b>400 11 104</b>	of backthair	P47173 PAN	HOPPLE PLAN						
VD WORD	PL	M/PT	2477	PL /PTP	X/(IMAX				* * *
157	14.251 	0.99833	0.39847	0.57383	-1.0000 -1.0000				
157	AL PRESSIPE				V 48ma V				
ADDIT ION			PL / PTF	PL/PTP	A/1398A				
157 >ADD <b>IT 10%</b> VD WOPD	AL PRESSIPE PL 14.256	PL / PT) 2. 99868	P[ / PTF 0. 39861	PL/PTP 0.57403	X/DMAX 0.79300				
157 ADD <b>IT ION</b> VD 40PD 167	PL	PL/PD							
NO MOPO 167 172	PE 14.256 14.256	PL / PT 2. 99868 3. 99868	0.39861 0.39861	0.57403 C.57403	0.79300				
VN WNPN 167 172 > <u>ANN</u> IT <u>I</u> NW	PL 14.256 14.256 AL PRESSIME	PL/PD 2.99868 2.99868 PATEOS . 80	0.39861 0.39861 DEG SIMPUD L	0.57403 C.57403 PCATTON	0.79300 0.84400				
NANDIT ION VIOLENTE ION 167 172 NANDIT ION VIOLENTE	PL 14.256 14.256 AL PRESSIME PL	PL/PD 2.99868 0.99868 PATIOS . 80	0.39861 0.39861 DEG SIMPUD L	0-57403 C-57403 PLATTON	0.79300 0.84400				
ADD IT ION VO WOPD 167 172	PL 14.256 14.256 AL PRESSIME	PL/PD 2.99868 2.99868 PATEOS . 80	0.39861 0.39861 DEG SIMPUD L	0.57403 C.57403 PCATTON	0.79300 0.84400				

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NO INTITIONAL PRESCRIPT PAYING , PPTMARY PLUG   NO INTO	4854-I FWIS	S PRELIM	THARY DATA	06/17/70	CARDELL	RFC 10/24/79	23:23:50.452	FAC AX641	PGM C034	RUN 24
17. 10.395 0.72620 -0.34489 0.49319 0.72200 17. 13.495 0.99314 0.47118 0.46570 0.89200 17. 13.495 1.0077 0.47654 0.49632 0.91900 17. 13.495 1.0077 0.47654 0.49632 0.91900 17. 13.495 1.0077 0.47654 0.49632 0.91900 18. 14.496 1.0076 0.46540 0.46520 0.46600 18. 14.496 1.4076 0.40239 0.46911 0.57216 0.65000 18. 14.496 1.4076 0.40239 0.46911 0.57216 0.65000 2ADDITIONAL PRESSURE FATIOS, FLOW SPLITER D.O. VICTOR PL. 1.0076 0.40239 0.40711 0.57216 0.67000 2ADDITIONAL PRESSURE FATIOS, FLOW SPLITER D.O. VICTOR PL. 1.1180 0.46030 0.46230 0.46630 0.46620 0.46200 22. 14.271 1.1180 0.46030 0.47290 0.46724 0.50000 22. 14.271 1.1180 0.46030 0.47290 0.46725 0.46000 240017110181 PRESSURE FATIOS, FLOW SPLITER D.O. VID WINDOW PL. 1.1060 0.46030 0.47290 0.46725 0.46000 240017110181 PRESSURE FATIOS, FLOW SPLITER D.O. VID WINDOW PL. 1.1060 0.46030 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0.46730 0	> 407 [ T ] C 04	AL PRESSURE	PATTING , PPI	MAPY PLUG						
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117 14.179 0.99169 0.47091 0.67341 0.43100 127 14.187 0.99239 0.47125 0.67387 0.46900 137 14.120 0.99239 0.47125 0.67388 0.58000 137 14.120 0.99750 0.46893 0.67056 0.52200 152 13.963 0.97633 0.46732 0.66298 0.58000 155 14.224 0.99638 0.47324 0.67697 -1.0000 157 14.224 0.99638 0.47324 0.67697 -1.0000 157 14.234 0.99638 0.47324 0.67697 -1.0000 159 14.234 0.99638 0.47324 0.67697 -1.0000 151 16.249 0.99658 0.47324 0.67697 -1.0000 152 14.254 0.99658 0.47324 0.67697 -1.0000 153 14.254 0.99658 0.47324 0.67697 -1.0000 154 14.254 0.99693 0.47324 0.67697 0.79300 155 14.254 0.99693 0.47340 0.67697 0.79300 157 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300 159 14.254 0.99693 0.47340 0.67697 0.79300	107	14.194		0.47141	0.67412	0.39800		•		•
127	117	14.179			0.67341	0.43100				
14, 187	122	14.174	7.99134	0.47975	0.67317	0.44900				
13.7										
142 13.963 0.97633 0.46762 0.66298 0.58800 157 14.224 3.9969 0.47347 0.57677 -1.0000 157 14.224 0.99698 0.47347 0.57677 -1.0000 157 14.254 0.99698 0.47346 0.67677 -1.0000 152 14.254 0.99698 0.47324 0.67677 -1.0000 153 14.254 0.99698 0.47324 0.67677 -1.0000 154 17 10Mal PPESSUPE RATIOS 20 DEG SHPTUD LOCATION 156 14.254 0.99693 0.47340 0.67697 0.79300 157 14.254 0.99693 0.47340 0.67697 0.79300 157 14.254 0.99693 0.47340 0.67697 0.89400 158 172 14.254 0.99693 0.47340 0.67697 0.79300 159 179 14.254 0.99693 0.47340 0.67697 0.79300 179 179 PL PRESSUPE RATIOS 80 DEG SHPTUD LOCATION 159 13.545 0.94735 0.44966 0.64330 0.79300 150 13.545 0.94735 0.44966 0.64330 0.79300										
157 14.254 3.4365 0.47367 U.67877 -1.0000  157 14.769 0.47654 U.67873 -1.0000  150 HORD PL PITTO BLAPTY PL/PTP K/DMAX  152 14.255 0.59603 0.67360 0.67677 -1.0000  151 16.249 0.99658 0.47324 0.6767 -1.0000  152 16.259 0.99658 0.47324 0.6767 -1.0000  153 16.254 0.99658 0.47324 0.6767 0.79300  167 14.254 0.99693 0.47340 0.67697 0.79300  172 14.254 0.99693 0.47340 0.67697 0.84400  240DITIONAL PRESSURE RATIOS , 80 DEG SHPCUO LOCATION  VO MORD PL PL/PO PL/PTP K/DMAX  109 MORD PL PR/PO PL/PTP K/DMAX  109 MORD PL PR/PO PL/PTP K/DMAX  109 MORD PL PR/PO PL/PTP K/DMAX  109 MORD PL PL/PO PL/PTP K/DMAX  109 MORD PL PL/PO PL/PTP N/DMAX										
157 14.749 0.9965H 0.47324 0.67673 -1.0000  PARTITIONAL PRESSURE RATIOS , FAN WAZZE FLAN  ON WORD PL PLANT PLANT PLANT PLANT PLANT   157 14.254 0.9965H 0.47324 0.67677 -1.0000  PARTITIONAL PRESSURE RATIOS , 20 DEG SHEDUD LOCATION  ON WORD PL PLANT PLANT PLANT   167 14.254 0.99693 0.47340 0.67697 0.79300  177 14.254 0.99693 0.47340 0.67697 0.84400  PARTITIONAL PRESSURE RATIOS , 80 DEG SHEDUD LOCATION  ON WORD PL PLANT PLANT PLANT PLANT   167 14.254 0.99693 0.47340 0.67697 0.79300  PARTITIONAL PRESSURE RATIOS , 80 DEG SHEDUD LOCATION  ON WORD PL PLANT PLANT PLANT   169 13.545 0.94735 0.44966 0.64330 0.79300  167 13.446 0.94036 0.44664 0.63856 0.64400							· · · · · · · ·	- :		· · · ·
PO WORD PL PLYPT PLYPTP X/DMAX  157 14.256 0.99693 0.47340 0.67677 -1.0000  157 16.249 0.99678 0.47324 0.67677 -1.0000  DANDITIONAL PRESSURE RATIOS , 20 DEG SHROUD LOCATION  PO WORD PL PLYPT PLYPTP X/DMAX  167 14.256 0.99693 0.47340 0.67697 0.79300  177 14.254 0.99693 0.47340 0.67697 0.84400  DANDITIONAL PRESSURE RATIOS , 80 DEG SHROUD LOCATION  PO WORD PL PLYPT PLYPTP X/DMAX  189 13.545 0.94735 0.44966 0.64330 0.79300  187 13.446 0.94035 0.44654 0.64336 0.676400										
157 14.256 0.99693 0.47324 0.6767 -1.0000  DANTITINNAL PRESSURE RATIOS , 20 DEG SHROUD EDCATION  ON HORD PL MI/PD PL/PTP M/DMAX  167 14.256 0.99693 0.47340 0.67697 0.79300  177 14.254 0.99693 0.47340 0.67697 0.84400  DANDITIONAL PRESSURE RATIOS , 80 DEG SHROUD EDCATION  ON HORD PL MI/PD PL/PTF PL/PTP M/DMAX  189 13.545 0.94735 0.44986 0.64330 0.79300  187 13.446 0.94036 0.44654 0.63856 0.84400	*** I I I I I I I I I I I I I I I I I I	-	8475 y FAN	-4 <del>0771E-FL</del> M						
157 14.256 0.79503 0.47324 0.67677 -1.0000 DEATHTICHAL PRESSURE RATIOS . 20 DEG SHROUD EDITION  ON HORD PL ML/PD PL/PTP M/DMAX  167 14.256 0.99693 0.47340 0.67697 0.79300  177 14.254 0.99693 0.47340 0.67697 0.84400  DEATHTICHAL PRESSURE RATIOS . 80 DEG SHROUD EDITION  ON HORD PL ML/PD PL/PTE PL/PTP M/DMAX  ON HORD PL ML/PD PL/PTE PL/PTP M/DMAX  187 13.446 0.94036 0.44654 0.643856 0.84400	yn wnen	PL	PITPO	_51.4444	PL /PTP	X/DMAX				
14.249   0.99658   0.47324   0.6787   1.0000										
PARTITIONAL PRESSURE RATIOS . 20 DEG SHROUD LOCATION  VO MORD PL PL/PO PL/PTF PL/PTP X/DMAX  167 Î4-254 0.99693 0.47340 0.67697 0.79300  177 14-254 0.99693 0.47340 0.67697 0.84400  PARDITIONAL PRESSURE RATIOS . 80 DEG SHROUD LOCATION  VO MORD PL PL/PO PL/PTF PL/PTP X/DMAX  187 13-446 0.94036 0.44664 0.64330 0.79300  187 13-446 0.94036 0.44664 0.643856 0.84400										
70 HOPD PL PL/PD PL/PTF PL/PTP K/DMAX 167 14.254 0.99693 0.47340 0.67697 0.79300 177 14.254 0.99693 0.47340 0.67697 0.84400  PADDITIONAL PRESSURE RATIOS , 80 DEG SHPCHO LOCATION  70 HOPD PL PL/PD PL/PTF PL/PTP K/DMAX 187 13.545 0.94735 0.44986 0.64330 0.79300 187 13.446 0.94036 0.44654 0.63856 0.84400	-									••
167						# 40 ma #				
177 14.254 0.99693 0.47340 0.67697 0.84400  -ANDITIONAL PRESSURE RATIOS . 80 DEG SHPCHD LOCATION  VO HORD PL PL/PD PL/PTF PL/PTP X/DMAX  187 13.446 0.94036 0.44654 0.64330 0.79300  187 13.446 0.94036 0.44654 0.63856 0.84400	41) MITP()									
PARRITIRNAL PRESSURE RATIOS . 80 DEG SHPCHD LOCATION  VO HORD PL PL/PD PL/PTF PL/PTP X/DMAX  187 13.446 0.94036 0.44664 0.64330 0.79300  187 13.446 0.94036 0.44664 0.63856 0.84400	147									
VN 40PD PL PL/PT PL/PTF PL/PTP X/DMAX 1P2 13.545 0.94735 0.449R6 0.64330 0.79300 187 13.446 0.94036 0.44654 0.63856 0.84400		170275	O. Adba 3	U. 47540 _	U-01641	J. 594UU				•
1P? 13.545 0.94735 0.44986 0.64330 0.79300 187 13.446 0.94036 0.44654 0.63856 0.84400				DEG SHPPUD E	PLATION					
1°? 13.545 0.94735 0.44986 0.64330 0.79300 187 13.446 0.94036 0.44654 0.63856 0.84400	177		RATINS . 80							
187 13.446 0.94036 0.44654 0.63856 0.84400	172 >49017JON	AL PRESSURE			PL /PTP	X/DMAX				
	172 SANDTTINNM VN HORB	PL PRFSSURF	PL / PO	PI /PTF						
	177 <u>&gt;Andttiam</u> Va yapa 187	PL 13.545	M /PO 0.94735	Pt / PTF 0.44986	0.64339	0.79300				
	177 > <u>19011190M</u> Vo 4080 187	PL 13.545	M /PG 0.94735 0.94036	Pt / PTF 0 . 44986 0 . 44654	0.64339	0.79300				

HACA-I EWS	<	NARY DATA	06/13/70	CABOFII	RFC 10/74/79 23:24:46.654	FAC ANOAS	PGM F834	PNG 1468
SENDIT INN	AL PRESSUPE	PATINS . PPI	MARY PLUG					
מפחוצ חו	PL	P( /P1	PJ /PTF	PI /PTP	X/DMAX			•
32	12.907	0.90276	0.49951	0.72323	J. 72200			
7	13.944	0.97530	0.57064	0.74134	0.82000			
7	14.279	1.0001	0.55334	0.00110	3.91900			
?	14.502	1.0144	7. 56125	C.P1263	1.0170			
						the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	•	
AND IT ION	AT PRFSSIPE	RATIOS . FIG	W SPLITTER I	. 0.				
NU PREIBU	PL	PI / PO	PL/PTF	PL /PTP	XADAVR			
.2	13.745		0.53193	0.77017	J-42200			
7	13.151	0.91985	0.50896	0.73692	0.67000			
						-		and the contract of the same same and the same of the same same same same same same same sam
Ann I T I TH	AL PRESSIPE	PATIOS . FLO	W SPLITTEP F	· n.				
የበ ዘጠምን	PL	PL/PG	PL /PTF	PI /PTP	X/DP4X			
7	12-064	0.84382	. 2.46689	0.67601	J.50800			
2	15.485	1.0831	0. 59924	0.86766	0.58300			
2	14.283	0.99902	2.55276	0-60034	0-67000			
13011 10M	<del>al pressure</del>	AATLOS FJE	FT CO SHOULD					
P WORD.	PE	PL/PD	PL/PTE	PL/PIP	Y/DMAX			
97	14.749	0.99658	0.55141	U. 79838	-1.0000	• •		
12	14.238	2. 60704	103	0.79782	_1_0000			
27	14.233	0. 99553	9-550R4	0.79754	-1-0090			
	14.243	0.99673	0.55127	0.79010	-1.0000			
77	1706 VD	- Ve 7797.2.		A time of				
		0.00300	A ELGLA	A TOKEO	-1 0000			
37	14. 359	0.99332	0.54948 0.54408	0.79559	1.0000			
37 <u>42</u>	14. 359		0.54409					·
37 62 ADDITION	14. 359	0.99332 PATEOS . FIR PL/PII	0.54409	0.76777				
ADOLTION	14. 359 AL PRESSURE	0.99332 PATEOS . FIR PL/PII	0, 54409 SERPOY INLET PL/PYF	0.78777 PL/PTP	X/DMAX	· •		
ADDITION	14.198 14.359 AL PRESSURE PL 14.249	0.95332 PATIOS . FIR PL/PI 0.99658	0.54409 PERMAY INLET PL/PTF 0.55141	PL/PTP 0.79838	X/DMAX 0.39800			
37 62 ADDITION D WOPD 07 12	14.249 14.259 AL PRESSURE PL 14.249 14.238	0.98332 PATIOS . FIR PL/PI 0.99658 0.99588	0.54409 PL/PTF 0.55141 0.55103	PL/PTP 0.79638 0.79782	X/PMAX 0, 39800 0,43100	•		
37 62 ADDITION D WOPD 07 12 27	14.359 AL PRESSURE PL 14.249 14.238 14.233	0.99332 PATIOS - FIR PL/PII 0.99658 0.99588 0.99553	0.54409 PERMY INLEY PL/PYF 0.55141 0.55103 0.55084	PL/PTP 0.79838 0.79782 0.79754	X/PMAX 0.39800 0.43100 0.44900	•		
37 42 ADDITION D WOPD 07 12 27	14.249 14.239 14.239 14.233 14.233	0.99332 PATIOS . FIRE PL/PH 0.99658 0.99588 0.99583 2.99623	0.54408 IFRITAY INLEY PL/PYF 0.55141 0.55103 0.55084 0.55122	PL/PTP 0.79638 0.79779 0.79754 G.79810	X/DMAX 0.39800 0.43100 0.44400 0.45600	•		
37 42 ADDITION D WOPD 07 12 27 27	14.249 14.239 14.249 14.239 14.233 14.243	0.91332 PATIOS . FIRE PL/PI 0.99588 0.9953 2.99623 0.99309	0.54409 PL/PYF 9.55141 0.55103 0.55084 0.55122 0.54949	PL/PTP 0.79638 0.79782 0.79754 G.79559	X/DMAX 0.39800 0.43100 0.44900 0.4800 0.52200	•		
37 42 ADDITION D WOPD 07 12 27 27 37 43	14.249 14.239 14.239 14.239 14.233 14.243 14.198 14.198	0.91332 PATIOS . FIRE PL/PI 0.99658 0.99563 0.99563 0.9309 0.9309 0.98332	0.54409 PL/PYF 9.55141 0.55103 0.55122 0.54948 0.54948	PL/PTP 0.79838 0.79782 0.79754 G.79810 0.79550 0.78777	X/DMAX 0.39800 0.43100 0.44900 0.49600 0.52200 0.52800	•		
37 42 ADDITION D WOPD 07 12 22 27 37 42	PL 14.249 14.230 14.230 14.243 14.198 14.259 14.259 14.259 14.259 14.259 14.259 14.259	0.99332 PATIOS . FIRE PL/PI 0.99658 0.99588 0.99583 0.99523 0.99309 0.9832 1.9701	0.5408 PL/PTF 9.55141 0.55103 0.55084 0.55122 0.54448 7.54408	PL/PTP 0.79638 0.79782 0.79754 G.79550 0.76550 0.76777	X/PMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000			
37 42 ADDITION D WOPD 07 12 27 27 37 47	14.249 14.239 14.239 14.239 14.233 14.243 14.198 14.198	0.91332 PATIOS . FIRE PL/PI 0.99658 0.99563 0.99563 0.9309 0.9309 0.98332	0.54409 PL/PYF 9.55141 0.55103 0.55122 0.54948 0.54948	PL/PTP 0.79838 0.79782 0.79754 G.79810 0.79550 0.78777	X/DMAX 0.39800 0.43100 0.44900 0.49600 0.52200 0.52800	•		
37 42 ADDITION D WORD 07 12 22 27 37 41	PL 14-249 14-239 14-239 14-231 14-199 14-299 14-299 14-299 14-299 14-299 14-299 14-299	0.99332 PATIOS . FIRE PL/PI 0.99658 0.99588 0.99583 0.99523 0.99309 0.9832 1.9701	0,54409 PL/PYF 9,55141 0,55103 0,55084 0,55122 0,54949 3,54409 0,77378	PL/PTP 0.79638 0.79782 0.79754 G.79550 0.76550 0.76777	X/PMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000			
37 42 ADDITION D WOPD 07 12 22 27 37 42 42 42	PL 14.239 14.239 14.233 14.243 14.198 14.259 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298 14.298	0.99332 PATIOS . FIRE PL/PI 0.99658 0.99588 0.99583 0.99523 0.99309 0.9832 1.9701 11.99971	0,5408 PL/PTF 0.55141 0.55103 0.55084 0.55122 0.54448 0.5408 0.7458 0.7458	PL/PTP 0.79638 0.79782 0.79754 G.79810 0.79550 0.79550 0.78777 0.787118	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000	•		
37 42 ADDITION D WOPD 07 12 22 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 14.249 14.239 14.230 14.231 14.243 14.198 14.293 14.293	0.99332 PAYIOS . FIRE PL/PI 0.99658 0.99583 0.99523 0.99309 0.9932 1.9901 11,99971	0.54408 PL/PYF 0.55141 0.55103 0.55084 0.55122 0.54408 0.75408 0.75715	PL/PTP 0.79638 0.79774 G.79610 0.79550 0.79777 0.79777 0.79777 0.79777	#/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000	•		
37 42 ADDITION D WORD 07 12 22 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 14.239 14.239 14.231 14.198 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259 14.259	0.99332 PATIOS . FIRE PL/PN 0.9965R 0.99583 0.99523 0.99309 0.98332 1.9701 0.99971	0.54408 PL/PYF 0.55141 0.55103 0.55103 0.55122 0.54948 0.74408 0.75715	PL/PTP 0.79838 0.79782 0.79754 G_19610 0.79559 0.78777 0.87118 0.87090	#/DMAX 0.39800 0.43100 0.44400 0.4600 0.52200 0.52200 -1.0000	•		
37 42 ADDITION D WOPD 07 12 22 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 14.299 14.239 14.239 14.239 14.243 14.199 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299	0.99332  PATIOS . FIRE PL/PN 0.99658 0.99588 0.99583 0.99503 0.9932 1.9701 0.99971	0,5408 PL/PTF 0.55141 0.55103 0.55084 0.55122 0.54448 0.5408 0.7458 0.7458 0.7458 0.7458 0.7458	PL/PTP 0.79638 0.79754 G.79754 G.79810 0.74550 0.74550 0.78777 0.80118 0.80090	#/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000	•		
37 42 ADDITION D WOPD 07 12 27 27 37 40 40 40 40 40 40 40 40 40 40 40 40 40	PL 14.299 14.239 14.239 14.239 14.243 14.199 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299	0.99332 PATIOS . FIRE PL/PN 0.9965R 0.99583 0.99523 0.99309 0.98332 1.9701 0.99971	0,5408 PL/PTF 0.55141 0.55103 0.55084 0.55122 0.54448 0.5408 0.7458 0.7458 0.7458 0.7458 0.7458	PL/PTP 0.79638 0.79754 G.79754 G.79810 0.74550 0.74550 0.78777 0.80118 0.80090	#/DMAX 0.39800 0.43100 0.44400 0.4600 0.52200 0.52200 -1.0000			
37 42 ADDITION D WOPD 07 12 27 27 37 43 43 43 49 49 49 49 49 49 49 49 49 49 49 49 49	PL 14.299 14.239 14.239 14.239 14.243 14.199 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299 14.299	0.99332  PATIOS . FIRE PL/PN 0.99658 0.99588 0.99583 0.99503 0.9932 1.9701 0.99971	0,5408 PL/PTF 0.55141 0.55103 0.55084 0.55122 0.54448 0.5408 0.7458 0.7458 0.7458 0.7458 0.7458	PL/PTP 0.79638 0.79754 G.79754 G.79810 0.74550 0.74550 0.78777 0.80118 0.80090	#/DMAX 0.39800 0.43100 0.44400 0.4600 0.52200 0.52200 -1.0000			
37 42 ADDITION D WOPD 12 27 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 14.299 14.239 14.239 14.239 14.233 14.243 14.199 14.259 14.293 At 14.293 At 14.293 At 14.293 At 14.293	0.99332  PATIOS . FIRE PL/PH 0.99658 0.99583 0.99563 0.99309 0.9832 1.0701 H.99971 PTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT	0.5408 PL/PYF 0.55141 0.55103 0.55103 0.55122 0.54409 0.74530 0.74530 0.55315 DFG SHPOUN 1 PL/PYF	PL/PTP 0.79638 0.79782 0.79754 G.79810 0.79559 0.76777 0:87118 0.87090 PL/PTP 0.8011R 0.80090	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 -1.0000			
37 42 ADDITION D WOPD 07 12 22 27 37 42 42 42 42 42 42 42 42 42 42 43 44 44 42 44 44 44 44 44 44 44 44 44 44	PL 14.299 14.299 14.299 14.233 14.243 14.199 14.059 14.299 14.299 PL 14.299 PL 14.299	0.99332  PATIOS . FIRE PL/PN 0.99658 0.99588 0.99583 0.99309 0.9832 1.9701 0.99971 PTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT	0.54408 PL/PTF 0.55141 0.55103 0.55103 0.55103 0.55122 0.54408 0.54408 0.74538 0.74538 0.55315 DEG SHPRIPR 1	PL/PTP 0.79638 0.79754 G.79810 0.79550 0.79550 0.78577 0.80118 0.80090  OCATION PL/PTP 0.80118	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
37 42 ADDITION D WOPD 07 12 27 37 42 42 43 49 40 41 41 41 41 41 41 41 41 41 41 41 41 41	PL 14.298 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293	0.99332  PATIOS . FIRE PL/PN 0.99658 0.99583 0.99583 0.99309 0.9832 1.9701 0.99971  PATIOS . 20 PL/PN 1.9901 0.99971	0.54408 PL/PYF 0.55141 0.55103 0.55103 0.55084 0.55122 0.54408 0.75518 0.75518 0.75518 0.75518 DFG SHPININ 1 PL/PYF 0.55334 0.55315	PL/PTP 0.79838 0.79782 0.79784 G.79754 G.79810 0.74550 0.76777 0.87118 0.87090 PL/PTP 0.80118 0.80090	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 -1.0000			
37 42 ADDITION D WOPD 07 12 22 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 14.298 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293	0.99332  PATIOS . FIRE PL/PN 0.99658 0.99588 0.99583 0.99309 0.9832 1.9701 0.99971 PTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT	0.54408 PL/PYF 0.55141 0.55103 0.55103 0.55084 0.55122 0.54408 0.75518 0.75518 0.75518 0.75518 DFG SHPININ 1 PL/PYF 0.55334 0.55315	PL/PTP 0.79838 0.79782 0.79784 G.79754 G.79810 0.74550 0.76777 0.87118 0.87090 PL/PTP 0.80118 0.80090	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
37 42 ADDITION D WOPD 07 12 27 37 47 47 47 47 47 47 47 47 47 47 47 47 47	PL 14.299 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293	0.99332  PATIOS . FIRE PL/PN 0.99588 0.99583 0.99583 0.99302 1.9701 0.99371  PATIOS . 20  PL/PN PL/PN	0.54408 PL/PYF 0.55141 0.55103 0.55103 0.55084 0.55122 0.54408 0.75515 0.755330 0.55315 DEG SHPININ 1 PL/PYF 0.55334 0.55315	PL/PTP 0.79638 0.79782 0.79754 G.79650 0.79650 0.76777 0.87118 0.87090 PL/PTP 0.80118 0.80090 PL/PTP 0.80118 0.80090 PL/PTP	X/DMAX 0.39800 0.49100 0.49100 0.4900 0.52200 0.52200 0.58800 -1.0000 -1.0000 -1.0000 X/DMAX 0.79300 0.84400			
O WOPD 07 112 22 27 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	14.249 14.249 14.239 14.239 14.231 14.259 14.259 14.259 14.279 14.279 14.279 14.279 14.279 14.279 14.279 14.279 14.279 14.279 14.279 14.279 14.279	0.99332  PATIOS . FIRE PL/PH 0.99588 0.99583 0.99583 0.99583 1.9701 0.99971  PATIOS . PO PL/PH 1.0001 0.99971  PATIOS . PO PL/PH 0.95856	0.54408 REBOTHY INLET PL/PTF 0.55141 0.55103 0.55084 0.55122 0.54408 0.55122 0.54408 0.7558 0.55315 DEG SHPININ 1	PL/PTP 0.79838 0.79754 G.79810 0.79554 G.79810 0.79550 0.78577 0.80118 0.80090 PL/PTP 0.80118 0.80090 PCATION	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 1.0000 1.0000 0.79300 0.74400			
37 42 ADDITION OF LICE 27 27 37 42 27 37 42 27 37 42 42 42 42 43 42 43 44 47 47 48 48 48 48 48 48 48 48 48 48 48 48 48	PL 14.299 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293	0.99332  PATIOS . FIRE PL/PN 0.99588 0.99583 0.99583 0.99302 1.9901 0.98332 1.9901 0.99971 PATIOS . 20  PL/PN PL/PN	0.54408 PL/PYF 0.55141 0.55103 0.55103 0.55084 0.55122 0.54408 0.75515 0.755330 0.55315 DEG SHPININ 1 PL/PYF 0.55334 0.55315	PL/PTP 0.79638 0.79782 0.79754 G.79650 0.79650 0.76777 0.87118 0.87090 PL/PTP 0.80118 0.80090 PL/PTP 0.80118 0.80090 PL/PTP	X/DMAX 0.39800 0.49100 0.49100 0.4900 0.52200 0.52200 0.58800 -1.0000 -1.0000 -1.0000 X/DMAX 0.79300 0.84400			
37 42 4001110N 10 MOPD 07 12 22 27 37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 14.299 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293 14.293	0.99332  PATIOS . FIRE PL/PH 0.99588 0.99583 0.99583 0.99583 1.9701 0.99971  PATIOS . PO PL/PH 1.0001 0.99971  PATIOS . PO PL/PH 0.95856	0.54408 REBOTHY INLET PL/PTF 0.55141 0.55103 0.55184 0.55122 0.54448 0.55122 0.74408 0.74338 0.75715 DEG SHERRIN 1 PL/PTF 0.55334 0.55315 DEG SHERRIN 1 PL/PTF 0.55338 0.55315	PL/PTP 0.79638 0.79772 0.79754 G.79810 0.79559 0.76777 0.87118 0.87090 PL/PTP 0.80118 0.80090 PCATION PL/PTP 0.80118 0.90090 PCATION PL/PTP 0.76793	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.52200 -1.0000 -1.0000 -1.0000 -1.0000  X/DMAX 0.79300 0.94400			

	PPFt 141	INAPY DATA	26/13/79	CAPPETI	PFC 10/25/	79 00:35:23.815	FAC PROFIL	PG# C934	RUN24
>400 FT FOR4	PPESSIRE	PATINS . PRI	MARY PLUG						
YN WARD	PI	PI / P1	PI / PTF	PL /PTP	Y/PMAX				
32	14-615	0. 98159	0. 54279	0.90866	0.72200				
37	14.944	1.0737	0.55504	0.92916	J. #2009				
47	15.099	1.9135	9.56042	0.93816	0.91900				
57	15.174	1.0192	0.56257	0.94344	1.0170				
AND IT FORA	PRESSIPE	PATTOS , FLO	W SPLITTER I	• n•					
AVD WOPD	PL	PL/PO	PI /PTF	PI /PTP	X /DHA X				
62	14, 785	0. 99 300	0.54910	0.91922	0.42200				
67	14-669	0. 98461	9. =4446	0.91145	0.67000		•		
		RATTOS . FLO				· · · · · · · · · · · · · · · · · · ·			
					.: = .:				
AVD HOPD	PL	PL /PG	PL /PTF	PL /PTP	X/DMAX				
77	13,001	0.87321	0.48286	0.80833	0.50000				
92	16-973	1.1295	0. 62405	1.0447	0.58300		•		
92	14.920	1.0021	0.55411	0.92760	9.67000				
->400 I T 10M4		aatins , far							
				- · · · · · · · · · · · · · · · · · · ·					
AL MUND	76	PL / PO	PL / PTF	PL 287	X /OHAX				
-107	14.475	0.97220	0.53760	0.89996	-1.0000	****			
-112	14,395	0.96616	45-3426	0.89437	-1.0000				
-122	14.385	0.2646	0.57426	0.89437	-1.0000				
-127	14-665	7. 99495	0. 54485	0.91176	-1.0000				
-137	14-050	0.91394	0.54429	0.91083	-1.0000				
-142	14.460	0.97119	0,53704	0.89903	1.0000		<u>.</u>		
-142		0.97119 PATIOS , FOP	0,53704 FPODY INLET	0.89903	1.0000	·			
>EDTITIONA	L PRESSURF	0.97119	0,53704	0.89903 PL/PTP		• - · · · · · · · · · · · · · · · · · ·			
>EDDITIONA AVO HOPD 107	PL 14.475	0.97119 PATIDS , FOP PL/PD 0.97220	0,53704 FRIDY INLET PL/PTF 0.53760	0.89903 Pt/PTP 0.8996	X/DMAX 9.39800		• •		
> # # # # # # # # # # # # # # # # # # #	PL 14.475 14.345	0.97119 PATIDS , FOP Pt /PD 0.97220 0.96616	0,53704 FPROV INLET PL/PTF 0,53760 0,53426	0.89903 Pt/PTP 0.89996 0.89437	X/DMAX 9.39900 0.43100				
>20017 IONA NO HOPD 107 112 127	PL 14.475 14.375 14.385	0.97119 PATIOS , FOP PL/PO 0.97220 0.96616 0.96616	0,53704 EPROV INLET PL/PTF 0.53760 0.53426 0.53426	0.89903 Pt/PTP 0.89996 0.89437 0.89437	X/DMAK 9.39800 0.43100 0.44900		•		
>EDDITIONA NO HOPD 107 112 127 127	PL 14-475 14-475 14-345 14-345 14-665	0.97119 PAYIDS , FOP PL/PO 0.97220 0.96616 0.98616 0.98695	0,53704 FPNDY IMLET PL/PTF 9.53760 0.53426 0.53426 0.54465	0.8993 Pt/PTP 0.89996 0.89437 0.9437 0.91176	X/DMAX 9.39800 9.43100 9.44900 9.48600				
>EDDIT INNA AVE HEPD 107 112 127 137	PRESSURF 14.475 14.345 14.345 14.665	0.97119 PAYIDS , FOP PL/PO 0.97220 0.96616 0.96616 0.98495 0.98394	0,53704 FPRDY INLET PL/PTF 9,53760 0,53426 0,53426 0,54469	0.8993 PL/PTP 0.89996 0.89437 0.89437 0.91176	X/DMAX 9.3900 0.43100 0.44600 0.52200				
>EDDITIONA AVE HOPD 107 112 127 127 127 127 137	PRESSURF 14.475 14.375 14.375 14.665 14.665 14.660	0.97119 PATIDS , FOP PL/PD 0.97220 0.96616 0.96616 0.98495 0.98394 0.97119	0,53704 FPODY INLET PL/PTF 0,53760 0,53426 0,53426 0,54468 0,54469 0,53704	0.8999A 0.8999A 0.89437 0.89437 0.91176 0.91087 0.91087	X/OMAX 9.3900 0.43100 0.4400 0.52200 0.58800		•		
>EDDIT IONA NO HOPD 107 112 127 127 137 142	PRESSURF PL 14.475 14.345 14.345 14.655 14.650 14.460	0.97119 PATIDS , FOP PL/PO 0.97 220 0.94616 0.94616 0.98495 0.97119 1.9731	0,53704 FPHDY INLFY PL/PTF 0.53760 0.53426 0.53426 0.54465 0.54409 0.53704	0.8999A 0.8999A 0.89437 0.89437 0.91176 0.91083 0.94654	X/DMAX 9.39000 0.43100 0.4400 0.52700 0.5800		•		
>EDDIT INNA AVE HEPD 107 112 127 127 137 142 -157	PRESSURF 14.475 14.345 14.345 14.665 14.650 14.460	0.97119 PAYIDS , FOP PL/PD 0.97220 0.96616 0.96616 0.98495 0.98394 0.97119 1.9931	0,53704 FPNDY INLFT PL/PTF 9,53760 0,53426 0,53426 0,54465 0,5465 0,54704 0,53704 0,53704	0.8999A 0.8999A 0.89437 0.89437 0.91176 0.91087 0.91087	X/OMAX 9.3900 0.43100 0.4400 0.52200 0.58800				
>EDDIT INNA AVE HEPD 107 112 127 127 137 142 -157	PRESSURF 14.475 14.345 14.345 14.665 14.650 14.460	0.97119 PATIDS , FOP PL/PO 0.97 220 0.94616 0.94616 0.98495 0.97119 1.9731	0,53704 FPNDY INLFT PL/PTF 9,53760 0,53426 0,53426 0,54465 0,5465 0,54704 0,53704 0,53704	0.8999A 0.8999A 0.89437 0.89437 0.91176 0.91083 0.94654	X/DMAX 9.39000 0.43100 0.4400 0.52700 0.5800		•		
>EDDITIONA AVO MOPD 107 112 127 127 137 147	PRESSURF 14.475 14.385 14.665 14.665 14.660 14.460 14.470 14.729	0.97119 PAYIDS , FOP PL/PO 0.97220 0.96616 0.96616 0.98495 0.97119 1.9931 1.9931 1.9937	0,53704  FPROV IMLEY  PL/PYF	0.89996 0.89996 0.89437 0.89437 0.91176 0.91083 0.92854 0.92854	X/DMAX 9.39900 0.43100 0.44900 0.52700 0.52700 0.5800 1.0000		•		
>EDDITIONA AVO HOPD 107 112 127 127 127 127 127 127 127 127 12	PRESSUPE PL 14.475 14.345 14.659 14.659 14.659 14.460 14.729	0.97119 PAYIDS , FOP PL/PO 0.97220 0.96616 0.96616 0.98495 0.97119 1.9927	0,53704  FPROV IMLET  PL/PTF 9,53760 0,53426 0,53426 0,54465 0,54465 0,54465 0,54465 0,53704 0,53704 0,53440	0.8993  Pt/PTP 0.89996 0.89437 0.94137 0.91176 0.91083 0.9454 0.92854	X/DMAX 9.39000 0.43100 0.4400 0.52700 0.5800 1.0000				
>EDDITIONA AVO MOPD 107 112 127 127 137 147	PRESSURF 14.475 14.385 14.665 14.665 14.660 14.460 14.470 14.729	0.97119 PAYIDS , FOP PL/PO 0.97220 0.96616 0.96616 0.98495 0.97119 1.9931 1.9931 1.9937	0,53704  FPROV IMLEY  PL/PYF	0.89996 0.89996 0.89437 0.89437 0.91176 0.91083 0.92854 0.92854	X/DMAX 9.39900 0.43100 0.44900 0.52700 0.52700 0.5800 1.0000				
>EDDIT IONA AVO HOPD 107 112 127 127 137 142	PRESSURF  14.475 14.375 14.375 14.665 14.665 14.660 14.994 16.929	0.97119 PAYIDS , FOP PL/PO 0.97220 0.96616 0.96616 0.98495 0.97119 1.9927	0,53704  FPHDY IMEY  PL/PYF 9,53760 0,53426 0,53426 0,54468 0,44409 0,53704 9,54467 0,54467 0,54467 0,54467	0.8993 Pt/PTP 0.89996 0.89437 0.91176 0.91083 0.92654 0.92654 0.92654	X/DMAX 3.39000 0.43100 0.44000 0.52200 0.58800 1.0000 X/DMAX -1.0000				
> ADDIT IONA  AVO HOPD  107  112  127  127  137  142  -157  > ADDIT IONA  > ADDIT IONA	PRESSURF  14.475 14.345 14.655 14.657 14.460 14.929 1 PRESSURE	0.97119  PATIDS , FOP  PL/PO 0.97220 0.94616 0.94616 0.98495 0.98394 0.97119 1.9927 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.9727 0.	0.53704  FPROV INLEY  PL/PTF	0.89993 Pt/PTP 0.89996 0.89437 0.91176 0.91176 0.91083 0.9364 0.92623 Pt/PTP 0.92854 0.92854	X/DMAX 9.39700 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 -1.0000				
>EDDIT INNA AVE WEED 107 112 127 127 147	PL 14.475 14.345 14.345 14.655 14.657 14.665 14.659 14.729 1 PRESSURE PL 14.934	0.97119  PATIDS , FOP  PL/PO 0.97220 0.96616 0.96616 0.98495 0.97119 1.9931 1.9927  PATIOS , FAN  PL/PO 1.9927  PATIOS , 20  PL/PO	0,53704  FPHOV INLEY  PL/PTF 0.53760 0.53426 0.53426 0.54465 0.54465 0.54465 0.54465 0.55704 0.57046 0.57046 0.57046 0.57046	0.89903  Pt/PTP	X/DMAX 9.39900 0.43100 0.44900 0.52700 0.58800 1.0000 1.0000 1.0000				
>EDDITIONA AVO HOPD 107 112 127 127 137 142 -157 >APDITIONA AVO HOPD 167 AVO HOPD 167	PRESSURF  14.475 14.375 14.375 14.665 14.665 14.660 14.904 14.929  PL 14.936 16.999  PRESSURF  PL 14.920	0.97119 PATIDS , FOP PL/PO 0.97220 0.96616 0.96616 0.98495 0.97394 0.97119 1.9731 1.9927 PATIOS , 20 PL/PO 1.0021	0,53704  FPIDY IMEY  PL/PYF 9,53760 0,53426 0,53426 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,554468 0,554468 0,554468 0,554468 0,554468 0,554468	0.8993 Pt/PTP O.89996 O.89437 O.91176 O.91087 O.91087 O.92854 O.92854 O.92854 O.92854 O.92760	X/DMAK 9.39000 9.43100 9.43100 9.4400 9.52200 9.5800 1.0000 1.0000 1.0000 1.0000 X/DMAX 9.79309				
>EDDIT INNA AVE WEED 107 112 127 127 127 137 142 -157 >ANDIT INNA AVE WEED AVE WEED 157 >ANDIT INNA AVE WEED 157 172	PRESSURF  14.475 14.345 14.650 14.650 14.460 14.994 14.929 1 PRESSURE  PL 14.920 14.920 14.915	0.97119  PATIDS , FOP  PL/PO 0.97220 0.94616 0.94616 0.9495 0.97119 1.9931 1.9927  PATIOS , FAN  PL/PO 1.9031 1.9031 1.9031 1.9031 1.9031	0,53704  FPROV INLEY  PL/PTF 0.53760 0.53426 0.54465 0.54467 0.53704 0.53704 0.53467 0.55467 0.55467 0.55467 0.55467 0.55467	0.89903  Pt/PTP	X/DMAX 9.39900 0.43100 0.44900 0.52700 0.58800 1.0000 1.0000 1.0000				
>EDDITIONA AVO HOPD 107 112 127 127 137 147	PRESSURF  14.475 14.345 14.650 14.650 14.460 14.994 14.929 1 PRESSURE  PL 14.920 14.920 14.915	0.97119 PATIOS , FOP PL/PO 0.97220 0.96616 0.96616 0.98495 0.98394 0.97119 1.9931 1.9927 PATIOS , 20 PL/PO 1.0021 1.0021 1.0021 1.0027 PATIOS , 80	0,53704  FPHDY IMLEY  PL/PYF 9,53760 0,53426 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,54468 0,55467 0,55446	0.89903  PL/PTP	X/DMAK 9.39000 9.43100 9.43100 9.4400 9.52200 9.5800 1.0000 1.0000 1.0000 1.0000 X/DMAX 9.79309				
> ADDITIONA  AVE HERD 107 112 127 127 127 127 127 127 127 127 12	PRESSURF  14.475 14.345 14.665 14.665 14.667 14.460 14.470 14.470 14.470 PRESSURF  PL 14.934 14.929 14.915 PRESSURF	0.97119  PATIDS , FOP  PL/PO 0.97220 0.94616 0.94616 0.94695 0.98394 0.97119 1.9931 1.9927  PATIOS , FOR  PL/PO 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931	0.53704  FPROV INLEY  PL/PTF  0.53760  0.53426  0.53426  0.54667  0.53704  0.53704  0.53704  0.53704  0.53467  0.53467  0.55446  DEG SIPRUP L  PL/PTF	0.89993  PL/PTP	X/DMAX 9.39900 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 X/DMAX 0.79307 0.84400				
>EDDIT IONA AVE WEED 107 112 127 127 137 142 -157 >APDIT IONA AVE WEED AVE WEED 167 >ADDIT IONA AVE WEED 172 >ADDIT IONA AVE WEED 172	PRESSURF  PL 14.475 14.345 14.659 14.665 14.659 14.460 14.929 14.929 14.929 14.920 14.915 PRESSURF  PL 14.920 14.915	0.97119  PATIDS , FOP  PL/PO 0.97220 0.94616 0.94616 0.9495 0.97119 1.9927  PATIOS , FOP 0.97119 1.9927  PATIOS , FOP 0.9717 PATIOS , FOP 0.97964	0,53704  FPHOV INLEY  PL/PTF 0.53760 0.53426 0.54465 0.54467 0.54467 0.57704 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467 0.57467	0.89903  PL/PTP	X/DMAX 9.39900 0.43100 0.43100 0.44900 0.52200 0.58800 1.0000 X/DMAX 0.79307 0.84400 X/DMAX 0.79307 0.84400				
> ADDITIONA  AVE HERD 107 112 127 127 127 127 127 127 127 127 12	PRESSURF  14.475 14.345 14.665 14.665 14.667 14.460 14.470 14.470 14.470 PRESSURF  PL 14.934 14.929 14.915 PRESSURF	0.97119  PATIDS , FOP  PL/PO 0.97220 0.94616 0.94616 0.94695 0.98394 0.97119 1.9931 1.9927  PATIOS , FOR  PL/PO 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931 1.9931	0.53704  FPROV INLEY  PL/PTF  0.53760  0.53426  0.53426  0.54667  0.53704  0.53704  0.53704  0.53704  0.53467  0.53467  0.55446  DEG SIPRUP L  PL/PTF	0.89993  PL/PTP	X/DMAX 9.39900 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 X/DMAX 0.79307 0.84400				
>EDDITIONA AVO HOPD 107 112 127 127 137 142 =157 >ANDITIONA AVO HOPD 167 177 >ANDITIONA AVD HOPD 167 187	PRESSURF  14.475 14.375 14.375 14.665 14.665 14.660 14.929 14.929 14.929 14.929 14.920 14.925 14.925 14.925 14.925 14.925	0.97119  PATIDS , FOP  PL/PO 0.97220 0.94616 0.94616 0.9495 0.97119 1.9927  PATIOS , FOP 0.97119 1.9927  PATIOS , FOP 0.9717 PATIOS , FOP 0.97964	0,53704  FPODY INLEY  PL/PTF	0.89903  PL/PTP	X/DMAX 9.39900 0.43100 0.43100 0.44900 0.52200 0.58800 1.0000 X/DMAX 0.79307 0.84400 X/DMAX 0.79307 0.84400				

	< PRFL 141	HAPY DATA	26/13/79	CAPRETI	REC 10/25/1	79 00:36:90.886	FAC BESEL	PG# C034	RUN 24
>APRITINA	AL PRESSIME	RATINS . PPI	MARY PIUG	Min gay consider the	. *\				
AD HUBD	PL	PL / PO	PL /PTF	PL/PTP	X/DMAX		AND AND COMMENT OF STREET OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDRESS OF STREET, AND ADDR		
37	13.999	0. 93154	0.46317	0.73529	0.72200				
27	15.007	1.9958	0.47951	0.79392	3. P2000				
47	15.407	1.0326	0.49125	0.81504	0.91900	_			
52	15.641	1.0483	0.49873	0. 82745	1.0170				
NATION AND A PROPERTY.	A1 00ECCIDE	PATINS . FIR	W COL ITTED 1	- 0-					مان المان المان المان المان المان المان المان المان المان المان المان المان المان المان المان المان المان الما
DELM UA	PL.	PL/PN	PL /PTF	PI /PTP	X / DMAX				
62	14.728		0.46960	0.77913	0.42200	-			
67	14.969	0.94291	0.44859	0.74427	0.67000				
>ADDITION	AL PRESSURE	RATIOS . FEO	W SPLITTER O					·	
VP HOPD	PL	PI /PI	PL /PTF	PL /PTP	Y/DMAX				
77	12.696	0.85089	0.40581	0.67163	0.50000				
87	17.114	1.1470	0.54568	0.90535	0.56300		-		
92	14.953	1-0021	2.47676	0.79101	2.67000				
24-417-3010	WE PRESSURE	PATEOS E PA					· ·- ·		
VD_WORD	. 21		PL/PTF	MATTE.	X/DMAX	<u>.</u>	A		- <del>-</del>
197	14.499	0.97107	0.561	0.76645	-1.0000				
112	14.388	0.95933	0.45077	0.76117	-1.0000				···
12?	14.363	0.46399	0-45R61	0.76090	-1.0000				
127	14.659	0. 98239	9.46737	0.77543	-1,0000				
137 _	14.649	0.96172	0.46705	0.77490	-1.0000	-			
149	14.438	0.96767	0.46037	0,76381	-1,0000				
SADDIT IOM	AI 805551185	RATIOS . FOR							
	-				·····				······································
AD MUSE	PL.	PL / P.7	PL/PTF	PL/PTP	X/DMAX				
107	14.498	0.97102	0.46196	0.76645	9.39600		•		
112	14.380	0.96433	0.45877	0.76117	0.43100				
	14.393	0.96399	9.45761	0.76099	0.44900				
			9. 46737	Q. 7.7543	0.48600				
122									
122 127	14.658	0-99239	0.46705	0_77490					
122 122 127	14.658	0.98172	0.44705	0.77490	0.52200				
122 122 137 142	14.658 14.449 14.438	0.99172 0.95767	0. 46037	0.76361	0.58800	•	· •		
122 127 127 142	14.658	0.98172		0.76381					
127 127 137 142 157	14.658 14.649 14.435 14.449	0.95767 0.95767 1.0018	0.46027 0.47860	0.76361 0.74077 0.75077	0.58800	•	· <del>-</del> ·		-
122 127 137 142 142 142 143 144 144	14.658 14.649 14.435 14.449	0.98172 0.95767 1.9710 1.0018	0.46027 0.47860 0.47860	0.76381 0.79079 0.79079	0.58800 -1.9900 -1.3909				
127 127 137 142 142 147 2400 17 104 VD HOPD	14.658 14.449 14.438 14.438 14.449 14.449	0.99172 0.95767 1.001P aatios FAN	0.46027 9.4760 0.47860	0.76361 0.74077 0.75079	0.58800 -1.9900 -1.9909 X/DMAK				
122 127 127 142 142 147 147 147 147 147 147 147 147 147 147	14.658 14.449 14.438 14.438 14.449 14.449	0.99177 0.95767 1.0018 847105 FAM	0.46027 9.47660 0.47660 MD7246 61 40	0.76381 0.74079 0.75079 PL/PTP 0.79075	0.58800 T. 7700 T. 0700 T. 0700 X/DMAX -1.0000				- -
122 127 127 142 142 147 2400 17 104 VD HOPD 152	14.658 14.449 14.438 14.438 14.449 14.449	0.99172 0.95767 1.001P aatios FAN	0.46027 9.4760 0.47860 MD7245 5148	0.76361 0.74079 0.75079	0.58800 -1.9900 -1.9909 X/DMAK				- -
127 127 127 142 142 157 2400 17 104 VD MOPD 157	14.658 14.449 14.438 14.449 14.449 14.449 14.449	0.99177 0.95767 1.0018 847105 FAM	0.46027 0.47660 0.47660 0.47660 0.47660 0.47660	0.76381 0.79077 0.79077 Pt /PTP 0.79075 0.29075	0.58800 T. 7700 T. 0700 T. 0700 X/DMAX -1.0000				
127 127 147 142 157 >ADDITION	14.658 14.449 14.438 14.438 14.449 14.449 14.958 14.969	0.99177 0.95767 1-9719 1-0018 ***********************************	0.46027 0.47660 0.47660 0.47660 0.47660 0.47660	0.76381 0.79077 0.79077 Pt /PTP 0.79075 0.29075	0.58800 T. 7700 T. 0700 T. 0700 X/DMAX -1.0000				-
127 127 127 142 157 540017109 VD MOPD 157 540017109	14.658 14.449 14.438 14.449 14.449 14.449 14.949 14.949	0.99177 0.95767 1.9716 1.0018 ***********************************	0. 46027 0. 47660 0. 47660 407245 5140 2. 47660 0. 47660 DFG SHROUD 1	0.76381 0.79079 0.79079 0.79075 0.79075 0.29075	0.58900 -1.9909 -1.9909 -1.0000 -1.0000				-
127 127 127 142 157 >ADDITION >ADDITION VD WORD 167	14.658 14.449 14.439 14.449 14.449 14.449 14.958 14.949	0.98172 0.95767 1-9718 1-0018 047105 FAN 1-0718 1-0718 PATIOS 20 PL/PD 1-0721	0. 46027 0. 47860 0. 47860 0. 47860 0. 47660 0. 47660 0. 67660	0.76381 0.74077 0.74077 0.79075 0.79075 0.29075	0.58900 -1.7700 -1.3707 -1.3707 -1.4000 -1.0000				•
127 127 127 142 157 >ADDITION VD WORD 152 >ADDITION VD WORD 167 172	14.658 14.449 14.438 14.449 14.449 14.958 14.949 41 PRESSUPF PL 14.953 14.953	0.99172 0.95767 1-9778 1-0018 847105 FAM 1-0718 1-0718 1-0718 1-0721 1-0921	0. 46027 0. 47860 0. 47860 0. 47660 0. 47660 0. 47660 PL/PTF 0. 47676	0.76361 0.79077 0.79077 0.79075 0.79075 0.79075 0.79101 0.79101	0.58900 -1.9900 -1.9900 -1.9900 -1.0000 -1.0000				•
127 127 127 142 157 162 157 240013104 157 240013104 167 172	14.658 14.449 14.438 14.449 14.449 14.958 14.949 41 PRESSUPF PL 14.953 14.953	0.98172 0.95767 1-9718 1-0018 847105 FAN 847105 FAN 1-0118 1-0118 1-018 947105 20 PL/PD 1-0921 PAYIOS 1-00	0. 46027 0. 47660 0. 47660 0. 47660 0. 47660 0. 47660 0. 47676 0. 47676 0. 47676	0.76361 0.79079 0.79079 0.79075 0.79075 0.29075 0.79101 0.79101 0.79101	0.58900 -1.7700 -1.3700 -1.3700 -1.0000 -1.0000 -1.0000 -1.0000 0.84400				•
122 127 127 142 1-7 >ADDITION 152 >ADDITION 167 172 >ADDITION 167 172  ADDITION	14.658 14.449 14.439 14.449 14.449 14.949 14.949 14.953 14.953 14.953	0.98172 0.95767 1-9718 1-0018 847105 FAM 1-0718 1-0718 PATIOS 20 PL/PO 1-9721 1-0021 PATIOS 20 PL/PO	0. 46027 0. 47660 0. 47660 0. 47660 0. 47660 0. 47660 0. 47676 0. 47676 0. 47676	0.76361 0.79079 0.79079 0.79075 0.79075 0.79075 0.79101 0.79101 0.79101	0.58900 -1.7700 -1.0707 -1.0707 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				•
127 127 127 142 157 >ADDITION VD WORD 167 167 172 >ADDITION VD WORD 107 VD WORD 107 VD WORD	14.658 14.448 14.448 14.449 14.449 14.958 14.958 14.953 14.953 14.953 AL PRESSURE PL 14.953	0.99172 0.95767 1-9776 1-0018 847105 FAM 1-0718 1-0718 1-0718 1-0721 1-0921 847105 FAM 91790 0.99210	0. 46027 0. 47860 0. 47860 MD7245 5140 9. 47660 0. 47660 PE SHROUN I PL /PTF 0. 47676 DEG SHROUN I PE SHROUN I	0.76361 0.79079 0.79079 0.79075 0.79075 0.79075 0.79101 0.79101 0.79101 0.79101	0.58900 -1.7700 -1.0707 -1.0707 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				•
127 127 127 147 142 157 240017104 VO HOPD 157 157 VO HOPD 167 172 240017104 VO HOPD 187	14.658 14.449 14.438 14.449 14.449 14.958 14.953 14.953 14.953 14.953	0.98172 0.95767 1.0018 0.47105 FAM M /PD 1.0018 PATIOS 20 PI /PD 1.0021 PATIOS 80 PI /PD 0.99210 0.99466	0. 46027 0. 47060 0. 47060 MD72LE ELAN 9. 47660 0. 47660 DFG SHROUN L PL/PTF 0. 47676 DFG SHROUN L PL/PTF 0. 47149 0. 45993	0.76361 0.79079 0.79079 0.79075 0.79075 0.79075 0.79101 0.79101 0.79101	0.58900 -1.7700 -1.0707 -1.0707 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				•
127 127 127 127 127 127 127 127 142 157 167 157 20017100 167 172 20017100	14.658 14.449 14.438 14.438 14.438 14.438 14.949 14.953 14.953 14.953 14.953 14.953 14.953 14.953	0.98172 0.95767 1-9718 1-0018 847105 FAM 9/PD 1-0718 1-0718 1-0718 1-0721 1-0921 PATIOS - 80 PM /PD 0.99210 0.96466 THRUST PAPAM	0. 46027 0. 47060 0. 47060 MD72LE ELAN 9. 47660 0. 47660 DFG SHROUN L PL/PTF 0. 47676 DFG SHROUN L PL/PTF 0. 47149 0. 45993	0.76361 0.79079 0.79079 0.79075 0.79075 0.79101 0.79101 0.79101 0.79101 0.76143	0.58900 -1.7700 -1.0707 -1.0707 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000	NSW 2,3538	CE4 0.0721218		•

TASA-I FUI	C PRFL14	INAPY DATA	06/13/79	CADDFIL	RFC 10/25/79 00:37:44.469	FAF 94641	PG= 1034 - PBG 1471	•
>4701 T TOP4	MI PPESSIPE	PATENS . PPE	AFLA MANU					
מפרע חע	PL	PI /PO	PE /PTF	PJ /PTP	Y/DMAX	- C	· · · · · · · · · · · · · · · · · · ·	
27	10.978	0.72916	0.29131	0.49857	0.72200			
37	14.795	0.04481	0.77747	0.63306	0.#2000			
47	15.434	1.0339	0.41305	9.69274	0.91900			
52	15.943	1.0700	0.47740	0.71696	1.0170			
	<del>-</del>	·		Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Committee of the Commit		and the second second second second second second second second second second second second second second second	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	
>Anni Tinn	IAL PRESSURE	RATIOS , FLO	W SM ITTER I	I+n+				
หก พกคก	PL	PL /PD	PL/PTF	PL /PTP	x/fmay			
52	15.244	1.0516	0.42923	3.69466	0.42200			
67	12.402	0.83130	0.33212	0.55701	J.67000			
							and the second control and the second control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of th	
NOT TECOR	IAL PRESSUPE	RATIOS . FLO	M ZMITAEK L	'- n.				
VO MORD	PL	PI /PN	PL /PTF	PL /PTP	X/PMAX			
77	10.438	9.67968	0.27954	0.46882	J. 50890			
P2	18.605	1.2471	0.49824	0.83562	0.5830)			
92	14,954	1.0024	0,40048	0.67165	0.47900			
ANGET INN	ME PRESSIPE	RATTOR & CUE	CLCA-SHELDIN					
/D WORD	PL	PL /PD	PL /PTF		X/RMAX			
107	14.525	0-02361		0.4527	-1.0000	2	•	
			0,38.97	U.#767				
112	14.450	0, 96 63	20, 206.97	0.64897	-1-0000		·	
177	14.467	0.46925	0. 4453	0.64944	-1.0000			
127	سبود لعدا	0.98800	0.39477	0-66200	-1.0000			_
	14.734	0.98767	0.39459	0.64178-	1.0000			
137	14.599	0.97863		0.65572	-1.0000			
147			0.39096					
147		RATIOS , FOR	0.39096					
147			0.39096					
ANDIT ION	ML PRESSIPE	RATIOS , FOR	0.3909P	0.65572	-1.0000			
ANDITION VO WORD	ML PRESSIPE	RATIOS , FOR	0.3909P FRIDY INLET	0.65572 PL/PTP	-1-000Q			
ANDIT ION VO WORD 197	ML PRESSIME PL 14.575	PL/PD 0.97361	0.3909F ERNDY INLET PL/PTF C.38497	0.65572 PL/PTP 0.65236	E/DMAK 0.39800			
>ANNT INN VO WORD 197 112	PL 14.525 14.450 14.460	MATIOS , FOR MI/PO 0.97361 0.96858 0.96925	0.39096 ERROV IMET PL/PTF C.38497 0.38697 0.38723	PL /PYP 0.45236 0.64899 0.64944	T/DMAX 0.39800 0.43100 0.44900	•		
ANDITION VO WORD 197 112 122	PL 14.525 14.525 14.450 14.460 14.739	MATINS , FOR ML/PO 0.97361 0.96858 0.96825 0.98800	0.39098 ERFOV INLET PL/PTF C.38497 0.38723 0.39472	P1 /PYP 0.45236 0.64894 0.64844 0.66200	-1.000Q_ X/DMAX 9.39809 9.43100 0.44900 0.48600			
>ANDITION  VO WORD  107  117  122  127	PL 14.525 14.450 14.460 14.739 14.734	PL/PD 0.97361 0.96858 0.96825 0.94800 0.98767	0.39098 ERFDV INLET PL/PTF C.38497 0.38697 0.38723 0.39472 0.39455	PL/PTP 0.65236 0.64895 0.64844 0.66200 0.66178	-1.0000 X/OMAX 7.39807 7.43100 0.44900 0.46600 0.52207			
DANDIT ION  VO WORD  107  117  122  127  137	PL 14.525 14.450 14.460 14.734 14.599	M/PD 0.97361 0.96858 0.96825 0.9880 0.98767 0.97863	0.3909P ERITOV IMET PL/PTF C.3R697 0.38697 0.39472 0.39456 0.3909R	PL /PTP 0.45236 0.64895 0.64944 0.66200 0.46178 0.65572	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.46600 0.52200 0.578000			
ANDITION O WORD 107 117 122 127 137 142	PL 14.525 14.525 14.450 14.460 16.739 14.734 14.509	MATINS , FOR M./PO 0.97361 0.96658 0.96925 0.98000 0.98767 0.97863	0.3909P ERMOV IMET PL/PTF C.3R497 0.3R697 0.38723 0.39472 0.39455 0.3909R	PL/PTP 0.65236 0.64895 0.64844 0.66200 0.617P 0.65572	-1.0000 X/DMAX 0.39800 0.44900 0.44900 0.52200 0.52200 0.58000			
ANDITION O WORD OT 117 127 127 137 142	PL 14.525 14.450 14.460 14.734 14.599	M/PD 0.97361 0.96858 0.96825 0.9880 0.98767 0.97863	0.3909P ERITOV IMET PL/PTF C.3R697 0.38697 0.39472 0.39456 0.3909R	PL /PTP 0.45236 0.64895 0.64944 0.66200 0.46178 0.65572	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.46600 0.52200 0.578000			
ADDIT ION IO WORD 197 12 22 27 37 42	PL 14.525 14.525 14.450 14.460 16.739 14.734 14.509	MATINS , FOR M./PO 0.97361 0.96658 0.96925 0.98000 0.98767 0.97863	0.39098 PERIDV INLET PL/PTF C.38407 0.38697 0.38723 0.39472 0.39455 0.39455 0.39455 0.39455	PL/PTP 0.65236 0.64895 0.64844 0.66200 0.617P 0.65572	-1.0000 X/DMAX 0.39800 0.44900 0.44900 0.52200 0.52200 0.58000			
PARRITION OF WORD 197 117 122 127 137 147	PL 14.525 14.525 14.450 14.450 14.739 14.736 14.539 14.539	PL/PR 0.97361 0.96858 0.96858 0.96800 0.98800 0.98767 0.97863 1.0031	0.39098 PERIDV INLET PL/PTF C.38407 0.38697 0.38723 0.39472 0.39455 0.39455 0.39455 0.39455	91/PYP 0.45236 0.64895 0.64894 0.66200 0.46178 0.65572 0.67218	-1.0000 X/DMAX 0.39800 0.44900 0.44900 0.52200 0.52200 0.58000	•		
PARRITION OF WORD 197 117 122 127 137 147	PL 14.525 14.525 14.450 14.460 14.739 14.734 14.539 14.444 14.539	MATINS , FOR MI /PO 0. 97361 0. 96858 0. 96825 0. 94800 0. 97863 1. 9097 1. 9031	0.39098 PERIDV INLET PL/PTF C.38407 0.38697 0.38723 0.39472 0.39455 0.39455 0.39455 0.39455	91/PTP	-1.000Q X/DMAX 0.39800 0.49100 0.44900 0.52200 0.52200 0.58000 1.0000	•		
PARRITION  // WORD  107  127  127  137  142  177  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD	PL 14.525 14.525 14.450 14.450 14.739 14.736 14.539 14.539	PL/PR 0.97361 0.96858 0.96858 0.96800 0.98800 0.98767 0.97863 1.0031	0.3909P FRITOV INLET PL/PTF C.3R407 0.3R697 0.38723 0.39472 0.39456 0.3909R 0.49107	91/PYP 0.45236 0.64895 0.64894 0.66200 0.46178 0.65572 0.67218	-1.0000 X/DMAX 9.39809 9.43100 0.44900 0.52209 0.52209 0.52209 -1.0000	•		
DARRITION  // WORD  // UPP  122  127  37  442	PL 14.525 14.525 14.525 14.525 14.529 14.734 14.529 14.908 ML PROPERTY PL 15.926 14.966	#47105 , FCP #4700 0.97361 0.96858 0.96825 0.94800 0.48767 0.97863 1:0031 P47103 y CAP	0.3909P ERMOV IMET  PL/PTF C.38407 0.38723 0.39472 0.39472 0.39472 0.39472 0.39472 0.39472 0.39472 0.39472 0.39472 0.39472	0.65572 P1 /PYP 0.65236 0.64895 0.64844 0.65200 0.6577 0.65572 0.67210	-1.0000 R/DMAX 7.39807 7.43100 0.44900 0.52207 0.52207 0.58000 -1.0000			
PARRITION  ON WORD  107  117  127  127  137  147  149  170  170  170  170  170  170  170  17	PL 14.525 14.450 14.450 14.739 14.734 14.509 14.450 15.905 PL 15.926 14.966 MI PRESSURE	#47105 , FCP #1/P0 0.97361 0.96858 0.96825 0.94800 0.48767 0.97863 1:0031 P47103 y CAP 1:0031 P47103 y CAP	0.3909P  FRIDV IMET  PL/PTF C.38497 0.38697 0.39472 0.39472 0.39472 0.39472 0.49074 0.49074  NOPPLE FIRST 0.49074  DEG SHPINIO 1	0.65472  PL /PTP 0.65236 0.64895 0.66200 0.6577 0.65772 0.677210	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.52000 -1.0000 -1.0000			
PARRITION  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD	PL 14.525 14.525 14.460 16.739 16.734 14.509 16.906  PL 16.906  MI PRESSIME PI	MATIOS , FOR MI/PO 0.97361 0.96858 0.96825 0.94800 0.94767 0.97863 1.9097 1.9031 PATIOS , FOR MI/PO MI/PO MI/PO	0.3909P  FRODY IMET  PL/PTF C.3R497 0.3R697 0.38723 0.39472 0.39472 0.39475 0.3909R 0.40101 0.40074  DEG SHPCUO 1 PL/PTF	91/PTP 0.65236 0.64895 0.64894 0.66200 0.6617P 0.65572 0.67210	-1.0000 X/DMAX 0.39800 0.4900 0.44900 0.52200 0.52000 1.0000 -1.0000 -1.0000 X/DMAX			
PARRITION  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  // WORD  /	PL 14.525 14.450 14.450 14.739 14.734 14.599 15.965 ML PRESSIRE PL 14.964	#L/PR 0.97361 0.96858 0.96858 0.96858 0.98800 0.98767 0.97863 1.9097 1.9031 PATIOS y FAM 1.0731 RATIOS , 20 PL/PR 1.0731	0.3909P ERMOV INLET  PL/PTF C.38407 0.38723 0.39472 0.39472 0.39472 0.39472 0.39472 0.40074  DESTRUCT  PL/PTF 0.40074	0.65572  PL/PYP 0.65236 0.64894 0.66200 0.6617P 0.65572 0.67210  PL/PYP 0.67210  PL/PYP 0.67210	X/DMAX			
PARRITION  OF WORD  OF 12  22  27  37  42  42  42  42  42  47  48  ARRITION  OF WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD	PL 14.525 14.525 14.460 16.739 14.739 14.539 14.539 14.964 MI PRESSIME PL 14.964 14.964	MATINS , FOR MI /PR 0. 97361 0. 96858 0. 94800 0. 94767 0. 97863 1. 9097 1. 9031 PATINS , 20 PI /PR 1. 9031 RATINS , 20 PI /PR 1. 9031	0.3909P  FRIDV IMET  PL/PTF C.3R497 0.38697 0.39472 0.39456 0.39456 0.39076 0.40101 0.40174  PI/PTF 0.40074 0.40074	91/PTP 0.65236 0.64895 0.64894 0.66200 0.66572 0.67210 91/PTP 0.67210 91/PTP 0.67210 91/PTP 0.67210	-1.0000 X/DMAX 0.39800 0.4900 0.44900 0.52200 0.52000 1.0000 -1.0000 -1.0000 X/DMAX			
PARRITION  OF WORD  OF 12  22  27  37  42  42  42  42  42  47  48  ARRITION  OF WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD  FOR WORD	PL 14.525 14.525 14.460 16.739 14.739 14.539 14.539 14.964 MI PRESSIME PL 14.964 14.964	#L/PR 0.97361 0.96858 0.96858 0.96858 0.98800 0.98767 0.97863 1.9097 1.9031 PATIOS y FAM 1.0731 RATIOS , 20 PL/PR 1.0731	0.3909P  FRIDV IMET  PL/PTF C.3R497 0.38697 0.39472 0.39456 0.39456 0.39076 0.40101 0.40174  PI/PTF 0.40074 0.40074	91/PTP 0.65236 0.64895 0.64894 0.66200 0.66572 0.67210 91/PTP 0.67210 91/PTP 0.67210 91/PTP 0.67210	X/DMAX			
PARRITION  VIOLENTE IN WORD  107  112  122  127  137  1462  147  PARRITION  VIOLENTE IN WORD  167  172  PARRITION  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLE	PL 14.525 14.525 14.525 14.450 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739	# / Pr 0. 97361 0. 96858 0. 96858 0. 96858 0. 98800 0. 98767 0. 97863 1.0031 PATIOS - 20 PI / Pr 1.0031 RATIOS - 20 PI / Pr 1.0031 1.0027 PATIOS - 40 PI / Pr	0.3909P  FERTOV IMET  PL/PTF C.38497 0.38697 0.39472 0.39472 0.39472 0.39472 0.49074  DEG SHPRUN 1  PL/PTF	91/PTP 0.65236 0.64895 0.64894 0.66200 0.66572 0.67210 91/PTP 0.67210 91/PTP 0.67210 91/PTP 0.67210	X/DMAX			
PARRITION  VIOLENTE IN WORD  107  112  122  127  137  1462  147  PARRITION  VIOLENTE IN WORD  167  172  PARRITION  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLENTE IN WORD  VIOLE	PL 14.525 14.525 14.525 14.450 14.450 14.739 14.734 14.529 14.529 15.965 ML PRESSIRE PL 14.964 14.964 14.959	RATIOS , FOR PL/PO 0.97361 0.96658 0.96858 0.98800 0.98767 0.97863 1.9097 1.0031 PATIOS , FAMP 1.0737 1.0731 RATIOS , 20 PL/PO 1.0737 1.0731 RATIOS , 20	0.3909P ERMOV INLET  PL/PTF C.38407 0.38723 0.39472 0.39472 0.39472 0.39472 0.39472 0.40074 0.40074 0.40074 0.40074 0.40074 0.40074	0.65572  PL/PYP 0.65236 0.64894 0.66200 0.6617P 0.65572 0.67210 0.67210 0.67210 0.67210 0.67210 0.67210 0.67210	X/DMAX 0.39800 0.44900 0.44900 0.52200 0.58000 1.0000 X/DMAX -1.0000 1.0000 X/DMAX 0.79300 0.84400			
PARRITION  // WIRD  107  117  122  127  137  147  149  149  149  149  149  149  14	PL 14.525 14.525 14.525 14.450 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739 14.739	# / Pr 0. 97361 0. 96858 0. 96858 0. 96858 0. 98800 0. 98767 0. 97863 1.0031 PATIOS - 20 PI / Pr 1.0031 RATIOS - 20 PI / Pr 1.0031 1.0027 PATIOS - 40 PI / Pr	0.3909P  FERTOV IMET  PL/PTF C.38497 0.38697 0.39472 0.39472 0.39472 0.39472 0.49074  DEG SHPRUN 1  PL/PTF	0.65572  PL/PTP 0.65236 0.64895 0.64844 0.66200 0.46178 0.65572 0.67210  01/PTP 0.67255 0.67210  PL/PTP 0.67210 0.67187  DFATION PL/PTP	X/DMAX 0.39800 0.4900 0.44900 0.46900 0.52200 0.52200 0.58800 -1.0000  X/DMAX 0.79300 0.84400			
DANDITION  VO WORD  197  122  127  137  142  142  142  142  142  142  142  14	PL 14.525 14.525 14.525 14.525 14.527 14.529 14.734 14.529 14.529 14.964 14.964 14.966 14.969 PL 14.964 14.959	MATINS , FOR MI /PO 0.97361 0.96858 0.96825 0.98800 0.98767 0.97863 1.9097 1.9031 PATINS , FOR MI /PO 1.0031 RATIOS , 20 MI /PO 1.0031 1.0027 PATINS , 40 MI /PO 0.99235	0.3909P ERMOV IMET  PL/PTF C.38497 0.38723 0.39472 0.39472 0.39472 0.39475 0.39074  WOFFIT FIRE 0.40074 DEG SHPCUO 1 PL/PTF 0.40074 0.40074 0.40074 0.40074 0.40074 0.40074	91/PTP 0.65572 0.64944 0.66570 0.66577 0.65572 0.67210 01/PTP 0.67210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0167210 0166492	#/DMAX 0.39800 0.43100 0.44900 0.46900 0.52200 0.52200 0.52000			

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7 15.2 2 16.2 ADDITIONAL PRES N MOPO PL 2 15.2 ADDITIONAL CRES N MOPO PL 2 19.2 2 19.5 ADDITIONAL PRES D WOPD PL 37 14.4 37 14.4 ADDITIONAL PRES D WORD PL 57 14.4 37 14.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7	309 1.01 233 1.01 ESSUPE RATIOS  532 1.10 646 0.91 ESSURE PATIOS  PL/PT 196 0.65 299 1.27 1959 1.05 1959 1.07 1950 0.91 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0.95 1950 0	248 0.37141 0.39310 , FLOW SPLITTER 267 0.40109 1352 0.33106 , FLOW SPLITTER 379 0.46602 014 0.36293 1797777 34677 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222 179777 0.35222	0.62113 0.66798 1.0. P1/PTP 0.68157 0.56257 F=D. P1/PTP 0.40482 0.75191 0.61672 P1/PTP 0.5960 0.59572 0.59654 0.60699 0.60692	2.91903 1.0170 2.62208 0.67000 2.67000 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300				
2 16.2 ADDITIONAL PRES D MOPD PL 2 19.2 2 19.2 2 19.2 2 19.2 2 19.2 2 19.2 2 19.2 2 19.2 2 19.2 2 19.2 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3 37 14.3	233 1.09 ESSUPE RAYIOS  .532 1.10 .646 0.91 ESSURE PAYIOS  PL/PF .299 1.26 .299 1.26 .299 1.26 .299 1.27 .299 1.06 .299 1.27 .299 1.07 .299 1.07 .299 1.07 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .290 0.99 .	0.39310 , FLOW SPLITTER  267 0.40109 1352 0.33106 , FLOW SPLITTER  27 0.40109 27 0.33106  27 0.23823 28 0.46602 214 0.36291  27 0.35222 27 0.35223 27 0.35223 28 0.3573 28 0.3573 28 0.3573	0.66798  I.D.  PL/PTP	I-0170  #/OMAK 0-42200 0-67000  #/OMAK 0-50000 0-58300 0-47000  #/OMAK -1-0000 -1-0000 -1-0000 -1-0000				
2   16.2  ADDITIONAL PRES  D WOPD PL  2   16.2  ADDITIONAL PRES  D WOPD PL  22   19.2  24.4  27   14.4  27   14.4  27   14.4  27   14.5  ADDITIONAL PRES  D WORD PL  37   14.5  17   14.5  17   14.5  17   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  27   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5  28   14.5	233 1.09 ESSUPE RAYIOS  .532 1.10 .646 0.91 ESSURE PAYIOS  PL/PF .299 1.26 .299 1.26 .299 1.26 .299 1.27 .520 0.99 .470 0.96 .740 0.96 .740 0.96 .740 0.96 .750 0.97 .755 0.98 .755 0.98	0.39310 , FLOW SPLITTER  267 0.40109 1352 0.33106 , FLOW SPLITTER  27 0.40109 27 0.33106  27 0.23823 28 0.46602 214 0.36293  27 0.35222 27 0.35223 27 0.35223 28 0.3573 28 0.3573 28 0.3573 28 0.3573	P1 /PTP	Y/DMAX 0-52200 0-67000 X/DMAX 0-50000 0-58300 0-67000 X/DMAX -1-0000 -1-0000 -1-0000 -1-0000				
16.2 16.2 16.2 16.2 16.2 16.2 16.2 16.2	1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,00	7 PI/PTF 7 0. 40109 7 0. 33106 7 0. 40109 7 0. 33106 7 0. 33106 7 0. 23823 7 0. 46602 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223 7 0. 35223	Pt /PTP 0.68157 0.56257 F-D. Pt /PTP 0.40482 0.75191 0.61672 Pt /PTP 0.5960 0.59572 0.59654 0.60699 0.60692	0.42200 0.67000 X/0MAX 0.50000 0.58300 0.47000 X/0MAX -1.0000 -1.0000 -1.0000 -1.0000				
2 16.5 7 13.6 ADDITIONAL CRES D MOPD PL 2 19.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 37 14.5 ADDITIONAL PRES D WORD PL 3	.532 1.10 .646 0.91  SSURE PATIOS  PL/PF  1959 1.05  1959 1.06  1959 1.07  1959 1.06  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  1959 1.07  19	267 0.40109 1352 0.33106  , FLOW SPLITTEP 15736 0.23823 159 0.46602 114 0.36291  7 PL/PTF 1202 0.35223 159 0.45105 1673 0.35720 1673 0.35720 1673 0.35720 1673 0.35720	0.68157 0.56257 Fan. Pt /PTP 0.40482 0.75191 0.61672 0.59660 0.59572 0.59654 0.60669 0.60669	0.42200 0.67000 X/0MAX 0.50000 0.58300 0.47000 X/0MAX -1.0000 -1.0000 -1.0000 -1.0000				
7 13.6  ADDITIONAL RES  D MOPD PL  2 19.5  ADDITIONAL PRES  D MOPD PL  27 14.9  12 19.6  27 14.7  14.7  15.7  14.7  15.7  14.7  15.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  17.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7  16.7	### PATION   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   PL/PR   P	1352 0.33106  , FLOW SPI IVYEP  1736 9.23823 159 0.46602 114 0.36293 1797 0.35223 1797 0.35223 1797 0.35223 1797 0.35223 1797 0.35223 1797 0.35223 1797 0.35223 1797 0.35223 1797 0.35223 1797 0.35223 1797 0.35223	0.56257  F-D.  Pt /PTP 0.40482 0.75191 0.61672  0.59860 0.59572 0.59654 0.60766 0.60069	X/OMAX Q-50500 Q-58300 Q-58300 Q-67000 X/OMAX -1.0000 -1.0000 -2.0000 -1.0000				
ADDITIONAL CRES D MOPD PL 07 14.5 12 14.5 12 14.6 137 15.1 14.7 15.7 14.7 17 14.5 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 1	PL/PT 196 0.05 299 1.27 299 1.27 1959 1.05 1959 1.05 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 195	, FLOW CPI ITTEP  1	PL /PTP	X/OMAX 0.50000 0.58300 0.47000 X/OMAX -1.0000 -1.0000 -2.0000 -1.0000				
D WOPD PL  27 19-2  28-5  D WOPD PL  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3  27 14-3	PL/PF  1196	M /PTF 5736	0.40482 0.75191 0.61672 0.5960 0.5960 0.59572 0.5966 0.6069	0.50000 0.58300 2.47000 X/00AX -1.0000 -1.0000 -2.0000 -1.0000				
7 9.01 7 9.01 7 10.2 2 19.5 2 19.5 0 WOPD PL 07 14.7 12 19.5 27 14.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7 37 15.7	1196 0.65 299 1.27 299 1.27 1959 1.05 1959 1.05 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1950 0.97 1955 0.98 1955 0.98	7.23 9.23 9.35 9.36 9.36 9.36 9.36 9.36 9.36 9.36 9.36	0.40482 0.75191 0.61672 0.59860 0.59572 0.59654 0.60669 0.60669	0.50000 0.58300 2.47000 X/00AX -1.0000 -1.0000 -2.0000 -1.0000				
2 14.2 2 19.5 2 19.5 2 19.5 2 19.5 2 14.7 2 19.6 2 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3 14.7 3	209 1.26 259 1.00 259 1.00 259 2.00 250 0.00 250 0.	159 0.46602 114 0.36291 1 PL/PTF 1202 0.35222 179 9.35032 1673 0.35720 1673 0.35720 1673 0.35720 1673 0.35720 1673 0.35720 1673 0.35720	0.75191 0.61672 0.59860 0.59572 0.59654 0.60766 0.60069	0.58300 2.67000 X/RIAX -1.0000 -1.0000 -2.0000 -1.0000				
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2 14.5 10 MOPD PL 12 14.5 12 14.5 12 14.5 137 14.7 14.7 14.7 14.7 15.7 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 17 14.7 18 18 18 18 18 18 18 18 18 18 18 18 18 1	959 1.05 959980 ****109 1520 2.91 450 0.98 450 0.99 155 0.99 1765 0.99 1705 0.98 55980 ************************************	0,36291  1 PL/PTF 1202 0,35224 1239 9:35057 1673 0,35760 1641 0,35820 1659 0,35675 1659 0,35675	0.61672 0.5980 0.5980 0.59572 0.59656 0.6069 0.60692	7.67000 X/RMAX -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
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-31 693.95	.770 O. 9"		.0430 FY	APF 7.7444				

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AVD WOPD	PL	PL/PO	PL/PTF	PI /PTP	X/Deax		Marriage - Marriage - 11111 and	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	which is the species on a
32	9.1492	0.54381	2.17472	0.29817	0.72200				
37	13.611	9,99977	0.29214	0.49855	0.87000				
47	11.593	3.77446	0.245#2	0.42463	0.91900				
52	14.502	1.1024	0.35427	0.69446	1.3170				
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AND MORD	PL	PL / PO	PI /PTF	PL /PTP	X/DMAX				
62	16.719	1.2595	0.40179	0.68567	0.42200				
67	15.543	1.0384	0.73762	0.56934	0.67900				
>4001TIONA	L PPFSSIPF	PATINS , FLO	W SPLITTER O	). D.					
AVD WORD		PL/PO	PL /PTF	PL /PTP	X/DMAX				
	PL								
77	11,083	0.74042	0.1789	0.40597	2.50000				
R2	15.514	1.0367	0. ±3309	0.56843	0.58300				
92	15,004	1.9924	0.32704	0,54959	0.67000		<del></del>		
MODITY HOME	L PRESSURE	<del>nation y fai</del>	<del>e des casado</del>						
	PL	PL/PO	9/PTF	21.00	X/DMAX		4 Aug		
-107	14.590	202399	0. 21293	0.53404	-1.0000				
-112	14.510	0.96932	-1147	0.53146	-1.0000				
-127	14.525	2-07032	0.31174	0.53202	-1.0000				
-127	14.824	0. 98901	0.31776	0.56227	-1-0000				
	-15.944	2.99169	0.31861	0.54377	-1,0000			1 1	÷ =
-137 _									
	14.874	0.99368	0.31 026	0.54483	-:.0000			*	
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>4701110NA	14.874 L PPESSURE	0.9936A RATERS : FRP	O.31°26 ERFOY IMET	0.54483 PL /PTP	-1.0000-		•		
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>4001710NA AVD WIPD 107 112 122 127 137	14.874 L PRESSURE PL 14.583 14.510 14.525 14.804 14.844	0.99368 PATEIS : FIP P: /PI 7.97399 0.96932 0.97932 0.98901 7.99168	0.31 926 ERPOY IMLET PL /PTF C. 21 293 0.31 143 0.31 175 0.31 776 0.31 776	PL /PTP 0.53494 0.53148 0.53202 0.54227 0.54373	x/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200		• •		
>4001710NA AVD WIPD 107 112 122 127 137	14.874 L PPESSURE PL 14.583 14.510 14.525 14.804 14.844 14.876	0.99368 PATEIS FIP PC /PI 9.97399 0.96932 0.97032 0.98901 7.99168 1.99368	0.31°26 ERIMY IMET PL/PTF G. 212°3 0.31143 0.31175 0.3176 0.31861 0.31861	0.54483 PL/PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483	X/DMAX 0.39800 0.43100 0.44900 0.46600 0.52200 0.58800		•		
>4001710NA AVD WIPD 107 112 122 127 137	14.874 L PRESSURE PL 14.583 14.510 14.525 14.804 14.844	0.99368 PATEIS : FIP P: /PI 7.97399 0.96932 0.97932 0.98901 7.99168	0.31 926 ERPOY IMLET PL /PTF C. 21 293 0.31 143 0.31 175 0.31 776 0.31 776	PL /PTP 0.53494 0.53148 0.53202 0.54227 0.54373	x/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200		• • • • • • • • • • • • • • • • • • • •		
>AODITIONA AVD WIPD 107 117 129 127 137 147 147	PRESSURE PL 14.583 14.510 14.525 14.804 14.874 14.876	0.99368 PATERS FRP P. /PR 9.97399 0.97932 0.97932 0.98901 1.99168 1.99368 1.99368	0.31926 ENTRY IMET  PL /PTF 6.21293 0.31143 0.31176 0.3176 0.3176 0.3176 0.3176	0.54483 P1 /PTP 0.53404 0.53146 0.53202 0.54227 0.54373 0.54483	X/DMAX 0. 39800 0.43100 0.44900 0.52200 0.52800		•		
>ADDITIONA NVD WOPD 127 117 129 127 137 147 147 147	PESSURE PL 14.580 14.510 14.525 14.804 14.844 14.876 14.999 14.999	0.99368  PATERS FRP  P. /PR	0.31°26 ENDOY IMET  PI /PTF 6.212°3 0.31175 0.3176 0.3176 0.3176 0.31861 0.31926 0.21°4	0.54483 PL/PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483 0.74440 10.74440	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52800 -1.0000		•		
>AODITIONA AVD WIPD 107 117 127 127 137 142 143 143 143 144 2400111044	PRESSURE PL 14.589 14.510 14.525 14.814 14.876 14.876	0.99368 PATERS FRP P. /PR 2.97399 0.96932 0.97032 0.98901 3.99168 1.9920 1.9920 PATERS PAR	0.31 926 ENDOV IMLET  PI /PTF 6.21293 0.31175 0.31776 0.31776 0.31776 0.31776 0.31776	PL /PTP 0.53494 0.53149 0.53202 0.54227 0.54373 0.54493 0.54490	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58000 -1.0000		• •		
>ADDITIONA NVD WOPD 127 117 129 127 137 147 147 147	PESSURE PL 14.580 14.510 14.525 14.804 14.844 14.876 14.999 14.999	0.99368  PATERS FRP  P. /PR	0.31°26 ENDOY IMET  PI /PTF 6.212°3 0.31175 0.3176 0.3176 0.3176 0.31861 0.31926 0.21°4	0.54483 PL/PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483 0.74440 10.74440	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52800 -1.0000		•		
>AODITIONA AVD WIPP 127 117 129 127 137 147 147 -152 AVD WIPP -152 -152 -152	PL 14.540 14.540 14.510 14.525 14.816 16.846 16.846 14.976 14.976	0.9936A  PATERS FRM  P. /PR	0.31°26  ENDOY IM.EY  PI /PTF 6.212°3 0.31175 0.3176 0.3176 0.3176 0.3176 0.3176 0.3176 0.3176 0.3176	0.54483 PL/PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483 0.74440 0.74440 0.54940	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000		• •		
>ADDITIONA AVD WOPD 137 112 127 137 142 142 143 143 144 145 145 145 145 147 147 147 147 147 147 147 147 147 147	PL 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.99 14.99 14.99 14.99 14.99 14.99 14.99 14.99 14.99 14.99 14.99 14.	0.9936A  PATERS FRM  PC /PR	0.31°26 ERION IMET  PL /PTF	0.54483 PL /PTP 0.53404 0.53148 0.53202 0.54227 0.54773 0.54463 0.74490 PL /PTP 0.54040 0.54940	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 1.0000 -1.0000 X/DMAX -1.0000		• •		
>ADDITIONA  NO WORD  107  117  127  127  137  147  147  147  -141  -141  -141  >ADDITIONA  NO WORD	PL 14.580 14.580 14.510 14.525 14.804 14.904 14.909 14.909 14.909 14.909 14.909	0.9936A  PATERS : FRP  P. /PR	0.31 °26  ENDOY IMET  PL /PTF	0,54483 PL /PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483 0.74400 0.54960 0.54960	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 -1.0000 X/DMAX				
>ADDITIONA AVD WOPD 127 117 129 127 137 147	PL 14.540 14.540 14.510 14.525 14.804 14.844 14.844 14.999 14.999 14.999	0.9936A  PATERS : FRP  P. /PR	0.31 926  ENDOY IMET  PI /PTF 6.21293 0.31175 0.31776 0.31761 9.31926 0.2199  WYPTF 0.32199  DEG SHORINI II  PI /PTF 0.32194	0.54483 PL /PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483 0.74440 0.74940 0.54940 0.64940	X/DMAX 0.39800 0.43100 0.44900 0.46600 0.52200 -1.0000 -1.0000 X/DMAX -1.0000 X/DMAX 0.79300				
>ADDITIONA  IVD WIPP  127  127  127  137  142  -152	PL 14.583 14.510 14.525 14.814 14.844 14.844 14.876 14.999 14.999 14.999	0.9936A  PATERS FRM  PC /PR	0.31 °26  ERION IMET  PL /PTF	0,54483 PL /PTP 0.53404 0.53148 0.53202 0.54227 0.54473 0.54483 0.74490 0.54960 0.54960 0.54960 0.54960 0.54960 0.54960 0.54960	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 -1.0000 X/DMAX				
>ADDITIONA AVD WOPD 127 117 129 127 137 147 147 147 147 147 220171000 AVD WOPD 167 177 >ADDITIONA	PL 14.583 14.510 14.525 14.814 14.844 14.844 14.876 14.999 14.999 14.999	0.9936A  PATERS : FRP  P. /PR	0.31 926  ENDOY IMLEY  PI /PTF	PL /PTP 0.53404 0.53140 0.53202 0.54227 0.54373 0.54403 0.74400 0.54940 0.54940 0.54940 0.54959	X/DMAX 0.39800 0.43100 0.44900 0.46600 0.52200 -1.0000 -1.0000 X/DMAX -1.0000 1.0000 X/DMAX 0.79300 0.84400				
>ADDITIONA  NO WORD  107  117  127  137  147  147  147  147  240011104A  AVD WORD  167  177  >ADDITIONA  AVD WORD  167  177  >ADDITIONA  AVD WORD	PL 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 14.999 15.999	0.9936A  PATERS : FRM  P. /PR	0.31 °26  ERION IMET  PL /PTF	0.54483 PL /PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483 0.74480 0.74480 0.54940 0.54940 0.54959 0.54959	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX 0.79300 0.79300 0.79400				
>ADDITIONA  NO WORD  107  117  127  127  137  147  147  147  -152  -152  >ADDITIONA  NO WORD  167  172  >ADDITIONA  LVD WORD  167  172  >ADDITIONA  LVD WORD  167	PESSURE PL 14.580 14.510 14.525 14.804 14.476 14.999 14.999 14.999 15.999 15.996 PE 14.999 15.996 PE 14.999 15.996	0.9936A  PATERS : FRM  P. /PR	0.31 926 ENDOY IMET  PI /PTF	0,54483 PL /PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54463 0.74460 0.54940 0.54940 0.54940 0.54959 0CATION PL /PTP 0.54940	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 X/DMAX 0.79300 0.79300 X/DMAX 0.79300				
>ANDITIONA  NOD WOPD  127  117  129  127  137  147  147  -159  -159  >ANDITIONA  AVD WOPD  167  179  >ANDITIONA  AVD WOPD  167  179  >ANDITIONA  AVD WOPD  167  179  179  187	PESSURE PL 14.580 14.510 14.525 14.804 14.846 14.899 14.999 14.999 15.994 18.999 15.994 19.999	0.9936A  PATERS : FRP  PC /PR	0.31 926  ENDOY IMET  PI /PTF	0.54483 PL /PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483 0.74480 0.74480 0.54940 0.54940 0.54959 0.54959	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX 0.79300 0.79300 0.79400				
>ANDITIONA  NOD WOPD  127  117  129  127  137  147  147  -159  -159  >ANDITIONA  AVD WOPD  167  179  >ANDITIONA  AVD WOPD  167  179  >ANDITIONA  AVD WOPD  167  179  179  187	PL 14.999 15.999 PL 14.645 14.189 PESSURE	0.9936A  PATERS : FRP  P. /PR	0.31 926  ENDOY IMET  PI /PTF	0,54483 PL /PTP 0.53404 0.53148 0.53202 0.54227 0.54373 0.54483 0.74440 0.74940 0.54940 0.54940 0.54959 0CATION PL /PTP 0.53641 0.51940	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 X/DMAX 0.79300 0.79300 X/DMAX 0.79300	ns= 2,4589	(FM 0.402)136		

	S PRELIM	TPIARY DATA	06/13/79	CADDELL	PEC 10/25/79 00:41:54.119	FAC ANANI	PGM CO36 RUN 1474
>ADDIT ION	AL PRESSIRE	RATIOS , PPI	MAFY PIUG				
VP WCPD	PI	Pt / Pt	PL/PTF	PL /PTP	X/DHAX		The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th
32	. 9. 3385	0.61670	0.17068	0-29161	0.72230		
37	16.473	1.0878	0.3010#	0.51439	0.82000		
47	13.573	0.89633	0.24808	0.42383	0.91900		
52	16.942	1.1122	0.30783	0.52592	1.0170		
ADDITION	AL OPESSIBE	RATIOS . FLO	u CDI ITTER I				الهيول المعاهين الواد المستنفية المحمول الماعمين
AU MUBD	PĻ	PI /PO	PL /PTF	PL /PTP	X/DMAX		
62	22.069	1.4573	0.49334	0-68909	0.42200		
67	14.584	1.2273	0.33967	0.58031	0.67000		
ATO ET TOM	AL PRESSURE	PATINS . FLO	W SPLITTER C	n.n.			
n woen	PL.	Pt./P0	PL /PYF	PL /PTP	X/DMAX		
77	13.019	0.85973	0 - 23 795	Q.40652	0.50800		
12	14.260	1.205A	0.33374	0.57018	0.58300		
2	15.145	1.0002	0.27682	0.47293	0-67900		
MARKET THE	AE PRESSIEC	RETINAL EUR	CTC= SHERVE				
'U MUBE _	PL	PL/PO	PL/PTF	PLANT	X/DMAX.		
07	14.726	0.97246	0.26915	0.45983	-1.0000		•
12	14.661	0.96820	26 797	Q.45781	-1.0000	•	
22	14.691	0-04971	0.25693	0.45843	-1.0000		
27	14.960	2. 9A 797	0,27344	0746716	-1.0000		·
37	14.995	0.99028	7-27498	0.46625	-1.0000	* * * *	
سسجما	15,025	0.99226	0.27463	0,46919	-1.0000		
NOT TICON	15,025	0.99226 RATIOS . FCR	0.27463	0,46919	1.00000-,	···· - ·	
ADDITION	15.025 AL PRESSUPE	0.99226 RATIOS . FCR	0.27463 ERMY INLET	0.46919 PL/PTP	-1.0006.		
ADDITION O HORD	15.025 AL PRESSUPE PL 14.726	0.99226 RATIOS . FCR PL/PO	0.27463 ERODY INLET PL/PTF 0.26915	0.46919 PL/PTP 0.45983	X/DMAX 0.39800	•	· - · · · · · · · · · · · · · · · · · ·
ADDITION O WORD	15.025 AL PRESSUPE PL 14.726 14.661	0.99226 RATIOS . FCR PL/PO 0.97248 0.96820	0.27463 ERMY INLET PL/PTF 0.26915 0.26797	0,46919 PL/PTP 0.45983 0.45781	X/DMAX 0.39800 0.43100		
ADDITION OF HORD	15.025 AL PRESSUPE PL 14.726 19.661 14.691	0.99226  RATIOS . FCR  PL/PN 0.97248 0.96820 0.96951	0.27463 ERONY INLET PL/PTF 0.26915 0.26797 0.26833	0,46919 Pt/PTP 0.45983 0.45781 0.45843	X/DMAX 0.39800 0.43100 0.44900	•	
ADDITION  /D WORD  107  112  122	15.025 AL PRESSUPE PL 14.726 14.661 14.601 14.960	0.99226  RATIOS . FCR  PL/PO 0.97248 0.96820 0.96951 2.98797	0.27463 ERMNY INLET PL/PTF 0.26915 0.26797 0.26783 0.27346	0,46919 PL/PTP 0.45983 0.45781 0.45843	-1.0000- X/DMAX 0.39800 0.43100 0.44900 0.4600	•	- · · - · · · · · · · · · · · · · · · ·
ADDITION /D WORD 107 112 172 27	15,025 AL PRESSUPE PL 14,726 14,661 14,661 14,960 14,995	0.99226  RATIOS . FCR  PL/PO 0.97248 0.96820 0.96951 2.98797 0.99028	0.27463 ERCRIY INLET PL/PTF 0.26915 0.26797 0.26797 0.27346 0.27409	0,46919 PL/PTP 0.45983 0.45781 0.45716 0.46825	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200	•	
ADDIT ION /D WORD 07 112 122 27 137	15,025 AL PRESSUPE PL 14.726 14.661 14.641 14.960 14.95 15.025	0.99226  RATIOS . FCR  PL/PO 0.97248 0.96820 0.96951 2.98797 0.99028 0.99226	0.27463 ERRINY INLET PL/PTF 0.26915 0.26797 0.26797 0.27346 0.27409 0.27463	0,46919 -PL/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46919	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800	•	
ADDIT ION OF HORD OF 12 72 27 37 42	15,025 AL PRESSUPE PL 14,726 14,661 14,661 14,960 14,995	0.99226  RATIOS . FCR  PL/PO 0.97248 0.96820 0.96951 2.98797 0.99028	0.27463 ERCRIY INLET PL/PTF 0.26915 0.26797 0.26797 0.27346 0.27409	0,46919 PL/PTP 0.45983 0.45781 0.45716 0.46825	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200	•	
ADDIT ION  D WORD  07  12  12  27  37  42	15,025 AL PRESSUPE PL 14,726 14,661 14,960 14,995 15,025 17,149 15,140	0.99226  RATIOS . FCR  PL/PN 0.97248 0.96820 0.96951 2.98797 0.99028 0.99226	0.27463 ERRINY INLET  PL/PTF 0.26915 0.26797 0.26833 0.27346 0.27409 0.27463 0.27467	0,46919  PL/PTP 0.45983 0.45781 0.4583 0.45716 0.46825 0.46919 0.47777	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58600 -1.0000		
ADDITION  // HORD  OF  112  172  27  37  42	15,025 AL PRESSUPE PL 14,726 14,661 14,960 14,995 15,025 17,149 15,140	0,99226  RATIOS . FCR  PL/PO 0,97248 0,96820 0,96851 1,98797 0,99028 0,99226 0,99426 0,99484	0.27463 ERRINY INLET  PL/PTF 0.26915 0.26797 0.26833 0.27346 0.27409 0.27463 0.27467	0,46919  PL/PTP 0.45983 0.45781 0.4583 0.45716 0.46825 0.46919 0.47777	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58600 -1.0000		
ADDIT ION  // WORD  // OT  12  17  27  37  42  40  40  40  40  40  40  40  40  40	15,025 AL PRESSUPE PL 14,726 14,661 14,681 14,950 14,995 15,025 15,140 PL	0,99226  RATIOS , FCR  PL/PN 0,97248 0,96820 0,96951 2,98797 0,90228 0,99226 0,9926 0,9926	0.27463 ERODY INLET  PL/PTF 0.26915 0.26797 0.26833 0.27346 0.27409 0.27463 0.27677	0,46919  P1/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46819 0.47777	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000		
ADDITION  /D WORD  107  112  122  27  137  42	15,025 AL PRESSUPE PL 14.726 14.661 14.661 14.960 14.995 15.025 17:140 19.140 AL PRESSUPE	0.99226  RATIOS . FCR  PL/PO 0.97248 0.96820 0.96951 2.98797 0.99028 0.99226 0.99226 0.99226	0.27463 ERRINY INLET  PL/PYF 0.26915 0.26797 0.26833 0.27346 0.27409 0.27463 0.27409 0.27672	0,46919  PL/PTP 0.45983 0.45783 0.45783 0.46716 0.46825 0.46919 0.47777	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000		
ADDITION  // WORD  OF  12  72  27  37  42	15,025 AL PRESSUPE PL 14.726 14.661 14.681 14.960 15.025 15.025 15.140 PRESSUPE PL 15.140	0.99226  RATIOS . FCR  PL/PN 0.97248 0.96820 0.96851 2.98797 0.99028 0.99226 0.99226 0.99749 0.9974	0.27463 ERODY INLET  PL/PTF 0.26915 0.26797 0.26933 0.27344 0.27409 0.27463 0.27677 0.27677	0,46919  PL/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46825 0.46717 0.47277 0.47277	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 -1.0000 -1.0000	•	
ADDIT ION  // WORD  OF  112  72  27  137  42  42  42  47  40  47  40  47  40  47  40  40  40	15,025  AL PRESSUPE  PL 14.726 14.661 14.960 14.995 15.025 19.140  AL PRESSURE	0.99226  RATIOS . FCR  PL/PN 0.97248 0.96820 0.96851 2.98797 0.99028 0.99226 0.99426 0.99426 0.99484 RATIOS . 728	0.27463 ERRINY INLET  PL/PTF 0.26915 0.26797 0.26833 0.27356 0.27469 0.27463 0.27477 0.27677  PL/PTF 0.74422 0.27672  DEG SHPRUD 1	0,46919  PL/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46919 0.47277 0.47277 0.47277 0.47277	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 -1.0000	•	
ADDITION  // WORD  OF    112    12    12    13    42    42    47    ADDITION  // WORD  // WORD  // WORD	15,025  AL PRESSUPE  PL 14.726 19.661 14.691 14.995 15.025 17:140  AL PRESSUPE  PL 15.140  AL PRESSURE	0.99226  RATIOS . FCR  PL/PN 0.97248 0.96820 0.96951 2.98797 0.99028 0.99226 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.9926 0.	0.27463 ERRINY INLET  PL/PYF 0.26915 0.26797 0.26833 0.27344 0.27409 0.27463 0.27677 0.27677 0.27677  PL/PYF 0.77412 0.27672 DEG SHPRUD 1	0,46919  P1/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46919 0.47277 U.47777 P1/PTP 0.47277 D.47272  RCATION P1/PTP	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 -1.0000 X/DMAX		
ADDITION  // HORD  112  122  127  137  142	15,025  AL PRESSUPE  PL 14.726 14.661 14.960 14.995 15.025 19.140  AL PRESSURE	0.99226  RATIOS . FCR  PL/PN 0.97248 0.96820 0.96851 2.98797 0.99028 0.99226 0.99426 0.99426 0.99484 RATIOS . 728	0.27463 ERRINY INLET  PL/PTF 0.26915 0.26797 0.26833 0.27356 0.27469 0.27463 0.27477 0.27677  PL/PTF 0.74422 0.27672  DEG SHPRUD 1	0,46919  PL/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46919 0.47277 0.47277 0.47277 0.47277	-1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000		
ADDITION  D HORD  O7  12  72  27  37  42  42  42  42  47  ADDITION  CO HORD  67  72	PL 14.726 14.661 14.661 14.960 15.140 AL PRESSURE PL 15.140 AL PRESSURE PL 15.130 15.130	0,99226  RATIOS . FCR  PL/PN 0,97246 0,96820 0,96820 0,99026 0,99026 0,99084 0,99984 1,99984 RATIOS . 70 PL/PN 0,99918 0,99918	0.27463 ERRINY INLET  PL/PYF 0.26915 0.26797 0.26833 0.27346 0.27463 0.27477 9.27677  PL/PYF 0.744.12 0.27672  DEG SHPRUD 1 PL/PYF 0.27654 0.27654	0,46919  P1/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46919 0.47217 U.47717  P1/PTP 0.47277 0.47272  DCATION P1/PTP 0.47246 0.47246	X/DMAX 0.39800 0.43100 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 X/DMAX 0.79300	•	
ADDITION  // HORD  // HORD  // 112  // 12  // 12  // 13  // 142  // 17  ADDITION  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  // HORD  //	15.025  AL PRESSUPE  PL 14.726 14.661 14.671 14.960 14.995 15.025 17.140  PL 15.140  AL PRESSUPE  PL 15.130 15.130 AL PRESSUPE	0,99226  RATIOS , FCR  PL/PN 0,97248 0,96820 0,96851 1,98797 0,90228 0,99226 0,9926 0,9926 0,9926 0,9928 RATIOS , 798 RATIOS , 20  PL/PN 0,99918 0,99918 RATIOS , 80	0.27463 ERODY INLET  PL/PTF 0.26915 0.26797 0.26833 0.27346 0.27409 0.27463 0.27463 0.27677 0.27677  PL/PTF 0.27672  DEG SHROUD 1  PL/PTF 0.27654 0.27654 0.27654	0,46919  PL/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46919 0.47277  PL/PTP 0.47277 0.47277  DCATION  PL/PTP 0.47246 0.47246	X/DMAX 0.39800 0.43100 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000 X/DMAX 0.79300 0.84400	•	
ADDITION  // WORD  OF  112  172  27  137  42  42  43  442  45  47  ADDITION  // WORD  // WORD  // WORD	15,025  AL PRESSUPE  PL 14.726 14.661 14.960 14.995 15.025 19.140  AL PRESSUPE  PL 15.140  AL PRESSURE  PL 15.130 15.130 AL PRESSUPE  PL	0.99226  RATIOS . FCR  PL/PN 0.97248 0.96820 0.96851 2.98797 0.99028 0.99226 0.9944 0.99984 RATIOS . 72P PL/PN 0.99918 RATIOS . 80 PL/PN	0.27463 ERRINY INLET  PL/PTF 0.26915 0.26797 0.26797 0.26733 0.27346 0.27463 0.27477 0.27677  PL/PTF 0.77422 0.27672  DEG SHPOUD 1  PL/PTF 0.27654 0.27654 0.27654	0,46919  PL/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46919 0.47277 U.47777  PL/PTP 0.47277 0.47277 0.47246 0.47246 0.47246	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 -1.0000 -1.0000 X/DMAX 0.79300 0.84400		
ADDIT ION  // WORD  112  172  173  142  171  ADDIT ION  // WORD  67  172  ADDIT ION  // WORD  67  172  ADDIT ION  // WORD  67  172	15,025  AL PRESSUPE  PL 14.726 14.661 14.661 14.960 14.995 15.025 17:140  AL PRESSUPE  PL 15.140  AL PRESSURE  PL 15.130 15.130 AL PRESSUPE  PL 14.991	0,99226  RATIOS . FCR  PL/PN 0,97248 0,96820 0,96851 2,98797 0,99028 0,9926 0,9948 0,99984 RATIOS . 70 PL/PN 0,99918 0,99918 0,99918 RATIOS . 80 PL/PN 0,99917	0.27463 ERRINY INLET  PL/PYF 0.26915 0.26797 0.26833 0.27346 0.27409 0.27463 0.27677 0.27677 0.27677 0.27677 0.27677 0.27676 0.27676 0.27654 0.27654 0.27654 0.27654 0.27198	0,46919  P1/PTP 0.45983 0.45781 0.45843 0.46716 0.46825 0.46919 0.47217 U.47717  P1/PTP 0.47277 U.47277 U.47246 0.47246 0.47246 0.47246 0.47246	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 -1.0000 -1.0000 X/DMAX 0.79300 0.84400  X/DMAX 9.79300		
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POTTTC'A	AT PRESSIRE	PATINS . PP	MAPY PLIIG							
IN WITE	PL	PI, / PO	PL/PTF	PL /PTP	X /OMA X					
12	9, 7335	0.64527	0.16241	9.27639	0.72200					
7	17.416	1.1546	0.29059	0.49455	0.02000					
7	15.039	0,99699	0.25093	0.42704	2.91900					
			0.28250							
57	16. 937	1.1779	13. 24230	0.49097	1.0170					
ANT TINM	AL PRESSIPE	PATINS . FLO	W SPLITTER I	.n.						
n weep	PL	<b>PL / P</b> በ	PL /PTF	PI /PTP	x/DMAx					
2 _	23,497	1.5443	0.39875	9.47862	9.42209					
.7	19.329	1.2514	0.32251	0.54886	3.67000					
ANDIT ION	AL PRESSUPE	RATIOS . FLO	W SPLITTER P	.n.						_
r wran	PL	PL /PO	PL /PTF	PL /PTP	X/DMAX					
7	14-250	2.94467	9.23776	0.40463	0.50R00					
2	20.043	1.3287	0.33447	0.56914	0.58300					
2	15.129	1.0029	0.25243	0.76714	0.67000					
	AL PRESSIES							· · · · · · · · · · · · · · · · · · ·		_
บัลเชย	PL	FL/PD	PL/PTF	مجوعيات.	X/DMAX				-	
07	14.769	9-97911	0.24667	0.41939	-1.0000					
12	14.719	J. 97 580	17. 74559	0.41797	-1.0000					
27	14.744	2-07755	3.24601	0.41868	-1.0000					
	14.989	0.99368	0.25010	Q.425£3	-1.0000					
21										
37	15.744	0.99732	0.25101 0.25160	0.42719 0.42818	-1.0000 -1.0000	···	· · · · · · · · · · · · · · · · · · ·		· .	
ADDIT IDN	15.744	0.99964 RATINS , FOR	0.75160 FREDY THEFT	0.42719 0.42717	-1.0000 -1.0000					
ADDITION	15.744 15.779 AL PRESSIPE	0.99964 RATINS , FOR	0.25160 FREDY INLET PL/PTF	0.42719 0.42717 PL/PTP	-1.0000 -1.0000 X/DMAX					
ANDIT INN	15.744 15.779 AL PRESSIPE PL 14.769	0.99964 RAYIUS , FUR PL/PU 0.97911	7.75160 ERCDY INLET PL/PTF 0.24643	0.42719 0.42818 PL/PTP 0.41939	-1.0000 -1.0000 X/DMAX_ 0.29800		•			
ADDITION	15.744 15.779 AL PRESSIPE	0.99964 RATINS , FOR	0.25160 FREDY INLET PL/PTF	0.42719 0.42717 PL/PTP	-1.0000 -1.0000 X/DMAX					
ADDIT INN/ D WORD 07	15.744 15.779 AL PRESSIPE PL 14.769	0.99964 RAYIUS , FUR PL/PU 0.97911	7.75160 ERCDY INLET PL/PTF 0.24643	0.42719 0.42818 PL/PTP 0.41939	-1.0000 -1.0000 X/DMAX_ 0.29800				·	
ADOLT ION/ O MORD 07 12	15.744 15.779 AL PRESSIPE PL 14.769 14.719 14.744	0.99964 RATIOS , FOR PL/PO 0.97911 0.97580 0.97745	9.75169 PERCOV INLET PL/PTF 0.24643 0.24559 0.24601	0.42710 0.42818 PL/PTP 0.41930 0.41797 0.41868	-1-0000 -1-0000 x/0max 0-29800 0-43100 0-44900		• • • • • • • • • • • • • • • • • • • •		·	
ADDIT IDN/ ID WORD 07 12 22	15.744 15.779 AL PRESSIPE PL 14.769 14.719 14.744 14.989	0.99964  RATINS , FOR  PL/PO 0.97911 0.97580 0.97745 0.99363	9.75169 PREDV INLET PL/PTF 0.24643 0.24559 0.24601 0.25010	0.42710 0.42818 PL/PTP 0.41930 0.41797 0.41868 0.42563	X/DMAX 0.29800 0.43100 0.44900 0.48600					
ADOLT INN D WORD 07 12 27 27	75.744 15.779 AL PRESSIME PL 14.769 14.719 14.744 14.989 15.344	0.99964  RATINS , FOR  PL/PO 0.97911 0.97580 0.97585 0.99369 7.99732	9.75169 PL/PTF 0.24643 0.24559 0.24601 0.25010 9.25101	0.42710 0.42818 0.42818 0.41939 0.41797 0.41868 0.42563 0.42719	1.0000 1.0000 X/DMAX 0.29800 0.44900 0.48600 0.52200		•		-	
ADOLT INN D WORD 07 12 27 27	75.744 15.779 AL PRESSIBE PL 14.769 14.719 14.744 14.989 15.344 15.379	0.99964  RATINS , FOR  PL/PO 0.97911 9.97580 0.97369 0.99369 0.99369	9.75169 PERCOV INLET PL/PTF 0.24643 0.24559 0.24601 0.75010 9.25101 0.75160	0.42710 0.42818 PL/PTP 0.41930 0.41707 0.41868 0.42710 0.42818	-1.0000 -1.0000 X/DMAX 0.29800 0.43100 0.44900 0.52200 0.58800		•		-	
37 ADDIT INNI D. MORD 07 12 22 27 27 42	75.744 15.779 AL PRESSIBE PL 14.769 14.719 14.744 14.989 15.344 15.379	7,9964 RATINS , FCP PL/PN 0,97911 2,97580 0,9745 0,99369 7,99732 0,9964	9.75169 PL/PTF 0.24643 0.24559 0.24501 0.25010 0.25101 0.25160 0.2523	0.42719 0.42818 PL/PTP 0.41939 0.41797 0.41868 0.42719 0.42719	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.5200 0.5200 0.58800				-	-
37 ADDIT IDN/ D MORD 07 12 22 27 37 42	75.744 15.779 AL PRESSIME PL 14.769 14.719 14.744 14.744 15.379 15.144 15.379	9.9964  RATINS , FOR  PL/PO 0.97911 2.97510 0.97745 0.99369 7.99732 0.99964 1.0076	9.75169 PRODY INLET PL/PTF 0.24643 0.24559 0.24601 0.25010 0.25101 0.25160 0.2793	0.42710 0.42818 0.42818 0.41939 0.41797 0.41868 0.42710 0.42710 0.42818 0.42710	-1.0000 -1.0000 X/DMAX 0.29800 0.43100 0.44900 0.52200 0.58800		• • • • • • • • • • • • • • • • • • • •			
37 ADOLT INN D. MORD 07 12 27 27 27 47	75.744 15.779 AL PRESSIBE PL 14.769 14.719 14.744 14.989 15.344 15.379 15.174	7,9964  RATINS , FCP  PL/PC  0,97911  2,97580  0,97745  0,99369  7,99732  0,9964  1,9775	9.75169 PERCOV INLET PL/PTF 0.24643 0.24559 0.24561 0.25010 0.25101 0.25101 0.25160 0.27239	0.42719 0.42818 0.41939 0.41797 0.41868 0.42719 0.42719 0.42718	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000		•			-
37 40 40 70 10 10 12 22 27 37 42 42 42 42	75.744 15.779 AL PRESSIPE PL 14.769 14.719 14.744 15.344 15.379 15.344 15.379 15.174 PL	9,9964  RATINS , FMP  PL/PN 0,97911 0,97580 0,97745 0,99369 7,99732 0,9964 1,0076	9.75169 PREDV INLET PL/PTF 0.24643 0.24559 0.24601 0.25010 0.25101 0.25101 0.25101 0.2723	0.4271Q 0.42818 PL/PTP 0.4193Q 0.41797 0.41868 0.4271Q 0.4271Q 0.42818 0.42948 7.42948	-1.0000 -1.0000 X/DMAX 0.29800 0.43100 0.44900 0.52200 0.58800 -1.0000		•			-
37 ADDIT INNI D MORD 07 12 27 37 42 37 42	75.044 15.079 AL PRESSIDE PL 14.769 14.719 14.744 14.989 15.079 15.124 15.124 PL 15.124	9.9964  RATINS , FMP  PL/PN 0.97911 2.97580 0.97745 0.99369 7.99732 0.90964 1.9076 1.0076	9.75169 PRODY INLET PL/PTF 0.24643 0.24559 0.24501 0.25101 0.25101 0.25101 0.25103 0.2753 0.2753	0.42710 0.42818 0.42818 0.41939 0.41797 0.41868 0.42719 0.42818 0.42719 0.42818 0.42719 0.42846	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52200 0.58800 -1.0000 X/DMAX -1.0000		•			-
37 ADOLT INNI D. MORD 07 12 27 27 27 42 42 42 42 42 42 42 43 44 47 47 47 47 47 47 47 47 47 47 47 47	75.744 15.779 AL PRESSIBE PL 14.769 14.719 14.744 14.989 15.344 15.379 15.174 PL 15.174 PL 15.124	9,9964  RATINS , FCP  PL/PC 0,97911 2,97580 0,97745 0,99369 7,99732 0,99464 1,9976 1,9976	9.75169 PERFOY INLET PL/PTF 0.24643 0.24559 0.24501 0.25101 0.25101 0.25101 0.25101 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.2730 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00	0.4271Q 0.4281R 0.4193Q 0.41797 0.4186R 0.4271Q 0.4271Q 0.4271Q 0.4271Q 0.4271Q 0.4271Q 0.4271Q	-1.0000 -1.0000 X/DMAX 0.29800 0.43100 0.44900 0.52200 0.58800 -1.0000					-
37 ADDIT INNI D MORD 07 12 27 27 27 47 47 47 49 49 49 49 49 49 49 49 49 49 49 49 49	75.744 15.779 AL PRESSIBE PL 14.769 14.719 14.744 14.989 15.344 15.379 15.174 PL 15.174 PL 15.124	9,9964  RATINS , FCP  PL/PC 0,97911 2,97580 0,97745 0,99369 7,99732 0,99464 1,9976 1,9976	9.75169 PRODY INLET PL/PTF 0.24643 0.24559 0.24501 0.25101 0.25101 0.25101 0.25103 0.2753 0.2753	0.4271Q 0.4281R 0.4193Q 0.41797 0.4186R 0.4271Q 0.4271Q 0.4271Q 0.4271Q 0.4271Q 0.4271Q 0.4271Q	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52200 0.58800 -1.0000 X/DMAX -1.0000					-
37 ADDIT INNI D MORD 07 12 27 27 27 37 42 22 27 27 37 42 22 27 27 37 42 27 27 27 27 27 27 27 27 27 27 27 27 27	15.044 15.079 AL PRESSIDE PL 14.769 14.719 14.744 15.079 15.124 15.124 AL PRESSIDE PL 15.124 AL PRESSIDE	7,9964  RATINS , FCP  PL/PN 0,97911 2,97580 0,97745 0,99369 1,99732 0,9946 1,0076  PL/PN  PL/PN  PL/PN	9.75169 PERCOV INLET PL/PTF 0.24643 0.24555 0.24561 0.25101 0.25101 0.25101 0.25103 0.2233 PERCOV INLET PL/PTF DEG SHPCUD I	0.42719 0.42818 0.41939 0.41797 0.41868 0.42719 0.42818 0.42818 0.42818 0.42848 0.42848 0.42848	-1.0000 -1.0000 x/omax 0.29800 0.43100 0.44800 0.52200 0.52200 0.52200 1.0000 -1.0000 -1.0000 -1.0000					-
37 ADDITION D MORD 07 12 27 37 42 D MOPD 52 57 ADDITION D MOPD 67	75.044 15.779 AL PRESSIPE PL 14.769 14.719 14.744 14.989 15.344 15.174 15.174 PL 15.174 AL PRESSIPE PL 15.124	9,9964  RATINS , FCP  PL/PC 0,97911 2,97580 0,97745 0,99369 7,99732 0,99464 1,9976 1,0076  PL/PC 1,0026  PATIOS , 20  PL/PC 1,0026	9.75169 PRODU INLET PL/PTF 0.24643 0.24559 0.24501 0.25101 0.25101 0.25101 0.25101 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723	0.42719 0.42818 0.41939 0.41797 0.41868 0.42719 0.42718 0.42718 0.42946 0.42946 0.42946 0.42946	-1.0000 -1.0000 X/DMAX 0.29800 0.43100 0.44800 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000					
37 ADDITION D MORD 07 12 27 37 42 D MOPD 52 57 ADDITION D MOPD 67	15.044 15.079 AL PRESSIDE PL 14.769 14.719 14.744 15.079 15.124 15.124 AL PRESSIDE PL 15.124 AL PRESSIDE	7,9964  RATINS , FCP  PL/PN 0,97911 2,97580 0,97745 0,99369 1,99732 0,9946 1,0076  PL/PN  PL/PN  PL/PN	9.75169 PERCOV INLET PL/PTF 0.24643 0.24555 0.24561 0.25101 0.25101 0.25101 0.25103 0.2233 PERCOV INLET PL/PTF DEG SHPCUD I	0.42719 0.42818 0.41939 0.41797 0.41868 0.42719 0.42818 0.42818 0.42818 0.42848 0.42848 0.42848	-1.0000 -1.0000 x/omax 0.29800 0.43100 0.44800 0.52200 0.52200 0.52200 1.0000 -1.0000 -1.0000 -1.0000					
ADDIT IDNI D MORD 07 12 27 37 42 27 37 42 42 42 42 42 42 43 44 47 47 47 47 47 47 47 47 47 47 47 47	PL 15.124 15.124 15.124 15.124 15.124 15.124	0,99964  PL/PN 0,97911 0,97780 0,97745 0,99369 1,99732 0,9946 1,0076  PL/PN 1,0026 PATINS , 20 PL/PN 1,0026 1,0026	9.75169 PRODU INLET PL/PTF 0.24643 0.24559 0.24501 0.25101 0.25101 0.25101 0.25101 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723 0.2723	0.4271Q 0.4281R 0.4281R 0.4193Q 0.41797 0.4186R 0.4271Q 0.4281R 0.4281R 0.4284A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A	-1.0000 -1.0000 X/DMAX 0.29800 0.43100 0.44800 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000					
O HORD 07 12 27 27 27 27 37 42 42 42 42 42 43 44 45 46 47 48 49 49 49 49 49 49 49 49 49 49	PL 15.124 15.124 15.124 15.124 15.124 15.124	0,99964  PL/PN 0,97911 0,97780 0,97745 0,99369 1,99732 0,9946 1,0076  PL/PN 1,0026 PATINS , 20 PL/PN 1,0026 1,0026	9.75169 PERCOV INLET PL/PTF 0.24643 0.24559 0.24561 0.25101 0.25101 0.25101 0.25103 0.27239 PERCOV INLET D.25235 DEG SHPOUD I PL/PTF 0.25247 DEG SHPOUD I	0.4271Q 0.4281R 0.4281R 0.4193Q 0.41797 0.4186R 0.4271Q 0.4281R 0.4281R 0.4284A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A	-1.0000 -1.0000 X/DMAX 0.29800 0.43100 0.44800 0.52200 0.58800 -1.0000 -1.0000 -1.0000 X/DMAX 0.79300					
37 ADDITION OF 12 27 37 42 37 42 42 42 43 44 44 44 44 44 44 44 44 44 44 44 44	PL 14.769 14.769 14.769 14.764 15.079 15.044 15.079 17.164 15.079 17.164 15.174 15.174 15.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174 17.174	0,99964  RATINS , FCP  PL/PN 0,97791 0,97745 0,99369 1,99732 0,9946 1,9976 1,0076 PATINS , PATINS , 20  PL/PN 1,0026 PATINS , 20  PL/PN 1,0026 PATINS , 80	9.75169 PERCOV INLET PL/PTF 0.24643 0.24559 0.24601 0.25010 0.25160 0.25160 0.25235 WCZIF FTRP 0.25235 DEG SHPCUD I PL/PTE 0.25245 0.25245 DEG SHPCUD I PL/PTE	0.42710 0.42818 0.42818 0.41939 0.41797 0.41868 0.42710 0.42818 0.42710 0.42818 0.42946 0.42946 0.42946 0.42946 0.42946 0.42946 0.42946 0.42946	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					-
37 ADOLT IDNI ID WORD 07 12 27 37 42	PL 14.769 14.769 14.769 14.769 15.174 15.174 15.174 15.174 15.174 15.174 15.174 15.174 15.174 15.174 15.174 15.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174 16.174	9,9964  RATINS , FCP  PL/PN 0,97911 9,97580 0,97745 0,99369 1,99732 0,9946 1,9076  PL/PN 1,0026 PATINS , 20  PL/PN 1,0026 PATINS , 80  PL/PN 1,9029 PATINS , 80	9.75169 PERCOV INLET PL/PTF 0.24643 0.24559 0.24601 0.25101 0.25101 0.25101 0.25103 0.27235 PERCOV INLET PL/PTF 0.25235 DEG SHPOUD I PL/PTF 0.25247 DEG SHPOUD I PL/PTF 0.25247	0.4271Q 0.4281R 0.4281R 0.4193Q 0.41797 0.4186R 0.4271Q 0.4281R 0.4281R 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A 0.4294A	-1.0000 -1.0000 -1.0000 -1.43100 -0.44900 -0.52200 -0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000					
37 ADDIT INN OF MORD OF 12 27 37 47 D MORD 52 EN OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR OF FOR 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32	9.6894	0.64319	0.16204	0.27667	0.72200				
37	17.132	1.1575	0.28486	0.49450	0.02000				
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57	16.738	1.1243	0. 28726	0.48364	1.0170				
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62	23.509	1.5905	0.39819	9.67985	0.42200				
47	19-240	1.2798	0. 32243	0.55051	0.67000				
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107	14.749	97646	0.74451-	0.42089	-1.0000				
112	15-695	0.97301	2025559	0.41932	-1.0000				
177	14.722	2-02915	7726614	0.47032	-1.0000				
127	14.972	0.99371	0. 25035	0.42745	-1.0000				
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VD WORD 112 127 127 127 142 17 142 17 157 157 167 167 167	PL 16.749 14.495 14.729 14.979 15.315 15.355 17.109 13.109 PL 15.130 15.130 15.135	PL/PO 0.97846 0.97491 2.97714 2.99371 0.99673 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.992	91/PTF 7.24651 0.24659 0.24618 0.25035 0.25117 0.25177 7.2727 0.25261 MP2/15 CLAP 0.75261 DEG SHPCUD 1	0.47089 0.41932 0.42932 0.42745 0.42773 0.42987 0.43130 PL/PTP 0.43116 0.49130	0.39890 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000		•		
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VD WORD 107 112 127 127 127 127 142 17 VD WORD 152 157 ADDITIONAL	PL 16.749 14.495 14.729 14.979 15.315 15.355 17.109 13.109 PL 15.130 15.130 15.135	PL/PO 0.97846 0.97491 2.97714 2.99371 0.99673 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.992	91/PTF 7.24651 0.24659 0.24618 0.25035 0.25117 0.25177 7.2727 0.25261 MP2/15 CLAP 0.75261 DEG SHPCUD 1	0.47089 0.41932 0.42932 0.42745 0.42773 0.42987 0.43130 PL/PTP 0.43116 0.49130	0.39890 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000				
VN WORD 197 112 127 127 127 142 17 142 17 157 201110000 157 177 177	PL 14.749 14.495 14.729 14.979 15.315 15.355 17.109 17.109 PL 15.130 PL 15.135 PL 15.135 15.135	PL/PO 0.97846 9.97491 2.97714 3.99371 0.99935 1.9925 1.9925 1.9925 1.9925 1.9925 1.9927 PATIOS 2.20 PL/PC 1.9927	PL/PTF 7.24651 0.24559 0.24618 0.25035 0.25117 0.25177 9.2727 9.27261 NOTES SEPTION 1 PL/PTF 0.25261 0.25261 0.25261 0.25269	0.47089 0.41932 0.42932 0.42973 0.42977 0.43130 0.43130 0.43116 0.99130 0.43130 0.43130 0.43144	0.39890 0.43100 0.44900 0.52200 0.52200 0.58000 1.0000 1.0000 1.0000 1.0000				
VD WORD 107 112 127 127 127 127 142 142 142 142 143 144 147 147 147 147	PL 14.749 14.495 14.729 14.979 15.315 15.355 17.109 17.109 PL 15.130 PL 15.135 PL 15.135 15.135	PL/PO 0.97846 0.97846 0.97491 2.97714 2.99371 0.99673 1.9923 1.9923 1.9923 1.9923 1.9923 1.9923 1.9927 PATIOS 2.20 PL/PO 1.9923 1.9927	PL/PTF 7.24651 0.24559 0.24618 0.25035 0.25117 0.25177 9.2727 9.27261 NOTES SEPTION 1 PL/PTF 0.25261 0.25261 0.25261 0.25269	0.47089 0.41932 0.42932 0.42973 0.42977 0.43130 0.43130 0.43116 0.99130 0.43130 0.43130 0.43144	0.39890 0.43100 0.44900 0.52200 0.52200 0.58000 1.0000 1.0000 1.0000 1.0000				
VID WORD 197 112 127 127 127 142 127 142 157 24011 1004	PL 14.749 14.495 14.729 14.979 15.315 15.355 17.109 17.109 15.120 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125	PL/PO 0.97846 0.97846 0.97591 0.97714 0.99371 0.99935 1.9927 1.9927 1.9927 1.9927 1.9927 1.9927 1.9923 1.9927 1.9923 1.9927 1.9923 1.9927 PATIOS 20 PLOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30	PL/PTF 7.24651 0.24559 0.24618 0.25035 0.25117 7.2767 7.7767 7.7767 7.7767 0.7761 PL/PTF 0.75761 0.25761 0.25769 DEG SHPOID 1	0.47089 0.41932 0.42932 0.42973 0.42977 0.42987 0.43130  PL/PTP 0.43116 0.#9130  PL/PTP 0.43130  PL/PTP 0.43130  PL/PTP 0.43144	0.39890 0.43100 0.44900 9.52200 9.52200 9.52200 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
VN WORD 107 112 177 127 127 127 142 177 142 177 VN WORD 147 147	PL 14.749 14.495 14.729 14.979 15.315 15.355 17.109 15.100 15.105 15.100 PRESSUPE PL 15.175 15.110 PRESSUPE PL 14.925	PL/PO 0.97846 0.97846 0.97846 0.97846 0.97841 1.99371 0.99673 1.9927 1.9927 1.9927 1.9927 1.9927 1.9927 1.9927 1.9927 1.9927 1.9927	PL/PTF 7.24651 0.24559 0.24618 0.25035 0.25117 7.2727 9.27261 NOTES SHOULD 1 PL/PTF 0.25261 0.25261 0.25261 0.25261 0.25269 0.55269 0.55269	0.47089 0.41932 0.42932 0.42973 0.42977 0.42987 0.43130  PL/PTP 0.43116 0.43116 0.43130  PL/PTP 0.43130  PL/PTP 0.43130  PL/PTP 0.43144	0.39890 0.43100 0.44900 9.48600 0.52200 0.58600 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
VO WORD 112 127 127 127 142 17 142 17 152 157 167 177 177 177 177 177 177 177 177	PL 16.749 14.485 14.729 14.979 15.315 15.355 17.109 15.109 15.100 15.105 1 PRESSUPE PL 15.106 15.106 1 PRESSUPE PL 15.106 1 PRESSUPE PL 14.925 14.545	PL/PO 0.97846 0.97846 0.97591 0.97714 0.99371 0.99935 1.9927 1.9927 1.9927 1.9927 1.9927 1.9927 1.9923 1.9927 1.9923 1.9927 1.9923 1.9927 PATIOS 20 PLOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30 PATIOS 30	PL/PTF 7.24651 0.24559 0.24618 0.25035 0.25117 0.25177 7.2727 0.25261 PL/PTF 0.25261 PL/PTF 0.25261 0.25261 0.25269 DEG SHPOUN 1 PL/PTF 0.25261 0.25269 DEG SHPOUN 1	0.47089 0.41932 0.42932 0.42973 0.42977 0.42987 0.43130  PL/PTP 0.43116 0.#9130  PL/PTP 0.43130  PL/PTP 0.43130  PL/PTP 0.43144	0.39890 0.43100 0.44900 9.52200 9.52200 9.52200 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				

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	NASA-E FUT	s escilm	INAPY DATA	06/13/79	CARRETT	RFC 10/25/79	9 00:46:01.975	FAC RYSKI	PG# F034 #PG 147	UN24
	>4nnit inni	LI PRESSIME	PATIOS , PPI	MARY PLUG						
۸	AL HUBD	PL	PI / PI	PL / PTF	nt /PTP	X/DMAX				
	32	9.4476	0.62192	0.17233	0.29495	9.72200				
	37	14.479	1.0#56	0.70092	0.51486	0. 82000				
	47	13.500	0.48937	0.24644	0.42179	0.91900				
	52	16.954	1.1103	0. 30 766	0.52657	1.0170				
	>ADD I T IONA	AL PRESSIME	RATIOS . FLO	W SPITTER T	.n.					
A	אח אחתה	PL	PL/PD	PL/PTF	PL /PTP	X/DMAX				
	62	22.146	1.4589	0.40427	0.69191	0.42200				
	67	19.667	1.2295	0.34069	0.58309	0-67000			-	
	>APP   T   PN	AL PRESSURE	RATIOS , FLO	W SPLITTER O	ı.n.					
A	VO WORD	Pl	PI /PI	PL/PTF	PL /PTP	Y/DMAX				
	77	12.521	0.82482	0.22856	0.39118	0.50800				
	P.2	19.939	1. 31 15	0.36340	0.62196	0.58300		•	ir.	
	92	15,200	1.0713	9-27747	0.47488	0.67990				<del></del>
-	>400LT   PW	NE PRESSUPE	- <del>RATIOS 1_FS</del>	etar syraua						
Δ	VP WOPD	PL	PI,/PI	PL/PTF	PLANTE	X/DMAX				
	197	14.795	9.97465	0.27000	0.46223	-1.0000		-		•
		14 775	0.97070	74.000						
	112	14.735	2-07169	0.26898	0.46036	-1.0000				
	127	14.750			0.46083	-1.0000				
-	127	15.028	D. 98980	0.27427	0.46942	-1.0000				
-	127	15-075	0.99309	0.2751R	0.47051 0,47098	-1.0000 -1.0000				
	>AUULT LUM	15.075	0.99309	0.2751A FRODY INLET	0,47098	-1-0000				
	SAPOTT FINAL ORDER OV	15.075 AL PRESSUPE PL	0.99309 RATIOS . FOR	0.2751A ERNOV INLET PL/PTF	0,4709R	N/DMAN				
	) >ADDIT   INNA VP WORD 107	L5+075 L PRESSUPE PL 14-795	0.99309 RATIOS . FOR PL/PD 0.97465	0.2751A ERNOV INLET PI/PTF 0.2700A	PL/PTP 0.46223	X/DMAX 0.39800		•		
	>ADDIT   DNA >ADDIT   DNA VD WORD 107 112	15.075 AL PRESSUPE PL 14.795 14.735	0.99309 RATIOS . FOR PL /PD 0.97465 0.97070	0.2751A FRODY INLET PL/PTF 0.2700A 0.26898	PL/PTP 0,46223 0,46036	X/DMAX 0.39900 0.43100		• •		
	>ADDIT   DAI VD WORD 107 112 127	15.075 AL PRESSUPE PL 14.795 14.735 14.750	0.99309  RATIOS . FOR  PI /PO 0.97465 0.97070 0.97169	0.2751A FRODY INLET PI /PTF 0.2700A 0.2689A 0.26925	PL/PTP 0.46223 0.46036 0.46083	X/NMAX 0.3 9000 0.43100 0.44900		•		
A	>ADDIT (DN) VD WORD 107 112 122 127	15.075 AL PRESSUPE PL 14.795 14.795 14.750 15.025	0.99309 RATIOS , FOR PI /PD 0.97465 0.97070 0.97169 0.98980	0.2751A FRODY INLET PI / PTF 0.2700R 0.26925 0.26925 0.27627	PL/PTP 0-4623 0-46083 0-46083 0-46942	X/DMAX 0.3 9900 0.43100 0.4900 0.49600		• -		
В	>ADDIT IONA VO MORD 107 112 127 127 137	PL 14-795 14-795 14-735 14-750 15-925 15-060	0.99309  RATIOS , FOR  PI /PD 0.97465 0.97070 0.97164 2.99980 0.99210	0.2751A FRODY INLET PL/PTF 0.2700A 0.2669A 0.26925 0.27427 0.27427	PL/PTP 0.46223 0.46036 0.46042 0.47051	X/DMAX 0.39900 0.43100 0.44900 0.48600 0.52200		•		
B	>ADDIT (DN) VD WORD 107 112 122 127 137 142	PL 14. 795 14. 795 14. 795 14. 750 15.025 15.060 15.075	0.99309 RATIOS : FOR PI /PD 0.97465 0.97070 0.97169 2.98380 0.99210 0.99309	0.2751A FRODY INLET PL/PTF 0.2700A 0.2699B 0.76925 0.27427 0.27421 0.2751A	PL/PTP 0.46223 0.46036 0.46083 0.46083 0.46083 0.47051 0.47098	X/DMAX 0.3900 0.43100 0.44900 0.52207 0.58000		• •		
	>ADDIT IONA VO MORD 107 112 127 127 137	PL 14-795 14-795 14-795 14-795 15-925 15-960 15-975 19-299	0.99309  RATIOS , FOR  PI /PO 0.97465 0.97070 0.97169 0.99210 0.99210 0.99209	0.2751A FRODY INLEY PI / PYF 0.2700R 0.26898 0.26925 0.27427 0.27427 0.27427	PL/PTP 0.46223 0.46036 0.46083 0.46942 0.47051 0.47098	X/DMAX 0.39900 0.43100 0.44900 0.52207 0.58800		• •		-
	>ADDIT ION/ VO WORD 107 112 127 127 137 142	PL 14-795 14-795 14-795 14-795 15-925 15-925 15-975 17-299	0.99309  RATIOS , FOR PI / PD 0.97465 0.97070 0.97169 0.99210 0.99209 1.0713	0.27518 FRODY INLET PL/PTF 0.27008 0.2698 0.2698 0.27427 0.27427 0.27491 0.27518 0.27757	PL/PTP 0.46223 0.46036 0.46083 0.46083 0.46083 0.47051 0.47098	X/DMAX 0.3900 0.43100 0.44900 0.52207 0.58000		• · · · · · · · · · · · · · · · · · · ·		
8	>ADDIT   DN/ VN WORD 107 112 127 127 137 142 142	PL 14-795 14-795 14-795 15-925 15-060 15-975 19-209	0.99309  RATIOS , FOR  PI /PO 0.97465 9.97070 9.97169 9.9890 0.99210 0.99309 1.0713	0.2751A FRODY INLEY PI / PYF 0.2700R 0.26898 0.26925 0.27427 0.27427 0.2751A	0,4709F PL/PTP 0,4623 0,4603 0,46083 0,46942 0,47051 0,4709B 0,4748F	X/DMAX 0.39000 0.43100 0.44900 0.52200 0.52200 -1.0000		• · · · · · · · · · · · · · · · · · · ·		
	>ADDIT ION/ VO WORD 107 112 127 127 137 142 1 7	PL 14.795 14.795 14.795 14.795 14.795 15.025 15.060 15.075 19.299 17.200	0.99309  RATIOS , FOR P /PD 0.97465 0.97707 0.97169 0.99210 0.99210 0.99209 1.0713	0.2751A FRODY INLEY PI / PYF 0.2700B 0.2689B 0.26925 0.27427 0.27491 0.2751A TI-27747	PL/PTP 0.4623 0.46036 0.46083 0.46942 0.47051 0.47081 0.47088	X/DMAX 0,39900 0,43100 0,4900 0,52200 0,52200 0,52000 -1,0000		• · · · · · · · · · · · · · · · · · · ·		-
A	>ADDIT IONA  VO WORD  107  112  127  137  142  1  >MODIT IONA  VO WORD  152	PL 14.795 14.795 14.795 15.925 15.060 15.075 19.200 17.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200	0.99309  RATIOS , FOR  PI /PI	0.27518 FRODY INLET PI/PYF 0.27008 0.26898 0.26925 0.27427 0.27491 0.27491 U.Z7747 U.Z7747	0,47098 PL/PTP 0,46223 0,46036 0,46083 0,46942 0,47051 0,4708 0,47488	X/DMAX 0.39900 0.43100 0.4900 0.52200 0.58900 -1.0000 X/DMAX -1.0000		• · · · · · · · · · · · · · · · · · · ·		-
A	>ADDIT   DN/ VN WORD 107 112 127 127 137 142 142 142 142 142 144 145 145 147 147 147 147 147 147 147 147 147 147	PL 14.795 14.795 14.795 15.925 15.060 15.975 19.209	0.99309  RATIOS , FOR  P(/PO 0.97465 0.97070 0.97169 2.98980 0.99210 0.99205 1.0713  PATIOS , FAN  P(/PO 1.7713 1.0013	0.27518 FRODY INLEY PI / PYF 0.27008 0.26098 0.26925 0.27427 0.27491 0.27518 0.27747 0.27747 0.27747	PL/PTP 0.46223 0.46036 0.46083 0.46942 0.47051 0.47088 0.47488	X/DMAX 0,39900 0,43100 0,4900 0,52200 0,52200 0,52000 -1,0000		• · · · · · · · · · · · · · · · · · · ·		
A	>ADDIT   DAY  VI WORD  107  112  127  137  142  142  142  142  144  VI WORD  152  >ADDIT   DAY	PL 14.795 14.795 14.795 14.795 14.750 15.925 15.060 15.375 19.299 17.203 RC PRESSUPE	0.99309  RATIOS , FOR  PI /PH	0.2751A  FRODY INLEY  PI / PYF 0.2700R 0.26925 0.27627 0.2751A 0.2751A 0.2751A 0.2751A 0.27747 U-27747 0.27747	0,47098  PL/PTP 0,46223 0,46036 0,46083 0,46942 0,47098 0,47098 0,47488 0,47488 0,47488	**************************************		• · · · · · · · · · · · · · · · · · · ·		
A	>ADDIT ION/ VN HORD 107 112 122 127 137 142 142 142 142 142 144 VN HORD 152 152 >ADDIT ION/ VN HORD	PL 14-795 14-795 14-795 14-795 14-795 15-925 15-060 15-975 17-209 11-209 11-209 11-209 11-209 11-209	0.99309  RATIOS , FOR PI /PO O. 97465 0.97070 0.97169 0.99210 0.99210 1.0713 1.0713 PATTOS , FAN PI /PO T.7713 1.0013 RATIOS , 20 PI /PO	0.27518  FRODY INLEY  PI / PYF 0.27008 0.26925 0.27427 0.27427 0.27427 0.27747 0.27747 0.27747 0.27747 0.27747	PL/PTP 0.4623 0.46036 0.46033 0.46942 0.47051 0.47098 0.97996 0.47488 PL/PTP 0.47488 PL/PTP	X/DMAX 0.3900 0.49100 0.4900 0.48600 0.52200 0.58800 -1.0000 X/DMAX -1.0000 X/DMAX		• · · · · · · · · · · · · · · · · · · ·		
A	>ADDIT ION/ VO WORD 107 112 127 137 142 142 142 142 142 142 142 142 142 142	PL 14.795 14.795 14.795 14.795 15.925 15.060 15.975 19.209 IL PRESSUPE PL 15.205 IL PRESSUPE PL 15.205	0.99309  RATIOS , FOR  P  /PO 0.97465 0.97070 0.97169 2.98980 0.99210 0.99209 1.0713 1.0713  PATIOS , FAN  P  /PO 1.7011  RATIOS , 20  PL /PO 1.7017	0.27518 FRODY INLEY PI / PYF 0.27008 0.26025 0.27427 0.27427 0.27427 0.27747 10.27747 10.27747 0.27747 DFG SHROUD L PI / PYF 0.27756	PL/PTP 0.4623 0.46083 0.46083 0.46942 0.47051 0.47098 0.47488 0.47488 0.47488 0.47488 0.47488 0.47488	X/DMAX 0.3900 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 X/DMAX -1.0000				
A	>ADDIT ION/ VN HORD 107 112 122 127 137 142 142 142 142 142 144 VN HORD 152 152 >ADDIT ION/ VN HORD	PL 14-795 14-795 14-795 14-795 14-795 15-925 15-060 15-975 17-209 11-209 11-209 11-209 11-209 11-209	0.99309  RATIOS , FOR PI /PO O. 97465 0.97070 0.97169 0.99210 0.99210 1.0713 1.0713 PATTOS , FAN PI /PO T.7713 1.0013 RATIOS , 20 PI /PO	0.27518  FRODY INLEY  PI / PYF 0.27008 0.26925 0.27427 0.27427 0.27427 0.27747 0.27747 0.27747 0.27747 0.27747	PL/PTP 0.4623 0.46036 0.46033 0.46942 0.47051 0.47098 0.97996 0.47488 PL/PTP 0.47488 PL/PTP	X/DMAX 0.3900 0.49100 0.4900 0.48600 0.52200 0.58800 -1.0000 X/DMAX -1.0000 X/DMAX		• · · · · · · · · · · · · · · · · · · ·		
A	>ADDIT   INN/ VN WORD 107 112 122 127 137 142 142 144  >>ADDIT   INN/ VN WORD 157 >>ADDIT   INN/ VN WORD 167 172	PL 14.795 14.795 14.795 14.795 15.925 15.060 15.075 19.299 17.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.200 15.205	0.99309  RATIOS , FOR  P  /PO 0.97465 0.97070 0.97169 2.98980 0.99210 0.99209 1.0713 1.0713  PATIOS , FAN  P  /PO 1.7011  RATIOS , 20  PL /PO 1.7017	0.2751A  FRODY INLEY  PI / PYF	PL/PTP 0.46223 0.46036 0.46036 0.46036 0.46036 0.47038 0.47047038 0.47488 0.47488 0.47288 PL/PTP 0.47504 0.47504	X/DMAX 0.3900 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 X/DMAX -1.0000				
A	>ADDIT   DAM  VN WORD  107  112  127  137  142  142  142  144  VN WORD  157  >ADDIT   DAM  VN WORD  167  177  >ADDIT   DAM  VN WORD  167  172  >ADDIT   DAM  VN WORD	PL 14.795 14.795 14.795 14.795 14.750 15.925 15.060 15.375 19.293 17.203 18.200 15.200 15.200 15.200 15.200 15.200 15.200 15.205 15.205	0.99309  RATIOS , FOR PI / PO O. 97465 0.97070 0.97169 2.9990 0.99210 0.99210 0.99213 1.0713 PATIOS , FAN PI / PO 1.9017 1.0017 PATIOS , 80 PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI	0.27518  FRODY INLEY  PI / PYF 0.27008 0.26898 0.26925 0.27427 0.27491 0.27518 0.27767  WYYLE FLAN  DEG SHROUD L  PI / PYF 0.27756 0.27756  DEG SHROUD L  PI / PYF	PL/PTP 0.46223 0.46036 0.46036 0.46036 0.46036 0.47038 0.47047038 0.47488 0.47488 0.47288 PL/PTP 0.47504 0.47504	X/DMAX 0.3900 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 X/DMAX -1.0000				
A	>ADDIT IONA  VO WORD  107  112  127  137  142  142  142  240  152  >ADDIT IONA  VO WORD  167  172  >ADDIT IONA  >ADDIT IONA  >ADDIT IONA	PL 14.795 14.795 14.795 14.795 15.925 15.060 15.975 19.209 11 PRESSUPE PL 15.200 15.205 15.205 15.205 15.205 15.205 15.205 15.205 15.205 15.205 15.205 15.205	0.99309  RATIOS , FOR  P / PO 0.97465 0.97070 0.97169 2.98980 0.99210 0.99209 1.0713 1.0713 PATIOS , PATIOS , 20  PATIOS , 80	0.27518 FRODY INLEY PI / PYF 0.27008 0.26025 0.27427 0.27427 0.27427 0.27747 10.27747 10.27747 0.27747 DFG SHROUD L PI / PYF 0.27756 0.27756	PL/PTP 0.4623 0.46083 0.46083 0.46942 0.47098 0.47488 0.47488 PL/PTP 0.47488 PCATION PL/PTP 0.47504 0.47504	X/DMAX 0.3900 0.43100 0.44900 0.52200 0.52200 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000 X/DMAX 0.79300 0.84400				
A	>ADDIT   DAM  VN WORD  107  112  127  137  142  142  142  144  VN WORD  157  >ADDIT   DAM  VN WORD  167  177  >ADDIT   DAM  VN WORD  167  172  >ADDIT   DAM  VN WORD	PL 14.795 14.795 14.795 14.795 14.750 15.925 15.060 15.375 19.293 17.203 18.200 15.200 15.200 15.200 15.200 15.200 15.200 15.205 15.205	0.99309  RATIOS , FOR PI / PO O. 97465 0.97070 0.97169 2.9990 0.99210 0.99210 0.99213 1.0713 PATIOS , FAN PI / PO 1.9017 1.0017 PATIOS , 80 PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI / PO PI	0.27518  FRODY INLEY  PI / PYF 0.27008 0.26898 0.26925 0.27427 0.27491 0.27518 0.27767  WYYLE FLAN  DEG SHROUD L  PI / PYF 0.27756 0.27756  DEG SHROUD L  PI / PYF	PL/PTP 0.46273 0.46083 0.46083 0.46982 0.47098 0.47098 0.47488 0.47488 0.47488 0.47488 0.47504 0.47504 0.47504	*/DMAX 0.3 9700 0.4 3100 0.4 9700 0.4 9700 0.4 9700 0.5 2200 0.5 8700 -1.0000 -1.0000 **/DMAX 0.79300 0.84400 **/DMAX				
A	>ADDIT ION/ VN WORD 107 112 127 127 137 142 142 142 142 142 142 142 142 147 240 240 240 240 240 240 240 240 240 240	PL 14.795 14.795 14.795 14.795 14.795 14.795 15.925 15.060 15.975 19.209  RESSUPE PL 15.200 LS.200 AL PRESSUPE PL 15.205 15.275 AL PRESSURE PL 14.945 14.945	0.99309  RATIOS , FOR PI / PO O. 97465	0.27518  FRODY INLEY  PI / PYF 0.27008 0.26098 0.26098 0.27427 0.27427 0.27427 0.27747 0.27747 0.27747 0.27747 DEG SHROUD L  PI / PYF 0.27756 0.27756 0.27756 0.27756	PL/PTP 0.46223 0.46036 0.46036 0.46036 0.46042 0.47051 0.47048 0.47048 0.47488 0.47488 0.47288 PL/PTP 0.47504 0.47504 0.47504 0.47504 0.47504 0.46692	X/DMAX 0.3900 0.49100 0.4900 0.48600 0.52200 0.58800 -1.0000 X/DMAX -1.0000 X/DMAX 0.79300 0.84400				

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4454-1 FW1	IS PRELIMI	HAPY DATA	06/13/79	CADDFII	REC 10/25/1	79 00:47:42.025	FAC AVET	PG4 1934	RUN24
PATOLICIA	MAL PRESSUPE	PATINS . PPI	MAPY PLUG						
AVD HOPD	Pt.	PI /PO	PL /PTF	PL /PTP	x/DMAY	-			
32	B.1792	0.54123	0-17318	0-29630	0.72200				
17	13.797	0. 91 295	0.29711	0.49980	0.42000				
47	11.763	. 0.77838 .	0.24905	0.42613	0.91900				
52	16.664	1.1027	0.35283	0.60369	1.0170				
>ADDITIONA	VAL PRESSUPF	PATTOS . FLO	W SPI ITTER I	.n.	·			restation to the second constraint of the second second	Militaria (Militaria delle I edilli in delle) (secondeplemberari pepara se gappa geogra
AVD WOPD	P1	PL / PO	PI /PTF	PL /PTP	X/DMAY				
£2	18.717.	1.2518.	0.40053	0.68529	0.42200				
67	15.700	1.0389	0.33241	0.56875	0.67000				
>ADDIT ION	WAL PRESSURE	RATINS , FLO	W SPLITTER O	. D.					
AVD HUDD	PE	PL /PO	PI /PTF	PL/PTP	X/DMAX	•			
77	11-258	0.74498	0.23837	0.42784	0.50800				
<b>#</b> 2	15.840	1.0482	0.33538	0.57387	0.59300				
92	15-141	1,0019	0-32057	0.54848	0-67000				·
TOTAL TION	HL 19833978	**************************************	CTC- SHFTON						
AVD YORD		PL/PQ	PL/PTF	PLANTS	X/DMAX				
-107	14.741	0.97544	0.31211	0.53491	-1.0000	- <del> </del>	•	-	
-112	15-691	0.97947	- Vo 31084	0.53183	-1.0000				
-122	14-691	2-97213	31105	0.53220	-1.0000				
-127	14.054	0.98965	0.3166	0.54179	-1.0000				
-1?7	15.996	0. 99164	0. 71 729	174287	-1.0000		₩ · *		
-iغ	15.716	0.99362	0.31792	0.54356	1.0000				
	AL PRESSIPE								
AVD WOPD	PL	PL/P2	PL/PTF	PL/PTP	x/max			-	
107	14.741	0. 97544	0-31511	n.53401	0.39800		•		*
112	14.691	2.97147	7.21086	2.53183	0.43100				
17?	14.691	0.97213	0.31105	0.53270	0.44900	* <del>* *</del>			
127	14.956	0.99965	0.31665	0.54179	0.48600				
137	14.996	0.99164	7.31729	0.54287	0.52200				
142	15-016	9. 99362	0.31792	0.54396	0.58800				
	17.178	1.0009	00 00	- 0 0 0 0 0 0 0 0.	-1.0000	•	*		
-147	19-121	1.0700	0. 2014	0.74770		ă.			
	ML PRESSURF	PATENS - PAI	-407730 F189						
Market 1988 Annual Control		P[7911	11/11/	PL /PTP	Y/DMAY				
			0, 2707	-0.54794	-1.0000				
DEUM GAN	PL 15-126								
AVP WORD	15-126	1.0006	0.32014	0.54776	1-0000	-	= 4		
AVP WORD -157	15.126	1.0006	0.32014	0.54776		-	-		
AVD WORD -152 -157 ->ADDITION	15-126 19-121 WAL PRESSIME	1.0736 RATENS . 20	0.32014 DEG SHPNIN (	0.54776 NCATION	1-0000	-			
AVD WORD -1 = 2 -1 = 7 > ADD   T   ION AVD WORD	15.126 17.121 MI PRESSIME	1.0706 RATERS , 20 PL/PR	0.32014 DEG SHPPIID ( PL/PTF	0.54776 CATION PL/PTP	X/D#AX				
AVD WORD -1=2 -157 >ADDITION AVC WORD 167	15.126 19.121 MI PRESSIME PL 15.116	1.0006 RATIOS . 20 PL/PO 1.0007	0.32014 DEG SHPOIN ( P(/PTF 0.32004	0.54776 CATION  PL /PTP  0.54758	x/DMAX 0.79300		- ·		
AVP WORD -157 -157 ->ADDITION AVC WORD 167 172	15-126 17-121 WAL PRESSIME PL 15-116 15-116	1.0006 RATENS . 20 PL/PN 1.0007 1.0002	0. 32014 DEG SHROUN ( PL/PTF 0. 32004 0. 32004	0.54776 OCATION PL /PTP 0.54758 0.54758	X/D#AX		- ·		
AVP WORD -1-2 -1-57 >ADDIT ION AVC WORD 167 172 >ADDIT ION	PL 15-116 15-116 MAI PRESSURE	1.0006 RATIOS . 20 PL/PO 1.0007 1.0002 RATIOS . 40	0. 32014 DEG SHEDIM ( PL/PTE 0. 32004 0. 32004 DEG SHEDUD (	0.54776 CATION PL /PTP 0.54758 0.54758 CCATION	X/DMAX 0.79300 0.84400				
AVD WORD -157 -157 ->ADDITION 167 172 ->ADDITION AVD WORD	15-126 17-121  MAI PRESSIME PL 15-116 15-116 MAI PRESSIME PL	1.9996 RATTINS . 20 PL/PR 1.0007 1.9902 RATTINS . 40 PL/PR	0. 32014 DEG SHPOIN ( PL/PTE 0. 32004 0. 32004 DEG SHPOUD (	0.54776 CATION PL /PTP 0.54758 0.54758 CCATION PL /PTP	X/DMAX 0.79300 0.84400				
AVD WORD -1-2 -1-57 >ADDIT ION AVD WORD 167 172 >ADDIT ION AVD WORD 1P2	15-126 17-121 WAL PRESSIME PL 15-116 15-116 MAI PRESSIME PL 14-751	1.9996 RATINS . 20 PL/PN 1.0007 1.9902 RATINS . 40 PL/PN 0.97610	0.32014 DEG SHPPHP ( PL/PTF 0.32004 0.32004 DEG SHPPHD ( PL/PTF 0.31232	0.54776  CEATION  PL /PTP	X/DMAX 0.79300 0.84400 X/DMAX 0.79300				
AVD WORD -1=2 -1=7 >*DOIT ION AVD WORD 167 172 >ADOIT ION AVD WORD 1P2 1P7	15-126 17-121  MAI PRESSIME PL 15-116 15-116 MAI PRESSIME PL	1.9796 RATINS . 20 PL/PU 1.0007 1.2002 RATINS . 40 PL/PU 0.97610 0.94701	0.32014 DEG SHPPHIN L PL/PTF 0.32004 DEG SHPPHIN L PL/PTF 0.31232 0.20301	0.54776 CATION PL /PTP 0.54758 0.54758 CCATION PL /PTP	X/DMAX 0.79300 0.84400		-		

	IS PRELIM	INAPY DATA	06/13/79	CADDELL	REC 10/25/7	79 00:48:38.89)	FAC RX6X1	RUN24 PGM C034 RDG 1479
>400171004	IAL PRESSIDE	PATIOS . PRI	MARY PLIIS					
AU MUBU	PI	PL /P3	PL /PTF	PL /PTP	X/DMAX			
12	7.0720	0.46855	0-16964	0.28880	0.72200			
37	12.748	0.79820	0.28839	0.49199	0.82000			
47	15.447	1.0234	0.37052	0.63079	9. 91 900			
52	16.356	1.0936	0.39234	0.66793	1.9170			
>ADDIT IDA	IAL PRESSIPE	RATIOS , FLO	IN SPLITTER	I. D.				
VD WORD	PL	PL / ምባ	PL/PTF	PL /PTP	K/DMAX			
62	16.686	1.1055	0.40025	0.68140	0.42200			
£7	13.792	7.91378	0.33084	0.54323	0.67000			•
>ADDIT ION	AL PRESSIME	RATIOS , FLO	W SPLITTER I	n. n.				
VD WORD	PL	<b>ም</b> ር / ምኅ	PL/PTF	PL /PTP	X/DMAX	-		
77	9,7978	0.64847	0-23478	0.39970	0.50800			
02	18.460	1.2495	0.45239	0.77017	0.58300			
92	15-122	1,0019	0.36273	0.61757	0.67000			
V 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TC AMESSORE	RATSOS_3_F4E	CTOP SWEYING				•	
VP WORD	PL	PL /P()	PL/PTF	PL/239	X/DMAX			
197	14.712	7702471	0.35290	0.60078	-1.0000			
112	14.637	0.96974	0.24110	0.59772	-1.0000			
177	14.657	0.97102	0.35458	0.59854	-1.0000			
12,7	14.922	De 417.862	0.35793	0.60936	-1.0000			
177	14.962	0. 98904	0.35841	0.6101	-1-0000			
142	26.819	0.94564	0.35685	0.60752	-1-00000			
SATTITION	AL PRESSURE	PATINS , FOP	FRONY INLET					
AU AUBB	<b>O</b>	m 100	OH /OTE	01 (070	V 2000 V			
107	PL 14.712	PL/PO	PL/PTF 0.35290	PL /PTP 0-60078	X/DMAX 3.39400		* * *	
112	14.637	0. 96974	0.35110	0.59772	0.43100			
122	14.657	0.97107	0.35158				. <u>-</u>	
127	14.972	0. 78962	0-25793	0.59854 0.60936	0.44900			
137					0-48600			
142	14.942	0.98994 0.98564	0.35841 0.35685	0.61017	0.52200			
1-7		1.0019	. U. 30073	0.60752	0.58800			
163	15.172	1-0015		0.01772	-1.0000			
-	•	•	•		100000			-
2105 Li foi	AL BESSIME	PYTIOS - EVA	NOTTOF FLAG			***************************************		
AU MUND	PL	M-100	PETPTE	PI /PTP	X/DMAX_			
15?		1.0019	0.96273	0.61752	-1.0000			
157	15.127	1.0022	0.36285	0.61772	-1.0000			•
>vooltion	AL PRESSUPE	RATERS , 20	DEC SHAUD F	OCATION				
	PL	PL/PN	PL/PTF	PI /PTP	X/DMAX			
	15.12?	1.0319	0.76273	0.61752	0.79300			
167	16 117	1.0015	0.36261	0.6173?	0.84400			
167	15.117							
167 177		RATIOS , 80	DEG SHEPUD L	OCAT ION				
167 172 >400 [ T [0]		<del></del>	DEG SHROUD (		X/DMAX			
167 172 <u>&gt;400 T O</u> N VD WORD	PL	Pt /PO	PL/PTF	PI /PTP				
VD WORD 167 177 >40011100 VD WORD 182 187	AL PRESSIME	<del></del>			X/DMAX 0.79300 0.84400			

WASA-LEWIS	PREL[4]	INAPY DATA	06/13/79	CARDELL	REC 10/25/79	00:49:37.605	FAC AX6XI	PG4 C034	PC 1440
SADDIT IONAL	PRESSURF	RATIOS , PPI	MARY PLUG						
AVD MOPD	Pl.	PI /PO	PI /PTF	PI /PTP	X/DMAX			· • • • • • • • • • • • • • • • • • • •	<del>-</del> • · · · • • • · · · · • • • • • • • •
32	11.206	0.74187 .	0.29522	0.50183	0. 72200				
37	14.063	0.93080	0.37041	0.62963	0.82000				
47	15.443	1.0228	2.49703	0.69184	0-91900				
57	16.754	1.0631	0.42306	0.71914	1.0170				
SATTE TOTAL	PRESSURF	RATIOS . FLO	w SPLITTEP I	. n.					
AVD MOPP	PL	PL / PC	PL /PTF	PL/PTP	X/DMAX				
62	15.224	1.0079	0.40105	0-68177	0.42200				
57	12.446	0.02393	0.32788	0.55734	0.67009				
							······································		
>APPIT I PRAL	PRESSURE	RATIOS , FLO	W SPLITTER T	. D.					
AVD WOPD	PL	PL/PO	PL/PTF	PL /PTP	X/DMAX				
77		0. 57705	0.22963	0.39034	0.50800				
42	21.789	1.4425	0.57404	0.97577	0.58300				
92	15.144	1.0026	0.39897	0.67819	0.67000				<del></del>
>40017109AL	PAGEGURE	A41106 - 5JE	FTGR SIMOUS						
VO WORD	7	PL/PD	PL/PTF	PLOTE	X/DMAX				
-107	14.724	97480	0. 39 791	0.65939	-1.0000				
112	14-639	0.95714	29509	0.65559	-1.0000				
122	14.644	2-94-971	<b>33850</b> 1	0.65581	-1.0000				
127	14.919	0.99770	0.39709	0.66812	-1.0000				
137	14.919	0.98770	0.39305	0.06812	-1.0000				*
أخنستنفذ	.14.779	0. 97844	0.39936	0.66185	1.0000				
		EN .				<del>: •</del>			
\ADD   T 10444	SECTION	BATTOC COS	CBOOM IM CA						
		PATIOS . FOR							
VD WORD	PL	PL/PD	PL/PTF	PL/PTP	X/DMAX				
VD WORD	PL 14.724	PL/PD. 9.97480	PL/PTF 0.38791	0.65939	0.39800			-	
VD WORD 107 112	PL 14.724 14.639	PL/PD 0.97480 0.96918	PL/PTF 0.38791 0.38568	0.65939	0.39000 0.43100		. =	-	
VD WORD 107 112 122	PL 14.724 14.639	PL/PO 0.97480 0.96918 0.96951	PL/PTF 0.38791 0.38568 0.38581	0.65939 0.65559 0.65581	0.39800 0.43100 0.44900			-	
VD WORD 107 112 122 127	PL 14.724 14.639 14.644 14.919	PL/PD 0.97480 0.96918 0.96951 0.98770	PL/PTF 0.38791 0.38568 0.38581 0.39305	0.65939 0.65559 0.65581 0.66812	0.39800 0.43100 0.44900 0.48600			-	
VD WORD 107 112 122 127	PL 14.724 14.639 14.644 14.919	PL/PD 0.97480 0.96918 0.96951 0.98770	PL/PTF 0.38791 0.38568 0.38581 0.39305 0.39305	0.65939 0.65559 0.65581 0.66812 0.66812	0.39000 0.43100 0.44900 0.4600 0.52200				
VD WORD 107 112 122 127 137 142	PL 14.724 14.639 14.644 14.919 14.779	PL/PD 0-97480 0-96918 0-96951 0-98770 0-98770 0-97844	PL/PTF 0.38791 0.38581 0.78581 0.39305 0.79305 0.34936	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800				
VD WORD 107 112 122 127 137 142	PL 14.724 14.639 14.644 14.919 14.779	PL/PD D. 97480 O. 96918 O. 96951 O. 98770 D. 97770 O. 977844	PL/PTF 0.38791 0.38568 0.78581 0.39305 0.59305 0.36484	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185	0.39800 0.43100 0.44900 0.52200 0.52200 0.78900				
VD WORD 107 112 122 122 127 137 142 152	PL 14.724 14.639 14.644 14.919 14.779 15.130	PL/PD 9-97480 0-96918 0-96951 0-98770 9-9770 0-97844 1-0033	PL/PTF 0.38768 0.28581 0.28581 0.39305 0.30305 0.36484	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800				
VD WORD 107 112 122 122 127 137 142 152	PL 14.724 14.639 14.644 14.919 14.779 15.130	PL/PD D. 97480 O. 96918 O. 96951 O. 98770 D. 97770 O. 977844	PL/PTF 0.38768 0.28581 0.28581 0.39305 0.30305 0.36484	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185	0.39800 0.43100 0.44900 0.52200 0.52200 0.78900				
VD WORD 107 112 122 127 137 142 152 157 24001110MM	PL 14.724 14.639 14.644 14.919 14.779 14.779 15.130 17.139	PL/PD D. 97480 O. 96918 O. 96951 O. 98770 D. 97844 1.0032 1.0023	PL/PTF 0.38791 0.38568 0.28581 9.39305 0.39305 0.34936 0.36484	0.65939 0.65559 0.65581 0.66812 0.66812 0.66812 0.6185 0.43766	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 -1.0000				
VD WORD 107 112 122 122 127 137 142 152	PL 14.724 14.639 14.644 14.919 14.779 14.779 15.130 17.137	PL/PD 9-97480 0-96918 0-96719 0-98770 9-98770 0-97844 1-0022 1-0023	PL/PTF 0.38791 0.38568 0.78581 9.39305 0.57305 0.36364 0.36464 0.37469	0.65939 0.65559 0.65581 0.66812 0.66812 0.66812 0.67796	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 -1.0000				
NO WORD 107 112 122 127 127 137 142 152	PL 14.724 14.639 14.644 14.919 14.779 14.779 15.130 17.139	PL/PD 9-97480 0-96918 0-96951 0-98770 9-98770 0-97844 1-0022 1-0022	PL/PTF 0.38791 0.38568 0.28581 9.39305 0.39305 0.34936 0.36484	0.65939 0.65559 0.65581 0.66812 0.66812 0.66812 0.6185 0.43766	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 -1.0000				
VD WORD 107 112 122 127 137 142 152 157	PL 14.724 14.639 14.644 14.919 14.919 14.779 15.130 17.139 PL 15.130	PL/PD 9-97480 0-96918 0-96719 0-98770 9-98770 0-97844 1-0022 1-0023	PL/PTF 0.38791 0.38568 0.78581 0.39305 0.59305 0.36936 0.3686 0.3686 0.3686 0.3988	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185 0.47796 0.67796 0.67796	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 -1.0000				
VD WORD 107 112 122 127 137 142 152 157 >AODITIONAL	PL 14.724 14.639 14.644 14.919 14.919 14.779 15.130 17.139 PL 15.130	PL/PD 0.97480 0.96918 0.96951 0.98770 0.9770 0.97844 1.0023 1.0023 1.0023	PL/PTF 0.38791 0.38568 0.78581 0.39305 0.59305 0.36936 0.3686 0.3686 0.3686 0.3988	0.65939 0.65559 0.65581 0.66812 0.6612 0.6185 0.47704 0.67706 0.67706 0.67706 0.67706 0.67706	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 1.0000 X/DMAX -1.0000 -1.0000				
VD WORD 107 112 122 127 127 142 152 157 VO WORD 152 157 2A9D[T]ONAL	PL 14.724 14.639 14.644 14.919 14.779 15.130 17.139 PRESSURE	PL/PD 9.97480 0.96918 0.96951 0.98770 9.98770 0.97844 1.0023 1.0023 1.0023 1.0023 RAYIDS . 20	PL/PTF 0.38791 0.38568 0.78581 0.39305 0.50305 0.3646 0.37984 0.37984 0.39884 0.39884	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185 0.47790 0.07790 0.67790 0.67796 0.67796 0.67796	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 -1.0000 -1.0000 -1.0000				- · · ·
VD WORD 107 112 122 127 137 142 152	PL 14.724 14.639 14.644 14.919 14.919 14.779 16.130 17.139 PRESSURE PL	PL/PD 0.97480 0.96918 0.96951 0.98770 0.97744 1.0023 1.0023 1.0023 RAYIDS . 20	PL/PTF 0.38791 0.38568 0.39581 0.39305 0.30305 0.30494 0.39984 0.39984 0.39984 0.39984 0.39984	0.65939 0.65559 0.65581 0.66812 0.6612 0.6185 0.47704 0.67706 0.67706 0.67706 0.67706 0.67706	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 1.0000 X/DMAX -1.0000 -1.0000				
VD WORD 107 112 122 127 137 142 152 157 AGDITIONAL VD WORD 152 157 >AGDITIONAL VD WORD 167 172	PL 14.724 14.639 14.644 14.919 14.919 14.779 16.130 17.139 PRESSURE PL 15.139 PRESSURE PL 15.144 15.144	PL/PD 0.97480 0.96918 0.96951 0.98770 0.97744 1.0023 1.0023 RAYINS . 20 PL/PD 1.0026	PL/PTF 0.38791 0.38581 0.39305 0.50305 0.36936 0.3684 0.37984 0.39884 0.39884 0.39884 0.39884 0.39884	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185 0.47704 0.67706 0.67706 0.67706 0.67706 0.67706 0.67819 0.67819 0.67841	0.39800 0.43100 0.44900 0.52200 0.58000 -1.0000 X/DMAX -1.0000 X/DMAX 0.79300				
VD WORD 107 112 122 127 137 142 152 157 >ADDITIONAL VD WORD 152	PL 14.724 14.639 14.644 14.919 14.919 14.779 16.130 17.139 PRESSURE PL 15.139 PRESSURE PL 15.144 15.144	PL/PD 0.97480 0.96918 0.96951 0.98770 0.97744 1.0023 1.0023 1.0023 RAYINS . 20 PL/PD 1.0026 1.0029 RAYINS . 80	PL/PTF 0.38791 0.38581 0.39305 0.50305 0.36936 0.3684 0.37984 0.39884 0.39884 0.39884 0.39884 0.39884	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185 0.47704 0.67706 0.67706 0.67706 0.67706 0.67706 0.67819 0.67819 0.67841	0.39800 0.43100 0.44900 0.52200 0.58000 -1.0000 X/DMAX -1.0000 X/DMAX 0.79300				
VD WORD 107 112 122 127 137 142 152 157 >AODITIONAL VD HORD 167 177 >AODITIONAL	PL 14.724 14.639 14.644 14.919 14.779 15.120 17.120 17.130 15.139 PRESSURE PL 15.144 15.149 PPESSURE PL	PL/PD 9.97480 0.96918 0.96951 0.98770 0.97844 1.0023 1.0023 1.0023 RAYIDS . 20 PL/PD 1.0029 PATIOS . 80 PL/PD	PL/PTF 0.38791 0.38568 0.78581 0.39305 0.37305 0.36366 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37306 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006 0.37006	0.65939 0.65559 0.65559 0.65581 0.66812 0.66812 0.66812 0.6185 0.43704 0.43704 0.67706 0.67706 0.67706 0.67701 0.67701 0.67701 0.67701	0.39800 0.43100 0.44900 0.52200 0.52200 0.58900 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
VD WORD 107 112 122 127 137 142 152 157	PL 14.724 14.639 14.644 14.919 14.779 15.130 17.137 PRESSURE PL 15.130 PRESSURE PL 15.144 15.149 PPESSURE	PL/PD 0.97480 0.96918 0.96951 0.98770 0.97744 1.0023 1.0023 1.0023 RAYINS . 20 PL/PD 1.0026 1.0029 RAYINS . 80	PL/PTF 0.38701 0.38568 0.78581 0.39305 0.50305 0.36936 0.3686 0.3686 0.39886 0.39886 0.39886 0.39886 0.39886 0.39886 0.39886 0.39886	0.65939 0.65559 0.65581 0.66812 0.66812 0.66185 0.43704 0.77790 0.77790 0.67796 0.43796 0.67796 0.67819 0.67819 0.67841	0.39800 0.43100 0.44900 0.52200 0.58000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

									Run24
MASS-I FWIS	PRFLIM	INARY DATA	96/13/79	CAPPELL	PET 10/25/79	00:50:44.603	FAC BROXL	PG4 C034	PNG 1491
SAPPLITIONA	IF PRESSURE	PATIOS . PRI	MAPY PIUG						
AVP WORD	PL	PL / PN	PI /PTF	PI /PTP	X/DMAX	terrogeness and the second of the	entre de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la companion de la co	The Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Co	with the second property and the
32	14. 206	0, 93 736	0.44354	0.74839	0.72200				
37	15.270	1.0776	0.47677	0.89445	o. 82000				
47	15.655	1.0?30	0.48879	0.87472	0.91900				
52	15.883	1.0478	0.49581	0.83657	1.0170				
>APRIT TORAC	L PRESSUPE	RATIOS , FLO	M CHITTER I	.n.					
AVO HORD	PL	PL / PO	Pt /PTF	PL /PTP	X/DMAY				
62	14.911	0.98384	0.46554	0.78550	0.42200				
67	14.351	0. 94692	0.44807	0.75602	0.67000	,			
SADDITIONA	L PRESSURE	PATERS , FLO	W SPLITTER O	.0.		***************************************			
AVD MORD		Pt /PO	PL/PTF	PL/PTP	X/DMAX				
77	12.697	0.83778	0.39643	0.66688	0.50800				
92	17.963	1.1787	0.55774	0.94106	0.58300				
92	15,190	1-0923	0-47428	0.80024	0.67000				
		AARIOC , FUE	CTOS CURGUS						
							-		
AND MUSD	PE	PL/PO	PL /PTF	11/23	X/DMAX				
-107	14.736	0.97736	0.46000	177629	-1.0000				
-112	14.641	0. 70604	245712	0.77129	-1-0000				·
-127	14.646	0.96627	0.46646	0.77155	-1.0000 -1.0000				
-127	14.941								
-137	16-16	0.98417	0.46570	0.74577	-1.0000	· •			
						• •			
-137	14.596	0.98417	0.46570 0.45883	0.74577	-1.0000	· ·	· · · · · · · · · · · · · · · · · · ·		
-137	14.596	0.98417 0.98967	0.46570 0.45883	0.74577	-1.0000				
-137 -142 >A001T IONA	14-696 LL PRESSURE	0.98417 0.98967 RATIOS , FOP	0.46570 0.45883 FRODY INLET	0.77416	-1.0000	· · · · · · · · · · · · · · · · · · ·	•		
-137 -142 >A001T IONA	14.696	0.98417 0.98967 RATIOS , FOP	0.46570 0.45883 FRNDY INLET PL/PTF	0.74577 0.77416 P1/PTP	-1.0000 -1.0000	· · ·			
-137 -142 >ADDIT IDNA AVD WORD 107	14.696 14.696 IL PRESSURE PI 14.736	0.98417 0.98967 RATIOS , FOP PL/PO 0.97230	0.46570 0.45883 FRMDY INLET PL/PTF 0.46008	0.78577 0.77416 PL/PTP 0.77629	-1.0000 -1.0000 X/DMAX 0.39800				
-137 -142 >A001T IONA AVD MOPD 107 112 122	PRESSURE 14.736 14.646 14.646 14.941	0.98417 0.98967 RATIOS , FOP PL/PO 0.97230 0.96604 0.96637 7.98582	0.46570 0.45883 FRODY INLET PL /PTF 0.46008 0.45712 0.45727 0.46648	0.78577 0.77416 Pt/PTP 0.77629 0.77129 0.77155 0.78708	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600		•		
-137 -142 >A001T IONA AVD MOPD 107 112 127 127 137	PRFSSURF 14.736 14.646 14.941 14.916	0.98417 0.96967 RATIOS , FOP PL/PO 0.97230 0.96604 0.96637 7.98582 0.99417	9.46570 0.45883 FRODY INLET PL /PTF 0.4608 0.45712 9.45727 9.46648 0.46570	0.78577 0.77416 P1/P1P 0.77629 0.77129 0.77155 0.78577	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200				
-137 -142 >A001T IONA AVD WOPD 107 112 122 127 137 142	PL 14.696 14.736 14.646 14.646 14.916 14.696	0-98417 0-98967 RATIOS FOP PL/PD 0-97230 0-96604 0-96637 7-98582 0-98417 0-96967	9.46570 0.45883 FRODY INLET PL/PTF 0.4608 0.45712 9.45727 0.46648 0.46570 0.45783	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77155 0.78577 0.77418	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.58800				
-137 -142 >A001T IONA AVD WOPD 107 112 122 127 137 142	PRESSURE 14.696 14.736 14.646 14.941 14.696 15.145	0-98417 0-98967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 9-98582 0-9817 0-96967	9.46570 0.45883 FRODY INLET PL /PTF 0.46008 0.45712 9.45727 9.46648 0.46570 0.46570 0.4583	P1/PTP 0.77416 P1/PTP 0.77629 0.77129 0.77155 9.78708 0.7677 0.77418	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52800				
-137 -142 >A001T IONA AVD WOPD 107 112 127 127 137 142	PL 14.646 14.646 14.916 14.696 15:145	0-98417 0-98967 RATIOS FOP PL/PD 0-97230 0-96604 0-9637 0-98582 0-98417 0-96967	9.46570 0.45883 FRODY INLET PL/PTF 0.4608 0.45712 9.45727 9.46648 0.46570 0.46570 0.4570	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77155 0.78577 0.77418	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.58800				
-137 -142 >A001T IONA AVD WOPD 107 112 127 127 137 142	PL 14.646 14.646 14.916 14.696 15:145	0-98417 0-98967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 9-98582 0-9817 0-96967	9.46570 0.45883 FRODY INLET PL/PTF 0.4608 0.45712 9.45727 9.46648 0.46570 0.46570 0.4570	P1/PTP 0.77416 P1/PTP 0.77629 0.77129 0.77155 9.78708 0.7677 0.77418	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52800		•		
-137 -142 >A001T IONA AVN WOPD 107 112 127 127 127 137 147 -147 -147 -2401T IONA VO WORD	PL 14.696 14.736 14.646 14.916 14.696 15.125	0-98417 0-96967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 9-98582 0-98417 0-96967 1-9996 1-9990	9.46570 0.45883 FRODY INLEY PLANT O.4608 0.45712 0.45727 0.46570 0.46570 0.4583 0.4745	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77155 0.78577 0.78577 0.77418 0.90977	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000		•		
-137 -142 >A001T IONA AVD WOPD 107 112 127 127 137 142 153 -147 -2001T IONA VD WORD -152	PL 14.696 14.736 14.646 14.646 14.916 14.696 15.145	0-98417 0-98967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 0-98502 0-98417 0-96967 1-0790	9.46570 0.45883 FRODY INLET PI /PTF 0.4608 0.45712 9.45727 9.46648 0.46570 0.46570 0.46570 0.46570 0.47575 0.47575	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77129 0.78577 0.78577 0.77418 0.90971	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX -1.2000		•		
-137 -142 >A001T IONA AVN WOPD 107 112 127 127 127 137 147 -153 -147 -2001T IONS VO WORD	PL 14.696 14.736 14.646 14.916 14.696 15.125	0-98417 0-96967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 9-98582 0-98417 0-96967 1-9996 1-9990	9.46570 0.45883 FRODY INLEY PLANT O.4608 0.45712 0.45727 0.46570 0.46570 0.4583 0.4745	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77155 0.78577 0.78577 0.77418 0.90977	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000		•		
-137 -142 >A001T IONA AVD WOPD 107 112 127 137 147 142 153 VD WORD -152 -157	PRESSURE  14.696  14.736  14.646  14.941  14.696  15.195  15.195	0-98417 0-98967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 0-98502 0-98417 0-96967 1-0790	9.46570 0.45883 FRODY INLET PL /PTF 0.46008 0.45712 9.45727 9.46648 0.46570 0.46583 9.4459 0.47459	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77155 0.78708 0.78708 0.78718 0.7071 0.7071 0.70077	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX -1.2000				
-137 -142 >A001Y IONA AVO WOPD 107 112 127 137 142 142 143 -152 -157 -A001T IONA AVO WOPD	PL 15.195 15.20)  IL PRESSURE  PL 14.736 14.646 14.941 14.696 15.195 15.270 PL 15.195 15.270	0-98417 0-98967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 0-98582 0-9817 0-96967 1-0926 1-0930 PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO	9.46570 0.45883 FRODY INLET PI /PTF 0.4608 0.45712 9.45727 9.46648 0.46570 0.46570 0.46570 0.47883 9.4743 0.47459 DEG SHPOUD 1	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77155 0.78577 0.77518 0.7051 0.70077 P1/PTP 0.80051 0.80077	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 X/DMAX				
-137 -142 ->A001T IONA AVO MOPO 107 112 127 127 137 142 -157 ->A001T IONA AVO MOPO 147	PI 14.696 14.736 14.646 14.646 14.916 14.696 15.195 15.195	0-98417 0-98967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 0-98417 0-96967 1-9026 1-0026 1-00726 1-00726 1-00726 1-00726	9.46570 0.45883 FRODY INLET PI / PTF 0.4608 0.45712 9.45727 9.46648 0.46570 0.46570 0.47883 9.4743 0.47459 DEG SHPOUD 1 PI / PTF 9.47443	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77157 0.76577 0.76577 0.77418 0.90977 P1/PTP 0.80051 0.80077	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX 0.79300				
-137 -142 >A001Y IONA AVO WOPD 107 112 127 137 142 142 143 -152 -157 -A001T IONA AVO WOPD	PL 15.195 15.20)  IL PRESSURE  PL 14.736 14.646 14.941 14.696 15.195 15.270 PL 15.195 15.270	0-98417 0-98967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 0-98582 0-9817 0-96967 1-0926 1-0930 PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO PL/PO	9.46570 0.45883 FRODY INLET PI /PTF 0.4608 0.45712 9.45727 9.46648 0.46570 0.46570 0.46570 0.47883 9.4743 0.47459 DEG SHPOUD 1	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77155 0.78577 0.77518 0.7051 0.70077 P1/PTP 0.80051 0.80077	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 X/DMAX				
-137 -142  >A001T INNA  AVD WOPD 107 112 127 127 137 142 142 143 -177  >A001T IONA  AVD WOPD 147 172	PL 14.696 14.646 14.646 14.916 14.696 15.195 15.29)  PL 15.195 15.199	0-98417 0-98967 RATIOS , FOP PL/PO 0-97230 0-96604 0-96637 0-98417 0-96967 1-9026 1-0026 1-00726 1-00726 1-00726 1-00726	9.46570 0.45883 FRODY INLET PI /PTF 0.4608 0.45712 9.45727 0.46648 0.46570 0.4583 9.4743 0.47459 DEG SHPOUD 1 PI /PTF 9.47443 0.47428	0.78577 0.77416 PI/PTP 0.77629 0.77129 0.77155 0.78577 0.77418 0.9091 0.90077 PI/PTP 0.80051 0.80024	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX 0.79300				
-137 -142  >A001T INNA  AVD WOPD 107 112 127 137 142 143 -137 -147 -157  >A001T IONA  AVD WOPD 147 172	PL 14.696 14.646 14.646 14.916 14.696 15.195 15.29)  PL 15.195 15.199	0.98417 0.98967 RATIOS FOP PL/PO 0.97230 0.96604 0.96637 0.98417 0.98967 1.0090 0.7103 FAM PD 1.0726 1.0730 RATIOS 20 PL/PO 1.0726 1.0726 1.0726 1.0726 1.0726 1.0726	9.46570 0.45883 FRODY INLET PI /PTF 0.4608 0.45712 9.45727 0.46648 0.46570 0.4583 9.4743 0.47459 DEG SHPOUD 1 PI /PTF 9.47443 0.47428	0.78577 0.77416 PI/PTP 0.77629 0.77129 0.77155 0.78577 0.77418 0.9091 0.90077 PI/PTP 0.80051 0.80024	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX 0.79300				
-137 -142 ->A001T IONA AVO MOPD 107 112 127 127 137 142	PL 14.696 14.736 14.646 14.916 14.696 15.195 15.195 15.195 15.197	0-98417 0-96967 RATIOS _ FOP PL/PO 0-97230 0-96604 0-96607 0-98582 0-98417 0-96967 1-0026 1-0026 1-0020 RATIOS _ 20 PL/PO 1-0126 1-0126 1-0126 1-0126 1-0127 PATIOS _ 80	9.46570 0.45883 FRODY INLET PL/PTF 0.46008 0.45712 9.45727 9.46648 0.46570 0.46570 0.47883 9.4743 0.47459 DEG SHPOUD 1	0.78577 0.77418 PI/PTP 0.77629 0.77129 0.77155 0.78577 0.77418 0.70517 0.70418 0.7051 0.7051 0.7051 0.7051 0.7051 0.7051 0.70051 0.70051	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX -1.2000 -1.0000 X/DMAX 0.79300 0.84400				
-137 -142 ->A001T IONA AVD WOPD 107 112 127 127 137 142 -157	PL 14.646 14.646 14.646 14.646 14.696 15.145 19.220 14.696 15.125 15.270 14.696 15.195 15.197 15.197 15.197	0-98417 0-96967 RATIOS FOP PL/PO 0-97230 0-96604 0-96607 0-98417 0-98417 0-98417 0-98417 0-98417 0-96967 1-0726 1-0726 1-0726 1-0726 1-0726 1-0726 1-0726 1-0727 PATIOS 80 PL/PO PL/PO PL/PO 1-0726 1-0726 1-0727 1-0726 1-0727 1-0727 1-0727 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728 1-0728	9.46570 0.45883 FRODY INLET PL/PTF 0.46008 0.45712 9.45727 9.46648 0.46570 0.46570 0.47659 NO.47459 DEG SHPOUD 1 PL/PTF	0.78577 0.77416 P1/PTP 0.77629 0.77129 0.77129 0.77577 0.77517 0.77518 0.70517 0.70077 0.70051 0.80077 0.80051 0.80024	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

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	v	ASA-I FWIS	P0F1 T41	IHARY NATA	06/13/79	CANNELL	PEC 10/25/7	9 00:51:59.#35	FAC ANGNI	PGM C934	RUN 2.4	P
				PATINS , PRI								•
	AV	n within	PL	PL / PO	PI /PTF	OL /PTP	X/DMA X				- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	
	33		14.851	0.98055	0.53949	0.91712	0.72200					
	3°		15.190 15.310	1.0923	0.55147 0.55615	0.9374P 0.94549	0.82009 3.91900					
_	5;		15.390	1.0155	0.55873	0.94981	1.0170					D
		SANDITIONAL PRESSUPE RATIOS . FLOW SPLITTED 1.D.							e y namen namen i de la praceida de estado		The state of the second second second second	
	AV	D MUST	PL	F4 / PO	PL /PTF	PL /P TP	x/0mAx			-		
	. 6		14.990	0.98979	0.54457	0.92575	0.42200					_
	6		14. 991	0.98253	0.54058	C-91897	2.67000					•
	. >	APPIT TONA	PRESSIRE	RATIOS , FLOR	SPLITTER O	.n.				<del></del>		
	AVI	C WARD	PI	PL /PO	PL / PTF	PI /PTP	X/DMAX					•
	7			9.86367	9.47598	0-00761	9.50900					
	8		16.893	1.1154	0.61370	1.0433	0.50300					
	92	2	15,185	1_0026	0.55165	0_93778	0.67000					
	>1	POTTION	. PASSCURS	AATICESAC	C <u>t Ch</u> Chirolib	<del></del>			-			•
344		WORD	71	PL/P3	PL/PTF	PLEATING TO	X/DMAX					
4	-19		14.77	0.97198	0.53620	0.90910	-1.0000 -1.0000					
	=1.5 -1.5		14.621 14.616	0.94538	0.53097	0.90262	-1.0070				<del></del>	
	-12	27	14.901	0.98385	0. 141	0.92020	-1.0000					
	-11		_14:101	0.98253	C. 5405#	0.91097	-1.0000					
	-19	_	14.6.76	9 ₊ 96 991 _	0.53314	0.90098	-1.0000					D
				RATIOS . FOR						<u> </u>		_
		? WCRD )7	14.721	PL/PO	PL/PTF 0. 51478	0.90910	X/DMAX 0-39800		7	-		
		[2	14.621	9.96538	0, "3115	0.90293	9.43109					_
		??	14.616	7.96505	0.53097	0-90262	0-44900					Ð
		27	14.901	2-98385	Q. 54121	0.92020	0.48600					
		17 42 _	14.991	0.98253 0.96901	7. 53314	0.91097 0.90632	0-52200 0-5000					•
	ىيىد	<del></del>	14.676					•	••	•		_
	4	<del>,,</del>	194849	107717		11.430-1-	-1-0000					•
		TOTT TOWN		AA-1196 - FAN	401115 F14500							
		MUND	PE -	PL/PN	_PL COTO	PL/PTP	Y/MAY					
	-1°		15-160	1.0013	0. 55074	0.93624 	-1.0000 -1.0000					
	•						-1.00.0					
				RATIOS , 20								
		n <b>warn</b> 67	PI 15.165	PL/PO	PL/PTF 0.55092	PI /PTP 0.93655	x/DMAX 0.79300					
	1	5 ( 7 )	15.165	1.0013	0.55092	0.93655	0.74500					_
		ANNET IMMAI		RATIOS . RO								Ð
		n Mubu					X/(PAX					<u>.</u>
,		Number	PL 14.765	ም / ውበ ሳ. ዓላላ1 4	PI / PTF 0. 54367	PL/PTP 0.92421	0.79300					
	, i	P7	14.541	2.95011	0.52824	0.89799	2.84400					_
				THRIST PARAM								

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AT 24-1 LM14	. warflat	IMARY DATA	06/13/79	CADDELL	REC 10/25/	79 00:53:20.504	fac axexi	PG4 C034	PNG 1483
>470171000	I beecchee	PATTOS , PPT	MARY PLUG						
AVO WORD	PL	of /bu	PL /PTF	PL /PTP	X/DMAX	and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	mount was the second	· 6 4	
37	14.329	7.94780	0.52363	0.75154	0.72200				
77	15.323	1.0136	0.55997	G.F0370	0.82000				
47	15.463	1.0361	0.57239	0.87155	0. 91 900				
52	15.858	1.0480	0,57041	0.83174	1.0170				
NOT TECOM	L PRESSUPE	RATIOS . FLO	W SPI STTF# 1	. n.				No. 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1 - American - 1	man a comparable ser
A DE MORD	PL	PL/PO	PL / PTF	PL /PTP	X/DHAX				
- 62	15.290	0.99870	0. 55175	0.79190	0.42200				
67	14.573	9.964D0	0.53258	0.76438	0.67000				
NAULTICONS	L PRESSURF	PATINS , FLE	W SPLITTER O	. 0.	ur i ur sale - vinale entre Mentalement i remedia di		on announced Millionia formation provided antiferrogalistics of their	age or the printers of the highly regarded to the printers of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territory of the territor	anyah magasan familin 1980 on 1980 on 1980 dan mengalik magasi sajayan selili sebagai di
AVP WORD	PL	PL / PIT	M/PTF	PI /PTP	X/DMAX				
77	13.009	S9598 .0		0.68653	0,50800				
A2	16-977	1-1164	0.61676	0.86520	9.54300				
9?	15,143	1.0017	9.55340	0.79426	0.67000		**************************************		
STREET	L BRESSURE	ALTIOS EUS	CACO EMBORO			, ak			
AVD MORD	PL	et/Pn_	PL/PTF	PLEATE	X/DMAX		*		***
-107	14.708	9.97292	0.53751	0.77146	-1.0000				
-112	14.618	7,96697	43422	0.76674	-1,0000				
-177	14-673	0.96759	D. CARRO	0.76700	-1.0000				
-127	14.993	5. 9A515	0.54427	0.70116	-1.0000				
-137		0.98449	0.44399	0.77093	-1.0000				
-152	14-698	0.97226		0.073	-1.0000				
NOT TICKY	t PRESSIME	MATIOS , FOR	FRIDY INLET						
AND MURD	Pt	PL/PO	PL /PTF	PL /PTP	X/DMAX				
107	14.706	0.97202	0.52751	0.77146	0.39800		•		
112 122	14,616	0, 96697 9-96730	0.53422 0.53449	0.76674 0.76700	0.43100	-			
127	14.673 14.893	0. 98515	0.54427	0.78116	0.48600				
- 127	14,483	7.98449	0.54390	0.74043	0.52200				
147	14.698	0.07226	0.53714	0.77053	0.56800				
							* *		
	174143	1+7510	<del></del>						
************	<del>(</del>	007173 y 244	100710 F1 P2					and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
AVD WORD	PI	4.40		PL /PTP	X /DMAX				
-152	15.130	-1.7713	0.55321	0.79400	-1.0000				
-152	15.133	1.0910	0-44303	070374	-1.0000				
>vual i lum	I PPESSIME	RATINS , 20	DEG SHRPUP I	CATION				and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	
AVD WORD	PL	PL/ P1	PL /PTF	PL /PTP	X/DMAX				
167	15-133	1.0010	0.55703	0.79374	9.79300				
177	15.13#	1.0013	0.55321	0. 79400	0.84400				
PULLICIAS	L PRESSUPE	RATINS , 40	DEG SHREUD I	OFATION				the time time. And the expension of the	
BROW GVA	PL	PL/PO	Pt /PTF	PI /PTP	X \D## X				
102	15.069	9.99672	0.55066	0.79033	0.79300				

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1851-L FWT	S	INARY DATA	16/13/79	CARDETT	REC 10/25/79	90:54:03.848	FAC 98681	PG# C034	RUN29 PDG 1494
>A0017 [014	IAL PRESSUPE	PATIOS . PPI	MARY PLUG						
AU AUM U	PI	PL/PO	PL /PTF	PI /PTP	X/DMAX				
32	11.950	0.79949	0.37467	0.53410	U. 72200				
37	15-135	1.0714	0.47462	0.67459	0.82000				
67	15.863	1-0493	0.49733	0.7089£	0.91900				
52	14.212	1.0724	7.50830	0.72459	1.0170				
							recommendation of the same		
NOT TICEN	ML PRESSUPE	PATTOS , FLO	M SMITTER I	. n.					
ለው ማህክብ	PL	PL / PO	PA /PTF	PI /PTP	x /DMA x				
52	15.488	1.0245	0.48559	0.69222	0.42200				
47	13.379	7.88503	0.41548	0.59798	9-67000				
>A 77   T   T   N	AL PRESSIME	PATIOS . FLO	W SPLITTER F	`. n.				/ / ·• - /-	, and the state and an analysis of
AD MUSEU	PL	PL / PO	PL /PTF	PL /PTP	X/DMAX				
77	12.590	9-63214	0.39441	0.56224	0.50800				
12	17.726	1.1726	0.55576	0.792?5	0.58300				
92	15-138	1-0014	0-47562	D-67659	0.67000				
-A2211 10H	ML PRESSURE	PATIOS + ESE	<del>CTPP SHPOND</del>			-			
O HOPD	PE	. PL/PO	PL/PTF	PLEEP	X/DMAX				
07	14.688	0,97163	0.46052	0.65649	-1.0000				
112	15.599	0.95544	9055770	0.65247	-1.0000				
122	14.599	2.9456	0-45770	0.45247	-1.0000				
27	14.873	0.98386	0.46637	0,66475	-1.0000				
77	-14.858	0.98286	0.46585	0.44408	-1.0000	-		-	•
32	14.624	2.96733	Q.45849	0,65759	-1,0000				
APPLTICA	AL PRESSURE	RATIOS . FOR	ENOW THEEL						
/n 40#0	PL	PL/PO	PL/PTF	PI /PTP	X/DMAX				
07	14.688	9.97163	0.46952	0.65649	0.39800		•		
112	14.599	0.96568	0.45770	0.65247	0.43100				
22	14.599	7.96569	0.45770	0.65247	2.44900			-	
27									
	15-873	2.98386	0.46632	0.66475	Q_4860Q				
137	14. 959	J. 98286	0.46595	0.66498	0.52200				
47	14.624	0.96733	7.45849	0.45359	0.58800			•	
45		1.00?9		<del>0.07703</del> -	-1,0000-				
53	<del>\5₁\5}</del>			- n. #7726	-1:0000				
4001110	WE POF 13005	******	F44536-1344						
/N WNPN  52	PL	1.7020	THE TOTAL	PL /PTP	X/DMAX				
52	<u> 15.158</u> 15.153	1.0924	0.47509	0.67703	-1.0000 1.0000				
		PATINS . 20							
*								, er - and Lagranger (Mr. ) graph a children	
/ቦ ቁጣቀክ ኒኖን	PL 15.148	P( /P() 1.0020	PI /PTF 0_47493	PL/PTP 0.67703	X/DMAX 0.79300				
72	15.149	1- 9020	2.47403	0.67703	9-84400				
	AL PRESSUPE	PATINS . PO	DEG SIPOUN 1	OCATION				. Parker approximate the devices referred to	
ACTITION		Pt /PO	PL /PTF	PL /PTP	X/DMAX				
	P1								
en unen	PI 15-033				0. 79300				
AU AUDEU	15.033	0.99443	0.47137	0.67190	0.79300				
/N 4/1PN LP? L87	15.033 14.653		0.47137		0.79300 0.94409				

	uel pressure perins	PETITIO • PRIMERY	TARY PRUS					
AV) UNDO	Ē	3/5	PI /PTE	Pt /PTP	K/IMAX			
32	12.912	3,45119	02611.0	0.26209	0.12200			
1.5	15.655	1.9332	0.410.7	0.60223	0_0100			
42	16.759	1.1054	12017 0	0.66433	1.0170			
SANDIT INVAL	Sell PPFSSIBE	RATIOS , FICE	e callities !	٠٩.	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	• • • • • • • • • • • • • • • • • • • •	•	
AVO WOPD	, =	2/2	M /PTF	91 // 14	X/DMAX			
62 67	17.694	1.1618	0.46167	0.67719	0.42200			4
>4nni Tinmal	ML PRESSIBE RATIOS	RATINS . FIN	SPI ITTER	٦.9.	A. P	the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa		
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	8, 8773	9.58586		0.34149	0.5000			
n2 92	20.917 15.186	1.3834 1.0022	0.54855 0.39825	0.58416	0.58300 J. 6 7000			
tened to be con-	l 1.	75303 - 30leve						
	. /							
4Vn 4040		200	7/275	200	#/OHAX			
-112	14.601	0.0	0.38501	0.56474	-1.9900			
-172	14.641	D. Skory	105	0.56474	-1.0000			
-127		2.04668	0.39299	25.7	0000	ř		;
152	14.001	0.97678		0.4693A	0000	1		
>AODIT IDNAL	PRESSIRE	RATIOS . FORE	FOREBOON INLET		1			
AVD KORD		_	P1 /PTF	97 67	X/DMAT			
	14.761	0.97415		0.56782	0.3 5800	•		
112	14.641	0.96887	0.38501	9-56474	0.43100			
127	14.641	3, 96 AB7	0.38401	0.56474	0.44400			
1.1	14.941	9.986AR	0.39209	0.57512	0.52200			
142	16.401	0.07678	0,34916	0. 46916	0.54800			
137	4	#100 A	d leak to		0000-1			
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			1		- Trade			
-167	15.18	V	21697	2,58397	-1-0000			
15-	14:141	1.101#	21wor.0	2354201	-1-0000			
SANULT INNAL	HAL PRESSIPE	PATINS . 20 (	DEG SHOUND LY	PCATION	1			
Udum UAV	ĭ	71/10	P1 /P1F	Pt /PT?	x/max			
147	15.191	1.0016	1,39412	0.58397	0. 79309			
2.1	<u> </u>	C11.6•1	Je 12 / 7 F	7.581.0	00***			
SANDIT INNAL	IN PRESSIRE	PATINS . NO E	DEG SHPOUD TO	INCATION	· · · · · · · · · · · · · · · · · · ·	TO THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF THE PERSON OF		
AVD WIDER	ť	£ / £	PL/PTF	4747	K / DMAX			
- E	166.91	0.98536		0.57435	9. 79300			
177	16.401		0. 34003	0.55744	0.84400			
		TUBERT BADA	Tree					

4854-1 FW 19	S PRELIMI	HARY DATA	06/13/79	CAUDELL	REC 10/25/79 01:30:18.745	FAC RYSK!	PG4 C034 PI	PLINIA april or
1401 T [ CCA	AL PRESSUPE	RATIOS , PRI	MARY PLUG					
VD YOPD	Pl	PI /PO	PI /PTF	PL /PTP	X/DMAX	May make an an a	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	
32	7-5697	0.49925	0. 18086	0-26819	0.72200			
7	11.211	0.73930	0.26784	0.39718	0. 82000			
. 7	15.055	0.99294	0.35969	0.53338	0.91900			
57	16.669	1.0004	0.39826	0.5905#	1.0170			
WOLTECTA	LE PRESSURF	PATINS , FLN	W SPI ITTEP I	.0.		e Managara da esperante de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición del composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la composición de la co		to a serial control of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the second section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the section of the sectio
yn wnen	PL	M. /90	PL /PTF	PL /PTP	H/DMAK			
2	19-118	1-2609	0.45677	0.57734	0.42200			
.7	15.055	ŋ <b>. 99</b> 294	6. 35660	0.53338	0.67000			
Annition	AL PRESSURE	PATIOS . FLO	W SPLITTER I	.0.		n manadas (a chronisticaga), cho galellala usp inc magga col terretainan - b - i	Miles Miles of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the co	THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE P
IN WOPN	Pt	PL /PD	PL/PTF	PL /PTP	X/DMAX			
77 .	9.8354	0.64869	0.23499	C.34846	0.50800			
32	19. BSB	1.3977	0.47373	0.79248	0.58300			
12	15-180	1.0012	0.26268	0.53781	3.67999		origan solven men i den mysyy maken in Abenya sampa <del>ya didibilingaya s</del>	
4301210M	<del>11 - PRESSUPE</del>	<del>^^*</del>	<del>6 d sto - i see selte-</del>					
O NORD	7	PL/ PD	PL/PTF	PLEASE	X/DHAX			
07	14.755	2,97316	0.35253	0.52276	-1.0000			
LIZSL	14-695	0. 90066	04.2015	0.52025	-1.0000			
22	14.695	7.96930	35109	9.52063	-1.0000			
127	14.940	U. 98799	0.25 Jah	0.53072	~1.0000 .			
27	15-00	0.99931	0.35434	0.43143	-1.0000			
14>	14,940	0,98535	0,35695	0.52931	1.0000			
MOI TI COM	AL PRESSUPE	PATIOS . FOR	FACOY INLET					
O NOPD	PL	. PL/PO	PL/PTF	PL/PTP	X/DMAX		*	na
97	14.755	0.97316	0. 75253	0.52276	0.39800			
112	14.605	0.06854	0,35085	6.52028	0.43100	** **	e e e	
127	14.695	9.96920	0.35109	0.52063	0.44900			
21	14.980	0.94799	2.35192	9.53072_	0.48600			
47	15.000	0.9#931	0.35838	0.53143	0.52200			
	14.940	0.99535	0.35695	0.52931	0.5 6800			
					1.0000			
4	15-185	<u>1_0015</u>			1.0000		7	
57	15-145	-,	-107737-F440				7	
57							*	·
57	1-10535/01	-,		PL /PTP 0.53701	x/0MAx -1.0002		*	·
57 2007 (mu	PL	P-/40	_BL/FFF-F640	PI /PIP	x/DMAx		-	
57 20017 (mul (n unpn 62 57	PL 15.140 15.145	74-740 1-7717	0.7626F	PL/PTP 0.53781 0.53299	X/DMAX -1-0009			
57 20017 (mul (n unpn 62 57	PL 15.140 15.145	7./80 1.9717 1.0015	0.7626F	PL/PTP 0.53781 0.68799 FCAY[My	X/DMAX -1-0009			
ET LOUIT TOWN	PL 15.180 15.185  IL PPESSUPE	1.0117 1.0015 1.0015 PAYIOS . 20	MATERIAL I	PL/PTP 0.53781 0.68799 FCATERN	X/DMAX -1.0000 -1.0000			
ST PARTY TOWN F2 S7 PARTY TOWN	PL 15.180 15.185  AL PPESSUPE PL 15.180	PL/40 1-0717 1-0215 1-0215 PAY(05 - 20 1-0212	0.762P7 0.762P7 DEG SHROUD 1	PI /PTP 0.53781 0.63799 CCATEMN PI /PTP 0.53781	X/DMAX -1.0003 -1.0000 X/DMAX 0.79300			
IO MOPO 62 67 ADDET SONE ADDET SONE FOR MOPO 67	PL 15.180 15.185 NL PPESSUPE PL 15.180 15.180	PAYIOS , 20 PAYIOS , 20 PI /PN 1.0012 1.0012	0.36268 0.36268 0.36289 0.36268 0.36268	PL/PTP 0.53781 0.63790 FCATENN PL/PTP 0.53781 0.53781	X/DMAX -1.0000 -1.0000			
CONTRACTOR	PL 15.180 15.185 NL PPESSUPE PL 15.180 15.180 NL PRESSUPE	1.0015 1.0015 1.0015 20 /Pn 1.0012 1.0012	0.762F7 0.762F7 DEG SHROUD 1 M /PTF 0.3626F 0.3626F	PL/PTP 0.53781 0.63790 CCATENN PL/PTP 0.53781 0.53781	X/DMAX -1.0009 -1.0000 X/DMAX 0.79300 0.84400			
FOR HOPO FOR HOPO FOR HOPO FOR HOPO FOR HOPO FOR HOPO FOR HOPO FOR HOPO FOR HOPO FOR HOPO	PL 15.180 15.185 AL PPESSUPE PL 15.180 15.180 AL PRESSUPE	# / #0 1.971? 1.0015 PATIOS . 20 PI / PO 1.9012 1.9012 PATIOS . 80	# JATE 9. 36268 0. 76289 DEG SHROUD 1 PI /PTE 9. 36268 0. 36268 DEG SHROUD 1	PI /PTP 0.53781 0.63790  FCATION PI /PTP 0.53781 0.53781  PCATION PI /PTP	X/DMAX -1.0009 -1.0000 X/DMAX 0.79300 0.84400			
IO MOPO  E2  E57  ADDIT IOM  F7  F MOPO  E7  T7  ADDIT IOM  F7  ADDIT IOM  FF  FF  FF  FF  FF  FF  FF  FF  FF	PL 15.180 15.185 AL PPESSUPE PL 15.180 15.180 AL PRESSUPE PL 14.780	PATIOS - 20 PATIOS - 20 PATIOS - 20 PATIOS - 20 PATIOS - 80 PATIOS - 80 PATIOS - 80	# 4477 9-34268 0-36268 0-36268 0-36268 0-36268 DEG SHPPUN LI PLATE 0-35312	PL /PTP 0.53781 0.63790 FCAYENN PL /PTP 0.53781 O.53781 FCATION PL /PTP 0.52364	X/DMAX -1.0000 -1.0000 X/DMAX 0.79300 0.#4400 X/DMAX 0.79300			
ID MOPO  F2  F3  FANORY JOHA  ID MOPO  F7  T7  ADDRY JOHA  ID MOPO  ADDRY JOHA  ID MOPO  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  ADDRY JOHA  A	PL 15.180 15.185 NL PPESSUPE PL 15.180 15.180 NL PRESSUPE PL 14.780 14.780 14.325	# / #0 1.971? 1.0015 PATIOS . 20 PI / PO 1.9012 1.9012 PATIOS . 80	M / PTF 0.36268 0.36268 0.36268 DFG SHPPIN 1	PI /PTP 0.53781 0.63790  FCATION PI /PTP 0.53781 0.53781  PCATION PI /PTP	X/DMAX -1.0009 -1.0000 X/DMAX 0.79300 0.84400			

11   12   13   13   14   15   15   15   15   15   15   15	X/DMAX 3.72200 0.82000 2.91900 1.9170 1.9170 0.42200 0.67000 0.58300 0.58300 0.58300 0.58300 0.58300 0.58300 0.10000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		
1.   1.   1.   1.   1.   1.   1.   1.	X/DMAX 0. 67000 1. 91900 1. 91900 1. 91900 0. 67000 0. 67000 0. 5 8409 0.		
	0.62000 0.91900 1.0170 0.42200 0.67000 0.58300 0.58300 0.58300 0.58300 0.58300 0.67000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		
	2.91900 1.0170 0.42200 0.67200 0.67200 0.58300 0.58300 0.58300 0.58300 0.47200 1.0000 1.0000 1.0000 1.0000		
	1.0170  1.0170  0.42200  0.42200  0.52200  0.52300  0.52300  0.52300  0.52000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000  1.0000		
	X/DMAX 0.42200 0.67200 0.67000 0.58300 0.58300 0.58300 0.58300 1.0000 1.0000 1.0000 1.0000 1.0000		
17.166	0.42200 0.67200 0.67000 0.58300 0.58300 0.58300 0.47000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
17.100   1.4313   0.45905   0.53815	0.67000 0.67000 0.58300 0.58300 0.58300 0.47000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
17.100	0.67000 0.58300 0.58300 0.58300 0.47000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
	x / (max d. 5 0 0 0 0. 5 8 4 0 0 0. 5 8 4 0 0 0. 4 7 0 0 0 -1. 0 0 0 0 -1. 0 0 0 0 -1. 0 0 0 0 -1. 0 0 0 0 -1. 0 0 0 0 -1. 0 0 0 0 -1. 0 0 0 0		
11.20m   PI	X/PMAX  0.50000  0.50000  0.470000  -1.00000  -1.00000  -1.00000  -1.00000  -1.00000  -1.00000  -1.00000  -1.00000		
11.20m   0.71975   0.23725   0.35002   15.813   1.0450   0.33515   0.46791   15.166   0.33515   0.46791   0.47491   0.47491   0.47491   0.47491   0.47791   0.31264   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.46291   0.4729   0.31740   0.46291   0.46291   0.4729   0.31174   0.46291   0.46291   0.4729   0.31174   0.46291   0.46291   0.4729   0.31174   0.46291   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.4729   0.	0.50000 0.58300 0.58300 0.47000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
15.833   1.0650   0.33515   0.46793     15.168   1.0311   0.32107   0.47991     14.776   0.97472   0.31264   0.46994     14.776   0.97472   0.31264   0.46994     14.979   0.97472   0.31264   0.46994     14.999   0.97472   0.31740   0.46994     14.999   0.97472   0.31740   0.46994     15.953   0.99472   0.31134   0.46924     15.953   0.99472   0.31134   0.46924     14.723   0.99472   0.31134   0.46924     15.918   0.99472   0.31134   0.46924     15.918   0.99472   0.31134   0.46924     15.918   0.99472   0.31134   0.46924     15.918   0.99472   0.31134   0.46924     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47131     15.918   0.99472   0.31164   0.47111     15.918   0.99472   0.99472   0.31164   0.47111     15.918   0.99472   0.99472   0.31164   0.47111     15.918   0.99472   0.99472   0.31164   0.47111     15.918   0.99472   0.99472   0.31164   0.47111     15.918   0.99472   0.99472   0.31164   0.47111     15.918   0.99472   0.99472   0.31164   0.47111     15.918   0.99472   0.99472   0.31111     15.918   0.99472   0.99472   0.31164   0.47111     15.918	0.58300 0.47000 1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
	x/DM4x -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
	x/DMAx -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
14.768	x/bhax -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
14,773   0,5734   5,31134   0,46051     14,974   0,94924   0,3176   0,46091     15,953   0,99353   0,3176   0,47131     15,953   0,99353   0,3176   0,47131     11,764   0,4772   0,3134   0,46091     14,764   0,9772   0,3134   0,46091     14,764   0,9772   0,3134   0,46091     14,764   0,9772   0,3134   0,46091     14,764   0,9772   0,3134   0,46091     14,764   0,9717   0,31184   0,46091     15,918   0,9717   0,31184   0,4702     15,918   0,99353   0,31864   0,4702     15,918   1,9701   0,52072   0,4704     15,153   1,9701   0,52072   0,4704     15,153   1,9701   0,52072   0,4704     15,153   1,9701   0,52072   0,4704     15,154   1,9701   0,52072   0,4704     15,155   1,9701   0,52072   0,4704     15,157   1,9701   0,4707   0,4707     15,158   1,9701   0,4707   0,4707     15,159   1,9701   0,4707   0,4707     15,159   1,9701   0,4707   0,4707     15,159   1,9701   0,4707   0,4707     15,159   1,9701   0,4707   0,4707     15,159   1,9701   0,4707   0,4707     15,150   1,9701   0,4707   0,4707     15,150   1,9701   0,4707     15,150   1,9701   0,4707     15,150   1,9701   0,4707     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701     15,150   1,9701   0,4701     15,150   1,9701   0,4701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701     15,150   1,9701	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
14.773 9.2477 5.1165 0.46078 15.753 0.9922 0.31165 0.46078 15.753 0.99353 0.31766 0.47131 15.753 0.99353 0.31766 0.47131 11.764 0.9777 0.31261 0.46229 14.704 0.9777 0.31134 0.46091 14.704 0.9777 0.31134 0.46091 14.704 0.9777 0.31134 0.46091 15.918 0.9717 0.31134 0.46091 15.918 0.9717 0.31165 0.46091 15.918 0.9717 0.31165 0.46091 15.918 0.99353 0.31164 0.47131 15.918 1.9701 0.37074 15.153 1.9701 0.37074 15.153 1.9701 0.37074 15.153 1.9701 0.37074 15.153 1.9701 0.37074 15.153 1.9701 0.37074 15.153 1.9701 0.37074	-1.9000 -1.0000 -1.0000 -1.0000 -1.0000		
	-1.0000 -1.0000 -1.0000		
	4 0000 X/D4AX		
### ### ##############################	X/DHAX	en de la companya de la companya de la companya de la companya de la companya de la companya de la companya de	
### ### ### ### #### #################	X/DMAX		
HOPO PE	X/D4ax		
14.764 0.97472 0.31261 14.708 0.07076 0.31134 14.708 0.07175 0.31134 15.318 0.99353 0.3176 15.318 0.99353 0.3176 15.318 1.0701 1.3707 15.153 1.0701 1.3707 15.153 1.0701 1.3707 17.153 1.0701 1.3707 17.153 1.0701 1.3707 17.153 1.0701 1.37076 17.153 1.0701 1.37076		•	
1.723	0017	•	
15-918	0.15100		
15.318	00,4 8600		
15.053	3,52203		
	0.5 FRMO		
	0000		
15.153   1.09701   7.32025   1.09701   7.32025   1.09701   7.32025   1.09701   7.32025   1.09701   7.32025   1.09701   7.32025   1.09701   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.00201   1.002			
15.153 1.0001 2.2015 15.153 1.0001 0.32015 011 10041 PRESSURE RATIOS , 20 DEG SWROUD INCA			
17.173 1.0001 0.32075 017 [0.44] PRESSURE RATIOS , 20 DEG SHROUD INCA	# COMPA		
OTT TOWAL PRESSURE RATIOS , 20 DEG SHROUD LOCATI	1-0000		
APPO EL SEURE RATIOS , 20 DEG CHROUD LOC	Section 1		
110/10 U4/10 10 U0/1			
	X/DMAX		
7 15.14# 0.999#n 0.72065	0.79300		
	0.84400		
STOTITIONAL PRESSIBE PATION . NO DEG SHPCHO LOCATION			
(a) k	*COMBX		
14,743 2,97307 0,31234	0.79300		
14.243 7.94271	3.84400		
FI THEIST PAPAMETERS			

MASA-LEWIS	S PRFLIMI	INAPY DATA	06/13/79	CANNETT	REC 10/25/79 01:03:47.284	FAC SHEKE	PG4 C034 PDG 1	1499 1499
>800   T   [08]	AL PRESSUPE	PATINS . PRI	HARY PLUG					
VO WOPD	PL	Pt /Pfl	PL / PTF	PL /PTP	Y/DMAX			
32	10.441	3.68940	0-19056	0-27667	0.72200			
37	18.809	1.2419	9.34327	0.49839	0.82000			
47	14-546	0. 96040	0.26547	0.38543	0.91900			
52	16.855	1-1129	0.30761	0.44661	1.0170			
אחון דן מרמ<	AL PRESSURE	PATINS . FLO	W SPLITTER I	.n.		· y		
VD WOPD	PL	PI /PO	PL/PTF	PL/PTP	x/DMAX			
52	25-196	1.7032	0. 47079	0.68353	0.42200			
67	20.948	1.3931	0.32231	0.55507	0.67000		-	
>Anni Tinna	AL PRESSUPE	RATTOS , FEO	W SPLITTER O	.n.				· <del></del>
אחשה חע	PL	PL/PN	PI / PT F	PL /PTP	X/DMAX			
77	. 13-031	D. 86 04Q	0. 23 783	0.34529	0.50800			
P2	18.394	1.2145	0.33570	0.48740	0.58300			
92	15.171	1.0017	0.27687	0.40198	0.67000			······································
1001-10W	AL-PRESSURE	PAT105 & CUE						
D WORD	PL	PL/PQ	PL/PIF	PLANT	X/DMAX			
107	14.796	0.97624	0.26988	0.3917R	-1.0000		•	
112	14.731	0.07	U. 6884	0.39033	-1.0000			
22	14.741	0.07 727	0.34903	0.39059	-1.0000			
27	15.006	2.99076	0.27386	0.39761	-1.0000			
	15.051	0.99373	0.2746R	0.3 000	-1.0000		-	
137	1 20 0 71	06 7 1313			_ 110000			
	15.081	0,99571	0.27523	0.39960	1-0000		w	
152	15.081		0.27523		1-0000			
	15.081	0,99571 RATIOS . FOR	0.27523	0+39960	1-0000			<del></del>
SAND LT INNI	15.081 AL PRESSIME PL	0,99571 PATIOS - FOR	0.27523 EPPDY INLET	0.39960 	X/DMAX	· · · · · · · · · · · · · · · · · · ·		
AND LT 1044 /D H1.RD	15.081 AL PRESSIME PL	0,99571 PATIOS . FOR PL/PO 0.97624	0.27523 EPPDY INLET PL/PTF 0.26985	PL/PTP _ 0.39178	X/DMAX 0-39900			
AND [T ION/ /D WIRD 107	15.081 AL PRESSIME PL 14.786 15.731	0,99571 PATINS , FOR PL/PN 0.97624 0,97261	0.27523 EPPDY [NLET PL/PTF 0.26985 0.26884	PL/PTP_ 0.39178 0.39033	X/DMAX 0.39000 0.42190	· · · · · · · · · · · · · · · · · · ·		
SAND [T ] [ NV. PD WERD 107 112 122	15.081 AL PRESSURE PL 14.786 14.731 14.741	0,99571  PATINS . FOR  PL/PN 0.97624 0,97261 0.97327	0.27523 EFFCDY INLET PL/PTF 0.26985 0.26884 0.26503	PL/PTP	X/TMAX 0.39800 0.43100 0.44900			
52 200 ET 1044 70 ET 20 107 112 122 127	15.081 AL PRESSIRE PL 14.786 14.731 14.741 15.006	0,99571  PATIOS . FOR  PL/PO 0.97624 0,97661 0.97327 0.99076	0.27523 EPPDY INLET PL/PTF 0.26985 0.26984 0.26983 0.27386	PL/PTP _ 0.39178	x/DMAX 0.39800 0.43190 0.44900 0.48600			
PAND LT INNA 70 MIRD 107 112 127	15.081 PRESSIME PL 14.786 14.731 14.741 15.006 15.051	0,99571  PATIOS . FOR  PL/PO 0.97624 0.97327 0.99373	0.27523 PEPCDY [NLET PL/PTF 0.26985 0.26984 0.26903 0.27386 0.27468	PL/PTP 0.39178 0.39033 0.39059 0.39761 0.39880	X/DMAX 0.39800 0.42100 0.44900 0.48600 0.52200			
PAND [T INN/ /D WIRD 107 112 22 127 137 142	15.081 AL PRESSIME 14.786 14.731 14.741 15.006 15.051 15.081	0,99571  PATINS FOR  PL/PN 0.97624 0,97261 0.97327 0.99076 0.99373 0.99571	0.27523 PEPCDY [NLET PL/PTF 0.26985 0.26984 0.26903 0.27386 0.27386 0.27468 0.27523	PL/PTP 0.39178 0.39178 0.39059 0.39761 0.39880 0.39960	X/DMAX 0.39000 0.43100 0.44900 0.48600 0.52200			
MAND LT INNI VD HI RD 107 112 22 27 137 142	15.081 AL PRESSIME PL 14.786 14.731 14.741 15.006 15.051 15.081	0,99571 PATIOS - FOR PL/PO 0.97624 0,97261 0.97327 0.99373 0.99571	0.27523 PEPCDY INLEY PL/PTF 0.26985 0.26983 0.27386 0.27468 0.27523	PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39940	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.57800			
ADD [T IDNA /D WI.RD 107 112 127 127 137 142	15.081 PL 14.786 14.781 14.781 15.006 15.051 15.091 15.091	0,99571  PATIOS - FOR  PL/PO 0.97624 0,97327 0.99373 0.99373 0.99571 1.0013	0.27523 PEPCDY [NLET PL/PTF 0.26985 0.26984 0.26903 0.27386 0.27386 0.27468 0.27523	PL/PTP 0.39178 0.39178 0.39059 0.39761 0.39880 0.39960	X/DMAX 0.39000 0.43100 0.44900 0.48600 0.52200			
DADD LT ION/ VD HI AD 107 112 22 127 137 142 157	15.081 AL PRESSIME PL 14.786 14.731 14.741 15.006 15.051 15.081	0,99571  PATIOS - FOR  PL/PO 0.97624 0,97261 0.97327 0.99373 0.99571 2:0019 1.0017	0.27523 EPPCDY [NLET PL/PTF 0.26985 0.26984 0.26593 0.27386 0.27468 0.27523 0.27523	PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39840 0.39840	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800			
DAND LT INNI  VD WI-RD 107 112 127 137 142 142 143 145 145 145 145 145 145 145 145 145 145	PL 14.786 14.786 14.781 14.781 15.906 15.051 15.981 19.160 15.171	0,99571  PATIOS - FOR  PL/PO 0.97624 0,97621 0.97327 0.99076 0.99373 0.99571 1.0017	0.27523 EPPDY INLET PL/PTF 0.26985 0.26983 0.27586 0.27386 0.27468 0.27523 0.27523	PL/PTP 0.39178 0.39178 0.39059 0.39761 0.39880 0.39960 0.39960	x/DMAX 0.39800 0.49100 0.44900 0.52200 0.57800 1.0000			
ADD [T ION]  /D WI-RD  107  112  27  137  42  142  152  /D WORD  152	PL 14. 786 14. 731 14. 741 15. 906 15. 951 15. 981 15. 166 PL 15. 166 15. 166	0,99571  PAYIOS - FOR  PL/PO 0.97624 0.97327 0.99076 0.99373 0.99571 1.9917 1.9917	0.27523 PL/PTF 0.26985 0.26984 0.26903 0.27386 0.27468 0.27523 0.27523	PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39960 0.49195 0.40198	X/DMAX 0.39800 0.43190 0.44900 0.48600 0.52200 0.58600 1.0000			
DAND LT INNA VD NI RD 107 112 127 137 142 142 143 144 144 144 144 144 144 144 144 144	PL 14.786 14.786 14.781 14.781 15.906 15.051 15.081 19.100 16.171 M. PRESSURE PL 15.166	0,99571  PATIOS - FOR  PL/PO 0.97624 0,97261 0.97327 0.99373 0.99571 2:0019 1.0017	0.27523 PEPCDY INLEY  PL/PTF 0.26985 0.26983 0.27386 0.27468 0.27523 0.27523 0.27567	PL/PTP 0.39960  PL/PTP 0.39178 0.39059 0.39761 0.39880 0.3980 0.3980	x/DMAX 0.39800 0.49100 0.44900 0.52200 0.57800 1.0000			
DAND LT INN/ PD WI AD 107 112 27 127 137 142 152 157 100 WORD 152 157	PL 14.786 14.786 14.781 14.781 15.906 15.051 15.081 19.100 16.171 M. PRESSURE PL 15.166	0,99571  PAYIOS - FOR  PL/PO 0.97624 0.97327 0.99076 0.99373 0.99571 1.9917 1.9917	0.27523 PEPCDY INLEY  PL/PTF 0.26985 0.26983 0.27386 0.27468 0.27523 0.27523 0.27567	PL/PTP 0.39960  PL/PTP 0.39178 0.39059 0.39761 0.39880 0.3980 0.3980	X/DMAX 0.39800 0.43190 0.44900 0.48600 0.52200 0.58600 1.0000			
PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRETTIONS  PARRE	PL 14.786 14.781 14.781 15.006 15.051 15.061 15.051 15.061 15.166 15.171 AL PRESSUPF	0,99571  PATIOS . FOR  PL/PO 0.97624 0,97261 0.97327 0.99076 0.99373 0.99571 1.0017 1.0017 1.0017 PATIOS . 20 PL/PO	0.27523 PEPCDY INLEY PL/PTF 0.26985 0.26985 0.27686 0.27386 0.27386 0.27523 0.27523 0.27523 0.27527 0.27687 DEG SHROUD I	PL/PTP 0.39960  PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960	X/DMAX 0.39800 0.43190 0.44900 0.52200 0.57800 1.0000 -1.0000			
PARRETTIONS  VP WIRD  107  112  127  137  142  157  PARRETTIONS  VP WORD  152  PARRETTIONS  VP WORD  167	PL 14.786 14.786 14.781 14.781 15.906 15.051 15.981 17.166 15.171  AL PRESSUPF PL 15.176	0,99571  PATIOS - FOR  PL/PO 0.97624 0,97261 0.97327 0.99373 0.99571 1.0017  PATIOS - FOR 1.0017  PATIOS - 20  PL/PO 1.0020	0.27523 PEPCDY INLEY PL/PTF 0.26985 0.26983 0.27386 0.27468 0.27468 0.27523 0.27567 0.27687 DEG SHROUD I PI/PTF 0.27696	PL/PTP 0.39960  PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39960 0.39960 0.39400 0.40185 0.40185 0.40185 0.40211	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 10000 x/DMAX -1.0000 -1.0000			
PARRETTIONS  VD WIRD  107  112  127  137  142  157  PARRETTIONS  VD WORD  159  PARRETTIONS  VD WORD  157	PL 14.786 14.781 14.781 15.006 15.051 15.061 15.051 15.061 15.166 15.171 AL PRESSUPF	0,99571  PATIOS . FOR  PL/PO 0.97624 0,97261 0.97327 0.99076 0.99373 0.99571 1.0017 1.0017 1.0017 PATIOS . 20 PL/PO	0.27523 PEPCDY INLEY PL/PTF 0.26985 0.26985 0.27686 0.27386 0.27386 0.27523 0.27523 0.27523 0.27527 0.27687 DEG SHROUD I	PL/PTP 0.39960  PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960 0.39960	X/DMAX 0.39800 0.43190 0.44900 0.52200 0.57800 1.0000 -1.0000			
DAND LT ION/ VD WI-RD 107 112 127 127 127 142 142 152 2001110W VD WORD 152 157 20001110W VD WOSD 167 172	PL 14.786 14.781 14.781 15.006 15.051 15.051 15.061 15.071 17.160 15.171 AL PRESSURE	0,99571  PATIOS - FOR  PL/PO 0.97624 0,97261 0.97327 0.99373 0.99571 1.0017  PATIOS - FOR 1.0017  PATIOS - 20  PL/PO 1.0020	0.27523 PEPCDY INLEY  PL/PTF 0.26985 0.26985 0.27689 0.27386 0.27469 0.27523 0.7767 0.27687  DEG SHROUD 1  PI/PTE 0.27687	PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39960 0.40195 0.40195 0.40185 0.40185 0.40185 0.40185 0.40185 0.40185 0.40185 0.4018	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 10000 x/DMAX -1.0000 -1.0000			
2000   TINNA YO KI RD 107 112 127 127 127 142 142 143 144 145 200   TINNA YO WORD 167 200   TINNA YO WORD 167 200   TINNA YO WORD 167 200   TINNA YO WORD	PL 14.786 14.786 14.781 14.781 15.006 15.051 15.091 19.100 15.171 ML PRESSUPE PL 15.176 15.171 AL PRESSUPE PL 15.176 15.171 AL PRESSUPE PL	0,99571  PATINS . FOR  PL/PN 0.97624 0,97624 0,97627 0.9976 0.99373 0.99571 1.0017  PATINS . 20  PL/PN 1.0020 1.0017  PATINS . 80  PL/PN	0.27523 PEPCDY INLEY PL/PTF 0.26985 0.27686 0.27687 0.27523 0.77523 0.77523 0.77687 DEG SHROUD I PI/PTE 0.27687 DEG SHROUD I PI/PTE	PL/PTP 0.39960  PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39960 0.40195 0.40185 0.40185 0.40211 0.40198	X/DMAX 0.39800 0.43190 0.44900 0.48600 0.52200 0.578000 1.0000  X/DMAX -1.0000 -1.0000  X/DMAX 0.79300 0.84400			
PARRITIONS  VO WIRD  107  112  127  137  142  142  152  157  PARRITIONS  VO WORD  167  177  PARRITIONS  VO WORD  167  179  PARRITIONS	PL 14.786 14.781 14.781 15.006 15.051 15.061 15.051 15.166 15.171 AL PRESSUPF PL 15.176 15.171 AL PRESSUPF PL 14.996	0,99571  PATIOS . FOR  PL/PO 0.97624 0,97261 0.97327 0.99076 0.99373 0.99571 1.0017  PATIOS . 20  PL/PO 1.0020 1.0017  PATIOS . RO  PL/PO 0.99010	0.27523 PEPCDY INLEY PL/PTF 0.26985 0.26985 0.26983 0.27386 0.27523 0.27523 0.27523 0.27523 0.27687 DFG SHROUD 1 PI /PTF 0.27368	PL/PTP 0.39960  PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39960 0.49199 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198 0.40198	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.57800 1.0000 -1.0000 X/DMAX 0.79300 0.64400			
2000   T   TONY  VD   WI & D  107  117  129  127  137  142  157  2001   TONY  VD   WORD  157  2001   TONY  VD   WORD  187  187	PL 15.06 15.071 15.006 15.071 15.006 15.071 15.166 15.171 AL PRESSUPE PL 15.176 15.176 15.171 AL PRESSUPE PL 14.996 14.606	0,99571  PATINS . FOR  PL/PN 0.97624 0,97624 0,97627 0.9976 0.99373 0.99571 1.0017  PATINS . 20  PL/PN 1.0020 1.0017  PATINS . 80  PL/PN	0.27523 PEPCDY INLEY PL/PTF 0.26985 0.26985 0.2786 0.27386 0.27386 0.27523 0.27523 0.27527 0.27687 DEG SHROUD I PI/PTF 0.27687 DEG SHROUD L PI/PTF 0.27368 0.27368	PL/PTP 0.39960  PL/PTP 0.39178 0.39059 0.39761 0.39880 0.39960 0.40195 0.40185 0.40185 0.40211 0.40198	X/DMAX 0.39800 0.43190 0.44900 0.48600 0.52200 0.578000 1.0000  X/DMAX -1.0000 -1.0000  X/DMAX 0.79300 0.84400			

>&NO TT (ANA) 300 HAPA 32 37 47	PI.	RATIOS . PPT	HAPY PEUG					
~? *7 47			-					
~? *7 47		Pt /Pil	PL /PTF	PL /PTP	X/DMAY		-	
² 7 47	10.976	0. 72345	0.19479	0.27066	0.72200			
47	19.332	1.2743	0.37548	0.47674	0. 02000			
	16.202	1.0680	0.27278	3,39655	7.41400			
	13.012	).A5765	0.21506	0.32086	1.0170			
SATOLT LUNA	PRESSUPE	RETINS . FIR	W SPLITTER I	• n•				
AU MUBU	PL	PL / PO	PL/PTF	PL /PTP	x /OMA x			
62	27.569	1.8172	0.46415	0.67984	0.42200			
47	21.753	1,4338	0.36622	0.53641	9-67009			
AMOLT FOCA	L PRESSUPE	PATIOS . FLO	W SPLITTED P	1. D.				
ለሁ ጠብቴህ	PL	PL/PO	PL/PTF	PL /PTP	X/DMA X			
77	14-117	0, 93050	0.~3767	0,34812	0.50000			
92	19.957	1.3155	0.33600	0.49215	0.58300			
92	15.212	1.0227	0.25611	0.37513	0.67000			
-		antion 4 the						
עט אטאט יי	PL.	PL/PO	PL/PTF	PLARA	X/DMAX	9		
107	14.842	0:01830	0.24988	0.36600	-1.0000			
11?	14.787	0.0746	9.74895	0.36465	-1.0000			
122	14.812	0.924	0.7 -037	J.36526	-1.0000			
127	15.072	0. 99347	0. 25775	G-37168	-1.0000			
137	-19:127	0.99709	0.25468	0.31-02	-1.0000			
162	15.177	1.7701	0.25544	0.37414	1.0000			
>ADDITIONAL	L PRESSURE	RATIOS . FOR	ERODY INLET					
AU MUBU	Pt	PL /PO	Pt / PTF	PL/PTP	X/DMAX			
	14.842							
197		7.97837	0.249RR	0.36600	0.39M00			
112	14.797	7. 97468	0.24895	0.36465	9-43100			
2י ו	14.912	0.97637	0.74937	0.36526	0.44900			
127	15,072	1,99347	0.25375	0.37169	0.48600			
137	15.127	J. 9970a	3.25469	0.37303	0.52200			
147	15.172	1.9991	0.25544	0.37414	U. 5 #800			
1-5	15.207	1.0024	0.25603	0.37501	-1.0000		•	
147	15.237	1.0924	0∙ इनस्त्र-	0.37903	-1.0000			
TODE TOM	_ PRECEURE	AATUOS , FAM	-NO2715-5145	<u> </u>				
AU AUBD	PL	- Maria	BL###F	PLIPTP	K/DMAX			
152	15.207	1:0724	77-24643	0.37. 71	-1.0000			
157	-17.237	1.0024	1.256-33	9.37501	-1-0000			
AND TT FORM	PRESSUPE	RATIOS , 7	DEG SHROUP I	PCAT FON				
VP WPRN	Pl	PL / PTI	PL/PTF	PL /PTP	X/DMAX			
1+7	15.212	1.0027	0.25611	0.3751?	0.79300		~	
172	15.237	1.0024	0.25603	2.37501	0.84400			
>APDITIONA:		RATIOS - 55		PCATEON				
VD WORD			PL /PTF	Pt /PTP	X/DMAX			
	P1	P[ /Pf]						
[82	14.997	0.98810	7.25241	0.36970	0.79300			
187	14.597	0.96116	0.24550	0.35959	0.84400			
	. MFASHRED	THRUST PAPAM	FTERS					

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>&ODETEDNA &VD WOPD 32 -7 47 -52	P1 11.345	PI/PO							
32 27 47	11.345								
32 27 47	11.345		DI / DTF	PI /PTP	X/DMAX				
47		0.72628	0.18521	0.27061	9.72200				
47 .	19.371	1.2737	0.72482	0.47460	0. 02000				
	16.256	1.0629	0.27258	0.39828	0.91900				
č	13.091	0. 86014	0.21934	0.37049	1.0170				
>£001TIONA	[ PBFSSUPF	PATIOS . FLO	W SPLITTEP I	• n•					
AVO WOPD	PL	ቦቲ / ቀኅ	PI /PTF	PI /PTP	7/D#A7				
62	27-646	1-8179	0.46358	0.67735	0.42200				
67	21.411	1.4742	0.36573	0.53438	0.67000				
SAPOLT LUNAL	L PRESSUPF	RATIOS . FLD	H SPITTER C	•n•					
TAD MUND	PL	PL / PD	OL /PTF	PL /PTP	x/DMAY		•		
77	14.221	0.93511	9.23846	0.34942	0.5080C				
97	20.176	1.3771	0.33714	0.49261	J.5#300				
32	15.245	1.0225	9.25565	0.37354	2-67999				<del></del>
740011104V	L POESSURE	AATIOS FJF	<del>CTOR SUROUR</del>						
NO MUND	~	PL/P0	PL/PTF	PLANT	7/044X				
-197	14.88	0.97851	0.24052	0.36459	-1.0000				
		0.97490	26.25.61	0.36325	-1-0000				
112	14-826								
-122	14.946	2.9267	0.24894	0.36374	-1.0000				
-127	15.116	3, 99397	0.24267	0.37035	-1.0000				
-1?7	14.166	0.99725	0.25431	0.37158	-1-0000				
-1.52	15.216	1.0095	0.25-15	0.37200	-1.0000			-	•
>ADDIT 10MA	L PRESSURE	PATINS . FOR	ERONY INLEY						
AVD WORD	PL .	PL/P0	PL/PTF	PL/PTP	x/Dmyx				
107	14.981	0.97951	0. 24 453	0.36459			•		
-					3.39000				
112	14. 726	0.97490	0.24761	0.36325	0.43100				
123	14.946	9. 37621	0.24494	0.36374	0.44980				
.127	15_116	0.29397	0.25247	0.37935	0.45600				
137	15.166	0.99725	0.25431	0.3715P	0.522 <b>0</b> 0				
142	15.216	1.0705	0.25515	0.37280	Ú-58800				
1 9 2	17.841	1.1724		3.37700	<del>-1.9999 -</del>				
157	17.240		<del></del>				4.0		
STATE TOWN	Fuerther.	**************************************							
AD MUND	PL	PYPA		PL /PYP	X/DMAX			-	
-152	15.251	1:1777	U-796-32	0.37366	-1. 3000				
157	15.246	1.0025	0.25565	0.37-5	-1-0000				
SAPOLT LONA	L PRESSURE	PATINS . 20	DEG SHAPUD I	PEATINN					
IVO MUBO	PL	Pt /PO	P1 / PTF	PI /PTP	Y/DMAX				
167	15.241	1.0927	0-2556	0.37347	0. 79300				
172	15.246	1.0025	0.25565	0.27354	0.14500				
		PATIOS . NO							
_5_5****									
	PI	Pt / Pri	PI /PTF	PI /PTP	X/DMAY				
	15 631	A 08777		0.36803	o. 79300				
197	15.021	0.98772	0.25188						
147	14.601	0.96010	0.24483	0.35773	D. #4400				
197 197	14.601 . MEASIRED	0.96010 THPUST PARAM	0.24483	0.35773	0.84400	2.3803 CI	FM 7.7771197		

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7454-1 F415	F PRFL 141	NAPY PATA	04/13/79	CADDELL	PEC 10/25/7	9 01:12:13.943	FAC RYEXT	PG= CO34	PC 1491
SAPOITIONA	AL PRESSIBE	PATINS . PPI	MARY PHUG						
AVD HORD	PL	PI / PO	PI /PTF	PL /PTP	X/DMAY				
3.2	19.640	0.73106	0.19350	0.28101	3.72200				
37	18.905	1.2456	0.34380	0.49930	0.92000				
47	14.521	9.05674	0.26407	0.38350	J. 91900				
52	16.971	1.1116	9-30680	0.44556	1.0170				
> ADD I T I DNA	AL PRESSURE	PATINS , FLO	W SPLITTER I	.n.				· · · · · · · · · · · · · · · · · · ·	
		PL/PO	Pt / PTF	PL /PTP	w 40M A w				
NO WORD	PL				X/DMAX				
62	25.929	1.7784	9.47154	0.68481	0.42200				-
67	20.855	1.3741	0.37926	G.55079	J.67000				
>ADDITIONA	AL PRESSUPE	RATIOS . FLO	M CAFILLED U	.n.					
VP WPP	PL	PL /PN	PL / PTF	PL /PTP	X/DHAX				
77	13,176	0.86812	0.23961	0.3479R	0.50800			•	
A2	18.525	1.2796	0.37690	0.48924	0.58300		***		•
92	15.201	1.0015	0.27644	0.40146	0-67000				
>4001 T 10NA	IL PRESSURE	RATTUS : FUF	CIUR SHRIMM						
VD WORD		m /00	PL /PTF	PLANTS	X/DMAX				
	P	PL/PN						+	
107	14.011	0.97585	0.26934	0.39116	-1.0000	_			
112	14.756	0. 97223	0.26H34	0.38971	-1.0000	<u>.</u>			
122	14.776	0-9754	025671	0-39024	-1.0000				
		0.99100	0.27753	0.39773	-1.0000				
127	15 <u>.051</u>					and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		· ·	
-127		0. 99430	0.27444	0.39855	-1.0000			•	<del> </del>
-127 -137								•	
-127 -137 -162	15.126	0. 99430	0.27444	0.39855	-1.0000			· · · ·	
-127 -137 -152 >ADDIT IDNA	15.126	0. 99430 0. 99660	0.27444	0.39855	-1.0000			· · · · · · · · · · · · · · · · · · ·	
-127 -137 -162	15.126	0.99430 0.99660 PATEOS , FPR	0.27444 0.27507 ERCOY THEFT	0.39948	-1.0000 1.0000		ī		
>ADDIT ICHA	15.126 15.126 IL PRESSURE PL 14.811	0. 99430 0. 99660 PATEOS , FOR PL/PO 0. 97585	0.27444 0.27507 ERCOV INLET PL/PTF 0.26934	0.39948 0.39948 PI /PTP 0.39116	-1.0000 -1.0000 X/DMAX 0.39800		ī	· · · · · · · · · · · · · · · · · · ·	
-127 -137 -152 	75.091 15.126 IL PRESSIRE PL 14.811 14.756	0.99430 0.99660 PATEOS , FOR PL/PO 0.97585 0.97223	0.27444 0.27507 ERCOV INLET PL/PTF 0.26934 0.26934	0.39948 0.39948 PI /PTP 0.39116 0.38971	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		ī.		
-127 -137 -162 >ADDIT IPNA AVD WORD 107 112 122	PL 14-711 14-756 14-776	0.99430 0.99660 PATEOS , FOR PL/PO 0.97585 0.97535	0.27444 0.27507 ERCOV INLET PL/PTF 0.26934 0.26834 0.26871	0.39948 0.39948 PI /PTP 0.39116 0.3971 0.39024	#/DMAX 0.39800 0.43100		τ	· · · · · · · · · · · · · · · · · · ·	
-127 -137 -162 >ANDITIONA AVO WORD 107 112 122 127	PRESSIRE  14.911  14.756  14.776  15.041	0.99430 0.99660 PATEOS , FOR PL/PO 0.97585 0.97223 0.97354 0.99100	0.27444 0.27507 ERCOV INLET PL/PTF 0.26034 0.26836 0.26871 0.27353	0.39948 0.39948 PI /PTP 0.39116 0.39971 0.39024 0.39723	X/DMAX 0.39800 0.43100 0.48600		1		
127 137 162 >ARDIT IPMA 107 WORD 107 112 122 127 127	PRESSIRE  14.811 14.756 14.776 15.041 15.391	0. 99430 0. 99660 PATIOS , FOR PL/PN 0. 97585 0. 97384 0. 99100 0. 99430	0.27444 0.27507 ERPDY INLET PL/PTF 0.26934 0.26834 0.26834 0.27353 0.27444	0.39948 0.39948 PI /PTP 0.39116 0.39771 0.39024 0.39723 0.39855	1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200		<b>t</b>		
127 137 162 >ARDIT IPMA 107 112 122 127 127 142	PL 14-811 14-756 14-776 15-041 15-126	0. 99430 0. 99660 PATEOS , FOR PL/PO 0. 97585 0. 97374 0. 99100 0. 99430 0. 99660	0.27444 0.27507 ERCOV INLET PL/PTF 0.26434 0.26471 0.27353 0.27444 0.27507	0.39948 0.39948 PI/PTP 0.39116 0.3971 0.39024 0.39723 0.39855 0.3948	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200		ī		
127 137 162 >ADDIT IONA VO WORD	PRESSIRE  14.811 14.756 14.776 15.041 15.391	0. 99430 0. 99660 PATIOS , FOR PL/PN 0. 97585 0. 97384 0. 99100 0. 99430	0.27444 0.27507 ERPDY INLET PL/PTF 0.26934 0.26834 0.26834 0.27353 0.27444	0.39948 0.39948 PI /PTP 0.39116 0.39771 0.39024 0.39723 0.39855	1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200		ŧ		
127 137 162 >ARDIT IPMA IVN WORD 107 112 122 127 127 127	PL 14-811 14-756 14-776 15-041 15-126 15-126 15-126 15-126	0. 99430 0. 99660 PATEOS , FOR PL/PO 0. 97585 0. 97585 0. 97354 0. 99100 0. 99660 1. 99660	0.27444 0.27507 ERCOV INLET PL/PTF 0.26934 0.26834 0.26871 0.27353 0.27444 0.27507 0.27507	0.39048 0.39948 PI /PTP 0.39116 0.39971 0.39024 0.39723 0.39855 0.39948	1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.59800		1		
-127 -137 -162 >ANDIT IPMA BAYN WORD 107 112 122 127 127 147	PRESSURE PL 14.811 14.756 14.776 15.041 15.126 15.126 15.126	0.99430 0.99660 PATIOS , FOR PL/PO 0.97585 0.97354 0.97354 0.99100 0.99430 0.99430 0.99660 1.99660	0.27444 0.27507 ERCOV INLET PL/PTF 0.26934 0.26834 0.26871 0.27353 0.27444 0.27507 0.27507	0.39048 0.39948 PI /PTP 0.39116 0.39024 0.39723 0.39855 0.39948 0.40133	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.59800 1.0000		T		
127 137 162  >ANDIT INNA VN WORD 107 112 127 127 127 147	PL 14.911 15.126 14.911 14.756 14.776 15.041 15.126 15.126 15.126 15.126 15.126	0. 99430 0. 99660 PATEOS , FOR PL/PO 0. 97585 0. 97585 0. 97354 0. 99100 0. 99400 0. 99400 1. 99460 1. 99460 1. 99460	0.27444 0.27507 ERCOV INLET PL/PTF 0.26934 0.26831 0.26871 0.27353 0.27444 0.27507 0.27507	0.39048  PI /PTP 0.39116 0.39024 0.39723 0.39855 0.3948 0.40133	*/DMAX 0.39800 0.43100 0.52200 0.59800 1.3000 1.3000		1		
127 137 162  >ARDIT IPMA IVN WORD 107 112 122 127 127 147 147 149	PRESSURE PL 14.811 14.756 14.776 15.041 15.126 15.126 15.126	0.99430 0.99660 PATIOS , FOR PL/PO 0.97585 0.97354 0.97354 0.99100 0.99430 0.99430 0.99660 1.99660	0.27444 0.27507 ERCDY INLET PL/PTF 0.26934 0.26831 0.27837 0.27444 0.27507 0.27507	0.39048 0.39948 PI /PTP 0.39116 0.39024 0.39723 0.39855 0.39948 0.40133	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.59800 1.0000		*		
127 137 162  >ANDITIONA  VN HORD 107 112 127 127 127 147 147 157 157 169 VN HOPD 159 157	PL 14.811 14.756 14.776 15.041 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97585 0. 97384 0. 99100 0. 99400 0. 99600 1. 9940 1.  0.27444 0.27507 ERCOV INLET PL/PTF 0.26934 0.26831 0.27833 0.27444 0.27507 0.27507 0.27507 0.27507 0.27507 0.27507 0.27507 0.27507 0.27507	0.39048  0.39948  PI /PTP 0.39116 0.39074 0.39723 0.39855 0.39948 0.40133 0.40133 0.40133	-1.0000 1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.59800 1.3000 X/DMAX -1.0000		T			
127 137 162  >ADDIT IONA  VO WORD 107 112 122 127 127 127 142 157 142  >ADDIT IONA  VD WORD 152 157 >ADDIT IONA	PL 14-811 14-756 14-776 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97585 0. 97354 0. 99430 0. 99430 0. 99430 0. 99430 0. 99430 1. 99450 1. 99	0.27444 9.27507 ERCOV INLET PL/PTF 0.26934 0.26871 0.27353 0.27444 0.27507 0.27507 0.27507 0.27435 0.27435 0.27435	0.39048  0.39948  PI /PTP 0.39116 0.39713 0.39024 0.39723 0.39855 0.39948 0.40133 0.40133 0.40133	-1.0000 1.0000 1.0000 0.39800 0.43100 0.44900 0.52200 0.59800 1.3000 1.3000 1.0000 -1.0000		T		
127 137 162  >ARRITINA  VO WORD 107 112 122 127 142 157 142	PL 15.126  14.776 14.776 15.041 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97585 0. 97585 0. 97585 0. 97585 0. 99430 0. 99430 0. 99430 0. 99430 0. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99	0.27444 0.27507 ERCDY INLET PL/PTF 0.26934 0.26831 0.27353 0.27444 0.27507 0.27507 0.27507 0.27507 0.27507 0.27507	0.39048  PI /PTP 0.39116 0.3971 0.39024 0.39723 0.39723 0.39024 0.40123 0.40123  PL/PTP 0.40123 0.47123	-1.0000 1.0000 1.0000 0.39800 0.43100 0.44900 0.52200 0.59800 1.0000 1.0000 -1.0000		T		
127 137  >ADDIT IONA  VO WORD  107 112 127 127 127 142	PL 14.776 14.776 15.041 15.126 14.776 15.041 15.126 15.126 15.126 15.126 15.126 15.126	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97585 0. 97354 0. 99430 0. 99430 0. 99430 0. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99	0.27444 9.27507 ERCDY INLET PL/PTE 0.26934 0.26831 0.27435 0.27444 0.27507 0.27507 0.27507 0.27507 0.27507 0.27507 0.27507	0.39048 0.39948  PI /PTP 0.39116 0.39074 0.39723 0.39855 0.39948 0.40133 0.40133 0.40133 0.40133 0.40133	*/DMAX 0.39800 0.43100 0.44900 0.52200 0.59800 1.9000 */DMAX -1.0000 -1.9000				
127 137 162 >ADDIT IONA VO WORD 107 112 127 127 127 142 157 >ADDIT IONA VD WORD 159 157 >ADDIT IONA VD WORD 167 172	PL 15.196 15.196 15.196 15.196 15.196 15.196 15.196 15.196 15.196 15.196 15.196	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97585 0. 97354 0. 99100 0. 99430 0. 99430 0. 99430 0. 99430 1. 99160 1. 9912 1. 9912 1. 9912 1. 9912 1. 9912 1. 9912 1. 9912 1. 9912 1. 9912 1. 9915	0.27444 0.27507 ERCOV INLET PL/PTF 0.26934 0.26831 0.27353 0.27444 0.27507 0.27507 0.27507 0.27635 DEG SHROUD L PL/PTF 0.27635 0.27635	0.39048 0.39948 PI /PTP 0.39116 0.39713 0.39024 0.39723 0.39048 0.40133 0.40133 0.40146	-1.0000 1.0000 1.0000 0.39800 0.43100 0.44900 0.52200 0.59800 1.0000 1.0000 -1.0000		•		
127 137 162  >ADDIT IONA  VO WORD 107 112 127 127 127 142 157 157  >ADDIT IONA  VD WORD 159 157  >ADDIT IONA  VD WORD 167 172	PL 15.196 15.196 15.196 15.196 15.196 15.196 15.196 15.196 15.196 15.196 15.196	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97585 0. 97354 0. 99430 0. 99430 0. 99430 0. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99430 1. 99	0.27444 0.27507 ERCOV INLET PL/PTF 0.26934 0.26831 0.27353 0.27444 0.27507 0.27507 0.27507 0.27635 DEG SHROUD L PL/PTF 0.27635 0.27635	0.39048 0.39948 PI /PTP 0.39116 0.39713 0.39024 0.39723 0.39048 0.40133 0.40133 0.40146	*/DMAX 0.39800 0.43100 0.44900 0.52200 0.59800 1.9000 */DMAX -1.0000 -1.9000		T		
-127 -137 -142 -152 -17 -17 -17 -17 -17 -17 -17 -17 -17 -17	PL 14-811 14-756 14-776 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97384 0. 99100 0. 99430 0. 99430 0. 9960 1. 9942 1. 9912 1.	0.27444 0.27507  ERCOV INLET PL/PTF 0.26934 0.26834 0.26871 0.27353 0.27444 0.27507 0.77444 0.27507 0.77445 0.27535 0.27644 0.27535 0.27635 0.27635 0.27644 0.27635 0.27644 0.27635	0.39948 0.39948 0.39948 0.39116 0.3971 0.39074 0.39723 0.39855 0.39855 0.39848 0.40133 0.40133 0.40133 0.40146 0.40133 0.40146	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		•		
-127 -137 -162 -162 -17 -162 -17 -12 -12 -12 -12 -12 -12 -12 -12 -12 -12	PL 14.811 14.756 14.776 15.041 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126 15.126	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97585 0. 97354 0. 99430 0. 99430 0. 99430 0. 99430 0. 99430 1. 99100 PL/PO 1. 99100 PL/PO 1. 99100 PL/PO 1. 99100	0.27444 0.27507  ERCOV INLET PL/PTF 0.26934 0.26834 0.26871 0.27353 0.27444 0.27507 0.27435 0.27435 DEG SHROUD L PL/PTF 0.27635 0.27644 DEG SHROUD 1 PL/PTF 0.27325	0.39685 0.39948 0.39948 0.39116 0.39713 0.39024 0.39723 0.39855 0.39048 0.40133 0.40123 0.40133 0.40146 0.40133 0.40146 0.40133 0.40146	-1.0000 1.0000 1.0000 0.39800 0.43100 0.44900 0.52200 0.59800 1.3982 1.0000 -1.0000 -1.9000				
-127 -137 -162 -162 -167 -197 -107 -112 -127 -127 -127 -127 -127 -127 -12	PL 14-811 14-756 14-776 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126 15-126	0. 99430 0. 99660 PATIOS , FOR PL/PO 0. 97585 0. 97384 0. 99100 0. 99430 0. 99430 0. 9960 1. 9942 1. 9912 1.	0.27444 0.27507  ERCOV INLET PL/PTF 0.26934 0.26834 0.26871 0.27353 0.27444 0.27507 0.77444 0.27507 0.77445 0.27535 0.27644 0.27535 0.27635 0.27635 0.27644 0.27635 0.27644 0.27635	0.39948 0.39948 0.39948 0.39116 0.3971 0.39074 0.39723 0.39855 0.39855 0.39848 0.40133 0.40133 0.40133 0.40146 0.40133 0.40146	-1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				

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	S PRELIM	INARY DATA	06/13/79	CARRELI	REC 10/25/79 01:14:31.799	FAF RX6X1	PG4 C034 PNG 1492
SENDITION	AL PRESSUPE	PATIOS . PRI	MARY PILIG				
AVD WORD	PĮ	PL / PO	PL /PTF	PL /PTP	X/DMAX		
32	9.1781	0.67268	0.19299	0.28255	ú.72200		
37	14.441	0.94F25	0.30365	0.44457	0.82000		
47	11.935	0.75370	0 25096	0.36742	0. 91900		
52	17.796	1.1359	0.36369	0.53248	1-0170		
>ADDITIONA	AL PRESSURE	RATIOS . FLO	W SPLITTER I	. n.			
ORDW OVA	PL.	PI /PI	PI /PTF	PL /PTP	X/DMAX		•
52	22.347	1.4490	0.46400	0.67934	0.42200		_
67	1 7.406	1.1430	9.36609	0.53586	V-67000		
NOT TECOM	AL PRESSURE	PATIOS . FLO	W SPLITTER O	. D.			
AVD WOED	Pt	PL /PD	PI / PTF	PL /PTP	X/DMAX		
77	11.360	0-74592	D. 23886	0.34971	0.50800		
A2	15.991	1.0501	0.37525	0.49230	0.58300		
92	15.256	1-0216	0.32079	0-46967	Q.6 7000		
<b>→4<u>98L₹10</u>N</b>	<del>4L PRESSURE</del>	**************************************	CEOP : SHPOUR :				
				31 03	, 45ma v		
AVD WORD . -107	PL	PL/PD	PL/PJF	1 6776	X/DBAX		and the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o
-107 -112	14.866	0.97222	0.31250	0.45766	-1.0000		
-122	14.806	0.97774	2.31132	0.45581	-1.0000		
-127 -	14.926 15.086	0.99061	0.31721	0.45642	-1.0900 -1.0000		
-137	14.000	0.99357	0.3171	0.46572	1.0000		The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th
-162	15.156	0.99521	0.31869		-1.6000		
		PATIOS . FOR	PL/PTF	PL/PTE	x/DMAX		
AVD WORD	. PL				0.30000		
107	14.966	0.97616	0.31259	0.45766	0.39800		
107 112	14.866	0.97616	0.31132	0.45581	0.43190		
107 112 122	14.866 14.806 14.826	0.97616 0.97222 0.97354	0.31132	0.45581_			
107 112 122 127	14.866 14.806 14.826 15_086	0.97616 0.97222 0.97354 0.99061	0.31132 0.31174 0.31721	0.45581 0.45642 0.46443	0.431 <u>00</u> 0.44900 0.48600		
107 112 122 127	14.866 14.806 14.826 15.086 15.131	0.97616 0.97222 0.97354 0.99061 0.99357	0.31132 0.31174 0.31721 0.31816	0.45581 0.45642 0.46582 0.46582	0.43190 0.44900 0.49600 0.52200		
107 112 122 127 137 142	14.866 14.806 14.826 15.086 15.131 15.156	0.97616 0.97222 0.97354 0.99061 0.99357 0.99521	0.31174 0.31174 0.31721 0.31816 0.31869	0.45581 0.45642 0.46582 0.46582 0.46658	0.43100 0.44900 0.48600 0.52200 0.58800		
107 112 122 127 137 142	14.966 14.806 14.826 15.086 15.131 15.156	0.97616 0.97222 0.97354 0.99061 0.99357 0.97521	0.31132 0.31174 0.31721 2.31816 0.31869	0.45581 0.45642 0.46543 0.46582 0.46659	0.43100 0.44900 0.49600 0.52200 0.58800		
107 112 122 127 137 142	14.966 14.806 14.806 15.086 15.131 15.156 15.236	0.97616 0.9722 0.97354 0.99061 0.99357 0.99521 1.9997	0.31132 0.31174 0.31721 0.31721 0.31760 0.32070	0.45581 0.45642 0.46582 0.46582 0.46658	0.43100 0.44900 0.48600 0.52200 0.58800	-	
107 112 122 127 137 142 153	14.966 14.806 14.826 15.086 15.131 15.156 15.236 15.231	0.97616 0.97722 0.97354 0.99061 0.99357 0.9957 1.9991	0.31132 0.31174 0.31721 2.31721 2.31760 0.31760 0.32070	0.45581 0.45642 0.46543 0.46582 0.46580 0.46650	0.43100 0.44900 0.48600 0.52200 0.58800 1.0000	-	
197 112 122 127 137 142 143 143 144 147	14.966 14.806 14.806 15.086 15.131 15.156 15.236 15.231	0.97616 0.97222 0.97354 0.99061 0.99357 0.99357 1.9097 1.0909	0.31132 0.31174 0.31721 2.31816 0.31860 0.32080	0.45581 0.45642 0.46582 0.46582 0.46580 0.46782	0.43100 0.44900 0.48600 0.52200 0.58800 1.0000	-	
107 112 122 127 137 142 157 -A0017 INM	14.966 14.806 14.826 15.086 15.131 15.156 15.236 15.231	0.97616 0.97722 0.97354 0.99061 0.99357 0.9957 1.9991	0.31132 0.31174 0.31721 0.31761 0.31760 0.32070 0.32070 0.32070	0.45581 0.45642 0.46543 0.46582 0.46580 0.46650	0.43100 0.44900 0.48600 0.52200 0.58800 1.0000		
107 112 122 127 137 142 142 143 144 145 147 148 148 148 148 148 148 148 148 148 148	14.966 14.806 14.806 15.086 15.131 15.156 15.236 15.231 M. MESSUME PI 15.236 12.731	0.97616 0.97222 0.97354 0.99061 0.99357 0.99521 1.9997 1.9997	0.31132 0.31174 0.31721 0.31760 0.31760 0.32070 0.32070 0.32070 0.32070 0.32070	0.45581 0.45642 0.46543 0.46592 0.46659 0.46699 0.46905 0.46905 0.46905	0.43190 0.44900 0.48600 0.52200 0.58800 -1:0000 -1:0000		
197 112 122 27 137 142 142 143 144 147 149 149 149 149 149 149 149 149 149 149	14.866 14.806 14.806 15.086 15.131 15.156 15.236 15.231 At apprecure	0.97616 0.97222 0.97354 0.99061 0.99357 0.97521 1.9907 1.9705 1.9705 1.0701	0.31132 0.31174 0.31721 0.31860 0.31860 0.32070 0.32070 0.32070 0.32070 0.32070	0.45581 0.45642 0.46543 0.46592 0.46592 0.46659 0.46907 0.46905 0.46905 0.46905 0.46905	0.43190 0.44900 0.48600 0.52200 0.58800 -1:0000 -1:0000 -1:0000		
107 112 122 127 127 142 142 143 144 147 148 149 149 149 149 149 149 149 149 149 149	14.966 14.806 14.806 15.086 15.131 15.156 15.236 15.231 M. MESSUME PI 15.236 12.731	0.97616 0.97722 0.97754 0.99061 0.99357 0.97521 1.9909 1.9909 1.9900 1.9900 1.9900	0.31132 0.31174 0.31721 0.31760 0.31760 0.32070 0.32070 0.32070 0.32070 0.32070	0.45581 0.45642 0.46543 0.46592 0.46659 0.46699 0.46905 0.46905 0.46905	0.43190 0.44900 0.48600 0.52200 0.58800 -1:0000 -1:0000		
197 112 122 27 137 142 142 143 144 147 149 149 149 149 149 149 149 149 149 149	14. 966 14. 806 14. 806 15. 086 15. 131 15. 156 15. 236 15. 236 15. 236 15. 236 15. 236 15. 236	0.97616 0.97722 0.97754 0.99061 0.99357 0.97521 1.0007 1.0007 1.0007 1.0007 1.0001 PATINS . 20	0.31132 0.31174 0.311721 0.31860 0.31860 0.32000 0.32000 0.32000 0.32000 0.32000 0.32000 0.32000 0.32000 0.32000 0.32000 0.32000	0.45581 0.45642 0.46543 0.46543 0.46592 0.46659 0.46907 0.46907 0.46905 0.46905 0.46905	0.43190 0.44900 0.48600 0.52200 0.58800 -1:0000 -1:0000 -1:0000		
197 112 122 127 127 142 142 1442 147 240015 INN AVO WORD 167 172	14.966 14.806 14.806 15.086 15.131 15.156 15.236 15.236 15.231 AL PRESSURE PL 15.231	0.97616 0.97722 0.97754 0.99061 0.99357 0.97521 1.9901 1.9901 1.9901 1.9901 1.9901	0.31132 0.31174 0.31721 0.31860 0.31860 0.32800 0.32800 0.32800 0.32926 0.32926 0.32926 0.32926	0.45581 0.45642 0.46543 0.46572 0.46659 0.46790 0.46905 0.46905 0.46890 0.46890 0.46890	0.43190 0.44900 0.48600 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000		
107 112 122 127 137 142 153 167 167 167 172 >60017 1089	14.966 14.806 14.806 15.086 15.131 15.156 15.236 15.236 19.721 AL PRESSURE PL 15.231 AL PRESSURE	0.97616 0.97722 0.97754 0.99061 0.99357 0.99357 0.99357 1.9091 1.9091 1.0001 PATIOS 20 PATIOS 80 PATIOS 80	0.31132 0.31174 0.31721 0.31860 0.31860 0.32070 NOTTHE FLAN 0.32070 NOTTHE FLAN 0.32070 DEG SHPOUD 1 PL/PTE 0.32026 0.32026	0.45581 0.45642 0.46582 0.46582 0.46580 0.46800 0.46800 0.46800 0.46890 0.46890 0.46890	0.43190 0.44900 0.48600 0.52200 0.58800 1:0000 1:0000 1:0000 X/DMAX -1.0000 -1.0000 0.84400		
197 112 122 127 137 142 147 24017 10N AVD WORD 167 172 24017 10N AVD WORD	14.966 14.806 14.806 15.086 15.131 15.156 15.236 15.236 15.236 15.231 AL PRESSURE PL 15.231 AL PRESSURE PL 15.231	0.97616 0.97222 0.97354 0.99061 0.99357 0.99357 1.9997 1.9997 1.0901 PATIOS 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 2	0.31132 0.31174 0.31721 0.31860 0.31860 0.32076 NATTLE FLAN 0.32076 DEG SHPOUN 1 PL/PTE 0.32026 0.32026 0.32026	0.45581 0.45642 0.46542 0.46542 0.46542 0.46540 0.46407 0.46905 0.46905 0.46905 0.46890 0.46890	0.43190 0.44900 0.48600 0.52200 0.58800 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000		
197 112 122 127 127 142 142 1442 147 240015 INN AVO WORD 167 172 240017 INN AVO WORD 182	14. 966 14. 806 14. 806 15. 086 15. 131 15. 156 15. 236 15. 236 15. 231 AL PRESSURE PL 15. 231 AL PRESSURE PL 15. 231 AL PRESSURE PL 14. 941	0.97616 0.97722 0.97754 0.97061 0.99367 0.9957 1.0907 1.0907 1.0901 1.0901 1.0901 1.0901 1.0901 1.0901 1.0901 1.0901 1.0901	0.31132 0.31174 0.31721 0.31860 0.32070 0.32070 0.32070 0.32070 0.32070 0.32070 0.32070 0.32070 0.32070 0.32070	0.45581 0.45642 0.46562 0.46572 0.46650 0.4070 0.46600 0.46905 0.46890 0.46890 0.46890 0.46890 0.46890	0.43190 0.44900 0.48900 0.52200 0.58800 -1:0000 -1:0000 -1:0000 -1:0000 0.79300 0.84400		
107 112 122 127 127 142 142 143 147 148 149 149 149 149 149 149 149 149 149 149	14. 966 14. 806 14. 806 15. 086 15. 131 15. 156 15. 236 15. 231  AL PRESSURE PL 15. 271 15. 271 15. 271 15. 271 14. 841 14. 841 14. 371	0.97616 0.97222 0.97354 0.99061 0.99357 0.99357 1.9997 1.9997 1.0901 PATIOS 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 20 PLAND 2	0.31132 0.31174 0.31721 0.31860 0.31860 0.32070 NOTTLE FLAS 0.32070 DEG SHPOUD 1 PL/PTF 0.32026 0.32026 0.32026 DEG SHPOUD 1 PL/PTF 0.31206 0.32026	0.45581 0.45642 0.46542 0.46542 0.46542 0.46540 0.46407 0.46905 0.46905 0.46905 0.46890 0.46890	0.43190 0.44900 0.48600 0.52200 0.58800 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000 -1:0000		

1454-I FWIS	PEFITM	THARY DATA	76/13/70	CANDELL	RFC 10/25/79	01:15:27.09?	FAC MYSKE	PG# C034	RUN24
APPITIONA	F batzenbt	PATINS . PPI	INTEA DI FIC						
IN AURO	PI	Pt /PO	PL / PTF	PL /PTP	X/DMAX				· · · · · · · ·
9.2	7-65 35	0.59416	0.12769	0.26958	9.72200				
17	11.293	0.74415	0.26965	0.39700	0.92000				
7	14.997	0.98766	0.25790	0.52811	0.41999				
2	16.522	1.0954	0.30603	0.58571	1.0170				
APPLITICES	L PRESSUPE	PATINS , FLO	W SPLITTER I	i.n.				** ** * **	
n wnen	PL	PL/PN	ואן / חדוך	Pt /PTP	X/DMAY				
2	19,241	1.24#0	0.45948	0.67801	0.42200				
7	15.092	0.99458	0.36040	0.53101	0.67000				
APPIT IPNA	1 PRESSURF	PATINS . FIN	W SPLITTEP C	`. n.					
n woen	Pt	Pt / Pf)	PL / PTF	PL /PTP	X/DMAX				
7	9.8167	0.64692	0.23442	0.34591	0.50800				
, 2									
? ?	18.912 15.187	1.2463 1.0008	0.45161 0.36267	0.66638 0.53515	0.58300 0.67000				
				<u> </u>	V40 1./90		<del></del>		
PWOTT IONY	- weeeine	******** <del>****</del>	<del>c ton - sureyn-</del>						
D_WORD .	PL	የኒ/የበ	PL/PTF	PLANTE	X/DMAX				
07	14.777	9-97382	0.352	0.52071	-1.0000				
12	14,707	0.96921	0.35121_	0.51824	-1.0000				
7?	14.712	D. DAY	11-36133	0.51842	-1-0000				
27	14.982	0.98733	0. 35778	0.52046	-1.0000				
	14.997	0.98832	0.35813	0 - 57 <del>84</del> 6	-1.0000				
	14.952	0. 9R535	0. 35706	0.52687	-1-0000				-
	14.952 L PRESSURF	0.98535	0.35706 ERPDY INLET	0.52687	1-0000	-			-
ANDITIONAL N WORD	14.952 L PRESSURF	0.98535 RATIOS : FOR PL/PO	0.35706 ERPDY INLET	0=52687 PL /PTP	X/D#AX				-
ADDITIONAL D WORD D7	14.952 L PRESSURE PL 14.777	0.98535 RATIOS , FOR PL/PO 0.97382	0.35706 ERPOY INLEY PL/PTF 0.35288	0.52687 PL /PTP C.52071	X/DMAX 0.39800				-
ADDITIONA B WORD 07	14.952 L PRESSURE PL 14.777 14.707	0.98535 RATIOS , FOR PL/PO 0.97382 0.95921	0.35706 ERPDY INLEY PL/PYF 0.35268 0.35121	0.52687 PL /PTP C.52071 O.51824	X/DMA K 0.39800 0.43100		•		-
ADDETEDNA D. WORD 07 12 22	14.952 L PRESSURE PL 14.777 14.707 14.712	0.98535 RATIOS , FOR PL/PD 0.97382 0.96954	0.35706 ERCOV INLET PL/PTF 0.35268 0.35121 0.35133	0.52667 PL /PTP C.52071 C.51824 O.51842	X/DMAX 0.39800 0.43100 0.44900	· · · · · · · · · · · · · · · · · · ·	•		-
62 AND ET EDMA D WORD 07 12 27	14.952 L PRESSURE PL 14.777 14.707 14.712 14.982	0.98535 RATIOS , FOR PL/PO 0.97382 0.96921 0.96954 0.98733	0.35706 ERCDY INLEY PL/PYF 0.35268 0.35128 0.25133 0.35778	0-52667 PL /PTP C-52071 C-51824 C-51842 C-52793	X/DMAX 0.39800 0.43100 0.44900 0.48600		•		-
ANDETENNA N WIRD 07 12 22 27	14.952 L PRESSURE PL 14.777 14.707 14.712 14.982 14.997	0.98535 RATIOS , FOR PL/PO 0.97382 0.96921 0.96954 0.98733 0.98832	0.35706 ERCDY INLEY PL/PYF 0.35268 0.35121 0.35133 0.35779 0.35813	PL /PTP C-52071 C-51874 C-51862 C-52703 C-52746	X/DMA K 0.39800 0.43100 0.44900 0.48600 0.52700		•		
ADDETEDNA D. WORD 07 12 27 27 37 42	14.952 L PRESSURE PL 14.777 14.707 14.712 14.982 14.997 14.952	0.98535 RATIOS , FOR PL/PO 0.97382 0.94921 0.96954 0.98733 0.98832 0.98535	0.35706 ERCDY INLET PL/PTF 0.35288 0.35121 0.35133 0.35779 0.35813 0.35706	0.52687 PL /PTP C.52071 C.51824 0.51842 0.52746 0.52687	X/DMAX 0.39800 0.43100 0.44900 0.68600 0.52700 0.58800		•		
ADDEVIONA D. WORD 07 12 22 27 37 42	14.952 L PRESSURE PL 14.777 14.707 14.712 14.982 14.997	0.98535 RATIOS , FOR PL/PO 0.97382 0.96921 0.96954 0.98733 0.98832	0.35706 ERCDY INLEY PL/PYF 0.35268 0.35121 0.35133 0.35779 0.35813	PL /PTP C-52071 C-51874 C-51862 C-52703 C-52746	X/DMA K 0.39800 0.43100 0.44900 0.48600 0.52700	-	•		
ADDITIONA D WORD 07 12 27 27 37 42 42 53	14.952 L PRESSUME 14.777 14.777 14.777 14.712 14.982 14.997 14.952 15.107 15.172	0.98535 RATIOS , FOR PL/PO 0.97382 0.96954 0.98733 0.98535 1.9095	0. 35706 PERMOV INLEY PL/PYF 0. 35268 0. 35121 0. 35133 0.35776 0. 35813 0.35706 7. 30755 9. 30231	0.52667  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52700 0.58800		•		-
ADDITIONA D MORD 07 12 27 27 37 42 42 42	14.952 L PRESSUME 14.777 14.777 14.777 14.712 14.982 14.997 14.952 15.107 15.172	0.98535 RATIOS , FOR PL/PO 0.97382 0.96954 0.98733 0.98535 0.98535 0.99555	0. 35706 PERMOV INLEY PL/PYF 0. 35268 0. 35121 0. 35133 0.35776 0. 35813 0.35706 7. 30755 9. 30231	0.52667  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52700 0.58800				
ADDET FONA D WORD 07 12 22 27 37 42 52 52 53 54 54 57 57	PE 14.777 14.777 14.777 14.712 14.992 14.997 14.952 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405 15.405	0.98535 RATIOS , FOR PL/PO 0.97382 0.96954 0.98733 0.98535 0.98535 1.9095 0.99535	0. 35706 PERMOV INLEY PL/PYF 0. 35268 0. 35121 0. 35133 0.35776 0. 35813 0.35706 7. 30755 9. 30231	0.52667  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52700 0.5800 1.0000	-	•		
ADDITIONAL D WORD D12 27 37 42 52 ADDITIONAL	PL 14.977 14.777 14.777 14.972 14.992 14.997 14.952 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172 15.172	0.98535 RATIOS , FOR PL/PO 0.97382 0.96954 0.98733 0.98535 1.9695 0.98535 1.9695 0.98535	0. 35706 FRODY INLEY PL/PYF 0. 35288 0. 35121 0. 25133 0.25779 0. 35813 0. 35755 2. 36231	PL /PTP C.52071 C.51874 C.51842 C.52703 C.52866 C.52867 C.53872 C.52867 C.73867	1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52700 0.58800 1.0000		•		
ADDET FONA D. WIRD 07 12 22 27 37 42 52 57 ADDET FONA D. WIRD 52 57	PL 14.777 14.777 14.777 14.772 14.992 14.992 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 15.142 PL 1	0.98535 RATIOS , FOR PL/PO 0.97382 0.96954 0.98733 0.98535 1.90595 2.99985 PATEOS , FRO	0. 35706 PERCOV INLEY  PL/PYF 0. 35268 0. 35121 0. 25133 0. 35776 0. 35813 0. 35706 0. 35706 0. 36231	0.52667  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 X/DMAX -1.9000		•		
ADDITIONAL D. WORD D. 12 27 37 42 52 57 ADDITIONAL	PL 15.192 15.192 1 PRESSUPE	0.98535  RATIOS , FOR  PL/PO 0.07382 0.96954 0.08733 0.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1	0. 35 706 PL/PTF 0. 35 268 0. 35 121 0. 25 133 0. 35 779 0. 35 779 0. 35 706 9. 36 755 9. 36 231 0. 36 755 0.	0.52687  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000		•		
ADDITIONA D WORD 07 12 27 27 37 42 42 42 52 57 ADDITIONA D WORD 52 57	14.952 L PRESSURE  PL 14.777 14.712 14.972 14.997 14.952 15.100 15.172  L PRESSUPE  PL	0.98535  RATIOS , FOR  PL/PO 0.07382 0.96954 0.98733 0.98535 1.9095 0.99985  PATIOS , FOR	0. 35706 PL/PTF 0. 35268 0. 35121 0. 25133 0. 35779 0. 35813 0. 35706 1. 35706 1. 36755 0. 36231 PL/PTF	0.52667  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52700 0.5 78800 1.0000 X/DMAX -1.0000				
ADDET FONA D. WORD 07 12 22 27 37 42 52 57 ADDET FONA D. WORD 52 57 ADDET FONA D. WORD 67	PL 14.972 14.777 14.777 14.777 14.772 14.992 14.997 14.992 15.142 PL 15.142 PRESSUPE PL 15.142	0.98535 RATIOS , FOR PL/PO 0.97382 0.96954 0.98733 0.98535 1.9095 0.99535 1.9095 0.99985 PATIOS , 20 PL/PO 1.0005	0. 35706 PERMOV INLEY  PL/PYF 0. 35288 0. 35121 0. 25133 0. 35778 0. 35813 0. 35706 0. 35813 0. 35706 0. 36251  MOTTLE PLAN  DLAN  O. 36251  DEG SHPRUD 1  PL/PYF 0. 36255	0.52667  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52700 0.58800 1.0000 1.0000 1.0000		•		
ADDITIONAL D WORD D WORD 52 57 ADDITIONAL D WORD 52 57 ADDITIONAL D WORD 67 72	PE 14.952 14.777 14.777 14.712 14.972 14.973 14.952 15.172 15.172 1 PRESSUPE PL 15.172 PL 15.172	0.98535  RATIOS , FOR  PL/PO 0.07382 0.96954 0.98733 0.98535 1.9095 0.99985  PATIOS , FOR  PL/PO 1.0005 1.0008	0. 35 TO6  FRODY INLEY  PL/PYF 0. 35 268 0. 35 121 0. 25 133 0. 35 776 0. 35 813 0. 35 706 7. 36 231  PL/PYF 0. 36 255 0. 36 267	PL /PTP C.52071 C.51842 C.52793 C.52846 C.52687 C.53446 C.53446 C.53446 C.53446 C.53446 C.53446 C.53446 C.53446 C.53446 C.53446 C.53446 C.53446 C.53446	X/DMAX 0.39800 0.43100 0.44900 0.52700 0.5 78800 1.0000 X/DMAX -1.0000				
ADDITIONA D WORD 07 12 27 27 37 42 42 52 57 ADDITIONA 0 WORD 52 57 ADDITIONA 67 72	14.952 L PRESSURE  PL 14.777 14.777 14.712 14.982 14.997 14.952 15.149	0.98535 RATIOS , FOR PL/PO 0.97382 0.96954 0.98733 0.98535 1.9995 2.99965 PATIOS , FAM PL/PO 1.0005 1.0006 RATIOS , 80	0. 35 TOE  FRODY INLEY  PL/PYF 0. 35 268 0. 35 121 0. 25 133 0. 35 776 0. 35 813 0. 35 776 0. 35 813 0. 35 776 0. 36 755 0. 36 231  DEG SHP DUD 1	0.52667  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52700 0.52700 0.58600 1.0000 1.0000 1.0000 1.0000 0.79300 0.84400		•		
ADDITIONAL D. WORD 07 12 27 37 42 42 42 43 40 52 57 ADDITIONAL D. WORD 67 72 ADDITIONAL D. WORD	14.952  L PRESSURE  PL 14.777 14.707 14.712 14.982 14.992 15.149 15.142 15.142 15.142 15.147  L PRESSUPE  PL 15.147 1 PRESSUPE	0.98535  RATIOS , FOR  PL/PO 0.97382 0.96954 0.98733 0.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1	0. 35 TO6  FRODY INLEY  PL/PTF 0. 35 268 0. 35 121 0. 25 133 0. 35 774 0. 35 775 7. 36 251  10. 25 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	0.52687  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 X/DMAX -1.0000 -1.0000 X/DMAX 0.79300 0.84400				
ADDITIONAL D. WIRD D7 12 27 27 37 42 42 52 57 ADDITIONAL D. WIRD 67 72 ADDITIONAL D. WIRD 92	PE 14.777 14.777 14.777 14.712 14.972 14.977 14.952 15.172 PPF 550PF PL 15.172 1 PRF 550PF PL 15.172 1 PRF 550PF	0.98535  RATIOS , FOR  PL/PO 0.07382 0.96954 0.98733 0.98835 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1	0. 35 TO6  FRODY INLEY  PL/PYF 0. 35 268 0. 35 121 0. 35 133 0. 35 774 0. 35 813 0. 35 775 0. 36 231  PL/PYF 0. 36 251  PL/PYF 0. 36 255 0. 36 267  DEG SHP DUD 1  PL/PYF 0. 35 264	PL /PTP C.52071 C.51842 C.52793 C.52846 C.52687 C.53446 C.53446 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53448 C.53515 CCATION	X/DMAX 0.39800 0.43100 0.44900 0.52700 0.58800 1.0000 1.0000 X/DMAX 0.79300 0.84400				
ADDITIONAL D. WIRD 07 12 27 27 37 37 42 57 57 ADDITIONAL D. WIRD 67 72 ADDITIONAL D. WIRD 92 PT	PL 15.192 15.192 17.172 1 PRESSUPE  PL 15.192 17.172 14.997 14.952 15.192 15.192 17.172 1 PRESSUPE  PL 15.192 15.192 15.192 17.172 1 PRESSUPE  PL 15.192 15.197 1 PRESSUPE	0.98535  RATIOS , FOR  PL/PO 0.97382 0.96954 0.98733 0.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1.98535 1	0. 35706 PERPOV INLEY PL/PYF 0. 35288 0. 35121 0. 35133 0. 35778 0. 35813 0. 35706 0. 36755 0. 36231 PL/PYF 0. 36255 0. 36267 DEG SHPPUD 1 PL/PYF 0. 35266 DEG SHPPUD 1	0.52687  PL /PTP	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 1.0000 X/DMAX -1.0000 -1.0000 X/DMAX 0.79300 0.84400				

	IS PPFLIMI	HAPY DATA	06/13/79	CADDELL	RFC 10/25/7	79 01:16:20.671	FAC REGET	PG= C034	RUN 24 RDG 1494
>ADDIT IO	IAL PRESSIBE	PATINS . PPI	MARY PLUG						
IVN WOPD	PI	PI /PN	PL /PTF	PI /PTP	X/DMAX	a the separate .			
32	6.9574	0.45276	2.18013	0.26266	0. 72200				
37	12.761	0.84254	9.33521	0.45678	0.42000				
47	15.606	1. 9304	0.40996	C.59776	0.91900				
52	16.726	1.1944	0.4393R	0.64066	1.0170		Annual Marketine comment of the second		
>600 TECOM	IAL PRESSIRE	PATIOS , FEO	W SPLITTER I	. n.					
LYN WORD	PL	PL / PO	PI / PT F	PL/PTP	X/DMAX				
62	17-651	1. 1654	0.46367	0.67609	0-42200				
67	13.736	0.97693	0.36087	0.57613	0.67000				•
>40011100	AL PRESSIPE	RATIOS . FLO	W SPLITTER C	'. n.		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s			
YD WORD		m /80	M /PTF	81 /878					
-	PL	PL/PN		PI /PTP	X/NMAX				
77	8.7090	0. 57502	9.22877 _	D.33358	0-50000				
*2	21-681	1.4315	0. 56953	0. F3044	0.58300				
92	15-166	1-0014	0-39840	0.53091	0-67000				
>AGD17-191	ML PRESSURE	RATIOS	CTOR SHROUD.				•		
VD WORD	PL	PL/PO	PL/PTF.	PLANT	X/DMAX				
107	14.751	0.97395	0.38750	0.56501	-1-0000	•			•
112		0.96861	38539		-1.0000				
	14-671			0.56195					
122	14.671	3-34-46-4	0.38429	0.56195	-1.0000				
127	14.936	0.98617	0.39236	0.57210	-1-0000	w mar			
137	14.936	0.98617	0.39736	0.57210	-1.0000 -1.0000				
		500	5500W 54W 55						
		RATIOS . FCR		01 /070	# 40M A #				
AU MOND	-PL	PL/PD	PL/PTF	PL/PTP	K/DHAK	·	•		
\VD ₩ <b>OPD</b> _	PL	PL/PD 0.97395	PL/PTF 0-36750	0.56501	0.39800				
VD WORD	PL 14.751 14.671	PL/PN 0.97395 0.96867	PL/PTE 0-38750 0-38539	0.56501 0.56195	0.39800 0.43100		•		
NO WORD 107 112 122	PL 14.751 14.671 14.671	PL/PN 0.97395 0.96867 0.96867	PL/PTF 0.38750 0.38539 0.38539	0.56501 0.56195 0.56195	0.39800		•		
NO WORD	PL 14.751 14.671	PL/PN 0.97395 0.96867	PL/PTE 0-38750 0-38539	0.56501 0.56195	0.39800 0.43100		•		
VP WORD 10" 112 122 127	PL 14.751 14.671 14.671	PL/PN 0.97395 0.96867 0.96867	PL/PTF 0.38750 0.38539 0.38539	0.56501 0.56195 0.56195	0.39800 0.43100 0.44900		•		
VP WORD 107 112 122 127	PL 14.751 14.671 14.671 14.936	PL/PN 0.97395 0.96867 0.96867 0.98617 0.98617	PL/PYF 0.38750 0.38539 0.38539 0.39236 0.39236	0.56501 0.56195 0.56195 0.57210 0.57210	0.39800 0.43100 0.44900 0.48600 0.52200		•		
VD WORD 107 112 122 127 127 137	PL 14.751 14.671 14.671 14.936 14.936	PL/PN 0.97395 0.96867 0.96867 0.98617 0.98617 0.97726	PL/PTF 0-38750 0-38539 0-38539 0-39236 0-39236 0-79881	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692	0.39800 0.43100 0.44900 0.48600 0.52200 0.58800		•	-	
VD WORD 107 112 122 127 137 142	PL 14.751 14.671 14.671 14.936	PL/PN 0.97395 0.96867 0.96867 0.98617 0.98617	PL/PYF 0.38750 0.38539 0.38539 0.39236 0.39236	0.56501 0.56195 0.56195 0.57210 0.57210	0.39800 0.43100 0.44900 0.48600 0.52200		•	-	
VD WORD 107 112 122 127 137 142 152	PL 14-751 14-671 14-671 14-936 14-936 14-701	PL/Pn 0.97395 0.96867 0.96867 0.98617 0.97617 7.97726	PL/PTE 0-38750 0-38539 0-39236 0-39236 0-79881	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.77127	0.39800 0.43100 2.44900 0.52200 0.58800		•		
VD WORD 107 112 122 127 127 137 142 152 153	PL 14.751 14.671 14.671 14.936 14.936 14.701 17.174	PL/Pn 0.97395 0.96867 0.96867 0.98617 0.98617 0.97726	PL/PTE 0-38750 0-38539 0-39236 0-39236 0-79881	0.56501 0.56195 0.56195 0.57210 0.57210 0.56652 0.77127	0.39800 0.43100 9.44900 0.48600 0.52200 0.58800 1.0000				
VD WOPD 107 112 122 127 137 147 147 147 147	PL 14.751 14.671 14.671 14.936 14.936 14.801 17.170 15.174	PL/PR 0.97395 0.96867 0.96867 0.98617 0.98617 0.97726 1.9070	PL/PTE 0.38750 0.38539 0.38539 0.39236 0.29236 0.79881 2.39600	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.99129 0.99129	0.39800 0.43100 9.44900 0.52200 0.52200 0.58000 1.0000		•		
VD WOPD 107 112 122 127 137 147 147 152 167 VD WOPD	PL 14-751 14-671 14-671 14-936 14-201 17-176 PL 15-176	PL/PR 0.97395 0.96867 0.96867 0.98617 0.97617 0.97726 1.9020	PI /PTE 0.38750 0.38539 0.38539 0.39236 0.29236 0.29381 2.2900 MOZYLE ELAS	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.77127 0.78127	0.39800 0.43100 9.44900 0.52200 0.58000 1.0000 1.0000 X/BMA X -1.0000				
VD WORD 107 112 122 127 137 142 152 163 VANGETION VN MORD 157	PL 14.751 14.671 14.671 14.936 14.936 14.201 17.174 15.176 15.176	PL/PR 0.97395 0.96867 0.96867 0.98617 0.97616 1.9020 1.9020 ATTOS FAM	PI /PTF 0.38750 0.38539 0.39236 0.39236 0.29236 0.2936 0.2936 0.2966 MOZYLE SLAS PI /BIF 0.39866	0.56501 0.56195 0.56195 0.27210 0.57210 0.56692 0.77127 0.77127	0.39800 0.43100 9.44900 0.52200 0.52200 0.58000 1.0000			-	
VD WORD 107 112 122 127 137 142 152 163 VANGETION VN MORD 157	PL 14.751 14.671 14.671 14.936 14.936 14.201 17.174 15.176 15.176	PL/PR 0.97395 0.96867 0.96867 0.98617 0.97617 0.97726 1.9020	PI /PTF 0.38750 0.38539 0.39236 0.39236 0.29236 0.2936 0.2936 0.2966 MOZYLE SLAS PI /BIF 0.39866	0.56501 0.56195 0.56195 0.27210 0.57210 0.56692 0.77127 0.77127	0.39800 0.43100 9.44900 0.52200 0.58000 1.0000 1.0000 X/BMA X -1.0000				
VD WORD 107 112 122 127 137 147 147 152 157 VD WORD VD WORD VD WORD	PL 14.751 14.671 14.671 14.936 14.936 14.201 17.174 15.176 15.176 IAL PRESSURF PL	PL/PR 0.97395 0.96867 0.96867 0.98617 0.98617 0.97726 1.9020 1.9020 1.9020 1.9020 PATIOS 20 PL/PR	PL/PTF  0.38750  0.38539  0.39236  0.39236  0.39881  PL/PTF  0.39866  DEG CHPOUN L	0.56501 0.56195 0.56195 0.57210 0.57210 0.56652 0.79129 0.79129 0.78129 0.78129 0.78129	0.39800 0.43100 9.44900 0.52200 0.57800 1.0000 1.0000 X/DMAX				
VD WORD 107 112 122 127 137 147 147 152 157 VD WORD VD WORD VD WORD	PL 14-751 14-671 14-671 14-936 14-936 14-201 17-174 15-176 15-176 15-176 IAL PRESSURE	PL/PR 0.97395 0.96867 0.96867 0.98617 0.97616 1.9070 1.9070 1.9070 1.9070 PATIOS 20 PL/PR 1.0017	PL/PTE 0.38750 0.38759 0.38759 0.39236 0.39236 0.39236 0.39881 0.39866 DEG SHPRUR I	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.77127 0.78129 0.58129 0.58129 0.58129	0.39800 0.43100 9.44900 0.52200 0.58000 1.0000 1.0000 X/DMA X -1.0000 -1.0000				
VD WORD 107 112 122 127 137 142 142 142 142 143 144 145 147 147 147 147 147 147 147 147 147 147	PL 14.751 14.671 14.671 14.936 14.936 14.201 17.174 15.176 15.176 IAL PRESSURF PL	PL/PR 0.97395 0.96867 0.96867 0.98617 0.98617 0.97726 1.9020 1.9020 1.9020 1.9020 PATIOS 20 PL/PR	PL/PTF  0.38750  0.38539  0.39236  0.39236  0.39881  PL/PTF  0.39866  DEG CHPOUN L	0.56501 0.56195 0.56195 0.57210 0.57210 0.56652 0.79129 0.79129 0.78129 0.78129 0.78129	0.39800 0.43100 9.44900 0.52200 0.57800 1.0000 1.0000 X/DMAX				
VD WORD  107  112  122  127  137  147  152  157  >ADDITION  VD WORD  167  172	PL 14.751 14.671 14.671 14.936 14.301 17.176 15.176 15.176 15.176 15.176 15.176	PL/PR 0.97395 0.96867 0.96867 0.98617 0.97616 1.9070 1.9070 1.9070 1.9070 PATIOS 20 PL/PR 1.0017	PI /PTF 0.38750 0.38539 0.39236 0.39236 0.39236 0.39881 9.3986 0.39866 DEG SHPDUD I	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.77127 0.78129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129	0.39800 0.43100 9.44900 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000				
VD WOPD 107 112 122 127 137 142 142 143 144 145 145 147 147 148 149 149 149 147 147 147 147	PL 14.751 14.671 14.671 14.936 14.936 14.201 17.176 15.176 15.176 14. PRESSURE PL 15.171 15.176 14. PPESSURE	PL/PR 0.97395 0.96867 0.96867 0.98617 0.98617 0.97726 1.9020 1.9020 RATIOS _ FAM 1.9020 PL/PR 1.9020 PL/PR 1.9017 1.0007	PI /PTE 0.38750 0.38539 0.39236 0.39236 0.39236 0.39881 0.39866 0.39866 0.39866 0.39866 0.39863 0.39813	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.77127 0.77127 0.77127 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.7	0.39800 0.43100 9.44900 0.52200 0.58800 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
VD WOPD 107 112 122 127 137 147 147 152 157 >ANDITION VD WOPD 167 172 >ADDITION VD WORD	PL 14-751 14-671 14-671 14-936 14-936 14-201 17-176 15-176 15-176 15-176 15-171 15-156 IAL PRESSURE PL 15-171 15-156 IAL PRESSURE	PL/PR 0.97395 0.96867 0.96867 0.98617 0.97726 1.9020 1.9020 1.9020 RATIOS _ FAM PL/PR 1.0017 1.0007 RATIOS _ MO PL/PR	PL/PTE 0.38750 0.38759 0.38759 0.39236 0.39236 0.39881 0.39864 0.39866 DEG SHPNUN L PL/PTE 0.39813 DEG SHPNUN L	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.99129 0.99129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129	0.39800 0.43100 9.44900 0.52200 0.52200 0.58000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
VD WORD  107  112  122  127  137  147  152  157  >ANGITION  VN WORD  167  172  >ANGITION  VN WORD  167  172  >ANGITION  VN WORD  169  169  169  169  169  169  169  16	PL 14.751 14.671 14.671 14.936 14.936 14.201 17.176 15.176 15.176 15.176 15.171 15.176 14.891	PL/PR 0.97395 0.96867 0.96867 0.98617 0.98617 0.97726 1.9020 1.9020 1.9020 PATIOS FAM 1.0020 1.9020 PATIOS , 20 PL/PR 1.0017 1.0007 RATIOS , 80 PL/PR 0.98320	PI /PTF 0.38750 0.38759 0.38759 0.38759 0.39236 0.39236 0.39881 9.39866 0.39866 0.39866 0.39866 0.39867 0.39813 0.39813 0.39813	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.79127 0.79127 0.79127 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129	0.39800 0.43100 9.44900 0.52200 0.52200 0.58000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
VD WORD 107 112 127 127 127 127 127 147 147 152 157  ADDITION VD WORD 167 172  ADDITION VD WORD 162 162 167	PL 14.751 14.671 14.671 14.936 14.936 14.201 17.176 15.176 15.176 15.176 15.171 15.176 14. PRESSURF PL 15.171 15.156 IAL PRESSURF PL 14.456	PL/PR 0.97395 0.96867 0.96867 0.98617 0.98617 0.97726 1.9020 1.9020 PATIOS FAM 1.0020 PATIOS 20 PL/PR 1.0017 1.0007 RATIOS 80 PL/PR 0.98320 0.95467	PL/PTF 0.38750 0.38759 0.38759 0.39236 0.39236 0.3986 0.3986 0.3986 0.3986 0.3986 0.39873 0.39813 0.39813 0.39813 0.39813	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.99129 0.99129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129 0.58129	0.39800 0.43100 9.44900 0.52200 0.52200 0.58000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
VD WOPD 107 112 122 127 137 142 152 157 VD WOPD 167 167 172 VANDITION VD WORD 167 172 VD WORD 167 177 VD WORD 167 177 VD WORD 167 177 VD WORD 167 177 VD WORD 167 177 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD 167 VD WORD	PL 14-751 14-671 14-671 14-936 14-936 14-201 17-176  ML ARESSURE  PL 15-176 15-176 15-171 15-156 MAL PRESSURE  PL 15-171 15-156 MAL PRESSURE  PL 14-891 14-891 14-856 MEASURED	PL/PR 0.97395 0.96867 0.96867 0.98617 0.97826 1.9020 1.9020 1.9020 PATIOS FAM PL/PR 1.0017 1.0007  RATIOS 90 PL/PR 0.98320 0.95467 THPUST PAPAM	PL/PTE 0.38750 0.38759 0.38759 0.39236 0.39236 0.39236 0.39866 0.39866 0.39866 0.39866 0.39813 0.39813 0.39813 0.39813 0.39813 0.39813 0.39813	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.77127 0.78127 0.78127 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129	0.39800 0.43100 9.44900 0.52200 0.52200 0.58000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000				
NO WORD 107 112 127 127 127 127 147 147 147 147 148 NO WORD 167 172 >	PL 14-751 14-671 14-671 14-936 14-936 14-201 17-176  ML ARESSURE  PL 15-176 15-176 15-171 15-156 MAL PRESSURE  PL 15-171 15-156 MAL PRESSURE  PL 14-891 14-891 14-856 MEASURED	PL/PR 0.97395 0.96867 0.96867 0.98617 0.97826 1.9020 1.9020 1.9020 PATIOS FAM PL/PR 1.0017 1.0007  RATIOS 90 PL/PR 0.98320 0.95467 THPUST PAPAM	PL/PTF 0.38750 0.38759 0.38759 0.39236 0.39236 0.3986 0.3986 0.3986 0.3986 0.3986 0.39873 0.39813 0.39813 0.39813 0.39813	0.56501 0.56195 0.56195 0.57210 0.57210 0.56692 0.77127 0.78127 0.78127 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129 0.78129	0.39800 0.43100 9.44900 0.52200 0.52200 0.58000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	DSM 2.2848	CF4 0.0021240		

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v	
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	50 cf [44]	NARY DATA	06/13/79	CARDETT	REC 10/25/79 01:17:17.506	FAT AVEX!	PGM 7034 RDG 1495
APPLIT TOMA	E PRESSURE	RATIOS . PP I	MARY PLUG				
VO WOPD	PI	PL/PN	PI /PTF	PI /PTP	X/DMAX		A 1
32	12.138	7. 79935	0.38052	0.54585	0.72203		
37	15.223	1.0025	0.47724	0.694=7	0.82000		
47	15.918	1,0447	0.40002	0.71592	0.91900		
57	16.263	1.0710	0.50093	0.73134	1.0170		
>ATTTTTONA	L PRESSURE	RATIOS . FLO	W SPI ITTER I	.n.			The first of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the
מאחות מע	PĪ	PL / PO	PE /PTF	PI /PTP	X/DMAX		
62	15.473	1.0190	0.46507	0.69582	0.42200		
47	13.458	0.48624	0.47191	0.60521	9. € 7000		
APPLT LOCA	L PRESSUPE	PATINS . FLO	W SPLITTER P	.n.	n Talifa dagan a Makasakakaha salipu salah kaman ang magan a ang Manasaka makasaka manaka ang salah salah salah	After an other colleges control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of t	rente esta e una con sensi establicamen en company de debre establicado en anago, com a unique
VD WORD	PI	PL/Pfl	PL/PTF	PI /PTP	X/DMAX		
77	12.673	0.93458	0.39730	0.56991	. Q., 2500		
47	17.753	1.1691	0. 55453	0.79832	0.59300		
٥٧	15,203	1,0012	0.47661	0.6#368	Q.67900		-
SE SURE TIME	PPPSSURE	RATIUS, 2 COC	CITY SHERON				
VD WORD	PL	_PL/PD	PL/PTF	Plant	X/DMAX		
107	14.763	10-07222	0. 46283	0.66389	-1.0000		
112	14.663	0.96563	7,4596A	0.65940	-1.0000		
122	14-659	0.04530	17.64063	0.65917	-1-0000		
127	14.933	0. 98341	0.46815	0.67154	-1.0000		
137	14.013	0.98209	0.46752	0.6708			
152	14.683	0. 26642	0.46031	0-66029	-1:0000		
AMOUTIOGAZ	bbc22il8t	PATINS . FOP	EBLUA INFEA		-		
VO WERD	Pt	PL/PO	PL / PTF	PL/PTP	X/DMAX	_	
197	14.763	0.97222	0.46282	0.66389	0.39800	•	
112	14.663	0, 96563	0.45968	0.65940	0.43100		
127	14.658	0.96530	0.45053	0.45917	0.44900		
	14.933	0.98341	0.46815	0.67154	0,48600		
			0.46752	0.67064	0.52200		
127	14.913	0. 9#209	70 TO 172		0.76600		
127 137 142		0.98209 7.98895	9-46931	0.66029	0.52200 0.58800		
127 137 142	14.913 14.683			0.66079	0.58800		
27 137 142	14-913	7.96695	9-46931				
27   37   42	14.683 14.683 17.715	7.96695	0-46031	0.66029	0.58800 -1:0000	ik kalangan ang kalanda unang kanganan akangan da sa	
127 137 142 100 11 1000	14.013 14.683 19.115 19.215 PRESSURE	7, 96695 2, 718 1, 0018	0.46971 0.47642 0.47642	0.66029 0.65413 0.68413	0.58800 -1.0000 -1.0000 -1.0000		
127 137 142 122 123 124 124 127 128 128 128 128 128 128 128 128 128 128	14.013 14.683 10.15 19.215 19.215 Pt 15.213	7, 96,695 12-718 1-0718	0.46031 0.47692 0.41692 0.47693	0.66029 0.67413 0.68413 PI/PTP 0.68413	0.58800 -1.0000 -1.0000 -1.0000 */DMAX -1.0000		
127 137 142 12- 14- 14- 14- 14- 15- 15- 15- 15- 15- 15- 15- 15- 15- 15	14.013 14.683 19.115 19.215 PRESSURE	1.96695 1.718 1.0018	0.46971 0.47642 0.47642	0.66029 0.65413 0.68413	0.58800 -1.0000 -1.0000 -1.0000		
127 137 142 1-7 1-7 1-7 1-7 1-7 1-7 1-7 1-7 1-7 1-7	14.013 14.683 10.15 15.215 PL 15.213 15.213	7.96695 1.0018 1.0018	0.46031 0.47692 0.41692 0.47693	0.66029 0.6413 0.64413 0.64413	0.58800 -1.0000 -1.0000 -1.0000 */DMAX -1.0000		
127 137 142 142 142 143 144 144 145 145 145 145 145 145 145 145	14.013 14.683 14.25 15.215 PRESSUPE PL 15.213 L PRESSUPE	7.96695 1.0018 1.0018 1.0018 PAYINS . 20	0.46931 0.47692 0.47692 0.47692 0.47692 0.47692 0.47692	0.66029 0.6413 0.6413 0.6413 0.6413 0.6712	0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
127 137 142 1-7 14004T40NM VD 40RD 152 >ADD1T10NA VD 40RD 167	14.013 14.683 10.15 10.15 10.15 10.15 PL 15.213 15.213 L PRESSUPE PL 15.203	7.96695 1.0018 1.0018 1.0018 1.0018 PATIOS . 20 P/PD 1.0012	2.46931 10.47692 10.47692 0.47692 DEG SHPOUD 1 PI /PTF 0.47661	0.66029 0.6413 0.6413 0.6413 0.6413 0.6413 0.6413 0.64368	0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
127 137 142 1-7 14004T40NM VD 40RD 152 >ADD1T10NA VD 40RD 167	14.013 14.683 14.25 15.215 PRESSUPE PL 15.213 L PRESSUPE	7.96695 1.0018 1.0018 1.0018 PAYINS . 20	0.46931 0.47692 0.47692 0.47692 0.47692 0.47692 0.47692	0.66029 0.6413 0.6413 0.6413 0.6413 0.6712	0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
127 137 142 142 140 140 152 152 >ADDITIONAL VD WORD 167 172	14.013 14.683 14.583 17.715 15.715 PRESSUPE PL 15.213 L PRESSUPE PL 15.203 15.203	7.96695 1.0718 1.0718 1.0018 1.0018 PATIOS . 20 PI /PD 1.0012 1.0012	2.46931 10.47692 10.47692 0.47692 DEG SHPOUD 1 PI /PTF 0.47661	0.66079 0.6413 0.6413 0.6413 0.6413 0.6413 0.6413 0.6413 0.6413	0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000		
127 137 142 142 142 142 142 142 142 142 142 142	14.013 14.683 14.683 17.213 17.213 15.213 15.213 1 PRESSUPE PL 15.203 1 PRESSUPE	7.96695 1: 718 1:  9-46931 9-47692 9-47692 0-47692 0-47661 0-47661 0-47661 DEG SHPOUD 1	0.66079 0.6413 0.6413 0.6413 0.6413 0.6413 0.6413 0.6413 0.6413	0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			
127 137 142 142 143 144 147 140 140 140 140 140 140 140 140 140 140	14.013 14.683 19.215 19.215 19.215 15.213 L PRESSUPE PL 15.203 15.203 L PRESSUPE PL 15.203	7.96695 1.0718 1.0718 1.0018 PATIOS . 20 PI /PO 1.0012 1.0012 1.0012 RATIOS . 80 PI /PO 2.99379	9-46931 9-47672 9-47672 0-47692 0-47661 0-47661 DEG SHPOUN 1 PLAPE 0-47285	0.66029 0.67613 0.67613 0.67613 0.67613 0.67613 0.67613 0.67613 0.67613 0.67613	0.58800 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX 0.79300 3.84400		
127 137 142 142 140 140 157 157 260 157 260 177 260 177 260 177 260 187	14.013 14.683 17.215 17.215 PL 15.213 15.213 L PRESSUPE PL 15.203 15.203 L PRESSUPE PL 15.203 15.203 L PRESSUPE	7.96695 1: 718 1:  2-46931 10-47692 10-47692 0-47661 0-47661 DEG SHPOUD 1 PI /PTF 0-47661 PI /PTF 0-47285 0-46094	9.66029 J.67413 O.68413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413 O.67413	0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000			

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MASA-I FHIS	. perla	IMERY DATE	06/13/79	CADDETT	PFC 10/25/79 01:18:31.511	FAC REGEL	PG# 1034	PCNUA Peri 309
>ADDITION	IL PRESSURE	RATTOS . PRI	MAPY PLUG					
AU MUBD	PI	PI / PO	PL/PTF	PL /PTP	X/IMAX	·		
32	14.514	0. 95253	9.52704	0.76322	0.72200			
37	15.459	1.0144	0.56136	0.81291	0. 82000			
47	15.774	1.0352	0.57279	0.82947	J.91900			
52	15.964	1.0477	0. 47069	0.83946	1-0170			
>ADDITIONA	L PPESSURF	RATIOS , FLO	W SPIJTTEP I	I.P.	andronia a contributado de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión de la compansión			
VD WORD	P(	PL / PO	Pt /PTF	PL /PTP	x/DMAX			
62	15.209	0.99814	0.55228	0.79976	0-42200			
67	14.739	2.96730	9. 53521	0.77505	0.67000			•
		RATIOS . FLO					and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th	
VD WOPD	PL 13.304	PL /PO	PI / PTF	PL /PTP	X/PPAX			
77	13-204	0.86656_	0.47948	0.69433	0.50800			
P2	17.029	1.1176	0.61 735	0.89545	0.58300			
92	15-259	1_00.14	2. 55409	0.80239	0_67000			
M271719M	L PRESSURE	291103 v. £46	<del>6   90    </del> 10000					
VD WORD.	PL	PL/ PD	PL/PTF	PLANTE	X/DHAX			
107	14. 839	0.97386	0.53884	0.78031	-1.0000			
112	14-159	0.9664	D. 53594	0.77610	-1.0000			
122	14.769	2000977	52630	0.77663	-1.0000			
127	15.229	7, 94633	0.54574	0.79030	-1.0000			
137	15.024	<b>7.9860</b> 7	0.54556	0.79003	-1.0000			
4	14-244	0.97419	0.53903	0.78057	1_0000	•		
MOLTICOS	L PRESSURE	RATIOS . FOP	EPODY INLEY					
VD HORD	PL	PL/PO	PL/PTF	PL/PTP	Y/DMAX			
107	14.839	0.97386	0.53 AR4	0.78031	0.35000	•		
112	14.759	0.96861	0.53594	0.77610	0.43100			
122	14.769	2, 96 92 7	0.53639	0.77663	0.44900			
	15-029	2.98633	0. 54574	0-79030	0.48600			
177	15-074	3.98690	7.54556	0.79003	0.52200			
142	14.844	0.97419	0. =3903	0.78057	0.58800			
	14°564	1.0717	70-1676	0.40267	-1.0030			
57	15.264			0.49265 	-1.0000			
+0 <u>017 (</u> 744	L PRESSURE	FF 7102 - FAR						
ID HUBD	PL	PIPE		PL /PTP	X/OMAX			
(5)	15-244-	1.3017	0. 55.678		-1.0000			
	15.266	1.0917	0.5542A	0.00265	=1.0000 =1.0000		_	
>ADOTT TONA	L PRESSURE	PATINS . 20	<u>DEG SHPPUD 1</u>				, 	
/ግ ພጣዮክ	Pt	Pt /PN	PL / PTF	P[ / PTP	x/DMax			
147	15.249	1.7921	0. 55446	0.60292	0. 79300			
177	15.264	1.0017	0.55428	0.80292	0. 79300 0. 64400			
SANDET FORM		PATIOS . AO						
VD ₩ቦ₽D	Pl	Pt / Pfi	PI /PTF	PL /PTP	Y/DMAX			
mr 17	15.194	0.99716	0.55173	0.79897	9. 79300			
1 # 2		ソープタイトの	いっつつますべ	1)	7. 1.4200			
1#? 187			A E383A	A 770E7	A 84400			
197	14.874	3.972RP THRIST PAPAM	U-zieiO	0.77957	0.84400			

MASA-1 FMT	IS PPFLIM	ATAG YRAPI	06/13/79	CADDELL	REF 10/25/79 01	:19:44.747	FAT MESEL	PG# C034	PUN 24
>69917109	ILL PPFSSIIRF	RATIOS . PPT	MARY PLUG						
AVD WOPD	PI	PL / PO	PL /PTF	PL /PTP	X/DMAX				in an extension of the conformal first an apply on agricular again.
32	14.464	0.95172	0.52477	0.76147	J.72290				
77	15.409	1.0139	0. **905	0.81171	0. 62000				
47	15.729	1.0349	0.57066	0.02806	0.91900				
52	15.919	1.0474	0.57755	0-63806	1.0170				
>ADDITION	IAL PRESSIRE	RATIOS . FLO	W SPLITTEP I	1.0.					The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon
AL MUND	PL	PL /PP	PI /PTF	PI /PTP	x/DMAX				
62	15.169	0.99410	9,55934	0.79858	0.42200				
67	14.604	0-96685	0.53311	0.7735R	0.67000				
>ADDITION	IAL PRESSURF	RATIOS . FLO	W SPLITTER C	.n.	· · · · · · · · · · · · · · · · · · ·				
VO HOPO	PI ["]	PI /PO	PL /PTF	PI /PTP	X/DMAX				
77	13,145	9.864RT	0.47688	0.69198	0.50000				
82	16.974	1.1168	0.61587	0.89358	0.58300				
9.7	15,229	1.0020	0.55252	0.90174	0.67900				
PADDITION	2412224Q IA	. AATIOS FJE	CZOR SWROUD						
-	PL	PL/PG	PL/PTF	91.437	X/DMAX				
107	14.804	97409	0.53710	0.77937	-1.0000				
112	14.714	0. 96 11	3304	0.77463	-1,0000				
122	14.724	2-04-4-	7-1420	0.77516	-1.0000				
127	14.904	2. 98659	2.54403	0.78937	-1.0000				
137	4.979	0.98560	0.54345	0.78750	-1.0000				
152	14.799	0.97376	0.53692	0.77910	1-0000				-
NOT TICOR	IAL PRESSURE	PATINS , FOR	FPCDY INLEY						
yn wasa		PL / PO	PI/PTF	PL /PTP	x/DMAX				
107	PL 14.804	0.97409	0. 43710	0.77937	0.39800		▼		
112	14.714	0.96817	0.53284	0.77463	2.43100				
122	14.774	0.96 RR3	0.53420	0.77516	0.44900				-
127	14.794	0.98659	0. 54400	0.78937	0,48600				
127	14.979	2.98560	7.54745	0.78858	0.52200				
147	14, 700	0.97376	0.53692	0.77910	0.58800				
145	19.29		<del></del>	<del></del>					
197	190224	1.0070	110-172-7	OFFICE A	-1-0000				
فتعفضان الأذ	- PRI 5 1977	PATRICE T VIA	NUMBER OF						
VO HOPO	PĽ	PL/PI	-DIPPF	PL /PTP	x/DMAX				
152	15.234	1.0024	0. 64216	0.80200	-1.0000				
152	15.229	1.0020	0.55257	0-80174	1.0000				
>Annt Tinn	AT PRESSURE	PATINS , 20	NEG SHPRUN I	OCATION					
	Pl	PL / PO	PI / PT F	PL/PTP	x/DMAX				
VO WOED	15.234	1.0024	0.55770	0.40200	0.79300				
		1.0027	0.55289	0.00226	0. 94400				
147	15.239								
167 172	15.239	PATETS . PO	NEG SHPCUD L	DCATION					
147 172 >ADDIT TON	15.239				V JOHA V			*** · · · · · · · · · · · · · · · · · ·	
147 172 >ADDITTON	15.239 IAL PRESSIPE	Pt /Pn	PI / PT F	PE /PTP	X/D#AX			AND THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF T	
170 WORD 177	15.239 IAI PPESSIPE PL 15.159	P4 / PN No 99744	PI / PT F	PE /PTP 0.79805	0.79300			AND AND AND AND AND AND AND AND AND AND	
167 172 >ADDITTON IVO WOPD 187	15.239 IAI PPESSIPE PI: 15.159 14.789	Pt /Pn	PI / PTF D. 54698 D. 53656	PE /PTP				and and the second second second second	

4444-1 EM15	DBEF [4]	AT AD VP 14	06/13/73	CABDETT	REC 10/25/79	01:71:17,569	FAC 4XAXI	PG# C034	RUN24
>470[T]RNA	I PRFSSIPE	PATIOS . PPI	MESA SFIIC						
NU MUNU	PĮ	Pt /PD	PI /PTF	PL /PTP	X/DMAX	errogen wrong to us a super-			* **
32	14-873	0.94113	9-54048	0.91746	0.72200				
37	15,188	1.0019	2. 551 07	9.936#9	0.92000				
47	15.315	1.0105	0.55665	0.94461	0. 91 900				
52	15.395	1.0154	0.55935	0.94954	1.0170				
SAOD TECON	PRFSSIPF	RATIOS . FLO	M COLUTTED 1	.n.		the the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of the country of th			
VO WOPD	Pt	PL / PO	91 / PTF	PĮ /PTP	H/DM4H				
62	14.995	0. 98939	0-54502	0.92517	0.42200				
67	14.888	0.98712	2.54102	0.918?8	0.67000				
SAUDIT TONAL	PRESSIRE	MATINS . FIN	W SPETTER P	.n.	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s				
VA WAPA	PL	PL /PD	PL/PTF	PL /PTP	X/DMAX				
77	13.067	0-86204	0.47488	0.0610	0.50500				
*2	16-463	1-1124	3.61280	1.0402	0.58400				
92	15.193	1.0022	2.55211	U.9372C	0_67000		Marker garrent interester managine week trasps	and the second second second second	ajoto prominentario della per con constanta della manda di constanta di constanta di constanta di constanta di
\$4001110HM	t <del>- PRE33UPE-</del>	Refloi I fat	Green Shreen						
VO HORD	PE-	PL/PD	PL/PTF	- BLARTE	X/DMAX				
107	14.758	0.97355	0.53634	0.91036	-1.0000				
112	14.653	0.90040	7.53357	0.90574		Manager agreement of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of	Minimum		
122	14.673	0-04794	0 23351	0,9051?	-1.0000				
127	14.938	9.99542	3. 44.	0.92147	-1.0000				
137		0.99419	0.54211	0.05053	-1.0000				
132	14.718	9. 97091	0.53485	0.90790	-1-0000				
PADDITIONAL	L PPESSURE	PATIOS . FOR	EBUDY INTEL						
Ab Hubb	PL	PL/PD	PL/PTF	PL/PTP	XAMONX.				
107	14.758	0.97355	0.53639	9.01036	0.39900		•		
115	14.553	9. 96869	0. 43357	0.90574	0.43100				
127	14.673	7.96704	9.52721	0.99512	0.44900				
127	14.938	2.99542	3.54284	0.92147	0.48600				
137	14.918	0.99410	0. 4211	0.92023	0.52200				
14?	14.718	0.97091	0.53485	0.90790	0.58800				
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***	0.8927 *****	9. 6797	0.8797	0.8787	0.8777	C. 978	0.969	0.765	0.999	1.48	2.77	1.47	3. 764	23
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***	0.9125 *****	0. 9049	0. 9389	0. 9074	0.9074	0.934	9.º6F	7.474	0.000	1-47	2.11	1.44	0.361	25
	0.9965 *****	0.9036	0.0376	0.9016	0.9016	0.871	0.965	0.551	0.000	1.25	1. #2	1.45	0.359	26
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	62 67	15,589	1.0316	0.56622	9.06514	0-42200					
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13.559    0.4907    0.4901    0.4901    0.4900      15.154    1.0907    0.4901    0.4900    1.0900      15.154    1.0907    0.4900    1.0900    0.5900      15.155    1.0900    0.4900    0.4900    0.4900      15.150    1.0900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900      15.150    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900    0.4900	SAND I T FINA	PRESSIBE	•	SPL ITTE							:
13.559   1.0031   0.53010   0.53010   0.53000   17.319   0.53000   17.319   0.53000   17.319   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001   0.53001	AVD UVED	•		PI /PTE	91 /P TP	Y AMAX					
15.15   1.0033   0.5306   1.076   0.5390   1.0176   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0180   1.0	77	13,549	0-89677	0.49213	0.83883	0.50800					
15,159   1,0033   0,520a  0,385a  0,385a  0,4100a    15,779   0,275cc   0,133   0,250a  0,385a  0,385a    15,779   0,275cc   0,275cc   0,275cc   0,200a    15,770   0,275cc   0,275cc   0,275cc   0,200a    15,770   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0,275cc   0	:	17.366	1.1493	0.63059	1.0750	0.58303					
	92	15,159	1,0033	0.55061	0.93651	0.67000				- The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the	
14.73	AHBI THERA	IL PRESEURE-	44 1185 x 646	- C108-S-4013		١					
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1, 739   0, 70   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000   1, 1000	AVD WORD		7/3	PL/PTF		K/DMAY	,				
	-107	14.739	10000	25.55	0.91251	-1-0000					
	2112	20051	116-6-	12298 12298	0.90459	-1-0000					
	-14	770 71	9000		0.0150	2000-1-					
	-137	1	0.99163	0.54407		-1-0000					
	12-	14, 409	0,98613	711920	0.97747	2009					
14,739   0,07454   0,39404   0,39404   0,39404   0,39404   0,40744   0,37124   0,39404   0,40744   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,40745   0,407	4400			•		1					
14,734   0,37454   0,39400   0,39400   14,734   0,39400   14,734   0,37400   0,39400   14,734   0,37400   0,39400   14,734   0,37400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400   0,39400	Will a Time	,	1								
14,779   0,9754   0,9754   0,9304     14,674   0,97154   0,97154   0,9304     14,674   0,97154   0,97154   0,9104     14,034   0,97154   0,97154   0,9204     14,034   0,97154   0,9204   0,9104   0,4000     14,034   0,90154   0,91054   0,9204   0,9204     14,034   0,90154   0,9204   0,9204   0,9204     14,144   0,9204   0,9204   0,9154   0,900     15,144   0,9204   0,9204   0,9704   0,900     15,134   1,0017   0,4000   0,900   0,900     15,134   1,0017   0,4000   0,900   0,900     15,134   1,0020   0,4000   0,900   0,900     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   1,0020   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,134   0,00100   0,4000   0,4000   0,4000     15,140   0,00100   0,4000   0,4000   0,4000     15,140   0,00100   0,4000   0,4000   0,4000     15,140   0,00100   0,4000   0,4000   0,4000	AVN WORD	1	PL/P0	PI /PTF	PL /PTP	X/DMAX					
1, 60 4	101	14.739	1,97554	9646506	1,91251	0.35800		•			
14,770   0,974.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927.7   0,927		14,674	0.97124	0, 43299	0.0000	0.43100			•		
14,774   0,90143   0,4277   0,4277   0,4270     14,499   0,90143   0,4274   0,4274   0,4270     14,499   0,9013   0,4014   0,0274   1,0000     14,499   0,90143   0,4017   1,0000     15,14   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,0000     15,134   1,0017   1,4017   1,4017   1,4017     1,014   1,017   1,017   1,4017   1,4017     1,014   1,017   1,4017   1,4017   1,4017     1,017   1,017   1,4017   1,4017   1,4017     1,017   1,017   1,4017   1,4017   1,4017     1,017   1,017   1,4017   1,4017   1,4017     1,017   1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4017   1,4017     1,017   1,4017   1,4	121	14.964	0.99043	0.54252	0.92644	0.48600					
14, 499   0, 49613   0, 4214   0, 4224   0, 58600	117	14.770	0, 99143	1. 54437	0.92777	0.52200	The company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the company of the co				: !
	251	14.499	9.98613	7.54116	9.92242	9.58809					
######################################	15.2	-	1 90 33		200	0000					
	TOTAL TOTAL	54775544	M43 301148	317701							
5.144	440 4080	  •		P /424	97.07	* 4000 *					
	-142	15,144		\$600¥	0.03759	-1-000					
PRESSURE PATINS, 20 NEG SHEDUN INCATION  15.134 1.7017 7.54070 0.03697 0.79300  15.134 1.7017 7.54040 0.0372P 0.79300  15.139 1.0920 9.54040 0.0372P 0.79300  PE PRESSURE PATINS, EN NEG SHEDUN INCATION  14.154 0.93687 7.51417 7.87620 0.79300  13.430 7.01308 7.51417 7.87620 0.79300  13.430 7.01308 7.51417 7.85403 0.84400  ELI 201.01 CIGAA IC 1.7707 FTARE 2.6978 NSW 2.4454 CFW 0.0021174	-157	15.12	1.9323	3, 45006	2554	-1-0000					
PI 94/PM PL/PTP X/DMAX 15.134 1.7017 7.54070 0.03897 0.79300 15.134 1.7017 7.54030 0.0372P 3.84400 PPESSURE PATING, BO DEC SIBROUN INCATION PI PI/PM PI/PM PATE PI/PTP X/DMAX 14.154 0.936A7 7.51417 7.87620 0.79300 13.870 7.0130A 7.51417 7.85403 0.84400 13.870 7.0130A 7.51417 7.85403 0.84400	T T T T T T T T T T T T T T T T T T T		Č		101110						
15.134   1.7017   1.54070   0.017697   0.79300   15.134   1.7017   1.54070   0.017697   0.79300   15.134   1.7017   1.54070   0.01772   0.79300   0.01772   0.01772   0.01772   0.01772   0.01772   0.01772   0.01772   0.01772   0.01772   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300   0.79300		35/16 5 13	1	1							
15.134 1.7017 7.54-070 0.53697 0.79300 15.139 1.0020 9.54-089 0.5729 0.78900  perssure parins and ner, simplician interest of 10.0000 0.79300 15.154 0.93642 7.51412 7.87620 0.79300 13.430 7.01308 7.51412 7.85403 0.84400 13.430 7.01308 7.51412 7.85403 0.84400  elf 201.01 struct pare trick struct of 1.7707 FTARE 2.6978 0.4054 FFE 0.4074	AVO UPRO	ฮ	4/4	PL /PTF	PL/PT0	X/DMAX					
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VO WOPD	PI	የኒ / የብ	PI / PYF	PI /PTP	KADMAX			
12	14.038	1.0585	0.50266	G-85341	0.72200			
7	16.5A2	1.0944	01973	0.88240	3. 82000			
7	14.697	1.1020	0.57334	0.0001	0.91900			
ž	16.657	1.0994	U. E55UB	0.88635	1-0170			
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2	16.412	1-9F32	0.51441	0.87336	0.42200			
7	16.163	1.0667	0. 5065 8	0.86006	0-67000			
JAHOT T TONAL	PPFSSIPE	PATINS . FIN	M Zulliles u	.n.	* * * * · · · · · · · · · · · · · · · ·	t in the second constraint of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second constraints of the second con		Markada madanda isa salipi mila sala sa
ก พกรก	Pl .	Pf /PO	DĮ /PTF	PĮ /PTP	X/DMAY			
7	13.489	0.89023	9.42277	0.71777	0.50000			
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? ?	16.321	1.2092	0.57424	0.07494	0.58300			
£	15,169	1.0711	0.37541	<u>9.</u> P9714	9.67000	na i man artika erin Manag eksakuntanakan kan erin ini ara	A	or appears of on the observation of
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D MUSU	P	PL / Pri	PL/PTF	PLIPIA	X/DMAX			
יט	14.908	0.97731	0.46613	5.79709	-1.0000			
12	14.748	3.00536	- CAR725	0.78480	_1.0000	and a second second second second second second second second second second second second second second second	yanta ee ya aa yayaa tee	
27	14.773	0.975	0.46303	0.78613	-1.0000		· ·	
	15.243	0.99787	J. 57120	0.40049	-1.0000			
<i>C'</i>								
	- AFFER	0.90513	9.47750	0:40234	-1.0000			
37	15.023	0.99150	0.47086	0.79543				
27 37 52	15.023	3.99150	0.47086		-1.0000			
37 <u>52</u>	15.023		0.47086					
ADDIT IONAL	15.023	3.99150	0.47086 FROOV INLET					
ANDITIONAL	PRESSIME	).99150  PATENS , FNP PL/PN	0.47086  FRONY INLET  PL/PTF	0.79c43	1-0300 1-0300	•		
AND IT INNAL N HORD	15.023 PRESSIPE Pt 14.808	7.99150 PATINS , FNP PL/PN 0.97731	0.47086 FROOV INLET PL/PTF 0.46413	0.79 ⁶⁴³ P[ /PTP 0.78700	1,0300 Y/DMAX 0,39800			
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37 62 600 IT IONAL D. WORD 07 12 27 27	15.023 PRESSIME Pt 14.808 14.748 14.773 15.243	2.99150 PATINS , FNP PL/PN 0.97731 0.97534 0.97530 0.99282	0.47086 FRMDY INLET PL/PTF 0.46413 0.46403 0.46303 0.47149	0.79643 PL/PTP 0.78700 0.78680 0.78613 9.80049	1_0J00 Y/DMAW 0.39800 0.44500 0.44500 0.46600	•		
37 42 400 IT IONAL D. WORD 97 12 27 27	15.023 PRESSIME Pt 14.808 14.748 14.773 15.243 15.078	2.99150 PATINS . FNP M /PN 0.97731 0.97536 0.97530 0.99282 0.99282	0.47086 FRMDY INLET PL/PTF 0.46413 0.46225 0.46303 0.47149 2.47250	0.79643 PL/PTP 0.78700 0.78480 0.78613 0.80049 0.80235	1.0300 Y/DMAN 0.39809 9.43100 0.44500 3.48690 9.57200	•		
97 42 400 IT FONAL 0 WORD 97 12 22 27 27 37	15.023 PRESSIME Pt 14.808 14.748 14.773 15.043 15.078 15.023	2.99150  PATINS FRP  PL /PN 0.97731 0.97334 0.97520 0.99282 0.99583 0.99150	0.47086 ERMOY INLET PL/PTF 0.46413 0.46225 0.46303 0.47149 0.47250 0.47086	PL/PTP	1.0300 Y/DMAY 0.39800 0.43100 0.44500 3.48600 0.57200 0.57800			
97 ADD IT FONAL D. WORD 07 12 22 27 27 42	PRESSIME Pt 14.808 14.748 14.773 15.243 15.078 15.078	2.99150  PATINS , FNP PL /PN 0.97731 0.97334 0.97520 0.99282 0.99613 0.99150 1.99150	0.47086 FRIDY INLET PL /PTF 0.46413 0.46225 0.46303 0.47149 0.4725c 0.47086	PL/PTP	-1_0J00 */D#A¥ 0.39800 0.43100 0.44500 J.48690 9.57200 0.58800 1.9998	•		
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AND IT IONAL  OF HORD  17  17  27  27  47  42  52  AND IT IONAL	PRESSURE	2.99150  PATINS , FOP  PL /PN 0.97731 0.97530 0.99282 0.99513 0.99150 1.9917 1.9917	0.47086  FRODY INLET  PL /PTF	Pt/PTP	1_0J00 Y/DMAY 0.19800 0.43100 0.44500 J.48600 0.57200 0.58800 1.0000			
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13. 16.477   1.9450   3.98400   0.47071   3.72200   47   18.497   1.2770   0.45071   3.77375   0.91900   47   18.497   1.2770   0.45071   3.77375   1.0170   52   18.400   1.2466   0.45091   3.77479   1.0170   53001110MAL PRESSUPE BATIOS, FERN SPLITTER T.P.  WO WIRD PL PLPO PLYTTER PLYTE V/DMAX   7.72200   0.72241   7.42200   547   18.407   1.0574   7.7860   0.45559   0.67000   547   18.407   1.0574   7.7860   0.45559   0.67000   547   18.407   1.0574   7.7860   0.45559   0.67000   54001110MAL PRESSUPE PATIOS, FERN SPLITTER P.D.  WO WIRD PL PLYTON SPLITTER P.D.  WO WIRD PL PLYTON SPLITTER P.D.  WO WIRD PL PLYTON SPLITTER P.D.  10   18.4071   7.7860   0.4575   0.45750   0.45700   72   15.939   1.0011   0.7621   0.46590   0.45700   72   15.939   1.0011   0.7621   0.46590   0.46700   73   18.103   1.0011   0.7621   0.46590   0.46700   74   18.103   1.0011   0.7621   0.46590   0.46700   75   18.103   1.0011   0.7621   0.46590   0.46700   75   18.103   1.0011   0.7621   0.46590   0.46700   75   18.103   1.0011   0.7621   0.46590   0.46700   75   18.103   1.0011   0.7670   0.4670   0.46700   75   18.103   1.0011   0.7670   0.4670   0.4670   0.4670   0.4670   75   18.103   1.0011   0.7670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670   0.4670	וייון דנרכא<	of borddline	PATINS . PPI	MARY PLUG						
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17	77	16.477	1.0893	7.30400	0.67001					
1-2-6-0	37	19.425	1.2350	0.44674	7.759AA					
DEPOSITIONAL PRESSURE RATIOS	47	18.97)	1.2570	0.45591	0.77375	0.91900				
NOT WIRE PI PI PI PI PI PI PI PI PI PI PI PI PI	52	19.800	1.2466	0.45003	J.764 87	1.0176				
17.726 1.1761 7.42840 0.72341 2.42200 67 16.097 1.0674 7.38600 0.65656 0.67000  SANDIFIONAL PRESSURE PATIOS , FIRM SPLITTE P.D.  VAN ARROW PI PLEAT PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS PLANTS P	>ADDITION	AL PRESSURE	RATIOS . FLE	A cufitted l	.r.		<del></del>			
APOST 16,007 1,0074 3,198.00 0,6555 0,67003  ADDITIONAL PRESSURE MATIOS , FLOW SPLITTER C.D.  ADDITIONAL PRESSURE MATIOS , FLOW SPLITTER C.D.  TO 9,803 9,46443 9,23672 0,407255 0,50000  22 15,298 1,0011 0,74212 0,41560 0,67000  ADDITIONAL PRESSURE MATIOS , FLOTER CHORDS  WE WINDON TO 15,350 0,99867 0,75114 0,4167 1,2000 1,15115 1,158 1,2000 0,47000  107 15,158 0,99867 0,75114 0,4167 1,2000 0,1718 1,1590 0,47000  117 15,158 1,2001 0,7677 0,6114 0,7674 1,2000 0,1718 1,159 0,4000 0,47000  127 15,163 1,2001 0,7677 0,6114 0,7674 1,2000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,7000 0,4701 0,70	WIN WARD	Pt	PL /PO	PI / PTF	PL /PTP	X / DM A'K				
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	67	16.097	1.0674	7.38609	0.65656	0.67000				
77	>ADDITION	AT PRESSUPE	PATINS . FLO	W SPLITTEP P	·n,	**		<del></del>		
22 21.423 1.4206 0.51365 0.47161 0.58300 22 15.938 1.9011 0.75621 0.46180 0.67000  *********************************										
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127								•		
127	112	15.159	1.0951	9. 36356	0.61824	J-43100				
15, 15, 143				0.36404						
147 15.733	127			0.36220	0.61763					
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152	Fratition	M- DOCCCHOC	OFFICE CO	-NOTTIE FLAG		ــــــــــــــــــــــــــــــــــــــ				
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>ADDIT 109AL PRESSURE PATIOS . 20 DEG SHRDUD LOCATION  IVO HOPD DI DI/PD MI/PTE 91/PTP X/DMAX  167 15.139 1.0018 0.36236 0.61620 0.79300  177 15.139 1.0018 0.36236 0.61620 0.84400  >ADDIT 109AL PRESSURE PATIOS . 80 DEC SHRDUD LOCATION  IVI HOPD DI PI/PTE DI/PTE DI/PTE X/DMAX  182 14.018 0.92654 0.23622 0.57177 0.79300  187 13.269 0.92623 0.33503 0.56973 0.84400										
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1VI HOPD OF PLANT PLANTE OF PTP XADMAX 192 14-318 3-92954 3-23622 0-57177 3-79300 187 13-269 3-92623 (-33593 3-56973 3-84400						J. #440 ⁽ )				
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ayn aren		PI /PO	PI /PTF	Pt /PTP	X/NMAX			
	PI							
3.2	17.400	1.1566	2.37169	0.63238	). 72200			
7 7	23, 309	1.3490	4.43351	),77757	J.82000			
47	20.704	1.3692	0.43599	0.74860	J. 91 900			
52	27.299	1.3417	0.43118	0.73360	1.0170			
>annit iun	IAL PPESSUPE	RATIOS . FLO	W SPI ITTER I	. n.		* **		
AVD WORD	PI	Pt / PO	PL , PT F	PE /PTP	X/DMAY			
62	19.749	1.3060	0.41970	0.71408	0.42200			
47	17.945	1.1801	0.37923	0.64521	9 ₋ 67000			
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77	11.270	9. 74526		0.40747	0.50900			
PZ	15.875	1.0472	0. 3652	0.57254	0.58300			
92	15.130	1.0226	0.32153	0.54705	0.67900			
	M DRECEMPE	****	CTON CURRULA					
DAUN GAN	PE	PL/PQ	PL/PTF	PLANT	X/DMAX			
-197				0.54832				
	15.165	0029	0. 3222		-1.0000			
-112	15.255	1.000	2.2419	0.55157	-1.0000	·		<del></del>
-153	15.755	1,0000	0. 32619	0.55157	-1.0000			
-127	15.192	1,2039	9.32769	Q SAPAF	-1.0000			
	10,63.0	J. 0065A	0.32026	0.546	1.0000			
-137 -142		), 09658 0, 99989	0.37026 0.32137	0.54669	-1.0000 -1.0000			
-137 -1 <u>42</u> -2A001110N	15.120	0,99989 RATIOS . FOR	0+32132 EBODY INLET	0.54669	-17-4000			
-137 -142 -24221110N AVD HOPD	15.120	0,99989 RATIOS - FOR PL/PO	0+32132 FBCDY INLFT PL/PTF	0.546(9 PL/PTP	X/DMAX	-···•		
-137 -142 -24221110N AVD WOPD 107	15.120 PL 15.165	0,99989  RATIOS . FOR  PL/PO 1.0029	0.32132 FBCDY INLFT PL/PTF 0.37228	0.546(9 PL/PTP 0.54832	X/DMAX 2.39800	-···•		
-137 -142 -24201110N AVD HOPD	15.120	0,99989 RATIOS - FOR PL/PO	0+32132 FBCDY INLFT PL/PTF	0.546(9 PL/PTP	X/DMAX	- · · •		
-137 -162 -2A001110N AVD WOPD 107	15.120 PL 15.165	0,99989 RATIOS . FOR PL/PO 1.0029 1.0038	0.32137 EBODY INLET PL/PTF 0.37228 0.37419	0.546(9 PL/PTP 0.54832	X/DMAX 7.39800 0.42100	- · •		
-137 -142 -2A001TION AVD HOPD 107 112 127	15.120 PRESSUPE PL 15.165 15.255	0,99989  RATIOS . FOR  PL/PO 1.0029	0.32137 FRODY [NLFY PL/PTF 0.37228 0.37419 0.32419	0.546(9 PL/PTP 0.54832 0.55157 0.55157	X/DMAX 2.39800 0.42100 2.44900	· · •		
-137 -142 	PL 15.165 15.255 15.255 15.190	0,99989  RATIOS . FOR PL/PO 1.0029 1.0038 1.0038	0.32137 FBODY INLEY PL/PTF 0.37228 0.37419 0.32419 0.32260	PL/PTP 0-54832 0-55157 0-55157 0-554886	X/DMAX 7.39800 0.42100 9.44900 0.48600	···•		
-137 -142 -24091110N AVD WOPD 107 117 127 127 137	PL 15.165 15.255 15.255 15.255 15.270	0,99989 RATIOS . FOR PL/PO 1.0029 1.0048 1.0389 0.99658	0.32137 FBODY INLEY PL/PTF 0.37228 0.37419 0.32419 0.32419 0.32260 0.32026	PL/PTP 0.54832 0.55157 0.55157 0.554886 0.54489	X/DMAX 7.39800 0.42100 0.44900 0.48600 0.52200	•		
2A001110H AVD WOPD 107 117 127 127 127 127 127	PL 15.165 15.255 15.255 15.255 15.250 15.070 15.120	0,99989 RATIOS . FOR PL/PO 1.0029 3.0088 1.0388 1.0399 0.99558 0.99999	0.32137  FBODY INLET  PL/PTF 0.37228 0.37419 0.32419 0.32260 0.32026 0.32132	PL/PTP 0.54832 0.55157 0.55157 0.54886 0.54689	T-9000  X/DMAX  7.39800 0.42100 9.44800 U.48600 U.52200 0.58800	· •		
>A0011110N AVD WOPD 107 112 127 127 142 142	PL 15.165 15.255 15.255 15.255 15.270	0,99989 RATIOS . FOR PL/PO 1.0029 1.0048 1.0389 0.99658	0.32137 FBODY INLEY PL/PTF 0.37228 0.37419 0.32419 0.32419 0.32260 0.32026	PL/PTP 0.54832 0.55157 0.55157 0.554886 0.54489	X/DMAX 7.39800 0.42100 0.44900 0.48600 0.52200	•		
24001110N AVD WOPD 107 112 127 127 127 127 142 -152	PL 15.165 15.255 15.255 15.190 15.120	0,99989 RATIOS . FOR PL/PO 1.0029 1.0029 1.0038 1.0389 0.99658 0.99969	0.32137 FBODY INLEY PL/PTF 0.37228 0.37419 0.32419 0.32260 0.32026 0.32026 0.32132 0.37153	PL/PTP 0.54832 0.55157 0.55157 0.54886 0.54689 0.54669	X/DMAX 7.39800 0.43100 0.44900 0.48600 0.52200 0.58807	•		
2001110N AVD HOPD 107 117 127 127 127 142 -152 -157	PL 15.165 15.255 15.255 15.255 15.190 15.070 15.120 15.130 15.130 15.130	0,99989 RATIOS . FOR PL/PO 1.0029 1.0029 1.0788 1.0788 1.0789 0.99658 0.99990 1.0006	0.32137 FBODY INLEY PL/PTF 0.37228 0.37419 0.32419 0.32260 0.32026 0.32026 0.32132 0.37153	PL/PTP 0.54832 0.55157 0.55157 0.54886 0.54489 0.5469	7.9000 X/DMAX 7.39AD0 0.42100 9.44900 0.48600 0.52200 0.58800 1.0000	•		
2A001110N AVD WOPD 107 112 127 127 127 127 127 127 142 -152 -157 A001110N	PL 15.165 15.255 15.255 15.190 15.120 15.120	0,99989 RATIOS . FOR PL/PO 1.0029 1.0048 1.0388 1.0389 0.99658 0.99989	0.32137 FBODY INLEY PL/PTF 0.37228 0.37419 9.32260 0.32026 0.32132 0.32132	0.546(9 PL/PTP 0.54832 0.55157 0.55157 0.54886 0.54489 0.54669 0.54669	X/DMAX 7.39800 0.42100 9.44900 0.52200 0.58807 1.0000	•		
-137 -142 >AODITION AVD HOPD 107 112 127 127 127 127 127 127 12	PL 15.165 15.255 15.255 15.255 15.190 15.070 15.120 15.130 15.130 15.130	0,99989 RATIOS . FOR PL/PO 1.0029 1.0029 1.0788 1.0788 1.0789 0.99658 0.99990 1.0006	0.32137 FBODY INLEY PL/PTF 0.37228 0.37419 0.32419 0.32260 0.32026 0.32026 0.32132 0.37153	PL/PTP 0.54832 0.55157 0.55157 0.54886 0.54489 0.5469	7.9000 X/DMAX 7.39AD0 0.42100 9.44900 0.48600 0.52200 0.58800 1.0000	•		
2A001110N AVD WOPD 107 112 127 127 142 -152 -157 2A01110N AVO WOPD -152	PL 15.165 15.255 15.255 15.255 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120	0,99989 RATIOS . FOR PL/PO 1.0029 1.0048 1.0389 0.9958 0.9958 0.9990 1.0006 845505 . FAN	0.32137  FBODY INLEY  PL/PYF 0.37228 0.37419 9.32260 0.32026 0.32026 0.32153 0.32153 0.32153	PL/PTP 0.54832 0.55157 0.55157 0.54886 0.54489 0.54669 0.54669 0.54705	X/DMAX 7.39800 0.42100 0.48900 0.52200 0.58807 1.0000  X/PMAX -1.0000	•		
-137 -142 -24001110H AVD WOPD 107 117 127 127 127 137 142 -152 -157 	PL 15.165 15.255 15.255 15.255 15.190 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120	0,99989  RATIOS . FOR  PL/PO 1.0029 1.0028 1.0389 1.0389 0.9965P 0.99989 1.0006 1.0006 1.0006 1.0006 1.0006 1.0006 1.0006	0.32132  FRONY INLEY  PL/PTF 0.37228 0.37419 0.32260 0.32260 0.32132 0.32153 0.32153 0.32153 0.32153	0.54669  PL/PTP 0.54832 0.55157 0.55157 0.5486 0.54669 0.54669 0.54705 0.54705	*/nmax 7.39800 0.42100 0.42100 0.48900 0.52200 0.58800 1.0000 **/nmax -1.0000 -1.0000			
-137 -142 	PL 15.165 15.265 15.265 15.265 15.265 15.260 15.100 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120	0,99989  RATIOS . FOR  PL/PO 1.0029 1.0029 1.0038 1.0389 1.03990 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996 1.9996	0.32137  FRODY INLEY  PL/PTF 0.37228 0.37419 0.32419 0.32260 0.32026 0.32132 0.32153 0.32153 0.32151  DEG SHPOID I  PI/PTE	PL/PTP 0.54832 0.55157 0.55157 0.55486 0.54689 0.54669 0.54705 0.54705	X/DMAX 7.39800 0.42100 0.42100 0.48600 0.52200 0.58800 1.0000  X/DMAX -1.0000 -1.0000	•		
-137 -142 	PL 15.165 15.255 15.255 15.255 15.255 15.190 15.120 15.120 15.120 15.120 15.120 15.120 15.120	0,99989  RATIOS . FOR  PL/PO 1.0029 1.0038 1.0389 0.9965P 0.99900 1.0006  PATIOS . FAN PATIOS . 20  PL/PO 1.0006	0.32137  FBODY INLEY  PL/PYF 0.37228 0.37419 9.32260 0.32026 0.32026 0.32153 0.32153 0.32153 0.32153 0.32153	PL/PTP 0.54832 0.55157 0.55157 0.55486 0.54489 0.54669 0.54669 0.54705 PL/PTP 0.54705 0.54705	X/DMAX 7.39AR0 0.42100 9.44900 0.48600 0.57200 0.58800 1.0000 1.0000 X/DMAX 0.79300	•		
24001110H AVD WOPD 107 117 117 127 127 127 127 127 127 127 12	Pt 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.145	0,99989  RATIOS . FOR  PL/PO 1.0029 1.0029 1.0038 1.0389 1.0399 0.9965P 0.99969 1.0006 1.0006 PATIOS . 20  PL/PO 1.0006 1.0006 1.0006	0.32132  EBONY INLEY  0.37228 0.37419 0.32419 0.32260 0.32026 0.32132 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153	0.54669  PL/PTP 0.54832 0.55157 0.55157 0.55486 0.54669 0.54669 0.54705 0.54705 PL/PTP 0.54705 PL/PTP 0.54705 0.54766	X/DMAX 7.39800 0.42100 0.42100 0.48600 0.52200 0.58800 1.0000  X/DMAX -1.0000 -1.0000	•		
-137 -142 -24001110M AVD WOPD 107 112 127 127 142 -152 -157	PL 15.165 15.265 15.265 15.265 15.265 15.170 15.120 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.145	0,99989  RATIOS . FOR  PL/PO 1.0029 1.0038 1.0389 0.9965P 0.99989 1.0006 1.0006 1.0006 1.0006 1.0006 1.0015	0.32137  FBODY INLEY  PL/PYF 0.37228 0.37419 9.32260 0.32026 0.32026 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153	PL/PTP 0.54832 0.55157 0.55157 0.55486 0.54489 0.54669 0.54669 0.54705 0.54705 0.54705 0.54705 0.54760	X/DMAX 7.39400 0.42100 9.44900 0.48600 0.52200 0.58800 1.9000 1.0000 -1.0000 X/DMAX 0.79300 0.84400	•		
-137 -142 -2A001110M AVD WOPD 107 112 127 137 142 -152 -157	Pt 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.145	0,99989  RATIOS . FOR  PL/PO 1.0029 1.0029 1.0038 1.0339 0.9965P 0.99989 1.0006 1.0006 1.0006 1.0006 1.0006 1.0006 1.0006 1.0006 1.0006	0.32132  FRONY INLET  PL/PTF 0.37228 0.37419 0.32419 0.32260 0.32026 0.32132 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153	PL/PTP 0.54832 0.55157 0.55157 0.55157 0.5486 0.54669 0.54669 0.54705 PL/PTP 0.54705 PL/PTP 0.54705 0.54760 PL/PTP	X/DMAX 7.39800 0.42100 9.44900 0.52200 0.58809 1.0000 1.0000  X/DMAX 0.79300 0.84409			
-137 -142 -24001110M  AVD WOPD 107 117 117 127 127 127 127 127 127 -152 -157 -24001110M  AVD WOPD 167 177 -24001110M  AVD WOPD 167 177 -24001110M  AVD WOPD 187	Pt 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.130 15.145	0,99989  RATIOS : FOR  PL/PO     1.0029     1.0039     0.9965P     0.99969     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006	0.32132  EBONY INLEY  PL/PTF 0.37228 0.37419 0.32419 0.32260 0.32260 0.32132 0.32153 0.32153 0.32161  PL/PTF 0.32153 0.72165  DEG SHPOUD 1  PL/PTF 0.72975	PL/PTP 0.54832 0.55157 0.55157 0.55486 0.54669 0.54669 0.54705 0.54705 PL/PTP 0.54705 0.54760 PL/PTP 0.54765 0.54760	X/DMAX 7.39800 0.42100 9.44900 0.52200 0.52200 0.58809 1.0000 1.0000  X/DMAX 0.79300 0.84400	•		
-137 -142 -24001110M  AVD WOPD 107 112 127 127 142 -152 -157 -24001110M  AVD WOPD 167 177 -24001110M  AVD WOPD 167 177 -24001110M  AVD WOPD 187	PL 15.165 15.265 15.265 15.265 15.265 15.265 15.190 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120	0,99989  RATIOS - FOR  PL/PO 1.0029 1.0029 1.0038 1.0339 0.9965P 0.99900 1.0006 1.0006 1.0006 PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS - FAN  PATIOS	0.32137  FRONY INLEY  PL/PYF 0.37228 0.37419 0.32419 0.32260 0.32026 0.32132 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153	PL/PTP 0.54832 0.55157 0.55157 0.55157 0.5486 0.54669 0.54669 0.54705 PL/PTP 0.54705 PL/PTP 0.54705 0.54760 PL/PTP	X/DMAX 7.39800 0.42100 9.44900 0.52200 0.58809 1.0000 1.0000  X/DMAX 0.79300 0.84409			
-137 -142 -24001110M AVD WOPD 107 112 127 127 142 -152 -157 -24001110M AVD WOPD 167 177 -24001110M AVD WOPD 167 177 -24001110M AVD WOPD 187	PL 15.165 15.265 15.265 15.265 15.265 15.265 15.190 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120 15.120	0,99989  RATIOS : FOR  PL/PO     1.0029     1.0039     0.9965P     0.99969     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006     1.0006	0.32137  FRONY INLEY  PL/PYF 0.37228 0.37419 0.32419 0.32260 0.32026 0.32132 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153 0.32153	PL/PTP 0.54832 0.55157 0.55157 0.55486 0.54669 0.54669 0.54705 0.54705 PL/PTP 0.54705 0.54760 PL/PTP 0.54765 0.54760	X/DMAX 7.39800 0.42100 9.44900 0.52200 0.52200 0.58809 1.0000 1.0000  X/DMAX 0.79300 0.84400			

184 J- 65 30	2 DAEFIM	INARY DATA	06/13/79	CADDELL	PFC 10/25/79 07:16:47.789	FAC 98681	PGM C034 NDG 1504
ניחן דון (מיל	AT PRESSUPE	PATINS . PPI	MADA OFFIC				
VD WORD	PL	PI /PO	PI / PTF	PI /PTP	X/DMAX		
32	19.257	1.2744	0.35212	0.59063	0.72200		
77	22.052	1.4593	0.40227	0.68665	0.82000		
47	22.967	1.5132	0.41813	0.71203	0.91900		
52	22.632	1.4977	0.41383	0.79471	1.0170		
>tonit inn	AL PRESSIPE	PATIOS , FLO	W SPITTER I	. n.			
VD WOPT	0.4	PL/PÑ	PI /PTF	PĮ /PYP	x/DMAX		
	PL 23,437						
62 67	22.092	1.5509 1.4613	0.42855 0.40377	Q.72977 Q.68758	0.42200 9.€7000		
·	42.1172	114013	0.40577	94 CHY2C			
NOT 1 1 CC V	AL PRESSIRE	PATINS . FLO	W SPLITTER P	. n.			
VD WOPD	Pt	PL / PO	PL /PTF	PL/PTP	X/DMAX		
77	13.059	0.86409	0.23876	0.40659	0.50800	_	
97	19.39R	1.2175	0.37640	0.57286	0.59300		
97	15-148	1.0024	0.27698	<u>-47167</u>	0.67000		
- FUOTIEM	AL DRESSURE	0 A T LOS 5 15	CTOR SHROW				
VO WILD		<b>ም</b> ይ / ቦብ	PI / PTF	01 / 1934	X/DMAX		
107	15.074	0.99745	0. 27561	0.46933	-1.0000		•
112	15.148	1.0924	3.27698	0.47167	-1,0000 -1,0000		
122	15.198	1-0057	27729	0.47372	-1.0000		
127	15-203	1.0061	0.27799	0.47338	-1.0000		
		1.0017					and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
177							
137			0.27489 0.27597	0.46996	-1.0000		
137	15.093	0. 99877	0.27597	0.46996	1.0000		<del></del>
132	15.093		0.27597			·	<u>-</u>
132	15.093	0. 99877	0.27597		10000	· - ·	
>4771TION	15.093 AL PRESSURE PL	0.99877	0.27597 ERCOV THEFT	0.46996			-
142 >ADDITION VO MORD	15.093 AL PRESSURE	7. 99877 RATIOS + FOR PL/PO	0.27597 ERODY THEFT PL/PTF	0.46996 PL/PTP 0.46933	X/DMAX 0-39000		
142 >ADDITION VD WORD 197 112	15.093 AL PRESSURE PL 15.073 15.148	0. 99877  RATIOS . FOR  PL/PO 0.99745 1.0224	0.27597 ERCOV THEFT PL/PTF 0.27561 0.27698	0.46996 Pt /PTP 0.46933 0.47167	X/DMAX 0.39000 0-43100	•	-· · · · · · · · · · · · · · · · · · ·
142 >ADDITION VD WORD 197	15.093 AL PRESSURE PL 15.073 15.148 15.198	0.99877  RATIOS , FOR  PL/PO 0.99745 1.0057	0.27597 ERCOV THEFT PL/PTF 0.27561 0.27698 0.27789	0.46996 PL/PTP 0.46933	X/DMAX 0.39800 0.43100 0.44900	• • •	
142 >ADDITION VO MORD 197 112 122	15.093 AL PRESSURE PL 15.073 15.148	0. 99877  RATIOS . FOR  PL/PO 0.99745 1.0224	0.27597 ERCOV THEFT PL/PTF 0.27561 0.27698	Pt /PTP 0.46933 0.47167 0.47322	X/DMAX 0.39800 0.43100 0.44900 0.48600	• • •	
142 >ADDITION VD WORD 107 112 122 127	15.093 AL PRESSIRE PL 15.073 15.148 15.198 15.203	0.99877  RATIOS , FOR  PL/PO 0.99745 1.0057 1.0061	0.27597 PL/PTF 0.27561 0.2759 0.27789 0.27789	0.46996 PL/PTP 0.46933 0.47167 0.47322 0.47338	X/DMAX 0.39800 0.43100 0.44900	•	
142 >ADDITION VD MORD 107 112 127 127 137 142	15.093 AL PRESSURE PL 15.073 15.148 15.198 15.293 15.138	0.99877  RATIOS . FOR  PL/PO 0.99745 1.0024 1.0057 1.0061 1.0017	0.27597 PL/PTF 0.27561 0.27698 0.27799 0.27799	PL/PTP 0.46933 0.47167 0.47328 0.47136	X/DMAX 0.39800 0.43100 0.48600 0.52200	•	
142 >ADDITION VD MORD 197 112 127 127 137 142	15.093 AL PRESSURE PL 15.073 15.148 15.198 15.293 15.138	0.99877  RATIOS . FOR  PL/PO 0.99745 1.0057 1.0061 1.0017 0.99877	0.27597  PL/PTF 0.27561 0.27698 0.27789 0.27789 0.27789 0.27789	Pt /PTP 0.46933 0.47167 0.47328 0.47136 0.47136 0.46996	X/DMAX 0.39800 0.49100 0.48600 0.52700 0.58800	•	
142 >ADDITION VD WORD 197 112 127 127 137 142 152	15.093 AL PRESSURF PL 15.073 15.148 15.198 15.203 15.138 15.093 15.142	0.99877  RATIOS FOR  PL/PO 0.99745 1.0057 1.0061 1.0017 2.99877	D. 27597  ERRORY TNL FT  PL / PTF  9.27561 0.27569 0.27799 0.27799 0.27597 0.27597	0.46996 Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47136 0.46996	X/DMAX 0.39000 0.43100 0.44900 0.52200 0.52200 0.52200		
142 >ADDITION VD MORD 107 117 127 127 137 142 152 153 167	15.093 AL PRESSURE PL 15.073 15.148 15.198 15.203 15.138 15.093 15.142 15.093	0.99877  RATIOS . FOR  PL/PO 0.99745 1.0026 1.0017 2.99877 1.0026	D. 27597  ERRORY TNL FT  PL / PTF  9.27561 0.27569 0.27799 0.27799 0.27597 0.27597	0.46996 Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47136 0.46996 0.47213	X/DMAX 0.39#00 0.43100 0.44900 0.52700 0.52700 0.58#00 1.0000	•	
142 >ADDITION VD WORD 107 112 127 137 142 152 157 >ADDITION VD WORD	PL 15.093 AL PRESSURE PL 15.073 15.148 15.198 15.203 15.138 15.093 15.143 15.093	0. 99877  RATIOS , FOR  PL/PO 0. 99745 1. 0024 1. 0057 1. 0061 1. 0017 0. 99877 1. 0024 1. 0024	D. 27597  ERRORY INLEY  PL/PYF  0.27561 0.27698 0.27789 0.27789 0.27789 0.27560 0.27560 0.27560 0.27560	0.46996  Pt /PTP 0.46933 0.47167 0.47328 0.47338 0.47134 0.46996 0.47212	X/DMAX 0.39800 0.43100 0.44909 0.48600 0.52200 0.58800 1.0000 -1.0000	•	
142 >ADDITION VD WORD 107 117 127 127 137 142 152 153 	Pt 15.073 15.148 15.198 15.203 15.138 15.143 443 45.143	0.99877  RATIOS , FOR  PL/PO 0.99745 1.0026 1.0057 1.0061 1.0017 0.99877 1.0026 1.0034	9. 27597  ERCOV THEFT  PL/PTF  9. 27561  9. 27699  9. 27680  9. 27680  9. 27597  9. 27597  9. 27725	0.46996  Pt /PTP 0.46933 0.47167 0.47328 0.4738 0.47136 0.46996 2.47212 0.47213	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 1.0000	•	
142 >ADDITION VD WORD 107 112 127 137 142 152 157 >ADDITION VD WORD	PL 15.093 AL PRESSURE PL 15.073 15.148 15.198 15.203 15.138 15.093 15.143 15.093	0. 99877  RATIOS , FOR  PL/PO 0. 99745 1. 0024 1. 0057 1. 0061 1. 0017 0. 99877 1. 0024 1. 0024	D. 27597  ERRORY INLEY  PL/PYF  0.27561 0.27698 0.27789 0.27789 0.27789 0.27560 0.27560 0.27560 0.27560	0.46996  Pt /PTP 0.46933 0.47167 0.47328 0.47338 0.47134 0.46996 0.47212	X/DMAX 0.39800 0.43100 0.44909 0.48600 0.52200 0.58800 1.0000 -1.0000	•	
NO MORD 197 117 127 127 137 147 147 147 147 147 147 147 147 147	PL 15.073 15.148 15.198 15.293 15.138 15.293 15.134 15.443 44.08555406	0.99877  RATIOS , FOR  PL/PO 0.99745 1.0026 1.0057 1.0061 1.0017 0.99877 1.0026 1.0034	D. 27597  PL/PYF 0.27561 0.27698 0.27789 0.27789 0.27789 0.27597 0.27597 0.27597 0.2725 0.27725	0.46996  Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47136 0.46933 0.47136 0.47213 0.47213 0.47213 0.47213	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 1.0000		
NO MORD 197 117 127 127 137 147 147 147 147 147 147 147 147 147	PL 15.073 15.148 15.198 15.293 15.138 15.293 15.134 15.443 44.08555406	0. 99877  RATIOS . FOR  PL/PO 0. 99745 1. 0024 1. 0057 1. 0061 1. 0017 2. 99877 1. 0024 1. 0024 1. 0034	D. 27597  PL/PYF 0.27561 0.27698 0.27789 0.27789 0.27789 0.27597 0.27597 0.27597 0.2725 0.27725	0.46996  Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47136 0.46933 0.47136 0.47213 0.47213 0.47213 0.47213	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58800 1.0000 1.0000		
142 >ADDITION  VO MORD  107 112 122 127 137 142 152 157 >ADDITION	PL 15.073 15.148 15.198 15.293 15.138 15.198 15.293 15.138 15.193 15.143 15.163 AL PRESSURE	0. 99877  RATIOS , FOR  PL/PO 0.99745 1.0024 1.0057 1.0061 1.0017 0.99877 1.0024 1.7974 AATIOS , FAN  PL/PO 1.0034 RATIOS , 20	0.27597  PL/PTF 1.27561 0.27698 0.27789 0.27789 0.27789 0.27789 0.27789 0.27789 0.27789 0.27789 0.27789	0.46996  Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47134 0.46996 0.47213 0.47213 0.47213	X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 -1.0000 -1.0000 -1.0000		
142 >ADDITION  VD MORD 107 112 122 127 137 142 152 157  >ADDITION  VD MORD	15.093 AL PRESSURE PL 15.073 15.148 15.198 15.203 15.138 15.093 15.142 15.163 AL PRESSURE PL 15.163 AL PRESSURE	0. 99877  RATIOS , FOR  PL/PO 0.99745 1.0057 1.0061 1.0017 2.99877 1.0026 1.0036 1.0034 1.0034 RATIOS , CAN PL/PO	0.27597  PL/PTF 0.27561 0.27698 0.27789 0.27789 0.27789 0.27597 0.27597 0.27597 0.27725 0.27725	0.46996  Pt /PTP 0.46933 0.47167 0.47338 0.47139 0.47213 0.47213 0.47213	X/DMAX 0.39800 0.49100 0.48600 0.52700 0.58800 1.0000 1.0000 1.0000 -1.0000		
142 >ADDITION  VO MORD 107 112 122 127 137 142 152 157 >ADDITION  VO MORD 167 179	PL 15.163 15.163 AL PRESSURE PL 15.073 15.148 15.198 15.293 15.138 15.093 15.143 15.163 AL PRESSURE PL 15.163 AL PRESSURE PL 15.163	0. 99877  RATIOS . FOR  PL/PO	D. 27597  ERONY INLEY  PL / PYF	Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47134 0.46996 2.47213 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213	X/DMAX 0.39000 0.43100 0.44900 0.48600 0.52200 0.52200 0.52200 1.0000 1.0000 1.0000 1.0000 1.0000		
142 >ADDITION VD MORD 107 112 127 127 137 142 152 157 >ADDITION VD MORD 152 157 >ADDITION	PL 15.073 15.148 15.198 15.293 15.138 15.093 15.142 15.143 AL ORECCURE PL 15.163 AL PRESSURE PL 15.158 15.158 AL PRESSURE	0. 99877  RATIOS . FOR  PL/PO	D. 27597  PL/PYF	Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47136 0.46933 0.47136 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213	X/DMAX 0.39000 0.43100 0.44900 0.48600 0.52700 0.58000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		
142 >ADDITION  VO MORD  107 112 122 127 142 152 157  ADDITION  VO MORD  167 177  >ADDITION  VO MORD	PL 15.073 15.148 15.198 15.293 15.138 15.093 15.143 15.163 AL PRESSURE PL 15.163 AL PRESSURE PL 15.158 15.159 AL PRESSURE	0. 99877  RATIOS , FOR  PL/PO 0.99745 1.0224 1.0057 1.0061 1.0017 0.99877 1.0024 1.0034 1.0034  RATIOS , EAN  PL/PO 1.0031 1.0031  PATTOS , 80	9. 27597  ERONY THEFT  PL/PTF  9. 27561  9. 27699  9. 27690  9. 27690  9. 27597  9. 27597  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27725  9. 27776  PE/PTF  9. 27716  9. 27716  9. 27716  9. 27716	0.46996  Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47134 0.46996 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213 0.47198 0.47198 0.47198	X/DMAX 0.39800 0.49100 0.48600 0.52700 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX 0.79300 0.84400		
142 >ADDITION  VD WORD 107 112 127 127 137 142 152 157  ADDITION  VD WORD 167 179 >ADDITION  VD WORD 167 179 >ADDITION  VD WORD 167	PL 15.073 15.148 15.198 15.293 15.138 15.293 15.138 15.093 15.143 15.163 AL PRESSURE PL 15.163 AL PRESSURE PL 15.158 15.158 AL PRESSURE PL 15.158 15.158	0. 99877  RATIOS , FOR  PL/PO 0. 99745 1. 0024 1. 0057 1. 0061 1. 0017 7. 99877 1. 0024 1. 0034 1. 0034 1. 0034 RATIOS , FAN  PL/PO 1. 0034 RATIOS , 20  PL/PO 1. 0031 1. 0031 PATIOS , 80	9. 27597  ERONY INLEY  PL / PYF 9. 27561 9. 27698 9. 27789 9. 27789 9. 27789 9. 27725 9. 27725 9. 27725 9. 27725 9. 27725 9. 27725 9. 27725 9. 27725 9. 27725 9. 27725 9. 27725 9. 27726 9. 27726 9. 27716 9. 27716 9. 27716 9. 27716 9. 27716 9. 27716 9. 27716 9. 27716 9. 27716 9. 27716 9. 27716 9. 27716	Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47134 0.46996 2.47213 0.47213 0.47213 Pt /PTP 0.47213 Pt /PTP 0.47198 0.47198 PCATION Pt /PTP 0.44629	X/DMAX 0.39800 0.49100 9.44909 0.48600 0.52200 0.58800 1.0000 -1.0000 -1.0000 X/DMAX 0.79300 0.84400		
142 >ADDITION  VD MORD 107 117 127 127 137 142 152 157  ADDITION  VD MORD 167 177 >ADDITION  VD MORD 167 177	15.093 AL PRESSURE PL 15.073 15.148 15.198 15.203 15.138 15.093 15.143 15.093 15.163 AL PRESSURE PL 15.163 AL PRESSURE PL 15.158 15.159 AL PRESSURE PL 14.333 14.273	0. 99877  RATIOS , FOR  PL/PO 0.99745 1.0224 1.0057 1.0061 1.0017 0.99877 1.0024 1.0034 1.0034  RATIOS , EAN  PL/PO 1.0031 1.0031  PATTOS , 80	D. 27597  ERRORY INLEY  PL/PYE	0.46996  Pt /PTP 0.46933 0.47167 0.47322 0.47338 0.47134 0.46996 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213 0.47213 0.47198 0.47198 0.47198	X/DMAX 0.39800 0.49100 0.48600 0.52700 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX 0.79300 0.84400		

	F	****** D. T.	0/413433	CARRELL	000 1042547	0.000.00	F15 aug 11	200 000		•
1-121V	IDMAL PRESSUPE	INAPY DATA	76/13/7°	CAUDELL	KEC 1015211	9 0?:[#:25.024	FAC MXAXI	PG4 (034	PNG 1595	•
AND MUD		PL / PO	PI / PT F	P1 /PTP	X/DMAX					4
32 37	20.299 23.199	1.3473 1.5387	0.34027 0.38870	0.59763 0.67127	0.72200 9.82000					
47	24.452	1.6226	0.40990	0.70788	0.91900					
5.7	24.242	1.6087	0.40638	0.70191	1.0170					•
	ICHAL PRESSIPE					<del></del>				
		-								•
AVD WOP		PI /PN	PI /PTF	PL/PTP	X/DMAX					
- 67	24.912 22.399	1.6531	0.41761 0.37546	0.72120 0.64841	0.42200 0.67000					•
>47717	IONAL PRESSUPE	PATTOS . FLO	W SPLITTEP T	`. n.						
AVN WOP	n PL	PL /PO	PL /PTF	PL/PTP	X/DMAX					
77	14.195	0.94131	0.23779	0.41066	0.50800					
A 2	20. 259	1.3310	0.33625	0.54069	0.58300					•
92	15.120	1.0033	0.25346	0.43772						
->+6011	town byce the	AATIOS _ SJE	ctor sunger.		·					•
AVD WOR	P	PL/PO	PL/PTF	سسمها	Y/DMAX					
-107	15.965	0. 99969	0.25254	0.43613	-1.0000					- (
112	15.160	1.0000	7. 25413	0.43668	-1-0000					
-127	15.195	1_00	25472	0.43989	-1.0000					
-127	15.150	1.0253	C. 253 ap	0.43859	-1.0000					
-137	15.045	0.9983A	0.25220	0.43555	-1.0000			%:	•	
سستغدا-	15,745	0.99836	0.25550	0.43555	1.0000					
>ADDIT	INNAL PRESSURE	PATINS . FOR	FRODY INLET							
AVO HOP	D PL	PL/PO	PL / PTF	PL/PTP	X/DMAX					
107	15,065	0. 99969	0.25254	0.43613	0.39900		•			
112	15,160	1.0060	0.25413	0.43888	0.43100					
122	15.175	1.0043	0.25472	0.43989	0.44909					
127	15,150	1.0053	7.25396	2.43859	0.48600					
1 2 7	15.345	7.99836	2.25729	0.43555	0.52200					
147	15,045	7. 99836	0. 25220	0.43555	0.50800		-	-		•
-153	15-170-		A_2534/							
-1	1121	1.0007	9.2534	0.45706	-1+0000					
	lumin valdense	AATIONFAN	HOTTLE FLAS							
ለቁኮ ብሀቱ፤		120		PI /PTP	X/DMAX					•
-15?	15-120-	1.7737	25346	0.43772	-1.0000					
-151	15.125	1.0937	1. 2434 <u>4</u>	3.43786	-1.0000					
**************************************	INNAL PRESSURE	RATIOS . 20	DEG SHPOUD L	OCATION						
- AVO WOP		PL/PO	PL/PTF	PI /PTP	X/DMAY					
167	15.120	1.0033	0.25346	0.43772	7. 79300					
_ 172	15.110	1.0927	0.25329	0.43743	0.84400					
>4 <u>????</u>	JUNVI BUEZZIBE	RATINS + 80	DEG SHECUD L	NCATION						
C AYN WER		PI /PN	Pt / PTF	PL/PTP	X/DMAX					í
107	14.455	7.95977	0.24232	0.41847	0.79300					
107	14.470	).95557	0.24130	0.41689	0.84400					(
	H 5 . MEASIRED									•
(F-D) 1	129.0 FIC	1173.2	STOWN FO 3.P	1042 FT	APF 2.4507	DSM 2.351#	CFM 9.3321777			

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NASE-LEWI	S PRELIM	INAPY DATA	06/11/79	CANDETE	PEC 10/25/79	02:19:34-063	FAC MYEXE	PG# 1934	R.L.V - 5
>42011104	AI PPFSSIJPF	RATIOS , PPI	MAPY PLUG						
VP WOPP	PL -	PL / PO	M /PTF	PL /P TP	X/PMAX				
3.2	29.170	1.3392	0.33610	0.57443	0.72200				
7	23.312	1.5478	0.78847	0.66392	9.62000				
47	24.651	1,6367	0.4107P	0.70205	0.91900				
52	74.446	1.6231	0.49736	0.69655	1.0170				
	~	RATIOS . FLO							
									•
AU MUBU	PI	Pt /PO	PI /PTF	PI /PTP	X/DMAX				
£ 2	25.061	1.6639		0.71372	0.42200				
67	22.393	1.4961	0.3729#	0.63746	0.67900				
ADDIT ION	AL DRESSURE	RATINS . FLO	W SPEETTER P	·.n.					
n womb	PL	PL / PO	PL /PTF	PL /PTP	X/DMAX				
77	14.233	0.94477	0.23712	0.40526	0.50800				
7 ' <b>7</b> 2	20.145	1.3375	0.37569	0.57372					
2	15.094	1.0022	0. 25152	0.42987	0.57300 0.67900				
			-						
		AATIOS , EJE		<del> </del>					
IN WORD	PL	PL /PD	PL / PTF	PL/PER	X/DMAX				
.07	15.074	2000	0.25119-	0.42930	-1.0000				
12	15.164	1.0066	7.7269	0.43187	-1.0000				
72	15.174	1.0077	11.05206	0.43215	-1.0000				
27	15.115	1.0035	0.75186	C-43044	-1.0000				
									and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
	1119	0.99719	0- 25027	0-62776					
97	15.014 AL PRESSIME	0.99719 0.99686 RATIOS , FOR	0.25027 0.25019 ERCOY THIET	0.42760	-1.0000 -1.0000				
ANDITION	15.014 AL PRESSIME	0.99686  RATIOS . FOR	7.75019 ERCOV THLET PL/PTF	0.42760 PL/PTP	-1.0000 -1.0000 X/DMAX				
ADDITION	15.014 AL PRESSIME PL 15.074	0.99686  PATINS , FOP  PL/PN 1.0008	7,25019 ERFOY THLET PL/PTF 0,25119	9.42769 Pt /PTP 0.42930	-1.0000 -1.0000 X/DMAX 0.39800		- •		
ANDITION	15.014 AL PRESSIME PL 15.074 15.164	0.99686  RATIOS , FOP  PL/PO 1.0008 1.0068	0.25019 ERCOV THLET PL/PTF 0.25119 0.25269	0.42760 PL/PTP 0.42930 0.43187	-1.0003 -1.0000 X/DMAX 0.39800 0.43100		- •		
ADDITION	15.014 AL PRESSIME PL 15.074	0.99686  PATINS , FOP  PL/PN 1.0008	7,25019 ERFOY THLET PL/PTF 0,25119	9.42769 Pt /PTP 0.42930	-1.0000 -1.0000 X/DMAX 0.39800		• • •		
27 52 24 ADDITION 27 11:2 27 27	15.014 AL PRESSIME PL 15.074 15.164	0.99686  RATIOS , FOP  PL/PO 1.0008 1.0068	0.25019 ERCOV THLET PL/PTF 0.25119 0.25269	0.42760 PL/PTP 0.42930 0.43187	-1.0003 -1.0000 X/DMAX 0.39800 0.43100		•		
27 52 ADDITION PD WCPD 27 12 22 27	15.014 AI PRESSIME PL 15.074 15.164 15.174	0.99686 RATIOS , FOP PL/PO 1.0008 1.0068 1.0775	0.25019 ERMY THLET PL/PTF 0.25119 0.25289 0.25286	PL/PTP 0.42930 9.43187 0.43215 0.43044	X/DMAX 0.39800 0.43100 0.4600		- •		
27 62 0 ANDIT INN 0P WCPD 07 117 22 27	15.014 A1 PRESSUME PL 15.074 15.164 15.114 15.019	0.99686  PATINS , FNP  PL / PN 1.0008 1.0068 1.0775 1.0735 0.99719	0,25019 ERCOV THLET PL/PTF 0.25119 0.25269 0.25286 0.25186 0.25186	PL/PTP 0.42930 9.43187 0.43215 0.43044 0.42774	-1.0000 -1:0000 X/DMAX 0.39800 0.43100 0.44900 0.4600 0.52200		•		
27 62 ANDITION OF WOPD 27 12 27 27	15.014 A1 PRESSIPE PL 15.074 15.164 15.174 15.114	0.99686 PATINS , FRP PL / PR 1.0008 1.0068 1.0775 1.0035	7,25019 ERCOV INLET  PL/PTF	PL/PTP 0.42930 9.43187 0.43215 0.43044	X/DMAX 0.39800 0.43100 0.4600		•		
27 42 ANDITION: P WCPD 27 12 27 27 27	15.014 AI PRESSIME PL 15.074 15.164 15.174 15.114 15.019 15.014	0.99686  RATIOS , FOP  M / PO 1.0008 1.0075 1.0075 0.99719 0.99686	0,25019 ERCOV THLET PL/PTF 0,25119 0,25269 0,25286 0,25186 0,25027 0,25019	9.42769 PL/PTP 0.42930 9.43187 0.43215 0.43044 0.42774 3.42760	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.46600 0.52200 0.58800				
ADDITION  PD WCPD  77  12  27  27  42  42	15.014  A1 PRESSUME  PL 15.074 15.164 15.114 15.019 15.014	0.99686  PATINS . FRP  PI / PR 1.0008 1.0068 1.0775 1.0735 0.99719 9.99686	0,25019 ERCOV THLET  PL/PTF 0,25119 0,25269 0,25286 0,25186 0,25027 0,25019 0,35144	9.42769 PL/PTP 0.42930 9.43187 0.43215 0.43774 3.42760 0.43033	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.58800		•		
27 42 ADDITION: P WCPD 27 12 27 27 27 27 27 27	15.014  A1 PRESSUME  PL 15.074 15.164 15.114 15.019 15.014	0.99686  PATINS , FNP  PL/PN 1.0008 1.0068 1.0775 1.0735 0.99719 0.99686 1.9018	0,25019 ERCOV THLET  PL/PTF 0,25119 0,25269 0,25286 0,25186 0,25027 0,25019 0,35144	9.42769 PL/PTP 0.42930 9.43187 0.43215 0.43774 3.42760 0.43033	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200 0.5800 1.0000		•		
ADDITION:  P WCPD  77  12  27  27  42  42  42  40017 ION:	15.014  A1 PRESSIME  PL 15.074 15.164 15.174 15.114 15.019 15.014 15.019 15.014	0.99686  PATINS , FRP  PI / PR 1.0008 1.0068 1.0775 1.0735 0.99719 0.9986 1.0177	7,75019 ERCOV INLET  PL/PTF	PL/PTP 0.42930 9.42187 0.43215 0.43044 0.42774 3.42760 0.4363	-1.0000 -1:0000 X/DMAX 0.39800 0.43100 0.44900 0.4600 0.52200 0.58800 1.0000		•		
27 42 ADDITION PD WCPD 27 12 27 27 42 52 42 52 42 53 44 54 56 47 48 57 48 57 48 58 58 58 58 58 58 58 58 58 5	15.014  A1 PRESSUME  PL 15.074 15.164 15.174 15.114 15.019 15.014 15.019 15.014 15.000 17.070	0.99686  PATINS , FOP  PL / PO 1.0008 1.0068 1.0775 1.0935 0.99719 0.99686 1.0018 1.7777  AASSOS , FAN	7,75019 ERCOV THIET  PL/PTF	PL/PTP 0.42930 9.43187 0.43215 0.43044 0.42774 3.42760 0.43072 0.42771	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52200 0.58800 -1.0000		•		
27 42 40017 ION: 10 HOPD 27 27 27 27 27 27 27 27 27 27	PI 15.039  PI 15.074  15.164  15.174  15.116  15.019  15.019  15.019  15.090  PI 15.090  15.090	0.99686  PATINS . FOP  PI / PO 1.0008 1.0068 1.0775 1.0735 0.99719 0.99686 1.0018 1.0777	7,75019 ERCOV INLEY PL/PTF 0,25119 0,25269 0,25286 0,25186 0,25027 0,25027 0,25020 0,35144 0,25152	PL/PTP 0.42930 9.4315 0.43044 0.47774 3.42760 0.4362 0.42777	-1.0000 -1:0000 X/DMAX 0.39800 0.43100 0.44900 0.4600 0.52200 0.58800 1.0000		•		
27 42 ANDIT ION: P WCPD 27 12 27 27 27 27 27 27 27 27 27 27 27 27 27	PI 15.039  PI 15.074  15.164  15.174  15.116  15.019  15.019  15.019  15.090  PI 15.090  15.090	0.99686  PATINS , FOP  PL / PO 1.0008 1.0068 1.0775 1.0935 0.99719 0.99686 1.0018 1.7777  AASSOS , FAN	7,75019 ERCOV INLEY PL/PTF 0,25119 0,25269 0,25286 0,25186 0,25027 0,25027 0,25020 0,35144 0,25152	PL/PTP 0.42930 9.4315 0.43044 0.47774 3.42760 0.4362 0.42777	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52200 0.58800 -1.0000		•		
27 42 ADDITION: PO WOPD 27 27 27 27 27 27 27 27 27 27	15.014  AI PRESSIME PL 15.074 15.164 15.174 15.114 15.019 15.039 19.090 PL 15.099 15.099 15.099 AL PRESSIRE PL	0.99686  PATINS . FRP  PI / PN 1.0008 1.0068 1.0775 1.0935 0.99719 0.99686 1.0018 1.0777  AATIOS . FAN	7,75019 ERCOV INLEY PL/PTF	PL/PTP 0.42930 9.4315 0.43044 0.43774 3.42760 0.43033 0.42761 0.42973 0.42973 0.42973	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52200 0.58800 -1.0000 X/DMAX		•		
27 40017 ION 10 WOPD 17 17 27 27 27 27 27 27 27 27 27 2	PI 15.094  AI PRESSIME PL 15.074 15.164 15.174 15.116 15.019 15.019 15.090 17.094  AI PRESSIRE PI 15.094	0.99686  PATINS . FOP  PI / PN 1.0008 1.0068 1.0775 1.0735 0.99719 0.99686 1.0018 1.0777  AATION FAN  **AN **AN **AN **AN **AN **AN **AN	9,75019 ERCOV INLEY PL/PTF 0,25119 0,25269 0,25286 0,25186 0,25027 0,25019 0,35144 0,25152 DEG SHORIID 1 M/PTF 0,25152	PL/PTP 0.42930 9.43187 0.43044 0.43774 3.42760 0.4363 0.42777 0.42973 0.42987	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX -1.0000 -1.0000				
PANDITION  IP WIPD  17  117  27  27  27  27  27  27  27  2	15.014  AI PRESSIME PL 15.074 15.164 15.174 15.114 15.019 15.039 19.090 PL 15.099 15.099 15.099 AL PRESSIRE PL	0.99686  PATINS . FRP  PI / PN 1.0008 1.0068 1.0775 1.0935 0.99719 0.99686 1.0018 1.0777  AATIOS . FAN	7,75019 ERCOV INLEY PL/PTF	PL/PTP 0.42930 9.4315 0.43044 0.43774 3.42760 0.43033 0.42761 0.42973 0.42973 0.42973	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52200 0.58800 -1.0000 X/DMAX				
27 42 40017 ION 10 17 17 27 27 27 27 27 42 52 52 53 60 WOPD 52 57 60 WOPD 62 57 60 WOPD 62 67 67 67 67 67 67 67 67 67 67	15.014  At PRESSIME  PL 15.074 15.164 15.174 15.114 15.019 15.014 15.019 15.014 At PRESSIRE  PL 15.099 15.094 At PRESSIRE  PL 15.094 At PRESSIRE	0.99686  PATINS . FOP  PI / PN 1.0008 1.0068 1.0775 1.0735 0.99719 0.99686 1.0018 1.0777  AATION FAN  **AN **AN **AN **AN **AN **AN **AN	9,25019 ERCOV INLET  PL/PTF 0.25119 0.25269 0.25286 0.25027 0.25019 0.25027 0.25019 0.25144 0.211  MOZILE FLAG  PL/PTF 0.25152 0.25152	PL/PTP 0.42930 9.4315 0.43044 0.42774 3.42760 0.43032 0.42973 0.42973 0.42977 0.42987 9.42987	-1.0000 -1:0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 1.0000 X/DMAX -1.0000 -1.0000				
PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION  PADDITION	PL 15.074 15.164 15.174 15.114 15.019 15.014 15.090 19.0% AL PRESSIRE PL 15.090 15.094 AL PRESSIRE PL 15.094 AL PRESSIRE PL 15.094 AL PRESSIRE	0.99686  PATINS , FOP  PI / PO 1.0008 1.0068 1.0775 1.0735 0.99719 0.99686 1.0177 AATIOE , FAN  M/PD 1.0018 1.0722 PATINS , 70  PATINS , 80	9.75019 ERCOY INLEY PL/PTF 0.25119 0.25269 0.25286 0.25077 0.25017 0.25027 0.25014 0.25144 0.25152 DEG SHAPPHIN 1	PL/PTP 0.42930 9.4315 0.43046 0.47774 3.42760 0.4362 0.42771 PL/PTP 0.42973 9.42987 PCATION PL/PTP 0.42987 9.42987	-1.0000 -1:0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 0.79300 0.84400				
PANDIT INN  IP WIPD  107  112  27  27  27  27  27  27  27  28  ANDIT INN  IN WIPD  152  557  657  657  657  70 WIPD  167  70 WIPD	15.014  AI PRESSIME  PL 15.074 15.164 15.174 15.114 15.019 15.034 16.080 19.078  AL PRESSIME  PL 15.099 15.094  AL PRESSIME  PL 15.094  AL PRESSIME	0.99686  PATINS , FRP  PI / PRI 1.0008 1.0008 1.0075 1.0035 0.99719 0.99686 1.0018 1.0077 AATIOS , FAN  PRI PRI 1.0022 1.0022 PATINS , RO PI / PRI PRI PRI PRI PRI PRI PRI PRI PRI PRI	7.75019 ERCOV INLET  PL/PTF	PL/PTP 0.42930 9.43187 0.43215 0.43044 0.42776 0.42760 0.43673 0.42760 0.42973 0.42977 PL/PTP 0.42987 PCATION PL/PTP	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52200 0.58800 -1.0000 X/DMAX -1.0000 -1.0000 Y/DMAX 0.79300 0.84400				
ANDITION  IP WOPD  177  117  127  27  27  27  27  27  40  40  40  40  40  40  40  40  40  4	15.014  At PRESSIME PL 15.074 15.164 15.164 15.174 15.114 15.019 15.019 15.019 15.019 15.090 17.0%  At PRESSIRE PL 15.099 15.094 At PRESSIRE PL 15.094 At PRESSIRE PL 15.094 At PRESSIRE PL 15.094 At PRESSIRE	0.99686  PATINS . FOP  PI / PN 1.0008 1.0068 1.0775 1.0735 0.99719 0.99686 1.0777 AASTOS . FAN 1.0722  PATINS . 70 PI / PN 1.0022 1.7722  PATINS . R0 PI / PN 0.95970	9,25019 ERCOV INLET  PL/PTF 0.25119 0.25269 0.25286 0.25027 0.25010 0.25027 0.25010 0.25144 0.271  MOZILE FLAD  PL/PTF 0.25152 DEG SHPOHD 1  PL/PTF 0.25152 DEG SHPOHD 1  PL/PTF 0.24087	PL/PTP 0.42930 9.4315 0.43044 0.42774 3.42760 0.43032 0.42761 0.42973 0.42973 0.42987 0.42987 0.42987 0.42987 0.42987 0.42987	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.44900 0.52200 0.58800 -1.0000 X/DMAX -1.0000 -1.0000 Y/DMAX 0.79300 0.84400		•		
PARDITION  APP WPP  107  117  127  27  27  27  27  27  27  27	PL 15.074 15.164 15.174 15.164 15.174 15.114 15.219 15.214 15.299 17.274  AL PRESSURE PL 15.099 15.099 15.094 AL PRESSURE PL 15.094 AL PRESSURE PL 15.094 AL PRESSURE PL 14.454 14.454	0.99686  PATINS , FRP  PI / PRI 1.0008 1.0008 1.0075 1.0035 0.99719 0.99686 1.0018 1.0077 AATIOS , FAN  PRI PRI 1.0022 1.0022 PATINS , RO PI / PRI PRI PRI PRI PRI PRI PRI PRI PRI PRI	9.75019 ERCOV INLEY  PL/PTF 0.25119 9.25769 0.25286 0.25286 0.25077 9.25019 9.35144 9.271 0.25152  DEG SHPOUD 1 PL/PTF 0.24087 0.24087	PL/PTP 0.42930 9.43187 0.43215 0.43044 0.42776 0.42760 0.43673 0.42760 0.42973 0.42977 PL/PTP 0.42987 PCATION PL/PTP	-1.0000 -1.0000 X/DMAX 0.39800 0.43100 0.48600 0.52200 0.58800 -1.0000 X/DMAX -1.0000 -1.0000 Y/DMAX 0.79300 0.84400				

		005. ***	14464 0474	04.433.436		nce 10/25/70 00-41-12	<b>6</b> 46 amama	0cm	F	
	4451-1 FVIS		IMERY DATA	06/13/79	CADDETT	PEC 10/25/79 02:21:13.224	FAC 98681	PGM C734	PDG 1507	_
	28 1.0 (4 (1.448)	f bar //ms	RATIOS . PP	HARY PIUG						
-	AVD WOPD	Pt	bf \ btJ	bf \bak	PI /PTP	X/DMA X				_
	32	19.246	1.2749	0.35158	0.60008	0.77200				~
	37	21.954	1.4529	n <b>. 4</b> 0966	0.58386	3-82000				
	47	22.926	1.5105	D. 41654	0.71096	0-91900				
	5.7	27.606	1.4960	0.41753	0.70411	1.0170				
	PAULLIUNT	t PRESSUPF	PATINS , FLI	W CHITTEP I	1.D.					•
	AVP MEPS	PL	PI /PO	PI / PTF	PL /PTP	x \Umax				
	<u> </u>	23.421	1.5499	0-42740	0.72949	J. 42200				_
	67	22.941	1.4586	0.40277	0.69651	0.67000				-
	> ADDITIONAL	PRESSIRE	RATIOS . FLO	W SPLITTEP I	·_ n_		r <del>Tanada (1970-1974) angalako (niversitako (1990-19</del> 4-194 - An			
	AVD WOPD	PL	PL / PO	PL /PTF	PL /PTP	X/DMAX				-
	77	13.975	0.86530	0.23662	0.40720	3.50809				
	P2	18.411	1.2194	0.33598	0.57346	J.58300				
	92	15-151_	1.0026	0.27649	0.47192	<u>11-6 7000</u>				
	PAUDITIONAL	-005551105	BATIOS FU	CTCR_SHROW						•
	AMD 11000		- 400	m /nTr	24 222	* ******				
	AVD 40PD -107	PL	FL/PO	PL/PTF	PLIER	X/DHAX		-	-	
		15.741	2 99536	0.2744	0.46849	-1.0000				_
	-112 -12?	15.136 15.711	1-2016	621_	0.47145	_1_0000				
	-127		1.0053	N. P2759	0.47379	-1.0000				
	-117	15.191	1.0030	0.27722	0.67316	-1.0000 -1.1000			-	_
	-نافا-	15.121	1.0007	0.27594	0.47200	-1:000				
					94-19-0					•
	>ADDITIONAL	PRESSURE	PATINS . EN	ENCOY INLET						
	AVE WEED	PL	PL/PO	PL/PTF	PL/PTP	x/DMAX				•
	197	15.741	0. 99536	0.27448	0.46849	0.39800				
	112	15,136	1,0016	0.27621	0.47145	0.43100				
	127	15.211	1.0766	0.27759	0.47379	0.44900		2.0		
		15.191	1.0053	0.27722	0-47316	0-4 8600				
_	137	15.156	1.7230	0.27658	0.47237	0.52200				<del></del>
	147	15.121	1.9907	0.27594	0.47098	0.58800				
	-	14.14				1-0000				-
	-1-1	17-171	\$-97ZH	11-215-97	0:-18-5	<del></del>				•
_	- LOOLE COM	MESSUM	AATIOS FA	407715 FLA					· · · · · · · · · · · · · · · · · · ·	
	AVO HOPD	PL	77.400	PL / DT 5	PIPTP	X/DMAX				•
	-157	15.141	1.0939	1-21667	0.47273	-1.0000				-
	-157	-4	1.9126	0.27646	0.42192	-1.0000				
	DATE TITES	PRESSURE	PATINS , 20	DEG SHRPIJO I	DEATION					
	ልሃቦ ሦባፆቦ	PL	PL/PN	PI / PT F	P1 /PTP	X/BMAX				
	147	15.156	1.0030	0.27658	0.47207	0.79300			*	_
	177	15.156	1.0030	9.27658	0.47207	J. 84400				
						90 0-799				•
	~ >40014 IUNV	PRESSIME	CA . ZDITAR	DEC 2HEDOU"	DCATION					
	Udur unv	PL	Pt /PT	Pt / PTF	PI /PTP	X/DMAX				
	1	14.376	7. 74 804	0.26143	0.44627	0.79300				
	[ n 7	14.716	3.94976	9.25942	0.44279	0.84400				Ć.
			THPHST PAPER			ar 2 2012 - 004 2 4074	55H 0 0001170			<u> </u>
	_ {f=0} 1003.1	, ,,,	994.03	SIGMA IC 5.4	-47 FTS	RF 2.2917 NSM 2.4976	CF4 0.0021173			•

ASA-LEHTS	JOET LAI	HARY DATA	76/13/30	CARDELL	PFC 10/25/79 02:22	11.694	FOR SYNKE	PG4 C034	R.C.1/ PDG 1509
APDITIONA	f boccolbe	PATINE . PPIM	IVDA BITIC						
				PI /PTP	y / DMAX				
U SUBD	PI	bi You	PI /PTF		0.72200				
7	17.40P	1.1549	0.22500	0.63550					
7	2 7 <b>.</b> 368	1.7447	n.43335	C.7359F	J.8200-)				
7	27.693	1.3451	7.47571	0.75129	0.51900				
7	23.293	1.3397	0.43121	0.73676	1.0170				
					- **				
APPIT TONA	PRESSIPE	PATINS , FINE	4 SPLETTER T	.n.					
กษายา	PI	Pt / PO	PI / PTF	PI /PTP	X\UMBX				
		1.3001	0.41877	0.71 51	0.42700				
7	19.698		0.77902	0.64758	0.67000				
7	17.978	1.1767	0. 11402	U-6417-					
APPLITION	PRESSIME	RATINS , FIR	SPITTER O	. n.					
กฐาน	PL	PI / PO	PL / PT F	Pt /PTP	X AMOLX				
7	11,262	0.74327	0.23947	0.40906	0.50000				
		1.0433	0.33607	0.57429	2.58300				
2	15.878				0.67000				
2	15.198	1.0031	0.37310	0.55704					
-	+	**************************************	CALL CHARGE						
D MUBD	Pl	P) /PO	PI / PTF	PLEASE	X/IMAX				
07	15.228	10250	0.37376	U. 55317	-1.6000				
		1.0110	75.65	0.55640	-1.0000				
12	15.318		N-32507	0. = 54.9=	-1.0000				
77	15.333	1.0							
~ ~	15.243	1.9960	0.32406	0.55368	-1.0000				
21									
	73	0.00811	0.32150	6.50035	-1.0000				
37	15.159	0.09811 1.0004	0.32150 0.32225	0.5000	1.0000				
37	15.154	1.0004	0.32225					and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
	15.154	1.0004 PATIOS , FOP	0.32225 FRODY INLET	0. <<0<	0000				
37 42 422 IT INNA 10 WOPD	15.154 L PRESSIME	1.0004 PATIOS , FOP PL/PO	0.32225 FRODY INLET PL/PTF	0. EENEG	X/DPAX			an orași a desperii de desperii de desperii de de de de de de de de de de de de de	
37 42 47) [1 [ <u>11144</u> D. WOPD	15.158 it pressime pt 15.228	1.0004 PATIOS , FOP PL/PO 1.0050	0.2225 FBCDV INLET PL/PTF 0.32774	0.55056 PL /PTP 0.55313	7.39800			and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	
ATTITINA B WOPD	15.154 IL PRESSIME PL 15.228 15.316	1.0004  PATIOS , FOP  PL/PO 1.0050 1.0110	0.2225 FRODY INLET PL /PTF 0.32374 0.32561	0.55713 0.55713	X/DMAX 0.39800 0.43100		•		
37 42 43 43 43 43 43 43 43 43 43 43 43 43 43	15.158 it pressime pt 15.228	1.0004 PATIOS , FOP PL/PO 1.0050	0.2225 FBCDV INLET PL/PTF 0.32774	0.55059 PL /PTP 0.55313 0.55540 0.55695	X/NMAX 9.39800 0.43109 9.44900			andre de deservir estervir	
37 43 43 43 43 43 43 43 43 43 43 43 43 43	15.154 L PRESSIME PL 15.228 15.318 15.333	1.0004  PATIOS . FOP  PL/PO 1.0050 1.0110 1.0120	0.2225 FRODY INLET PI /PTF 0.32374 0.32561 0.32593	0.55713 0.55713	X/DMAX 0.39800 0.43100				
37 42 42 42 42 43 44 44 44 44 44 44 44 44 44 44 44 44	15.154 PRESSIME PL 15.228 15.318 15.333 15.243	1.0004  PATIOS . FOP  PL/PO 1.0050 1.0110 1.0120 1.02060	0.32275 FBODY INLET PI /PTF 0.32374 0.32561 0.32561 0.32606	PL /PTP 0.55313 0.55540 0.55695 0.55368	X/NMAX 9.39800 0.43109 0.44900		•		
37 42 42 42 42 11 Inna 9 Word 97 12 27 27 27	15.158 PL 15.228 15.318 15.333 15.243 15.123	1.0004  PATIOS . FOP  PL/PO 1.0050 1.0110 1.0120 1.0260 0.99811	0.32275 FBCDY INLET PL/PTF 0.32374 0.32561 0.32561 0.32566 0.32150	PL /PTP 0.55313 0.55695 0.55368 0.54937	X/DMAX 9.39800 0.43109 9.44909 9.52209		•		
37 42 42 42 42 11 INNA 0 WOPD 07 12 27 27 27 37	15.159 PL PRESSIME PL 15.228 15.318 15.333 15.243 15.173 15.159	1.0004  PATIOS . FOP  PL/PO 1.0050 1.0110 1.0120 0.99011 1.0004	0. 2225 FRODY INLET PL/PTF 0. 32374 0. 32501 0. 32501 0. 32506 0. 32150 0. 32725	PL /PTP 0.55313 0.5540 0.55695 0.55367 0.54037 0.55059	X/DMAX 0.39800 0.43100 0.44900 0.4600 0.52200 0.58800		•		
37 42 42 42 42 6 WOPD 07 12 27 27 27 42	15.158 PL 15.228 15.318 15.333 15.243 15.123	1.0004  PATIOS , FOP  PL/PO 1.0050 1.0110 1.0120 1.0260 0.9981 1.0004	0.2225 FRODY INLET PL/PTF 0.32374 0.32593 0.32593 0.32593 0.32150 0.32725	PL /PTP 0.55313 0.55569 0.55368 0.5437 0.55059	X/NMAX 9.39800 0.43109 9.44900 0.52200 0.52200		•		
37 42 47 47 47 47 47 47 47	15.159 PL PRESSIME PL 15.228 15.318 15.333 15.243 15.173 15.159	1.0004  PATIOS . FOP  PL/PO 1.0050 1.0110 1.0120 0.99011 1.0004	0. 2225 FRODY INLET PL/PTF 0. 32374 0. 32501 0. 32501 0. 32506 0. 32150 0. 32725	PL /PTP 0.55313 0.5540 0.55695 0.55367 0.54037 0.55059	X/DMAX 0.39800 0.43100 0.44900 0.4600 0.52200 0.58800		•		
37 42 47 47 6 WOPD 07 12 27 27 27 27 42 42	PE SSIME PE SSIME PL 15.228 15.318 15.333 15.243 15.173 15.159 15.169	1.0004  PATIOS , FOP  PL/PO 1.0050 1.0110 1.0120 1.0260 0.9981 1.0004	0.2225 FBCDY INLET PI /PTF 0.32374 0.3250 0.3250 0.3250 0.32150 0.32725 0.32725	PL /PTP 0.55313 0.55569 0.55368 0.5437 0.55059	X/NMAX 9.39800 0.43109 9.44900 0.52200 0.52200		•		
37 42 AND IT INNA OD WOPD 07 12 22 27 27 37 42 42	PL 15.228 15.228 15.316 15.333 15.243 15.123 15.123 15.123 15.143 15.144	1.0004  PATIOS : FOP  PL/PO 1.0050 1.0110 1.0120 1.0260 0.99811 1.0004 1.0021	0.2225 FBCDY INLET PI /PTF 0.32374 0.3250 0.3250 0.3250 0.32150 0.32725 0.32725	PL /PTP 0.55313 0.55540 0.55695 0.55368 0.54037 0.55059	X/DMAX 9.39800 0.43109 9.44900 0.52209 0.52209 0.58800 -1.0000		•		
37 42 42 42 50 60 60 60 60 60 60 60 60 60 60 60 60 60	PL 15.228 15.318 15.333 15.243 15.159 15.159 15.159 15.159 15.159 15.159 15.159 15.159	1.0004  PATIOS . FOP  PL/PO 1.0050 1.0110 1.0120 1.0206 0.99811 1.0204 1.004 1.004	0.2225 FBCDY INLET PI /PTF 0.32374 0.3250 0.3250 0.3250 0.32150 0.32725 0.32725	PL /PTP 0.55313 0.55540 0.55695 0.55368 0.54037 0.55059 0.55150 0.75128	X/NMAX 9.39800 0.43109 9.44900 0.5200 0.58800 -1.0000		•		
37 42 Ann it inna 07 12 27 27 27 27 42 42 42 42 43 43 44 47	PL 15.228 15.228 15.316 15.333 15.243 15.123 15.123 15.123 15.143 15.144	1.0004  PATIOS FOR  PL/PO 1.0150 1.0110 1.0120 1.0260 0.9981 1.0004 1.0014 1.0014	0.2225 FBODY INLET PI /PTF 0.32374 0.32503 0.32503 0.32503 0.32503 0.32225 0.32225 0.32225	0,55059 Pt /PTP 0.55313 0.55695 0.55368 0.54037 0.55059 0.55150	X/DMAX 9.39800 0.43109 9.44900 0.52209 0.52209 0.58800 -1.0000		•		
37 42 42 42 42 43 42 42 42 43 44 42 43 44 44 45 46 47 47 48 48 48 48 48 48 48 48 48 48 48 48 48	PL 15.228 15.316 15.333 15.243 15.159 15.159 15.163 15.163 15.163 15.163 15.163 15.163 15.163 15.163	1.0004  PATIOS FOR  PL/PO 1.0050 1.0110 1.0120 1.0260 0.99811 1.0004 1.0004 1.0005 1.0005 1.0005	0. 22225 FRODY INLET PI /PTF 0. 32374 0. 32503 0. 32503 0. 32503 0. 32503 0. 32725 0. 32725 0. 32726 0. 32726 0. 32726 0. 32726 0. 32726 0. 32726 0. 32726	PL /PTP 0.55313 0.55695 0.55695 0.55068 0.5607 0.55150 0.55150 0.55150	X/DMAX 9.39800 0.43100 9.44900 0.4600 0.52200 0.58800 -1.0000 -1.0000 X/DMAX -1.0000				
37 42 42 42 42 42 42 42 42 43 44 42 43 44 44 45 47 47 47 48 48 48 48 48 48 48 48 48 48 48 48 48	PL 15.193 15.194 15.276 15.333 15.243 15.159 15.159 15.163 15.164 PL 15.163 PL 15.163 PL 15.164	1.0004  PATIOS , FOP  PL/PO 1.0050 1.010 1.0120 1.0200 0.9881 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 PATIOS , FAM	0. 2225 FRODY INLET  PI /PTF 0. 32374 0. 32503 0. 32503 0. 32150 0. 32725 0. 32278 7. 22789 N0374F FAAS	0.55059 Pt /PTP 0.55313 0.55695 0.55697 0.55059 0.55059 0.55150 0.55150 0.55150	X/DMAX 9.39800 0.43100 9.44900 0.48600 0.52200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 -1.0000				
37 42 AND IT INNA B WOPD 07 12 22 27 27 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 15.228 15.228 15.318 15.333 15.243 15.159 15.159 15.159 15.163 17.168 PL PRESSURE	1.0004  PATIOS , FOP  PL/PO 1.0150 1.0110 1.0120 1.0204 1.0004 1.0074 PATIOS , FAM  PATIOS , 20 PL/PO	0.2225 FRODY INLET PI /PTF 0.32374 0.32593 0.32593 0.32406 0.32150 0.32725 0.32728 3.2728 3.2728 0.32245 0.32246 0.32246 0.32278	PL /PTP 0.55313 0.5569F 0.5536R 0.5569F 0.5536R 0.5407 0.55150 7.55150 PL /PTP 0.55150	X/DMAX 9.39800 0.43109 9.44900 0.52200 0.52200 0.58800 -1.0000 -1.0000 -1.0000		•		
37 42 42 40 MOPD 07 12 22 27 27 27 27 27 27 27 27 27 27 27 27	PL 15.228 15.316 15.333 15.243 15.123 15.124 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125 15.125	1.0004  PATIOS FOR  PL/PO 1.0150 1.0110 1.0120 1.026 0.9981 1.0004 1.0004 1.0004 1.0004 1.0004 PATIOS FAM  P/PO 1.0004 PATIOS 70	0. 22225 FRODY INLET  PI /PTF 0. 32374 0. 32503 0. 32503 0. 32503 0. 32725 0. 32278 0. 32278 0. 32289  NO224F FAMS 0. 32289  DEG SHRCHID 1	PL /PTP 0.55313 0.55695 0.55695 0.55068 0.56037 0.55059 0.55150 0.55150 0.55150 0.55150	X/DMAX 9.39800 0.43109 9.44900 0.5200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000		•		
37 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 15.228 15.228 15.318 15.333 15.243 15.159 15.159 15.159 15.163 17.168 PL PRESSURE	1.0004  PATIOS , FOP  PL/PO 1.0150 1.0110 1.0120 1.0204 1.0004 1.0074 PATIOS , FAM  PATIOS , 20 PL/PO	0.2225 FRODY INLET PI /PTF 0.32374 0.32593 0.32593 0.32406 0.32150 0.32725 0.32728 3.2728 3.2728 0.32245 0.32246 0.32246 0.32278	PL /PTP 0.55313 0.5569F 0.5536R 0.5569F 0.5536R 0.5407 0.55150 7.55150 PL /PTP 0.55150	X/DMAX 9.39800 0.43109 9.44900 0.52200 0.52200 0.58800 -1.0000 -1.0000 -1.0000		•		
37 42 600 11 1000 07 12 27 27 27 42 42 42 42 42 42 42 42 42 42 42 42 42	PL 15.228 15.228 15.318 15.333 15.243 15.159 15.169 15.169 15.163 15.169 PL 15.163 15.169	1.0004  PATIOS FOR  PL/PO 1.0150 1.0110 1.0120 1.026 0.9981 1.0004 1.0004 1.0004 1.0004 1.0004 PATIOS FAM  P/PO 1.0004 PATIOS 70	0.2225 FRODY INLET  PI /PTF 0.32374 0.32593 0.32593 0.32765 0.32778 3.2278  NO2245 F445  PI /PTF 2.32289  DEG SUPPLIE 1 0.32278 0.32278	PL /PTP 0.55313 0.56569 0.55698 0.55698 0.54037 0.55050 0.56150 0.55150 0.55150 0.55150 0.55150 0.55150	X/DMAX 9.39800 0.43109 9.44900 0.5200 0.58800 -1.0000 -1.0000 -1.0000 -1.0000 X/DMAX -1.0000 -1.0000		•		
37 42 42 42 43 43 44 47 47 47 47 47 47 47 47 47 47 47 47	PL 15.228 15.316 15.333 15.243 15.159 15.163 15.163 15.163 15.163 15.163 15.163 15.163 15.163 15.163 15.163 15.163 15.163 15.163 15.163	1.0004  PATIOS _ FOP  PL/PO 1.0150 1.0110 1.0120 1.020 0.99811 1.0004 1.0004 1.0004 1.0004 PATIOS _ FAM  P/-0 1.0004 PATIOS _ 70  PATIOS _ 70	0.2225 FRODY INLET  PI /PTF 0.32374 0.32593 0.32593 0.32765 0.32778 3.2278  NO2245 F445  PI /PTF 2.32289  DEG SUPPLIE 1 0.32278 0.32278	PL /PTP 0.55313 0.56569 0.55698 0.55698 0.54037 0.55050 0.56150 0.55150 0.55150 0.55150 0.55150 0.55150	X/DMAX  0.39800 0.43100 0.44900 0.48600 0.52200 0.58800 -1.0000 -1.0000 -1.0000 x/DMAX -1.C000 -1.7900		•		
37 42 42 40 WOPD 07 12 77 77 77 42 55 65 65 65 65 65 65 65 65 65 65 65 65	PL 15.193 15.193 15.193 15.193 15.193 15.193 15.193 15.193 15.193 15.193 15.193	1.0004  PATIOS , FOP  PL/PO 1.0050 1.0110 1.0120 1.0200 0.99811 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 PATIOS , FAM PL/PO 1.0001 1.0001 PATIOS , 90 PL/PO PATIOS , 90 PL/PO	0. 2225 FRODY INLET  PI /PTF 0. 32374 0. 32503 0. 32503 0. 32150 0. 32150 0. 3225 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278	0.55059 0.55313 0.555695 0.55695 0.55697 0.55059 0.46150 0.55150 0.75150 0.75150 0.75150 0.75150 0.75150	X/DMAX 9.39800 0.43109 9.44900 0.52209 9.5200 9.58800 -1.0000 -1.0000 -1.7090 X/DMAX 1.0900 -1.7999		•		
37 42 40 MOPD 07 17 17 27 27 27 27 27 27 27 27 27 27 27 27 27	PL 15.183 15.184 15.286 15.318 15.333 15.243 15.159 15.159 15.163 15.169 15.183 15.193 15.193 15.193 15.193	1.0004  PATIOS , FOP  PL/PO 1.0150 1.0110 1.0120 1.0204 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 1.0004 PATIOS , FAN  P/PO 1.0021 1.0021 PATIOS , 90 PL/PO 0.92309	0. 2225 FRODY INLET  PI /PTF 0. 32374 0. 32593 0. 32593 0. 3276 0. 3276 0. 32778 0. 3278 0. 3278 0. 3278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278 0. 32278	PL /PTP 0.55313 0.56569 0.55698 0.55698 0.54037 0.56150 7.55160 0.55150 0.55160 0.55160 0.55160 0.65160 0.65160	X/DMAX 9.39800 0.43109 9.44900 0.52200 0.58800 -1.0000 -1.7000  X/DMAX -1.C000 -1.79300 0.84400				
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444-1 EM1	d ubtiles	INAPY DETA	06/13/79	CARRETT	REC 19/25/79 02:23:57.806	FAC AX641	R / 1 PSM C034	
AND IT INV	AT PRESSURE	PATINS . PPI	MAPY PLUS					
n weep	PI	Pt /PT	PI / PTF	Pt /PTP	X/DMAY	•		
,	16-430	1.0982	0.39282	9.67924	J. 72200			
7	18.620	1.2340	0.44545	9.74005	0. # 2000			
7	18.375	1.2575	0.45295	0.77454	0.91900			
?	14.795	1.2456	0.44964	9.76719	1.0170			
ADD FT ION	AL DRESSIME	RATIOS . FLE	W SPLITTER I	. 0.	Committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the committee of the commit			
ח שוייפוי	Pl	PL / PO	PL / PT F	PL /PTP	XYDWAX			
2	17. 725	1.1746	0. 42404	0.72351	J.42200			
,	15-117	1.0676	0.38540	0.65758	a. 6 7 <b>20</b> 2			
LOUIT INK	AL PRESSIPE	PATINS . FLO	IN SPETTTER P	. n.	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	. 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WEED.	PL	PL / PO	PI /PTF	PI /PTP	X /DMAX			
7	9.7973	9.64927	0.23439	0.39991	0.50000			
1	21.491	1.4235	0.51388	0. 676 80	0.5P300			
	15.115_	1.0017	0.36159	0-61696				_
OFF TON	A-PRESSIPE	****** * EVE	<del>6-2 in - 21140113 -</del>					
MORD	PL	PL/PO	PL/PTF	PLANT	X/DHAX			
7	14.045	99967	0. 36087	0.61573	-1.0000			
2	15-175	1.0356	U.36203 _	0.61941				
7	15.160	1.0446	7.4267	0.61879	-1.0000			
7	15.150	1.0033	0.36219	0.61798	-1.0000			
	-47.745	3.99702	0.35002	0.7.1-10	-1.0000			
7	15.022	3. 99536	0.35937	0.61309	1.0000			
· 	15.022		0.35937					
27 2711104 HORD	15.022 AL PRESSURF	J. 99536 PATIOS . FOR PL/PO	0.35937 PL/PTF	9.6139# PL/PTP	X/DMAX			
27 2711104 HORD	15.022 AL PRESSURE Pt 15.085	0.99536 PATIOS - FOR PL/PO 0.99967	0.35937	9.6139#	1.1000	•		
7 201110W WORD 7	15.022 AL PRESSURF	J. 99536 PATIOS . FOR PL/PO	0.35937 PL/PTF	9.6139# PL/PTP	X/DMAX	•		
2011104 9 4089 7	15.022 AL PRESSURE Pt 15.085	0.99536 PATIOS - FOR PL/PO 0.99967	0.35937 EPPON INLET PL/PTF 0.36087 0.36303	0.6130A Pt/PTP 0.61573 0.61941	X/DMAX 0.39809 0.43100	•		
201110N 0 40RD	15.022 AL PRESSURF PL 15.085 15.175	PATIOS - FOR PL/PO 0.09967 1.0056	0.35937 PERDOY INLET PL/PTT 0.36987 0.36303 0.36267	9.61308 PL/PTP 0.61573 0.61941 0.61879	X/DMAX 0.39800 0.43100 0.44900	•		
2011104 0011104 0 WORD 7 2	15.022 AL PRESSURE Pt 15.085 15.175 15.160	0.99536 PATIOS . FOR PL/PO 0.99967 1.0056 1.0046	0.35937 HERDDY INLET PL/PTF 0.36087 0.76303 0.76267 0.36219	Pt/PTP 0.61573 0.61941 0.61879 0.61778	X/DMAX 0.39800 0.43100 0.44403 0.6600	•		
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77	6,6397	0.57235	0.22838	0.38712	0.50800			
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07	15.021	2 99510	0. 3970	0.47306	-1.0000			
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77	15.386	0.90941	0.39878	0.67507	0.44900			
77	15.116	1.0014	9. 20054	0.67731	0.48600			
77	15.126	1.0721	0.79984	0.67776	2.52200			
47	15.796	1.0001	0. 29905	0.67642	0.56600			
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77	16.571	1.0950	0. 57009	0.87917	0.82000			
47	16.696	1.1226	J. 52372	0.00527	J. 91900			
7	16.656	1.1996	0.52276	0.49368	1.0170			
ANDIT IONA	I PPESSIRE	PATINS . FIR	M CH ITTEP I	.9.				THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE P
n word	PI	P( /PO	PĮ /PTF	PI /PTP	X/IMAY			
62	16.391	1.0931	0-51444	0.86962	J. 42200			
. 7	16.136	1.0662	0.59644	0.85609	0.67009			
ANDIT TONA	PRESSIPE	PATIOS . FIC	W SPLITTEP O	. D.		Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate of the Common public rate		
חשיש חי	PL	PI /PD	PI / PTF	PI /PTP	XZNMAX			
77	13.531	2.89426	2.42466	. 0.71785	Q. 5000Q			
7	16.201	1-2027	0.57126	0.96565	0.58300			
22	15.171	1.0225	0.47615	0.50486	9-61000			
400171044	<del>ų - 00 ( 5 (10)</del>	atting , fur	cta timichs					
I WORD	PE	PL/PO	PL/PTF	سيبه عميان	X/DMAX			
107	14. 906	0.97834	0.4664	0.78551	-1.0000			
112	14.755	0.07-2	2.46312	0.78284	-1.0000			
27	14.776	- D- P- 1-5	7:44275	0.78392	-1.0000			
	15.254	3.99420	0.47222	0.79#25	-1.0000			_
	15. 391	0. 99717	0.47364	U. B. Trans	1.0000			
137			0.47364	0.79825	-1.0000 -1.0000			
SEDUCT TOWN	15.046 15.046	0.99717 0.99429 RATIOS . FOR	0-47222 ENTRY INLET	0.79825	-1:0000			
ער אחדף	15.791 15.046 1 PRESSUPE	0.99717 0.99429 RATIOS . FOR	0.47222 FRMY INLET PL/PTF	0.79825 Pt /PTP	x/DMAX			
PENDET TONA VN HOPP	15.046 15.046 1 PRESSUPE PL 14.936	0.99117 0.99429 <u>RATIOS . FOR</u> PL/PO 0.97834	0.47222 ENTRY INLET PL/PTF 0.46469	0.79825 Pt /PTP 0.7851	x/DMAX 0-39800	•		
137 163 2602 (T 104A 07 107 117	PL 14. 936 14. 756	0.99117 0.99429 RATINS . FOR PL/P1 0.97834 U.97503	0.47222 ERMY IMET PL/PTF 0.46469 0.4632	0.79825 PL/PTP 0.7851 0.78286	X/DMAX 0.39800 0.43100	•		
137 123 200 T 104A 107 117 112	PL 14. 936 14. 756 14. 776	0.99117 0.99429 RATIOS . FOR PL/P1 0.97834 0.97503 0.97635	0.47222 FRITTY   MLFT PL/PTF 0.46469 0.46375	0.79825 PL/PTP 0.7851 0.78286 0.78392	X/DMAX 0-39800 0-43100 0-44900	•		
0400 (T 10NA 0400 (T 10NA 040 (100 107 117 127 127	PL 14. 736 14. 776 15.065	0.9917 0.99429 RATINS . FOR PL/PN 0.97834 0.97503 0.97635 0.99520	0.47222 FRITIV IMET PL/PTF 0.46469 0.46375 0.46375	0.79825 Pt /PTP 0.7851 0.7856 0.78392 0.79825	X/DMAX 0.39800 0.43100 0.44900 0.46600			
137 2602 (7 10MA VN HOPD 107 112 127 127	PL 14.756 14.756 14.756 14.776 15.055 15.055	0.9917 0.99429 RATINS . FOR PL/PN 0.97834 0.97503 0.97635 0.99420 0.99717	0.47222 ERITHY IMET PL/PTF 0.46469 0.46375 0.46375 0.46375 0.47222 0.47364	0.79825 PL/PTP 0.7851 0.7826 0.7839 0.79825 0.89063	x/DMAX 0.39800 0.43100 0.44900 0.52200	•		
137 2600 UT 10NA 20 HOPD 107 112 127 127 147	PL 14,756 14,756 14,756 14,776 15,065 15,091 15,746	0.99117 0.99479 RATINS . FOR PL/PO 0.97834 0.97503 0.97635 0.99435 0.994717 0.99429	0.47222 FRITIV IMET PL/PTF 0.46469 0.46375 0.46375	0.79825 PL/PTP 0.7851 0.78286 0.78392 0.79825 0.89063 0.79825	X/DMAX 0.39800 0.43100 0.44900 0.58600 0.58600	•		
27 2004 1000 0 4000 12 22 27 27	PL 14.756 14.756 14.756 14.776 15.055 15.055	0.9917 0.99429 RATINS . FOR PL/PN 0.97834 0.97503 0.97635 0.99420 0.99717	0.47222 ERITHY IMET PL/PTF 0.46469 0.46375 0.46375 0.46375 0.47222 0.47364	0.79825 PL/PTP 0.7851 0.7826 0.7839 0.79825 0.89063	x/DMAX 0.39800 0.43100 0.44900 0.52200	•		
600 (T 10NA 10 MOPD 07 12 22 27 27 47 42	PL 14,756 14,756 14,756 14,776 15,065 15,091 15,746	0.99117 0.99429 RATINS . FOR PL/PN 0.97834 0.97503 0.97635 0.99420 2.99717 0.90429	0.47222 ERITHY IMET PL/PTF 0.46469 0.46375 0.46375 0.46375 0.47222 0.47364	0.79825 PL/PTP 0.7851 0.78286 0.78392 0.79825 0.89063 0.79825	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.57800	•		
200 LT JONA IN HOPP 07 12 22 27 27 37 47	PL 14. 436 14. 776 14. 776 14. 776 15. 045 15. 191 15. 146	0.99117 0.99429 RATINS . FOR PL/PN 0.97834 0.97503 0.97635 0.99420 2.99717 0.90429	0.47222 ERITHY IMET PL/PTF 0.46469 0.46375 0.46375 0.46375 0.47222 0.47364	0.79825 PL/PTP 0.7851 0.78286 0.78392 0.79825 0.89063 0.79825	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.57800	•		
27 200 LT JONA 0 HOPD 27 12 27 27 27 47 47 47 47 47 47 47	PL 14. 476 14. 476 14. 476 15. 055 15. 091 15. 191 15. 194	0.9917 0.99429 RATIOS . FOR PL/PT 0.97834 0.97503 0.97635 0.99420 2.9717 0.90429	0.47222 ERITHY IMET PL/PTF 0.46469 0.46375 0.46375 0.46375 0.47222 0.47364	0.79825 PI/PYP 0.78551 0.78286 0.78392 0.79825 0.89063 0.79825	X/DMAX 0.39800 0.43100 0.44900 0.52200 0.52200 0.58900	•		
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IASA-I FWT	c 082114	INAPY DATA	96/13/79	CADDELL	HEC 10/25/79	02:26:39.657	FAC AXAXI	PG4 (034	R.Z.*	•
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/ก มกคัก ั	PI	P1 /P()	PI /PTF	PL /PTP	X/DMAX		• • •		who we are a superior of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the st	
12	15.569	1.0265	0. * 6441	0.959#2	0.72200					
7	15.779	1.0350	0. 56065	0.56846	J-#2000					
7	15.754	1.0348	0.57112	0.97123	0.51900					
2	15.769	1.0397	0.57167	0.47214	1.0170					
Annit Inu	AL PHESSURE	PATENS . FLE	W CHITTEP I	n.	and the second second	•••		1.2.2.1.2.1.2.1.		
n warn	Pt	PL / PO	PI / PTF	PI /PTP	*/DMAY					
	15.626	1.0302	0.56641	0.96322	9.42200					
•	15.559	1.9250	3.55405	0.95921	1.67900					
ADD IT TOW	AT PRESSIRE	RATTINS . FEE	W SPLITTER F	<u>`. o.</u>						
n web	Pl	PL/P/I	PLIPTE	PL /PTP	x/fmax					
7	13.613	0. 89 758	0. 49351	0.43924	0.50800					
7	17.395	1.1469	0.63060	1.0724	0.5*300					
?	15.294	1.0075	0.55119	0.93731	2.67000		de vana - villever om man man man - made bedelikkildelik ille om m			
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D WOPD	10	PI /PN	PL / PTF	21.234	X/DMAX					
07	14.794	0.97543	0 5742	0.91202	-1.0000					
12	14.724	0. 97001	0.53124	0.90771	-1,0000					
22	14.764	D. Congress	=1522	0.91017	-1.0000				<del></del>	
77	15.310	2,99027	0.54	0.92590	-1.0000					
37	15.744	0.99192	0.54527	0.92744	-1.0000		•			
سند	14.959	0.98631	0.54229	0.97770	1-0000					
		RATIOS , FOR	FREDY TALET							
ብ ቁጥዶብ ሳን	PL 14.794	PL/PN ),97543	PL /PTF 0.53631	PI /PTP 0-91207	X /DMAX		•			
12	14.724	0.97001	0.53377	0.90771	0.39800					
77	14.764	7.07345	0.53522	0.91017	0.43100					
27	15.019	0.99027	0.54447	0.92590	0.44900					
~;·	15.744	0.99192	0.54537	0.92744	0-48600 0-52200					
42	14.959	0.98631	0.54770	0.92720	9.58800					
<u> </u>		184000		0.45551	9.78800					
<del></del>	150134		<del></del>	0499771	1.0000					
********		****	HOTZLE ELA							
n wash	PI	P(Tree)	DL 40TO	PI /PTP	X/NMAX					
57	15.225	1.77	0. ==11	0.93731	-1.0000					
<u> </u>	15.774	1.0025	0.55114	0.0373	-1-0000					
43011100	AL PPESSIPE	PATINS . 20	NEG SHPPUD 1	OCATION						·
P 1.3 I 4 B. L.M.	Pl	P( / P()	PI /PTF	PI /PTP	X/DMAX					
		1.0025	0.55118	0.03731	0.79300					
n was	15, 204		0. 5118	0.93731	0.74500					
70 WOPD	15.204 15.204	1.0925								
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37	16.391	1.0#32	0.50702	0.86758	0.82000				
47	15.491	1.0998	C. 60367	0.87287	0.91900				
52	15.456	1.39#2	0.59976	0.87155	1.0170				
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>410 I T I (NA	AL PRESSIME	PATINS , FEN	M SPLITTER F	`• D•	_				
AL AUEU	PL	PL / PO	PI /PTF	PI /PTP	X AMOLX				
77	13.716	0. 23696	0.42989	0.72642	0.50600				
<b>#</b> 2	17.471	1.1553	0.63675	0.92530	0.58300				
92	15-161	1.9925	0.55256	0.90296	0.67000				المالية المستوات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المسترات المس
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107	14.814	0.97971	0. 5399	7. 78469	-1.0000				
	14.766	3.340	2077-16	0.78204	-1.0000				
. <u>112</u> ·127		2.0000	53907	0.74336	-1-0000				
127	14.701	0.9949?	0.5483	0.79687					
137	15.056	0.9960	0.54946	0-29846	-1.0000				
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IVN WIRD	PL	PL/PO	PL /PTF	PL/PTP	X/DMAX				
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IVO WORD 107 112 122 127 137	PL 14. 916 14. 766 14. 791 15. 256 15. 776 15. 746	PL/PN 7.97971 0.97640 0.97806 0.99492 7.99697 9.99492	PL /PTF 0.53998 0.53916 0.53916 0.54937 0.54937	0.78469 0.78204 0.78336 0.79687 0.75846 0.75677	0.39800 0.43100 0.44900 0.52200 0.52200 0.52800		•		
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WO WORD 137 112 127 127 137 142 142 142 142 157 >ADDITION	PL 14.416 14.766 14.791 15.266 15.376 15.376 15.171 AL OPESSURE PL 15.171 15.171	PL/PN	PL /PTF 0.5399R 0.53816 0.53916 0.53907 0.54837 0.54837 0.54837 0.55822 PE / WTF 0.55292 DEC SHROUN 1 PL /PTF 0.55292 0.55292	0.78469 0.78204 0.78336 0.79687 0.79846 0.79677 0.79877 0.80323 0.80349 0.80349	0.39800 0.43100 0.44400 9.48600 0.52200 0.58800 1.0000 1.0000 -1.0000				
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32	0.		LMWbA bf ne		PFC 10/25/79 02:30		FAC 9X5X1	PGM CO34	PDG 1514
32		PL / PO							
	15.741		MANA	PI /PTP	X/DMAX				
		1.0400	0.49421	0.73R57	0.72200				
47	17.116	1.131*	9. 53749	0.77649	J. 82000				
	17.401	1.1507	0.54435	0.7#332	0.91900				
57	17.376	1.1490	0. 54556	0.78220					
>ATTITIONA	I PPESSUR	F RATIOS , FI			1-0170				
			time with fire the	1.17.				•	
AU NUBU	Pl	Pt / PG	PL /PTF	PL /PTP	X/DMA'X				
Y 5	16.496	1.1173	0.53049	0.7605P					
£ 7	16. 721	1.0594	0.50301	0.7211#	0.42200				
ADD 1 T 1004					0.67000				
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VID MINES	PI	P( / PI)	PI /PTF	0: 40.20					
77	13.615	0.90029		PI /PTP	X/DMAX				
P.7	14.226		9.42747	0.612#4	0.50800				
7		1.2052	9-57226	0.82047	O.58300				
·	15.199_	1.0038	0.47662	0.68336	9,67000				
<del>FOOTT TOME</del>	- PRE CEUPE		CTCR CHADUD	_		Week to the second	a management of the second of	· · · · · · · · · · · · · · · · · · ·	A
		-							
NOPO -	Phone	የር / ውን	PL /PTF	PLEASE	X/OMAX				
07	14.955	0.98233	0.4666	0.66872	-1.0000				
1.2	14.910	0.92935	17.46500	0.66669					
7.7	14.975	2.00776	3.45547		-1.0000				
77	15. 180-	0. 99721	0.67948	0.66737	-1.0000		**************************************	The same and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the s	
• •	15.175	1.0007		0.67885	-1.0000				
-	15.105	0.99887	0.47490	0.67000	-1.0000 -1.0000				
NUED I	PL	RATIOS , FOR	PI /PTF	PI /PTP		**	The state of the energy on a state was a		
7 7	14.955	0.98233	0.46642		X/DHAX				
2	14.917	9.97935	0.46500	0.66872	0.39800				
, ,	14.875	0. 99034		0.66669	0.43100				
7	15.080	0.99721	0.46547	0.66737	9.44903				
7	15.125		n. 47748	0.67885	J_48630				
. >	15.105	1.0302	0.47499	98054.0	7.52200			-	
	15175	7. 99AA7	7.47427	0.6799R	0.58800				
	15 175	1.0005	****		<del></del>				
	•	1.0025	0.47447	- <del>0.402[3</del>	<del>-1+9009</del>				
DOLL TOWN	<b>Gazzen</b> ot	AATION - FAN	HOTTLE FLAG						
		OL CED	_0-	PI /PTP	# # # # * * * * * * * * * * * * * * * *				
•	15.175	1.111135	0.47647		X/DMAX				
?	15.175	1.0025	9.47647	0.68317	-1.2000				
				7-4-43-13	-1.0000				
anti Linvr	PPFSSIIPF	P4TERS . 20 E	FE ZHENUN 10	CATION					
AULU B	•	PI / PO	PI / PTF	01 (0*-			The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		
7	15.175	1.0935	0.47647	PI /PTP	ALDMAK				
	15.175	1.0025		0.68313	ე <b>. 7</b> 930 <u>0</u>				
			9.47647	0.68313	0. F4400				
TOMAL TOMAL	DALCENDE	PATINS . PO N	FG SHPPUD IN	EATION					
1111			PI / PT S		to the second of department of	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	<del></del>		
AUBU bi	t	P( / P')		PI /PTP	X/DMAX				
AUBD B		P( / P·1 1. 93404							
ב ל מ יופחיף	14.175 13.940	7.93404	0.44349	0.63594	9-79200				
ב ל מ יופחיף	14.175 13.940	7.93404	0.44349						
ב ל מ יופחיף	14.125 13.949 ME45IPF9 :	7.93404 0.91518 Thenst Papame	0.44349	0.63594 0.62331	9-79*00				

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			0671414	CADDELL	Ket 10/53/14 05:	24-4-4				
>47717107	MI DOCKSIDE	PATIOS , PRI	MARY PHIG							
AVP 40FD	P1	ጣ / PO	M Note	P( /# TP	Y/DMA'X					
12	14.345	0.94589	3.37545	0.54716	3.72200					
27	17,830	1.1749	0.46639	0.67970	0.82000					
47	18.339	1.2402	0.49230	0.71746	J. 91900					
r.	19.754	1.2365	0.400#6	0.71534	1.0170					
**************************************	INT OPESSIBLE	BATINS . FLC	W SPLITTER I	.n.		× = =			··· <u>-</u>	
AVD HOPD	01	PI /PO	PI / PTF	Pt /PTP	X/IMAX					
62	17.553	1.1788	0-46797	0.68109	J. 42200					
67	14.575	1, 96096	1.78147	0.55594	0.67000					
>/07 11 004<	AL PRESSURE	RATIOS , FLO	IN CUT LLALE U	.D.	remain de la la la la la la la la la la la la la	Mindage, and they if it has made impact to the distribution of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the second state of the	and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t			
AVP WPPD	PL	PL / PO	PE /PTF	PL /PTP	Y/DMAX					
77	8.7033	9.57383	0.22779	0.33197	0.50000					
87	22.574	1.4984	0.59083	0.86104	0.58300					
92	15.185	1.0012	0.39744	0.5.920	Dat 1000					
				Wa 2.22U	DAT 1000	e data - remediane and - constitutions				
- truot Hon	tof successive	**************************************	ierca emano							
AVP WORD	PL	PL/P0	PL/PTF	PLESTA	X/DMAX		4			
-107	15.130	0-99558	0.39521	0.57596	-1.0000					1
112	_15-152	0.00481	7.39652	0.57787	-1.0000					
-127	15.229	1-0755	0.94435	0.58054	-1.0000					
-127	15.215	1.0032	0.39822	0.58035	-1.0000					
	124									
>400 11 COA<	15.175 15.125 IAL PRESSIME	1.0005 Q.99722 RATIOS . FOR	0.39717 0.39587 RERODY INLEY	0.5769Z	-1.0000 -1.0000				-	property and administration of the second
>ADDITION  AVD WORD  107 112	15-175 15-125 (AL PRESSIME PL 15-170 15-170	1.0005 0.99722 RATIOS . FCR PL/PD 1.99558 0.99887	0.39717 0.29587 REMONY [NLEY PL/PTF 0.39521 0.39652	0.57892 Q.57692 PL/PTP 0.57594 Q.57787	-1.0000 -1.0000 x/DMAX 0.39800 0.43120				-	
>ADDITION  AVD WORD  107  112  127	PL 15-175 15-125 PL 15-179 15-179 15-179	PL/PD	0.39717 0.29587 RERIMY INLEY PL/PTF 0.39521	0.57692 0.57692 PL/PTP 0.57596	-1.0000 -1.0000 x/DMAX 0.39800		•		- voices d'Amplessedensemblesseden est des re	
>ADDITION  AVD WORD  107 112	15-175 15-125 (AL PRESSIME PL 15-170 15-170	1.0005 0.99722 RATIOS . FCR PL/PD 1.99558 0.99887	0.39717 0.29587 REMONY [NLEY PL/PTF 0.39521 0.39652	0.57892 Q.57692 PL/PTP 0.57594 Q.57787	-1.0000 -1.0000 x/DMAX 0.39800 0.43120		•			
-1 27 -2 20 17 10 N avn wnpn 107 112 122 127 137	75.175 15.125 (AL PRESSIME PL 15.100 15.150 15.220 15.215 15.215	1.0005 0.99722 RATIOS . FCR PL/PD 1.99558 0.99867 1.0035 1.0032 1.0005	0.39717 0.29587 REMOV [MLFY PL/PYF 0.39521 0.39652 0.39652 0.39622 0.39717	0.57692 PL/PTP 0.57594 0.57767 0.58055 0.58055 0.57882	-1.0000 -1x0000 #/DMAH 0.39800 0.43120 0.44900		•		-	
>ADDITION  AVD WORD  107  112  127  127	75.175 15.125 IAL PRESSIME PL 15.170 15.150 15.220 15.221	1.0005 0.99722 RATIOS . FCM PL/PD 1.99558 2.99867 1.0035	0.39717 0.29587 RERODY [NLFY PL/PTF 0.39521 0.39657 0.39835 0.79822	0.57592 Q.57692 PL/PTP 0.57594 0.57767 0.59054 Q.58075	-1.0000 -1x0000 x/DMAX 0.19800 0.43100 0.44900 0.48600		•			
-1 27 -2 20 17 10 N avn wnpn 107 112 122 127 137	75.175 15.125 (AL PRESSIME PL 15.100 15.150 15.220 15.215 15.215	1.0005 0.99722 RATIOS . FCR PL/PD 1.99558 0.99867 1.0035 1.0032 1.0005	0.39717 0.29587 REMOV [MLFY PL/PYF 0.39521 0.39652 0.39652 0.39622 0.39717	0.57692 PL/PTP 0.57594 0.57767 0.58055 0.58055 0.57882	-1.0000 -1.0000 x/DMAX 0.39800 0.43100 0.44900 0.48600 0.52200					
-127 -200[Y ION AVD WOPD 107 112 127 127 137 142	PL 15-125 15-125 161 PRESSIBE PL 15-129 15-159 15-229 15-215 15-175 15-125	1.0005 0.99722 RATIOS . FCR PL/PO 0.99558 0.9987 1.0035 1.0032 1.005 0.99722	0.39717 0.29587 EERITY   NLFY PL / PYF 0.39657 0.39657 0.39815 0.29822 0.39717 0.39587	0.57692 PL/PTP 0.5759A 0.57787 0.58055 0.58075 0.57682 0.57692	-1.0000 -1.0000 x/DMAX 0.39800 0.43120 0.44900 9.48650 0.52200 0.58000					
-1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 1 * 7 -1 * 1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -	PL 15-129 15-129 15-129 15-129 15-129 15-129 15-175 15-125 15-125	1.0005 0.99722 RATIOS . FCR PL/PD 1.99558 1.0035 1.0032 1.0205 0.99722	0.39717 0.29587 RERITOY [NLFY PL/PTF 0.39521 0.39652 0.39835 0.39822 0.39722	0.57692 PL/PTP 0.5759A 0.57787 0.58055 0.58075 0.57682 0.57692	-1.0000 -1.0000 H/DMAH 0.39800 0.43120 0.44900 9.48600 0.52200 0.58000					
-1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1	PL 15-125 15-125 15-125 15-125 15-125 15-125 15-125 15-125 15-125 15-125	1.0005 0.99722 RATIOS . FCR PL/PD 1.90558 0.99887 1.0035 1.0032 1.0075 0.99722 1.0016	0.39717 0.29587 RERIDIV [NLFV PL/PTF 0.39521 0.39652 0.39652 0.39835 0.39822 0.39717 0.30587 0.30587	0.57692 PL/PTP 0.57594 0.57594 0.57787 0.58055 0.57882 0.57692 0.57692	-1.0000 -1.0000 x/0MAX 0.39800 0.43130 0.44900 9.48600 0.52200 0.58000 -1.0000		•			
-1*7	PL 15.175 15.125  PL 15.199 15.159 15.229 15.225 15.175 15.125 45.195 17.195	1.0005 0.99722 RATIOS . FCR PL/PD 1.9955R 0.9987 1.035 1.035 1.035 1.0275 0.99722 1.0414 1.7718	0.39717 0.29587 REMOTO INLEY PL/PYF 0.39521 0.39652 0.39835 0.29822 0.39717 0.30587 0.30324 0.97170	0.57692 PL/PTP 0.5759K 0.57787 0.58056 0.58075 0.57682 0.57682 0.57682 0.57682	-1.0000 -1.0000 x/DMAX 0.39800 0.43120 0.44900 0.52200 0.52200 0.58000 -1.0000 x/DMAX -1.0000		•			
-1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1 * 7 -1	PL 15-125 15-125 15-125 15-125 15-125 15-125 15-125 15-125 15-125 15-125	1.0005 0.99722 RATIOS . FCR PL/PD 1.90558 0.99887 1.0035 1.0032 1.0075 0.99722 1.0016	0.39717 0.29587 RERIDIV [NLFV PL/PTF 0.39521 0.39652 0.39652 0.39835 0.39822 0.39717 0.30587 0.30587	0.57692 PL/PTP 0.57594 0.57594 0.57787 0.58055 0.57882 0.57692 0.57692	-1.0000 -1.0000 x/0MAX 0.39800 0.43130 0.44900 9.48600 0.52200 0.58000 -1.0000					
>ADDITION  AVD WORD  107  112  127  127  147  142  157  AVD WORD  4VD WORD  -157	PL 15.125 15.127 15.127 15.129 15.129 15.229 15.215 15.125 15.125 15.125 15.125 15.125 15.125	1.0005 0.99722 RATIOS . FCR PL/PD 1.9955R 0.9987 1.035 1.035 1.035 1.0275 0.99722 1.0414 1.7718	0.39717 0.29587 RERITA INLEY PL/PTF 0.39521 0.39652 0.39835 0.39835 0.39835 0.39877 0.30370 0.39770	0.57492 0.57692 PL/PTP 0.5759A 0.57787 0.58035 0.57882 0.57882 0.57882 0.57882 0.57882 0.57882 0.57882 0.57850 0.57950	-1.0000 -1.0000 x/DMAX 0.39800 0.43120 0.44900 0.52200 0.52200 0.58000 -1.0000 x/DMAX -1.0000		•			
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-127 -240 UPPN  AVN WNPN  107 112 127 127 137 142 142 162 -167 -157 ->ADD [7 [GN  AVN WNPN  167 172	PL 15.175 15.125  IAL PRESSIBE  PL 15.179 15.159 15.229 15.215 15.175 15.125 15.175 15.125 15.175 15.125 15.175 15.125 15.175 15.125 15.175	1.0005 0.99722 RATIOS . FOR PL/PD 1.09558 0.99867 1.0235 1.0235 1.0235 1.0218 1.0218 PATIOS . 20	0.39717 0.29587 REMOV [MEFY PL/PYF 0.39652 0.39652 0.39717 0.30717 0.30587 0.30717 0.30720 0.3777 0.30770 DEG SHPCUN 1 PL/PYF 0.39783 0.39783	0.57492 0.57692 PL/PTP 0.5759A 0.57787 0.58054 0.58015 0.57882 0.57882 0.57882 0.57882 0.57889 0.7789 0.7789 0.7789 0.7789 0.77978 0.57978	-1.0000 -1.0000 H/DMAK 0.39800 0.43120 0.44900 9.48600 0.52200 0.58800 -1.0000 H/DMAK -1.0000 -1.0000					
-127 -240 UPPN  AVN WNPN  107 112 127 127 137 142 142 162 -167 -157 ->ADD [7 [GN  AVN WNPN  167 172	PL 15.175 15.125  IAL PRESSIBE  PL 15.179 15.159 15.229 15.215 15.175 15.125 15.175 15.125 15.175 15.125 15.175 15.125 15.175 15.125 15.175	1.0005 0.99722 RATIOS , FCM PL/PO 2.99807 1.0035 1.0032 1.0035 1.0032 1.0046 1.0018 1.0018 1.0018 1.0018 1.0018 1.0018 1.0018 1.0018	0.39717 0.29587 REMOV [MEFY PL/PYF 0.39652 0.39652 0.39717 0.30717 0.30587 0.30717 0.30720 0.3777 0.30770 DEG SHPCUN 1 PL/PYF 0.39783 0.39783	0.57492 0.57692 PL/PTP 0.5759A 0.57787 0.58054 0.58015 0.57882 0.57882 0.57882 0.57882 0.57889 0.7789 0.7789 0.7789 0.7789 0.77978 0.57978	-1.0000 -1.0000 H/DMAK 0.39800 0.43120 0.44900 9.48600 0.52200 0.58800 -1.0000 H/DMAK -1.0000 -1.0000					
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2	27-596	1.2497	9.47092	0.68943	0.42200				
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7	14.135	9.93271	0.23862	2.34934	0.5000				
7	19.074	1.3147	0.33635	0.49747	0.5#300				
2	15-296	1.0034	0.25470	0.37581	Q.6700Q				
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D WOPD .	Pl	PL/PD	PL/PTE .	21/24	DPAX				
97	15.251	1-0063	0.257	0.37602	-1.0000				
12	15.326	1.011	25972	C-37878 _	-1.0000				
??	15.321		7.7	0.37865	-1.0000				
77	15:251	1.0763	0.25746	0.37692	-1.0000				
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77		3.83527	0.21170	0.31064	0.72200			
47	23.469	1.5466	U"sales	0.57517	0.#2000			
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57	?f .1 89	1.7758	0.47741	0.64183	1.0170			
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AND MORD	Pt	Pt / P11	PI / PT F					
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47	23.430	1.4401	0.44840	0.67730	0.42200			
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TAU RUBD	PI	PL / PA	PI / PTF	PI /PTP	<b>* **</b> ***			
77	14.265	7. 94 076			7/044X			
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92	15.215		0.33629	0.49745	0.500			
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+restrice	<del>- PAFGGUDE</del>	******************************	<del>( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )</del>				- 120 0000	
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-177	15.270	1.0063	7. 25500	0.37424				
-117	15.340	1.01	7.25421		-1.1000			
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>A>>fTinma Nun winen 107 112 122	Pt 15.270 15.340 15.340	PATINS , FRE PI/PN 1.0063	PI /PTF 0-25504 0-25621	0.37277 Pt /PTP D.37424 0.37595	Y/N=&Y 3-3000 0-43100			
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>A791T [NNA! IVN WIPD 197 112 122 127 127 127 142	Pt 15.270 15.340 15.340 15.345 15.165	PATINS , FOR PI/PT 1.0067 1.0109 1.0109 1.0109 1.0053 1.0023	PI /PTF 0-25504 0-25504 0-25621 0-25621 0-25621 0-25329 0-25404	PI /PTP D.37424 0.37595 0.37595 0.37597 0.37166 0.37277	1,0000 Y/NMAY 3,3000 0.43106 3,44900 0,48600 2,52700 9,58000	•		
347917 [NMA NVN WNPH 107 112 122 127 127 127 147 142	PE 55(PE PL 15.270   15.340   15.340   15.255   15.165   15.213   45.305   46.310	PATINS , FRM PI/PT 1.0067 1.0109 1.0109 1.0109 1.2053 2.99937 1.0023	P1 /PTF 0-25504 0-25515 0-25621 0-25621 0-25621 0-25629 0-25404	PI /PTP D.37424 0.37595 C.37595 0.37147 0.37146 0.37277	#/neav J.39800 0.43106 J.44900 0.48600 2.57200 2.58800	•		
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>A2011 [MAN WIPE 107 112 122 127 127 127 127 142 142 142 143 144 VN WIPEN 157	PI 15.270 15.340 15.340 15.340 15.255 15.165 15.213 46.306 16.316	PATINS , FRM PI/PT 1.0061 1.0109 1.0109 1.0109 1.9751 7.99937 1.9723 1.3320 1.3320 1.0021	PI /PTF 0.25504 0.25504 0.25521 0.25621 0.25627 0.25329 0.25404 0.36404 0.36404	PI /PTP 0.37474 0.37595 0.37595 0.37597 0.37147 0.37146 0.37277	7/nmay 3.3000 0.43100 0.44900 0.48600 2.52700 0.58000 1.0000	•		
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>A221T[NAI NUT WIPT 107 112 127 127 127 147 142 142 142 143 143 144 201T IDNAI VD WIPT VD WIPT	PRESSIPE PL 15.270 15.340 15.255 15.165 15.213 44.305 46.316 PL 15.205 15.210 PRESSIPE	PATINS , FOWN PI/PN 1.0063 1.0109 1.0109 1.0253 0.99937 1.0023 1.0023 1.0023 PATINS , 20 0	PI /PTF 0.25504 0.25504 0.25521 0.25621 0.25629 0.25404 0.25104 0.25104 0.25404 0.25404 0.25404 0.25404	PI /PTP  0.37474 0.37595 0.37595 0.37587 0.37186 0.37277 0.37186 0.37277 0.37264 0.37277	7/nmay 3.3000 0.43100 0.44900 0.48600 2.52700 0.58000 1.0000	•		
>A2011 [MAI NVN WIPE 107 112 122 127 127 127 142 142 142 143 143 144 VN WIPEN 157 >A3011 [ONA) VN WIPEN 157 >A3017 [ONA) VN WIPEN 147	PI 15.270 15.340 15.255 15.145 15.213 16.305 16.316 PI 15.205 15.210 PF SSIPE 1	PATINS , FRMI PI/PN 1.0063 1.0109 1.0109 1.0109 1.023 1.0023 1.0023 1.0023 PATINS , 20 N	PI /PTF 0.25504 0.25504 0.25504 0.25621 0.25620 0.25620 0.25604 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.36104 0.3610	0.37277 P1 /PTP 0.37424 0.37595 0.37595 0.37367 0.37166 0.37277 0.37166 0.37277 0.37264 0.37277	#/DMA# 3.39800 0.43106 3.44900 0.48600 2.52700 9.58803 1.0000 1.0000 -1.0000	·		
>A221T[NAI NUT WIPT 107 112 127 127 127 147 142 142 142 143 143 144 201T IDNAI VD WIPT VD WIPT	PRESSIPE PL 15.270 15.340 15.255 15.165 15.213 44.305 46.316 PL 15.205 15.210 PRESSIPE	PATINS , FOWN PI/PN 1.0063 1.0109 1.0109 1.0253 0.99937 1.0023 1.0023 1.0023 PATINS , 20 0	PI /PTF 0.25504 0.25504 0.25521 0.25621 0.25629 0.25404 0.25104 0.25104 0.25404 0.25404 0.25404 0.25404	PI /PTP  0.37474 0.37595 0.37595 0.37587 0.37186 0.37277 0.37186 0.37277 0.37264 0.37277	#/NMAY 3.39800 0.49106 3.44900 0.48600 2.52700 0.58803 1.0000 1.0000 -1.0000	•		
242217 [PMAI AVP WPP 107 112 127 127 127 142 142 142 142 142 142 142 242 2	PRESSIDE  PL 15.270 15.340 15.255 15.165 15.213 45.205 46.316  PL 15.205 PF SSIDE  PL 15.205 PL 15.205	PATINS , FRMI PI/PN 1.0063 1.0109 1.0109 1.0109 1.023 1.0023 1.0023 1.0023 PATINS , 20 N	PI /PTF 0.25504 0.25504 0.25504 0.25621 0.25620 0.25624 0.25329 0.26404 0.26306 0.26404 0.26306 0.26404 0.26306 0.26404 0.26306 0.26404	PI /PTP 0.37474 0.37595 0.37595 0.37595 0.37596 0.37277 0.37244 0.37277 0.37244 0.37277 0.37264 0.37252	#/DMA# J.39800 0.43106 J.44900 0.48600 2.52700 9.58803 1.0000 1.0000 -1.0000	•		
242217 [FINAL  RVP WPP  107  112  122  127  127  142  142  142  14	PI 15.270 15.340 15.255 15.145 15.213 16.346 15.205 15.210 PPF SSUPE 15.205 15.200 PPF SSUPE 1	PATINS , FOWN PI/PN 1.0063 1.0109 1.0109 1.0109 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023 1.023	PI /PTF 0.25504 0.25504 0.25504 0.25621 0.25620 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.25624 0.2562	PI /PTP 0.37474 0.37595 0.37595 0.37595 0.37596 0.37277 0.37244 0.37277 0.37244 0.37277 0.37264 0.37257 0.37266 0.37252	#/DMA# J.39800 0.43106 J.44900 0.48600 2.52700 9.58803 1.0000 1.0000 -1.0000			
242217 [MAN AVD WIPPD 107 112 122 127 127 127 127 142 142 142 142 142 142 142 142 142 142	PRESSIPE PL 15.270 15.340 15.340 15.255 15.165 15.213 46.306 15.205 15.205 15.200 PRESSIPE PL 15.205	PATINS , FRM PI/PN 1.0063 1.0109 1.0109 1.0123 1.0023 1.0023 1.0023 PATINS , 20 N PI/PN PATINS , 20 N	PI /PTF  0.25504 0.25504 0.25504 0.25504 0.25620 0.25620 0.25604 0.25604 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606	PI /PTP 0.37474 0.37595 0.37595 0.37595 0.37596 0.37277 0.37244 0.37277 0.37244 0.37277 0.37264 0.37252	#/DMA# J.39800 0.43106 J.44900 0.48600 2.52700 9.58803 1.0000 1.0000 -1.0000	•		
242217 [PMAI  AVE WERPE  107  112  127  127  142  142  142  142  14	PI 15.270 15.340 15.340 15.255 15.165 15.213 45.305 15.215 PI 15.205 15.210 PPF \$\$ SUPE   PPF \$\$ SUPE   PPF \$\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	PATINS , FOWN PI/PN 1.0063 1.0109 1.0109 1.023 1.0023 1.0023 1.0023 PATINS , 20 n PI/PN 1.0029 1.0029 1.0029	PI /PTF 0.25506 0.25506 0.25521 0.25621 0.25620 0.25406 0.25306 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406 0.25406	PI /PTP 0.37474 0.37595 0.37595 0.37595 0.37596 0.37277 0.37244 0.37277 0.37244 0.37277 0.37264 0.37257 0.37266 0.37252	#/nmax J.3000 0.49106 J.44900 0.48600 2.52700 0.58003	•		
>A2011 [MAI  AVD WOPD  107  112  122  127  127  127  142  142  14	PI 15.270 15.340 15.340 15.340 15.275 15.165 15.213 16.316  PI 15.205 15.210  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100  PPF \$ 100	PATINS , Free PI/PN 1.0061 1.0109 1.0109 1.0109 1.0109 1.0023 1.0023 1.0023 PATINS , 20 n PI/PN 1.0029 1.0017 PATINS , 90 n	PI /PTF 0.25504 0.25504 0.25504 0.25504 0.25621 0.25620 0.25620 0.25604 0.25306 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606	PI /PTP  D. 37474  0. 37595  C. 37595  C. 37596  O. 37277  D. 37166  O. 37277  D. 37264  D. 37264  PI /PTP  D. 37264  O. 37252  CATION  PI /PTP	#/DMA# J.30800 0.43106 J.44900 0.48600 2.52700 0.58800 1.0000 1.0000 -1.0000 -1.0000 0.74300 0.84400			
>A2011 [MAI  AVD WOPD  107  112  122  127  127  127  142  142  14	PI 15.270 15.340 15.340 15.340 15.255 15.165 15.213 16.316  PI 15.205 15.210  PPF \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	PATINS , FOWN PI/PN 1.0063 1.0109 1.0109 1.023 1.0023 1.0023 1.0023 PATINS , 20 n PI/PN 1.0029 1.0029 1.0029	PI /PTF 0.25504 0.25504 0.25504 0.25504 0.25621 0.25620 0.25620 0.25604 0.25306 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606 0.25606	PI /PTP 0.37676 0.37595 0.37595 0.37595 0.37186 0.37277 0.37186 0.37277 0.37264 0.37277 0.37264 0.37252 PI /PTP 0.37264 0.37252 PI /PTP 0.37264 0.37252	#/nmax J.3000 0.49106 J.44900 0.48600 2.52700 0.58003	•		

		MAPY DETA	34/13/10	COPFII	PFC 19/25/7	9 02:47:34.307	tel dagai	PG4 (334	BUC 1253	
ENDET FONE	M PRESSIPE	PATINS . PPI	MANY MIG							
า นูกตุก	et -	Pt / PO	PI /PTC	PE /PTP	E\Uni\A					
2	12.102	0.79999	0. 221 31	0-32150	J. 72200					
÷	77.286	1.5195	0.42036	0.61179	0. #2707					
. 🕶	24.612	1.6270	0.45009	0.65463	0.91900					
,	24.352	1.6098	0.44533	0.64771	1.0170					
								-		
	ri nat / cilat	PATINS , FIN								
u Atab	£	Pt / PO	PL /PTF	PI /PTP	· March					
7	26-229	1.7338	0.47954	0.69761	0.42200					
,	73.471	1.5483	0.42832	0.+279+	G. e 7000					
APOIT IONA	I PRESSIPE	PATINS . FER	W SPLITTER 0	- n.				<del></del>		
n ween	Pi	m / PO	P) /PTF	PL /PTP	X /DMA X					
7	13.052	9.86294	Q.23869	0.34717	0.50600					
2	19.445	1.2193	0. 73 731	0.49059	0.58300					
ź	15.153	1-0217	0.27712	0.40305	0-47000					
							-			
Family 13-45	r <del>- estitust</del> -	**************************************								
D WORD	71	ñL/P9	PL/PT =	11/224	X/DHAX					
07	14.148	1.0027	0.27739-	0.40345	-1.0000					
12	15.248	1.0700	ATZTONE.	0.49558	-1.0000					
22	15.273	1,000	6-27031	0.47675	-1.0000					
2 7	15.209	T. 0054	0.27012	0.40457	-1.0000					
	14.11	1).119909	0.27639	0.57199	-1.0000					
77					- I . ((V-/U					
37 52 •20 • 7 • 200	15.143	1.0711	0., 7694	0.40279	1-3000					
670171994 n ynen	15.143		Do: 7694 EBITHY INLET PL/PTF						and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of t	<del></del>
62 670171994 0 4060	15.143 AL F≅ESSUPE PL 15.164	1.0711 PATINS . FRP PL/PN 1.2027	0.: 7694 <u>EDITIV IMLET</u> PL/PTF 0.27739	PL/PTP 0.40345	#/DMA# 0.39800		•			
62 670171994 n. ynen 17	15.143 AL F⊅ESSUPE PL 15.168 15.248	1.0311 PATINS . ENP PL/PN 1.9027 1.9080	0.27694 ERCTY [MET PL/PTF 0.27739 0.27886	0.40279 PL/PTP	F/DMAX		•			
62 600171994 6 4086 77 12	15.143 AL F≅ESSUPE PL 15.164	1.0711 PATINS . FRP PL/PN 1.2027	0.: 7694 <u>EDITIV IMLET</u> PL/PTF 0.27739	PL/PTP 0.40345	#/DMA# 0.39800		•			<u> </u>
62 * <u>701710%</u> n. km# n 17 12 22	15.143 AL F⊅ESSUPE PL 15.168 15.248	1.0)11 PATINS - ENP PL/PN 1.90.27 1.90.80 1.90.97 1.00.55	0.7694 EBMY IMET PL/PTF 0.27739 0.27886 0.27891	0.40279 PL/PTP 0.40345 0.40558	#/DMAX 0.39800 0.43120		•		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	-
62 6-00 17 10 NA 0 14 0 P P 0 7 12 12 22 27	15.143 AL PRESSUPE PL 15.168 15.248 15.273	1.0)11 PATINS . ENP PL/PN 1.2027 1.9080 1.0097	0.27694 ERCTY [MET PL/PTF 0.27739 0.27886	PL/PTP 0.40345 0.40358 0.40758	F/DMAX 0.39800 0.43100 0.44900					
42 42017 1044 0 4090 17 12 22 27 27	PL 15.169 15.169 15.249 15.273 15.209 15.113 15.140	1.0)11 paying _ enp P_/Pn 1.0027 1.0080 1.0097 1.0256 2.90900 1.0011	0/694 EBONY [MLET  PL /PTF 0.27739 0.27739 0.27836 0.27631 0.27630 G.27694	PL/PTP 0.40345 0.40358 0.40625 0.40625 0.40159 0.40279	#/DMA# 0.39800 0.43100 0.44900 0.49600 0.52700 0.52700		•			
42 400171094 0 14090 12 22 27 37 47	PL 15.164 15.164 15.248 15.273 15.209 15.113 15.143	1.0)11 #47105 a Free PL/P0 1.0027 1.0080 1.0097 1.0054 2.9090 1.0011	0.7694 EBONY IMLET PL/PYF 0.27739 0.27789 0.27891 0.27812 0.27839 0.27639	PL/PTP 0.40345 0.40558 0.40452 0.40159 0.40179	#/DMAX 0.39900 0.43130 0.44900 0.42700 0.52700 0.58800		•			
62 60017 1098 10 17 12 12 12 12 17 17 18 19 19 19 19 19 19 19 19 19 19	PL 15.16A 15.16A 15.24A 15.273 15.209 15.113 15.143 15.143	1.0)11  PATINS _ ENP PL/PN 1.90.77 1.90.80 1.90.75 7.90.90 1.90.71 1.90.75 1.90.70 1.90.70 1.90.70 1.90.70 1.90.70 1.90.70 1.90.70 1.90.70 1.90.70 1.90.70	0.7694 EBITHY IMLET  PL /PTF 9.27739 0.27886 0.27931 0.27839 0.27639 0.27644 0.277494	PL/PTP 0.40345 0.40358 0.40625 0.40625 0.40159 0.40279	#/DMA# 0.39800 0.43100 0.44900 0.49600 0.52700 0.52700					
62 60017 1098 10 17 12 12 12 12 17 17 18 19 19 19 19 19 19 19 19 19 19	PL 15.16A 15.16A 15.24A 15.273 15.209 15.113 15.143 15.143	1.0)11 #47105 a Free PL/P0 1.0027 1.0080 1.0097 1.0054 2.9090 1.0011	0.7694 EBITHY IMLET  PL /PTF 9.27739 0.27886 0.27931 0.27839 0.27639 0.27644 0.277494	PL/PTP 0.40345 0.40558 0.40452 0.40159 0.40179	#/DMAX 0.39900 0.43130 0.44900 0.42700 0.52700 0.58800		•			
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>270   T   1001	IL PPESSIPE	PATTOS , PPT	बाहर ज्याह						
Yr wren	P1	PI / PC	PI /PTF	PI /PT2	E/DMAX				
32	14-877	0.98098	0-35477	0.52251	0.72200				
7	19.444	1.2162	2.43984	0.64778	9. A2000				
67	19.785	1.2046	0.47181	0.69457	0.91900				
52	19,684	1.2990	9. 46 24?	0. 4 91 34	1.0170				
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62	19.355	1.2762	0.46155	0.67976	0-42200				
57	15.393	1.0150	0.16706	0.54041	0.67000				
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11	9-8629	2-65034	0.23520	0.34640	0-50000				
2	21.196	1.3976	0.50545	0.74442	0.58300				
2	15-202	1.0924	0.26253	0.53393	0.67000	··· · · · · · - ·- ·- · · · · · · ·			
4021-10m	<del>L-14213VPE</del> -	F#7273 y Eur	Core Supress						
D VCPE	PL	PL/ PO	PL/PTS	-244414	X/DMAX				
07	15.107	1.0014	0.34	0.53340	-1.0000				
12	15.252	1.000	20:0396	0.53694	-1.0000				
2?	15.293	1.000	W-Seece	0.51709	-1.0G00				
27	13.24	1.2251	0.3634	-0.53573	-1.0000				
37	15.147	7.99479	0.76122	0.53700	1.2000				
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27	15.293	1.00#4	J. 7646A	0.53709	0.44900				
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47	14. 167	0.94073	0.74027	0-50107	3. 79300				
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32	14.392	0.94718	0.37635	0.55014	0.72200		
77	17.473	1.1762	7.46726	0.68714	0.42000		
47	14.414	1.2384	0.49297	0.71930	3. 91900		
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77	8.7493	0.57581	9.27879	0. 33444	0.50800		
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97	15.222	1.001#	0.39475	0.54147	0.67909		
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137	15.177	29986	7.39688	0.58015	-1.0000		
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22	15.287	1,0347	0.46675	0. 58436	-1.0000		
27	15.262	1,0045	0.30010	0.58340	-1.0000		
137	-117	0.99951	0.39714	0.5005	-1-0000		
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77	17.180	1.1309	9.51657	0.77102	0.02000					
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177	14.000		0.4649	PLESTO	X/DMAX					
112	14.860	0.9784		0.66827	-1.0000					
122			C.56501	0.66687	-1-0000					
	14-990	D. C. TRIA	44697	0.46822	-1.0000					
27	13-126	9.09556	0.477	0.67877	-1.0000					
137	14.160	O. 99 786	0.47349	0.64034						
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